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July 21, 2000 L-00-085

U. S. Nuclear Regulatory Commission Attention: Document Control Desk Washington, DC 20555-0001

Subject: Beaver Valley Power Station, Unit No. 1 Docket No. 50-334, License No. DPR-66 License Amendment Request No. 284

Pursuant to 10 CFR 50.90, FirstEnergy Nuclear Operating Company requests an amendment to the above license in the form of changes to the technical specifications (TS) and UFSAR changes which warrant NRC review in accordance with 10 CFR 50.59(c). The proposed TS change modifies Specification 3.4.8 by reducing the Beaver Valley Power Station (BVPS) Unit 1 Reactor Coolant System (RCS) specific activity limit. This TS change will support revised safety analyses with higher primary-to-secondary leakage in accordance with the methodology described in NRC Generic Letter 95-05, "Voltage-Based Repair Criteria for Westinghouse Steam Generator Tubes by Outside Diameter Stress Corrosion Cracking." The resultant necessary UFSAR changes involve slightly increased control room thyroid dose values which warrants NRC review and approval.

The proposed TS changes for BVPS Unit No. 1 are presented in Attachment A. The safety analysis (including the no significant hazards evaluation) is presented in Attachment B.

Attachment C provides the proposed BVPS Unit 1 UFSAR changes. Attachment D provides an evaluation of BVPS Unit 1 release rate data as required by NRC Generic Letter 95-05 for TS changes involving RCS specific activity limits less than 0.35 microcuries per gram. Attachment E provides the BVPS Unit 1 Main Steam Line Break dose calculation which supports the proposed UFSAR changes in Attachment C.

These changes have been reviewed by the BVPS review committees. The changes were determined to be safe and do not involve a significant hazard consideration as defined in 10 CFR 50.92 based on the attached safety analysis. An implementation period of up to 60 days is requested following the effective date of this amendment.

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Beaver Valley Power Station, Unit No. 1 License Amendment Request No. 284 L-00-085 Page 2

If you have any questions regarding this matter, please contact Mr. Thomas S. Cosgrove, Manager, Licensing at 724-682-5203.

Sincerely,

Sen W Myers Lew W. Myers

Mr. D. S. Collins, Project Manager c: Mr. D. M. Kern, Sr. Resident Inspector Mr. H. J. Miller, NRC Region I Administrator Mr. D. A. Allard, Director BRP/DEP Mr. L. E. Ryan (BRP/DEP) Ms. M. E. O'Reilly (FirstEnergy Legal Department) Subject: Beaver Valley Power Station, Unit No. 1 BV-1 Docket No. 50-334, License No. DPR-66 License Amendment Request No. 284

I, Lew W. Myers, being duly sworn, state that I am Senior Vice President of FirstEnergy Nuclear Operating Company (FENOC), that I am authorized to sign and file this submittal with the Nuclear Regulatory Commission on behalf of FENOC, and that the statements made and the matters set forth herein pertaining to FENOC are true and correct to the best of my knowledge and belief.

FirstEnergy Nuclear Operating Company

w W. Mvers

Senior Vice President - FENOC

COMMONWEALTH OF PENNSYLVANIA

COUNTY OF BEAVER

Subscribed and sworn to me, a Notary Public, in and for the County and State above named, this $\underline{\mathscr{A}/\mathscr{A}}$ the day of $\underbrace{\mathscr{A}/\mathscr{A}}$, 2000.

Ince My Commission Expirés

Notarial Seal Shella M. Fattore, Notary Public Shippingport Boro, Beaver County My Commission Expires Sept. 30, 2002 Member, Pennsylvania Association of Notaries

ATTACHMENT A

Beaver Valley Power Station, Unit No. 1 License Amendment Request No. 284

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DPR-66

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BEAVER VALLEY - UNIT 1

XIX

(Proposed Wording)

Amendment No.-209-

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DPR-66 REACTOR_COOLANT_SYSTEM

SPECIFIC ACTIVITY

LIMITING CONDITION FOR OPERATION

- 3.4.8 The specific activity of the primary coolant shall be limited to: (0.20)
 - a. $\leq (0.35) \mu Ci/gram$ DOSE EQUIVALENT I-131, and

b. $\leq 100/E$ µCi/gram.

APPLICABILITY: MODES 1, 2, 3, 4 and 5

ACTION:

- MODES 1, 2, and 3*
 - a. With the specific activity of the primary coolant > (0.35)µCi/gram DOSE EQUIVALENT I-131 for more than 48 hours during one continuous time interval or exceeding the limit line shown on Figure 3.4-1, be in HOT STANDBY with Tavg < 500°F within 6 hours.
 - b. With the specific activity of the primary coolant > $100/\overline{E}$ μ Ci/gram, be in HOT STANDBY with T_{avg} < 500° F within 6 hours.

MODES 1, 2, 3, 4 and 5

6.20

(0.20

a. With the specific activity of the primary coolant > (0.35) μ Ci/gram DOSE EQUIVALENT I-131 or > 100/E μ Ci/gram, perform the sampling and analysis requirement of item 4a of Table 4.4-12 until the specific activity of the primary coolant is restored to within its limits.

SURVEILLANCE REQUIREMENTS

4.4.8 The specific activity of the primary coolant shall be determined to be within the limits by performance of the sampling and analysis program of Table 4.4-12.

* With Tavg 2 500°F

BEAVER VALLEY - UNIT 1 3/4 4-18 (next page is 3/4 4-20) Amendment No. 205-

(Proposed Wording)

TABLE 4.4-12

PRIMARY COOLANT SPECIFIC ACTIVITY SAMPLE AND ANALYSIS PROGRAM

MINIMUM

TYPE OF MEASUREMENT AND ANALYSIS

1. Gross Activity Determination

- 2. Isotopic Analysis for DOSE EQUIVA-LENT I-131 Concentration
- 3. Radiochemical for \overline{E} Determination
- 4. Isotopic Analysis for Iodine Including I-131, I-133, and I-135

FREQUENCY

3 times per 7 days with a maximum time of 72 hours between samples.

1 per 14 days

- 1 per 6 months
- a) Once per 4 hours, 14 whenever the specific activity exceeds 0.35 µCi/gram DOSE EQUIVALENT I-131 or 100/E µCi/gram, and
- b) One sample between 1, 2, 3 2 & 6 hours following a THERMAL POWER change exceeding 15 percent of the RATED THERMAL POWER within a one hour period.

FUntil the specific activity of the primary coolant system is restored within its limits.

(Proposed Wording)

BEAVER VALLEY - UNIT 1

3/4 4-20

Amendment No. 205-

DPR-66

1, 2, 3, 4

1,

1,

1#, 2#, 3#, 4#, 5#

MODES IN WHICH

SURVEILLANCE REQUIRED



(Proposed Wording)

DPR-66 REACTIVITY CONTROL SYSTEMS

BASES

3/4.4.7 CHEMISTRY

The limitations on Reactor Coolant System chemistry ensure that corrosion of the Reactor Coolant System is minimized and reduces the potential for Reactor Coolant System leakage or failure due to stress corrosion. Maintaining the chemistry within the Steady State Limits provides adequate corrosion protection to ensure the structural integrity of the Reactor Coolant System over the life of the plant. The associated effects of exceeding the oxygen, chloride and fluoride limits are time and temperature dependent. Corrosion studies show that operation may be continued with contaminant concentration levels in excess of the Steady State Limits, up to the Transient Limits, for the specified limited time intervals without having a significant effect on the structural integrity of the Reactor Coolant System. The time interval permitting continued operation within the restrictions of the Transient Limits provides time for taking corrective actions to restore the contaminant concentrations to within the Steady State Limits.

The surveillance requirements provide adequate assurance that concentrations in excess of the limits will be detected in sufficient time to take corrective action.

3/4.4.8 SPECIFIC ACTIVITY

The primary coolant specific activity is limited in order to maintain offsite and control room operator doses associated with postulated, accidents within applicable requirements. Specifically, the (0.35) μ Ci/gm DOSE EQUIVALENT I-131 limit ensures that the offsite dose does not exceed a small fraction of 10 CFR Part 100 guidelines and that control room operator thyroid dose does not exceed GDC-19 in the event of primary-to-secondary leakage induced by a main steam line break.

BEAVER VALLEY - UNIT 1

B 3/4 4-4

Amendment No.-205-

(d.20)

(Proposed Wording)

DPR-66 REACTOR COOLANT SYSTEM

BASES

3/4.4.8 SPECIFIC ACTIVITY (Continued)

The ACTION statement permitting POWER OPERATION to continue for limited time periods with the primary coolant's specific activity > $(0.35) \mu$ Ci/gram DOSE EQUIVALENT I-131, but within the allowable limit shown on Figure 3.4-1, accommodates possible iodine spiking phenomenon which may occur following changes in THERMAL POWER. Operation with specific activity levels exceeding $(0.35) \mu$ Ci/gram DOSE EQUIVALENT I-131 for more than 48 hours during one continuous time interval or exceeding the limits shown on Figure 3.4-1 must be restricted to ensure that assumptions made in the UFSAR accident analyses are not exceeded.

Reducing Tavg to < 500°F minimizes the release of activity should a steam generator tube rupture since the saturation pressure of the primary coolant is below the lift pressure of the atmospheric steam relief valves. This action also reduces the pressure differential across the steam generator tubes reducing the probability and magnitude of main steam line break accident induced primary-tosecondary leakage. The surveillance requirements provide adequate assurance that excessive specific activity levels in the primary coolant will be detected in sufficient time to take corrective action. Information obtained on iodine spiking will be used to assess the parameters associated with spiking phenomena. A reduction in frequency of isotopic analyses following power changes may be permissible if justified by the data obtained.

3/4.4.9 PRESSURE/TEMPERATURE LIMITS

All components in the Reactor Coolant System are designed to withstand the effects of cyclic loads due to system temperature and pressure changes. These cyclic loads are introduced by normal load transients, reactor trips, and startup and shutdown operations. The various categories of load cycles used for design purposes are provided in Section 4.1.4 of the FSAR. During startup and shutdown, the rates of temperature and pressure changes are limited so that the maximum specified heatup and cooldown rates are consistent with the design assumptions and satisfy the stress limits for cyclic operation.

During heatup, the thermal gradients in the reactor vessel wall produce thermal stresses which vary from compressive at the inner wall to tensile at the outer wall. These thermal-induced compressive stresses tend to alleviate the tensile stresses induced by the internal pressure. Therefore, a pressure-temperature curve based on steady state conditions (i.e., no thermal stresses) represents a lower bound of all similar curves for finite heatup rates when the inner wall of the vessel is treated as the governing location.

BEAVER VALLEY - UNIT 1

B 3/4 4-5

Amendment No. 205

6.20)

(Proposed Wording)

ATTACHMENT B

Beaver Valley Power Station, Unit No. 1 License Amendment Request No. 284 REVISION OF RCS SPECIFIC ACTIVITY VALUE

A. DESCRIPTION OF AMENDMENT REQUEST

This proposed license amendment would reduce the limit for RCS specific activity in Beaver Valley Power Station (BVPS) Unit No. 1 Technical Specification 3/4.4.8. The Dose Equivalent I-131 is requested to be lowered from the current value of $\leq 0.35 \ \mu$ Ci/gram to a value of $\leq 0.20 \ \mu$ Ci/gram as specified in Technical Specification 3.4.8.a (and associated Actions and Table 4.4-12). This change will also lower the 'Acceptable Operation' line on Figure 3.4-1 from 21 μ Ci/gram to 12 μ Ci/gram Dose Equivalent I-131 for 80-100% power, and a commensurate reduction for power between 20-80%.

In conjunction with the reduced Technical Specification limit for RCS specific activity, the BVPS Unit 1 control room and offsite doses have been reanalyzed to allow for higher primary-to-secondary leakage in accordance with methodology described in NRC Generic Letter 95-05, "Voltage-Based Repair Criteria for Westinghouse Steam Generator Tubes by Outside Diameter Stress Corrosion Cracking," and as previously approved in BVPS Unit 1 License Amendment No. 205. To allow for maximum primary-to-secondary leakage, the resultant control room thyroid dose values listed in the UFSAR for Main Steam Line Break will increase slightly from 29 REM to 30 REM. This increase in calculated dose warrants NRC review and approval.

B. DESIGN BASES

The steam generator tubes act as a barrier between the reactor coolant system (RCS) radioactively contaminated water and the normally non-radioactive secondary system water and steam. The safety function of the steam generator tubes is to prevent or mitigate the release of radioactive fission and activation products from the reactor coolant system to the secondary system, and subsequently to the environment during normal operation or following a design basis accident (DBA). During certain plant transient or accident situations, the secondary system may be vented to the atmosphere to serve as a heat removal path, thereby controlling the temperature of the nuclear fuel. Under these conditions, leakage across the steam generator tubes will result in a release of radioactive

fission and activation products to the environment. Technical Specification 3.4.8 limits the specific activity of the primary coolant during normal operation. This specific activity criteria limits the release of radioactive products for actual or projected steam generator tube leakage.

C. JUSTIFICATION

The current value of 0.35 μ Ci/gram for primary coolant in Technical Specification 3/4.4.8 was provided in BVPS Unit 1 License Amendment No. 205. The changes in this amendment were made pursuant to NRC Generic Letter (GL) 95-05, Voltage-Based Repair Criteria for Westinghouse Steam Generator Tubes by Outside Diameter Stress Corrosion Cracking.

FirstEnergy Nuclear Operating Company (FENOC) stated in two previous letters (L-00-041 and L-00-059) dated March 31, 2000 and May 5, 2000 that the recent inclusion of data from French reactors has caused statistical skewing of the lower voltage range data in the Steam Generator Degradation Specific Management (SGDSM) Database. This database is used to perform projected accident-induced leakage per GL 95-05 and was used for the BVPS Unit 1 Cycle 14. Thus, although the steam generator conditions as measured during the last (1R13) refueling were not significantly different from those measured during the previous (1R12) refueling, the projected End of Core (EOC) accident-induced steam generator leakage became significantly higher primarily because of the inclusion of French reactors data into the SGDSM Database which resulted in an increased Probability of Leakage (POL) due to statistical skewing of the correlation.

Although other industry generic solutions are being approached to address this SGDSM Database skewing at the lower voltage range, it is requested that the BVPS Unit 1 primary coolant specific activity limit be lowered in order to support BVPS Unit 1 revising its DBA dose analysis pursuant to GL 95-05 in order to offset the recently increased POL and allow continued BVPS Unit 1 operation.

GL 95-05 states that any reduction of RCS specific activity less than $0.35 \,\mu$ Ci/gram Dose Equivalent I-131 requires an evaluation of release rate data as described in Nuclear Technology, Vol. 94, p. 361 (1991), J. P. Adams and C. L. Atwood, The Iodine Spike Release Rate During a Steam Generator Tube Rupture. This evaluation was performed for BVPS Unit 1 and is provided in Attachment D. This evaluation shows that BVPS Unit 1 RCS Dose Equivalent

I-131 data fully supports lowering the Technical Specification RCS specific activity limit to 0.20 μ Ci/gram without compromising the Standard Review Plan assumption of a post-event iodine spike factor of 500.

D. SAFETY ANALYSIS

This proposed change which lowers the Technical Specification limit for Dose Equivalent I-131 is conservative and will not adversely affect the current calculated dose values for BVPS Unit 1 DBAs since a lower RCS specific activity will lower the calculated dose from any resultant steam generator tube leakage postulated during the DBA. As shown by the evaluation in Attachment D, the Standard Review Plan assumption for accident-induced steam generator tube leakage spike remains valid. Thus, the dose listed in the BVPS Unit 1 UFSAR from those DBAs which calculate and list a dose value in the BVPS Unit 1 UFSAR will remain bounding values, except for the Main Steam Line Break (MSLB) DBA.

The immediate effect upon receiving a revised lower primary coolant specific activity limit in Technical Specification 3.4.8.a would also result in a lower calculated MSLB dose value, if incorporated into the MSLB dose calculation without any other modifications. But the BVPS Unit 1 MSLB analysis is analyzed per GL 95-05 which states that a reduction on RCS iodine activity is an acceptable means for accepting higher projected leakage rates and still meeting the applicable limits of Title 10 of the Code of Federal Regulations Part 100 and GDC 19 utilizing currently accepted licensing basis assumptions. Thus, pursuant to this GL 95-05 methodology, the reduced RCS specific activity limit for Technical Specification 3.4.8.a will be used to allow for a higher POL, while still meeting the applicable regulatory dose limits. The MSLB control room thyroid dose value will increase slightly from the previous value of 29 REM to 30 REM (as shown in UFSAR Table 11.3-7) solely as a calculational convenience to allow for the maximum POL. This is consistent with the GL 95-05 methodology since the dose value will not exceed the previously approved regulatory limit (which is 30 REM for control room thyroid dose). Attachment E provides the new primary-tosecondary SG leakage limit in the faulted SG based on the reduced RCS specific activity. The new faulted SG leakage limit will be described in the UFSAR and will be used in the SG inspection program to comply with the SG tube repair criteria. Based on these analyses, the control room and offsite doses have been

analyzed and shown to comply with the regulatory limits; therefore, these changes do not significantly reduce the margin of safety of the plant.

Thus, the current BVPS Unit 1 MSLB calculated dose value will not decrease with a new lower RCS specific activity value in order to allow for a higher POL. However, the BVPS Unit 1 MSLB calculated dose values will remain within the limits specified in 10 CFR 50, Appendix A, GDC 19, and the radiological doses to the public will remain a small fraction of the regulatory limits specified in 10 CFR 100.11, using methodology previously accepted in BVPS Unit 1 License Amendment No. 205.

Thus, this requested license amendment will not adversely affect the current licensing bases.

E. NO SIGNIFICANT HAZARDS EVALUATION

The no significant hazard considerations involved with the proposed amendment have been evaluated. The evaluation focused on the three standards set forth in 10 CFR 50.92(c), as quoted below:

The Commission may make a final determination, pursuant to the procedures in paragraph 50.91, that a proposed amendment to an operating license for a facility licensed under paragraph 50.21(b) or paragraph 50.22 or for a testing facility involves no significant hazards consideration, if operation of the facility in accordance with the proposed amendment would not:

- (1) Involve a significant increase in the probability or consequences of an accident previously evaluated; or
- (2) Create the possibility of a new or different kind of accident from any accident previously evaluated; or
- (3) Involve a significant reduction in a margin of safety.

The following evaluation is provided for the no significant hazards consideration standards.

1. Does the change involve a significant increase in the probability or consequences of an accident previously evaluated?

The proposed change to the BVPS Unit 1 primary coolant specific activity limit is conservative with respect to the current value, does not invalidate the current Standard Review Plan assumption on accident-induced spiking, and does not change the RCS or steam generators' ability to meet its design bases.

Therefore, this change will not increase the probability of occurrence of a postulated accident or will not significantly increase the consequences of an accident previously evaluated since the change would continue to comply with the current BVPS Unit 1 and Unit 2 licensing basis as it relates to the dose limits of GDC 19 and 10 CFR Part 100.

2. Does the change create the possibility of a new or different kind of accident from any accident previously evaluated?

The proposed license amendment to the primary coolant specific activity limit does not change the way the RCS is operated. The proposed changes only involve changes to the primary coolant specific activity limit where continued power may occur. This reduced limit is conservative and does not alter the RCS or steam generators' ability to perform their design bases.

Therefore, these proposed changes do not create the possibility of a new or different kind of accident from any previously evaluated accident since the RCS and steam generator will continue to operate in accordance with their design bases.

3. Does the change involve a significant reduction in a margin of safety?

The proposed amendment does not involve revisions to any safety limits or safety system setting that would adversely impact plant safety. The proposed amendment does not adversely affect the ability of systems, structures or components important to the mitigation and control of design bases accident conditions within the facility. In addition, the proposed amendment does not affect the ability of safety systems to ensure that the facility can be maintained in a shutdown or refueling condition for extended periods of time.

The proposed license amendment to the primary coolant specific activity limit does not adversely change the way the RCS or steam generators are operated. This modification does not alter these systems' ability to perform their design bases. The existing safety analyses remain bounding. Therefore, the margin of safety is not significantly reduced.

F. NO SIGNIFICANT HAZARDS CONSIDERATION DETERMINATION

Based on the considerations expressed above, it is concluded that the activities associated with this license amendment request satisfy the requirements of 10 CFR 50.92(c) and, accordingly, a no significant hazards consideration finding is justified.

G. ENVIRONMENTAL CONSIDERATION

This license amendment request changes a requirement with respect to the installation or use of a facility component located within the restricted area as defined in 10 CFR Part 20. It has been determined that this license amendment request involves no significant increase in the amounts, and no significant change in the types of any effluents that may be released offsite, and that there is no significant increase in individual or cumulative occupational radiation exposure. This license amendment request may change requirements with respect to installation or use of a facility component located within the restricted area or change an inspection or surveillance requirement; however, the category of this licensing action does not individually or cumulatively have a significant effect on the human environment. Accordingly, this license amendment request the eligibility criteria for categorical exclusion set forth in 10 CFR 51.22(c)(9). Pursuant to 10 CFR 51.22(b) no environmental impact statement or environmental assessment need be prepared in connection with the issuance of this license amendment request.

H. UFSAR CHANGES

This proposed license amendment will result in changes to the BVPS Unit 1 UFSAR. See Attachment C for the proposed changes.

BVPS Unit 1 License Amendment Request (LAR) 1A-280 was sent to the NRC by FirstEnergy on May 12, 2000. LAR 1A-280 revised many BVPS Unit 1 UFSAR DBA calculated dose values. This LAR (1A-284) will only result in the Major Secondary System Pipe Rupture (MSLB) dose calculation to be revised (as described above in Section D) to allow for higher POL using methodology previously accepted in BVPS Unit 1 License Amendment 205. The attached proposed UFSAR changes are marked-up using the UFSAR pages previously issued via LAR 1A-280, since the methodology used to prepare LAR 1A-280 was also used to prepare LAR 1A-284.

ATTACHMENT C

Beaver Valley Power Station, Unit No. 1 License Amendment Request No. 284

Applicable UFSAR Changes

UFSAR Pages 14.2-24, 14.2-53, 14B-4

UFSAR Tables 11.3-7, 14.2-10, 14B-15, 14B-16

BVPS-1 FSAR

ERS-ALL

TABLE 11.3-7

POSTULATED CONTROL ROOM ACCIDENT DOSE, REM(5)(6)

(Design Basis Accidents at Unit 1)

Accident	CDE, Thyroid	EDFE	Skin DE	Notes
Main Charm Tine Break				
Main Steam Aine Steam	0.00.01	435-01	~15+00	2
Co-incident Spike	2.96+01	<2E-01	12700	Z .
Pre-incident Spike	1.4E+01	<2E-01	<1E+00	2
Small Line Break	2.0E+01	<2E-01	<1E+00	4
Steam Generator Tube Rupture				
Co-incident Spike	3.1E+00	<2E-01	<1E+00	4
Pre-incident Spike	1.9E+00	<2E-01	<1E+00	. 4
Rod Ejection Accident	7.7E+00	<2E-01	<1E+00	.4
Fuel Handling Accident	(6.3) 3+2E+00	<2E-01	<1E+00	4
Locked Rotor Accident	3.1E+00	<2E-01	<1E+00	1
Loss of Auxiliary AC Power	<1E+00	<2E-01	<1E+00	4
Waste Gas System Rupture				•
Line Break		<2E-01	3.9E+00	4
Tank Rupture		<2E-01	<1E+00	4
DBA LOCA	5.5E+00	7.1E-01	<1E+00	3

NOTES:

INSERT

- 1. Control Room isolation by area radiation monitor signal based on a setpoint with a safety limit dose rate of 1 mrem/hr gamma in the Control Room.
- 2. Isolation by manual operator action at T=30 minutes post-accident. In support of Alternate Repair Criteria for steam generators (ref. USNRC GL 95-05) the MSLB thyroid doses were maximized within applicable limits in order to establish the maximum allowable accident-included leakage against which tube leakage projections, based on poltage indication, are compared. Current values are based primary to secondary leakage (0-2-hour Exclusion Area on(S?0/ggm Boundary thyroid dose limiting). See Section 14.2.5.1.3.
- 3. Control Isolation actuated by CIB signal.
- ERS-JTL-99-015 4. No action required. JTL-99-015 . ERS - JTL - 99 - 009
- ruired. JTL-99-015 (ERS-JTL-99-610) (ERS-JTL-99-005 ERS-SFL-93-005 10, ERS-SFL-92-033 JZ, 12241/14110.39-5. References: -UR(B) 456, 14110.39-UR(B) 457 20, ERS-SFR-89-021 21, ERS-SFL-95-008
- 6. Listed dose values represent the limiting bounding value.

(12241/11700 · VR(B) - 480

BVPS-1 FSAR

ERS-BIL

TABLE 11.3-7

POSTULATED CONTROL ROOM ACCIDENT DOSE, REM(5)(4)

(Design Basis Accidents at Unit 1)

Accident	CDE,	ر کر		
LAR 14-27	4 Thyroid	$\left(\underline{EDf} E \right)$	<u>Skin DE</u>	Notes
Main Steam Line Break		\sim		
Co-incident Spike 3.0E+	01 2.9E+01)	<2E-01	<1E+00	2
Pre-incident Spike	1.4E+01	<2E-01	<1E+00	2
Small Line Break	2.0E+01	<2E-01	<1E+00	4
Steam Generator Tube Rupture				
Co-incident Spike	3.1E+00	<2E-01	<1E+00	4
Pre-incident Spike	1.9E+00	<2E-01	<1E+00	. 4
				مر م
Rod Ejection Accident	7.7E+00	<2E-01	<1E+00	. 4
	(6.3)			
Fuel Handling Accident	3-2E+00	<2E-01	<1E+00	4
Locked Rotor Accident	3.1E+00	<2E-01	<1E+00	1
•				•:
Loss of Auxiliary AC Power	<1E+00	<2E-01	<1E+00	4
Waste Gas System Rupture				
Line Break		<2E-01	3.9E+00	4
Tank Rupture		<2E-01	<1E+00	4
DBA LOCA	5.5E+00	7.1E-01	<1E+00	3

NOTES:

INSERT

1. Control Room isolation by area radiation monitor signal based on a setpoint with a safety limit dose rate of 1 mrem/hr gamma in the Control Room.

2. Isolation by manual operator action at T=30 minutes post-accident. LAR 1A-224 In support of Alternate Repair Criteria for steam generators (ref. change USNRC GL 95-05) the MSLB thyroid doses were maximized within applicable limits in order to establish the maximum allowable accident-included leakage against which tube leakage projections, based on voltage indication, are compared. Current values are based primary to secondary leakage (0-2 hour Exclusion Area on(z. Boundary thyroid dose limiting). See Section 14.2.5.1.3. ERS-JTL-99-01

3. Control Isolation actuated by CIB signal.

ERS-JTL- 99-010 4. No action required.

ERS-JTL-99-009 JTL-99-015 ERS-SFL-93 005 10, VERS-SFL-92-033 17, V12241/14110-39-5. References: -UR(B) 456, 14110.39-UR(B) 457 J8, ERS-SFR-89-021 x1, ERS-SFL-95-008

6. Listed dose values represent the limiting bounding value.

(12241/11760 - VR(B) - 480

The sequence of events is shown in Table 14.2-2.

Radiological Consequences

The radiological consequences of a main steam line break (MSLB) were re-analyzed in support of the Alternate Repair Criteria (ARC) for steam generators (ref. USNRC GL 95-05)⁽²⁵⁾. The MSLB is of interest due to the rapid depressurization of the secondary side and the high differential pressure across the steam generator tubes that can occur. Such conditions can result in accident-induced primary-to-secondary leakage. The ARC allows steam generator tubes having defects to remain in service with higher non-destructive examination (NDE) indications than would have been allowed under prior repair criteria, subject to conditions established in technical specifications. One such requirement is to project, on the basis of the NDE indication (voltage), the potential MSLB-induced leakage (95% prediction with 95% confidence), and the offsite and control room operator doses that could result.

In lieu of calculating the radiological consequence of this event with each operating cycle, an analysis was performed to establish a maximum allowable accident-induced leakage, against which the cycle leakage projections could be compared. This leakage rate is the maximum primary-to-secondary leakage that could occur with ooffsite and control room operator doses remaining within 30 day applicable limits. This re-analysis showed that the 30 rem 0-2 hour thyroid dose at the technology area boundary was limiting with a projected leakage of 8:0 gpm. Since steam generator tubes with NDE indications corresponding to potential leak rates greater than 8:0 gpm will be repaired, this is expected to be the bounding case for future operating cycles. To the room operator

The MSLE is assumed to occur between the containment wall and the main steam isolation valve, resulting in an unisolable release path to the environment. This re-analysis was performed using the guidance of the Standard Review Plan $(SRP)^{(27)}$ with two exceptions: (1) the dose calculation methodology (see Section 14B.8.5) is based on ICRP-26 and ICRP-30 principles rather than that described in the SRP, and (2) the primary-to-secondary leak rate is the 95% prediction 95% confidence leak rate projected on the basis of NDE indications rather than the value established by technical specification.

The analysis assumes that the unit is operating with technical specification primary and secondary coolant specific activities. In conjunction with this analysis, the reactor coolant system specific activity technical specification was reduced from 1.0 μ Ci/gm to 0.35 μ Ci/gm. A primary-to-secondary technical specification leakrate of 150 gpd is assumed in all steam generators prior to the event and in the remaining steam generators post-event. The thermodynamic analysis indicates that DNB is not exceeded and, therefore, no fuel damage is projected.

LAR 14-250

The sequence of events is shown in Table 14.2-2.

Radiological Consequences

LAR 1A -284

ccident induced

12 1A-254

LAI

The radiological consequences of a main steam line break (MSLB) were re-analyzed in support of the Alternate Repair Criteria (ARC) for steam generators (ref. USNRC GL 95-05)⁽²⁵⁾. The MSLB is of interest due to the rapid depressurization of the secondary side and the high differential pressure across the steam generator tubes that can occur. Such conditions can result in accident-induced primary-to-secondary leakage. The ARC allows steam generator tubes having defects to remain in service with higher non-destructive examination (NDE) indications than would have been allowed under prior repair criteria, subject to conditions established in technical specifications. One such requirement is to project, on the basis of the NDE indication (voltage), the potential MSLB-induced leakage (95% prediction with 95% confidence), and the offsite and control room operator doses that could result.

In lieu of calculating the radiological consequence of this event with each operating cycle, an analysis was performed to establish a maximum allowable accident-induced leakage, against which the cycle leakage projections could be compared. This leakage rate is the maximum primary-to-secondary leakage that could occur with ooffsite and control room operator doses remaining within 30 day applicable limits. This re-analysis showed that the 20 rem 0-2 hour thyroid dose at the technic area boundary was limiting with a projected heakage of 200 gpm. Since steam generator tubes with NDE indications corresponding to potential leak rates greater than 200 gpm will be repaired, this is expected to be the bounding case for future operating cycles. To future is absurded to compare the second to be the bounding case for future operating cycles.

The MSLB is assumed to occur between the containment wall and the main steam isolation valve, resulting in an unisolable release path to the environment. This re-analysis was performed using the guidance of the Standard Review Plan $(SRP)^{(27)}$ with two exceptions: (1) the dose calculation methodology (see Section 14B.8.5) is based on ICRP-26 and ICRP-30 principles rather than that described in the SRP, and (2) the primary-to-secondary leak rate is the 95% prediction 95% confidence leak rate projected on the basis of NDE indications rather than the value established by technical specification.

The analysis assumes that the unit is operating with technical specification primary and secondary coolant specific activities. In conjunction with this analysis, the reactor coolant system specific activity technical specification was reduced from 1.0 HGi/gm to 0.25 HCi/gm. A primary-to-secondary technical specification leakrate of 150 gpd is assumed in all steam generators prior to the event and in the remaining steam generators post-event. The thermodynamic analysis indicates that DNB is not exceeded and, therefore, no fuel damage is projected. <Page 14.2-53 Insert>

- 20. SWEC Calculation 12241/11700 UR(B)-480, Radiological Dose Consequences at the EAB, LPZ, and in the Control Room due to a Postulated LOCA at Beaver Valley Power Station, Unit 1, 1999.
- 21. DLC Calculation ERS-JTL-99-014, Safety Analysis of the Radiological Consequences of a Waste Gas System Rupture DBA at Unit 1, Control Room, EAB and LPZ doses, 1999.
- 22. DLC Calculation ERS-JTL-99-009, Safety Analysis of the Radiological Consequences of a Fuel Handling DBA at BVPS Unit 1, Control Room, EAB and LPZ Doses, 2000.
- 24. DLC Calculation ERS-SFL-95-008, Safety Analysis of the Common Control Room, EAB and LPZ Doses from a Main Steam Line Break Outside of CNMT at U1 with Increased Primary-to-Secondary Leakage, 1999.

<Page 14.2-53 Insert>

- 20. SWEC Calculation 12241/11700 UR(B)-480, Radiological Dose Consequences at the EAB, LPZ, and in the Control Room due to a Postulated LOCA at Beaver Valley Power Station, Unit 1, 1999.
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- 22. DLC Calculation ERS-JTL-99-009, Safety Analysis of the Radiological Consequences of a Fuel Handling DBA at BVPS Unit 1, Control Room, EAB and LPZ Doses, 2000.
- 24. DLC Calculation ERS-SFL-95-008, Safety Analysis of the Common Control Room, EAB and LPZ Doses from a Main Steam Line Break Outside of CNMT at U1 with Increased Primary-to-Secondary Leakage, 1999.

2000 LAR 14-284 Change

Insert

TABLE 14.2-10

PARAMETERS USED IN MAIN STEAM LINE BREAK RADIOLOGICAL ANALYSIS 2705 Power, MWt Lost Offsite AC Power Initial Primary Coolant Activity, Dose Equivalent I-131, uCi/g 0.35 Initial Secondary Coolant Activity, Dose Equivalent I-131, uCi/g 0.1 Table 14B-15 Initial Primary and Secondary Isotopic Concentrations I-131 1.16E+06 Concurrent Iodine Spike Release Rates, uCi/s I-132 1.12E+06 (Specific for the Main Steam Line Break) I-133 1.99E+06 I-134 1.24E+06 1.49E+06 I-135 Table 14B-16 Pre-accident Iodine Spike Concentrations 4 Iodine Spike Duration, (hours) Primary-to-Secondary Leak Rate 150 Pre-event, each SG, gpd 3.0. Affected SG Accident Induced gpm 150 Post event, each SG, gpd Steam Generator Fluid Content 148,104 +10% Liguid, 1bm 5,781 +10% Steam, 1bm RCS Liquid Content, 1bm 329,500 Total 314,500 Less Pressurizer Steam Release From Affected SG, 1bm 170,050 0-30 min (Initial content and 3.104 gpm) 1397 30 min - 8 hours (3.104 gpm) Steam Release from Intact SG, 1bm 366,776 0-2 hours 705,393 2-8 hours 8 Duration of Release, hours Iodine Partition Factor 1.0 Affected SG 1.0 Intact SGs (Initially) 0.01 Intact SGs (After 1 hour)

LAR 14-280

(Insert)

LAR 14-284

TABLE 14.2-10

PARAMETERS USED IN MAIN STEAM LINE BREAK RADIOLOGICAL ANALYSIS

Power, MWt	2705
Offsite AC Power	LAR 1A-284 Change Lost
Initial Primary Coolant Activity, Dose Equivalent I-131,	uci/g
Initial Secondary Coolant Activity, Dose Equivalent I-131	l, uCi/g 0.1
Initial Primary and Secondary Isotopic Concentrations	Table 14B-15
Concurrent Iodine Spike Release Rates, uCi/s (Specific for the Main Steam Line Break)	I-131 (1.16E+06) I-132 1.12E+06 I-133 1.99E+06
	I-134 I.24E+06
Pre-accident Iodine Spike Concentrations 6.59E+05	Table 14B-16
Iodine Spike Duration, (hours) 6.41E+05	4
Primary-to-Secondary Leak Rate Pre-event, each SG, gpd Affected SG Accident Induced gpm Post event, each SG, gpd LAR 2A-284	150 3.0 150
Steam Generator Fluid Content change Liquid, 1bm Steam, 1bm	148,104 +10% 5,781 +10%
RCS Liquid Content, 1bm Total Less Pressurizer	329,500 314,500
Steam Release From Affected SG, 1bm 0-30 min (Initial content and 3.104 gpm) 30 min - 8 hours (3.104 gpm)	170,050 1397
Steam Release from Intact SG, lbm 0-2 hours 2-8 hours	366,776 705,393
Duration of Release, hours	8
Iodine Partition Factor Affected SG Intact SGs (Initially) Intact SGs (After 1 hour)	1.0 1.0 0.01

boron concentration reduction rate by feed and bleed, ppm per second

= removal efficiency of purification cycle for
huclide

1 = radioactive decay constant

V = escape rate coefficient for diffusion into coolant

Subscript c refers to core

-B 1

Έ

LAR IA-280

Subscript w refers to coolant

Subscript i refers to parent nuclide

Subscript j refers to daughter nuclide

14B.4.1 <u>Reactor Coolant and Secondary System Equilibrium</u> <u>Activities</u>

The reactor coolant activities tabulated in Table 14B-6 are based on 1.0% failed fuel. While these activities were the basis of most design basis radiological analyses performed during original licensing, current analysis practice is to base many of these analyses on the primary and secondary equilibrium activities that correspond to the specific activity limits for reactor coolant and secondary coolant provided in technical specifications. Table 14B-15 tabulates these equilibrium activities.

14B.4.2 Reactor Coolant System Iodine Spiking

Two cases of iodine spiking are considered in current design basis radiological analyses. The first is the pre-incident spike which occurs such that the technical specification maximum 21 μ Ci/gm dose equivalent I-131 concentrations are reached just prior to accident initiation. The second case is the iodine spike that is initiated by the accident transient (i.e., coincident spike). For this case, regulatory practice requires analyses to include an iodine spike appearance rate that is 500 times the iodine appearance rate that would result in RCS equilibrium concentrations equal to the 0.35 μ Ci/gm technical specification. Table 14B-16 tabulates the pre-incident spike concentrations and the co-incident iodine spike appearance rates. Methodology for calculating co-incident

idme spike release rates.



Subscript j refers to daughter nuclide

14B.4.1 <u>Reactor Coolant and Secondary System Equilibrium</u> <u>Activities</u>

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14B.4.2 Reactor Coolant System Iodine Spiking

Two cases of iodine spiking are considered in current design basis radiological analyses. The first is the pre-incident spike which occurs such that the technical specification maximum $\frac{21 \ \mu Ci/gm}{dose}$ equivalent I-131 concentrations are reached just prior to accident initiation. The second case is the iodine spike that is initiated by the accident transient (i.e., 'coincident spike). For this case, regulatory practice requires analyses to include an iodine spike appearance rate that is 500 times the iodine appearance rate that would result in RCS equilibrium concentrations equal to the $-0.35 - \mu Ci/gm$ technical specification. Table 14B-16 tabulates the pre-incident spike concentrations and the co-incident iodine spike appearance rates. Methodology for calculating co-incident

idme spike release rates.

D LAR 1A-284 Deleted

14B-4

BVPS-1-UPDATED FSAR

TABLE 148-15

PRIMARY AND SECONDARY EQUILIBRIUM ACTIVITIES Corresponding to 0.35 µCi/qm Dose Equivalent I-131 in RCS⁽¹⁾

			8G	BG
		RCS	Liquid	Steam
Nuclide	μ	ci/gm	µCi/gm	µCi/gm
Kr-83n	4.02 8-02 4	65E-02-		-4-535-07- 6.45E-07
Kr-85m	1.412-01 2-	27E-01-		-2-21E-06-1.59 E-04
Kr-85	1.48 E+01 1-	-20E+00		1-17E-05-2.00E-04
Kr-87	9.446-02 2	-30E-01	•	1-26E-06 1.27 E-06
Kr-88	244 E-01 3-	46E-01-		
Kr-89	7.65E-03 1-	-09E-02		1.07E-07 -103E-07
Xe-131m	4.79 E-01 1-	17E-02		2-14E-07- 6.45E-00
Xe-133m	4.00 E -01 3-	.33E-01		3 ~25E-06- 5.42 <i>E</i> -06
Xe-133	2975+01 2-	84E+00		- 2.772-05 4.00E-04
Xe-135n	9.165-02 =	18E-01-		1-15E-06-261E-06
Xe-135	9.85E-01 3	.48E-01		3-402-06-1.44 E-05
Xe-137	1.89E-02 1	775-02-		-1-72E-07-255E-07
Xe-138	· 6·47E-02 77	-28E-02-		7 -10E-07- 7.72E-07
I-131	2.74 E-01 2-	.72E-01-	8.382-028-11E-02	8-11E-048.38E-04
I-132	1.08E-01 9	.48E=02	1.35E-02 1-44E-02	1-44E-04 1.35E-04
I-133	4115-01 4-	-34E-01-	9.13E-02 1-068-01	1-06E-039.13 E-04
I-134	6.05E-02 5	.932-02	1.76 5-03 2-543-03	2 ~545-05 1.76E-05
I-135	2.36 E-01 2	-28E-01-	3,19 E-02- 2-888-02	3 .882 -04 3.195-04

Notes:

- 1. Steam generator liquid based on 0.1 μ Ci/gm D.E. I-131 in steam generator.
- 2. Ref: HRS-SFL-96-012 r1, 1996 ERS-AJL-99-007

1 of 1

LAR 1A-284

			TABLE	14B-15		LAR 1A- Addition	284
		PRIMARY AND	SECONDARY	EQUILIBRIUM AC	TIVITIES		
Nuclide	Corresp Dose Equ RCS µCi/g	onding to 0.3 ivalent I-131 SG Liquid µCi/g	5 μCi/g in RCS ⁽¹⁾ SG Steam μCi/g	F	Corresp Dose Equ RCS µCi/g	oonding to 0.2 Nivalent I-131 SG Liquid <u>µCi/g</u>	0 μCi/g in RCS ⁽¹⁾ SG Steam μCi/g
Kr-83m	4.02E-02		6.45E-07		2.30E-02		3.695-07
Kr-85m	1.41E-01		1.89E-06		8.04E-02		1.148-04
Kr-85	1.48E+01		2.00E-04		8.44E+00		1.145-04
Kr-87	9.44E-02		1.27E-06	/	5.39E-02		7.205-07
Kr-88	2.64E-01		3.55E-06		1.51E-01		2.035-00
Kr-89	7.65E-03		1.03E-07		4.37E-03		5.885-00
Xe-131m Xe-133m Xe-133 Xe-135m Xe-135 Xe-137 Xe-138	4.79E-01 4.00E-01 2.97E+01 9.16E-02 9.85E-01 1.89E-02 6.47E-02		6.45E-06 5.42E-06 4.00E-04 8.61E-06 1.44E-05 2.55E-07 8.72E-07		2.74E-01 2.29E-01 1.69E+01 5.23E-02 5.63E-01 1.08E-02 3.70E-02		3.69E-06 3.10E-06 2.29E-04 4.92E-06 8.21E-06 1.46E-07 4.98E-07
I-131 I-132 I-133 I-134 I-135	2.74E-01 1.08E-01 4.11E-01 6.05E-02 2.36E-01	8.38E-02 1.35E-02 9.13E-02 1.76E-03 3.19E-02	8.38E-04 1.35E-04 9.13E-04 1.76E-05 3.19E-04		1.57E-01 6.17E-02 2.35E-01 3.46E-02 1.35E-01	8.38E-02 1.35E-02 9.13E-02 1.76E-03 3.19E-02	8.38E-04 1.35E-04 9.13E-04 1.76E-05 3.19E-04

Notes:

. . •

1. For iodine, steam generator liquid phase based on 0.1 μ Ci/g D.E. I-131 in steam generator, with 0.01 partitioning in steam phase

2. Ref.: ERS-AJL-99-007 Addition

TABLE 148-16

RCS IODINE SPIKE ACTIVITIES

Pre-incident Concentration, µCi/gm (Corresponding to 21 µCi/gm d.e. I-131)

I-131	(.645+0) -16-9-
I-132	6.48 E+00 -5.69-
I-133	2.46 E+01 25.4
I-134	3.63 E+00 3.96
I-135	1-426+01-23-7-

Co-incident Iodine Spike Appearance Rates, Ci/sec (500x Equilibrium Rate for 0.35 µCi/gm d.e_7-131)



Notes:

1. Ref: <u>ERS-SFL-96-012-r1, 1996</u> ERS - AJL -99-007

INSERT

PARAMETERS AND ASSUMPTIONS AND MODEL USED FOR CALCULATING IODINE RELEASE RATES INTO REACTOR COOLANT DUE TO A CONCURRENT IODINE SPIKE

Thyroid dose conversion factors	<u>Nuclide</u> I-131 I-132 I-133 I-134 I-135	<u>mrem/μCi</u> 1.08E+03 6.44E+00 1.80E+02 1.07E+00 3.13E+01
Nuclide decay constants (λ_r)	<u>Nuclide</u> I-131 I-132 I-133 I-134 I-135	<u>second</u> ⁻¹ 9.9783E-07 8.3713E-05 9.2568E-06 2.1963E-04 2.9129E-05

Technical Specification maximum allowable values

Limiting value specific to the accident

1.0

120 gpm

Table 14B-15

concentrations (EQ)

Formula for iodine loss constant

Reactor coolant system leakage (L)

Reactor coolant system mass (M)

Letdown purification removal (E)

Letdown purification flow rate (F)

Technical Specification equilibrium

 $\lambda_{\text{total}} = (F^*E/M) + (L/M) + \lambda_T$

Concurrent iodine spike release rate (RR)

 $RR = EQ * M * \lambda_{total}$

NOTES:

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Formulas for iodine release rates from EPRI Report, "Review of Iodine Spike Data from PWR Power Plants in Relation to SGTR with MSLE, TR-103680)" This Table is applicable to design basis accident analyses performed subsequent to December 1998.

TABLE 148-16

	RCS IODINE SPIK	LAR 1A-284 Addition	
	Pre-incident Conce		
	Corresponding to	Correspon	nding to
	$21 \ \mu C 1/g \ D.E. \ 1-131$	τ_121	
	I-131 1.64E+UI		9.40E+00
	I-132 6.48E+00	1-132	3.702+00
	I-133 2.46E+01	y 1-133	1.41E+01
	I-134 3.63E+00	/ I-134	2.08E+00
	I-135 1.42E+01	I-135	8.11E+00
	<u>Co-incident Iodine Spike Rate - Pa</u>	arameters, Assump	tions and Model
	Thyroid dose conversion factors	Nuclide	mrem/µCi
		1-131	1.08E+03
		T-132	6.44E+00
		T-133	1.80E+02
		T-133	1 075+00
		1-134	2 122101
		1-135	3.136401
	$\mathbf{W}_{\mathbf{r}}$ ide decay constants ()	Nuclide	second ⁻¹
	Nuclide decay constants (Mr)	T-121	<u>9 97935-07</u>
		1-131	9.97036-07
		1-132	8.3/136-05
		I-133	9.2568E-06
		I-134	2.1963E-04
	•	I-135	2.9129E-05
	Reactor coolant system leakage (L) Technical maximum al	Specification lowable value
at -	Reactor coolant system mass (M)	Limiting v to the acc	value specific cident
bun	Letdown purification removal (E)	1.0	
کُر U	Letdown purification flow rate (F) 120 gr	mc
	RCS Equilibrium concentrations (E	Q) Table	14B-15
	Formula for iodine loss constant	$\lambda_{\rm total} = (F^*E/I)$	$M) + (L/M) + \lambda_r$
	Co-incident iodine spike release rate (RR)	RR = EQ * M	* A _{total}
	Notes: 1. Formulas for iodine release rational for the second se	ted from EPRI Rep Plants in Relatio sign basis accide 1998.	ort, "Review of on to SGTR with nt analysis

LAR IA-284

LAR 14-254

ATTACHMENT D

Beaver Valley Power Station, Unit No. 1 License Amendment Request No. 284

Evaluation of BVPS Unit 1 Release Rate Data

Evaluation of BVPS Unit 1 Release Rate Data

BVPS has investigated the history of iodine spiking at Unit 1 in support of the effort to lower the Dose Equivalent I-131 Technical Specification 3/4.4.8 limit for the Reactor Coolant System (RCS) to 0.20 microcuries per gram. This analysis was performed pursuant to NRC Generic Letter (GL) 95-05, Section 2.b.4, for plants reducing their Dose Equivalent I-131 limit to justify the iodine spiking assumptions used in accordance with the Standard Review Plan.

GL 95-05 requires that the spiking analysis be performed using the methodology described in *The Iodine Spike Release Rate during a Steam Generator Tube Rupture*, J. P. Adams and C. L. Atwood, Nuclear Technology, Volume 94, page 361 (1991).

BVPS Unit 1 RCS iodine values were reviewed, starting with Cycle 5 data in 1985, and concluding with Cycle 13 data in the year 2000 (Cycle 5 was selected as the starting point since there is no fuel failure data prior to Cycle 5, and the iodine data prior to 1985 frequently lacks all of the data requirements listed in Adams and Atwood). Over 1600 RCS iodine analyses were reviewed; 56 of these were directly related to plant trips. Of the 56 trips reviewed, only 28 met all of the data requirements of Adam and Atwood:

- 1. Sufficient steady-state power prior to the plant trip to ensure an adequate buildup of iodine. The specific criterion used was a minimum of 5 days at steady-state power operation, resulting in a minimum of 35% of the steady state I-131 concentration. In nearly all cases, the steady-state power operation lasted several weeks to several months rather than the minimum of 5 days.
- 2. Knowledge of the steady-state iodine concentration.
- 3. Availability of at least one post trip chemistry sample taken 2 to 6 hours after the plant trip.
- 4. No post trip RCS perturbation (e.g., recriticality) prior to the RCS sample.
- 5. Availability of all requisite transient information (purification flow, plant trip date and time, post trip sample date and time).

Additionally, the purification flow rate had to be constant before and after the transient, as was stated in Adams and Atwood, Section II.C.

The 28 plant trips that met all of the data requirements of Adams and Atwood were then subject to analysis as described in their paper. The results are listed in Table 1. All values are well within the bounds of the data set listed in Adams and Atwood. One cycle (Cycle 7) operated defect free; the other cycles had defects ranging from one failed rod to 35 failed rods. In all cases, the release rate spike factor was well below the Standard Review Plan assumed value of 500.

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In addition, all RCS Dose Equivalent I-131 spike values were below the proposed RCS limit of 0.20 microcuries per gram. One RCS Dose Equivalent I-131 value, taken following the spike on May 7, 1994, comes very close to the proposed limit (1.969E-1 microcuries per gram), yet had a spike of only 91.82. Other recorded spike values were well below the proposed 0.20 microcuries per gram limit, and had spike factors well below 500 as well.

Finally, the maximum normalized release rate was calculated to be 7.463E-2 Ci/hr*Mwe. This release rate is far below the 95% confidence bound on the 90th percentile, given by Adams and Atwood as 1.09 Ci/hr*Mwe.

Therefore, using the methodology referenced by GL 95-05, the RCS Dose Equivalent I-131 data fully supports lowering the RCS Dose Equivalent I-131 Technical Specification limit to 0.20 microcuries per gram without compromising the Standard Review Plan assumption of a post-event iodine spike factor of 500.

It is noted that the BVPS Unit 1 RCS Dose Equivalent I-131 data is below most industry values because the BVPS Unit 1 fuel failure mechanisms (primarily grid-to-rod fretting) have placed most of the BVPS Unit 1 fuel failures in the peripheral regions of the core. The power factors in these peripheral regions are very low due to the BVPS Unit 1 use of low-leakage core designs. Therefore, although BVPS Unit 1 has had a number of fuel failures, they have occurred in rods where there was relatively little generation of fission products.
Table 1

 Evaluation of BVPS Unit 1 Iodine Release Rate Data

Sample Date & Time	% Power	I-131	DEI-131	DEI-131 SPIKE	R3(2) (Ci/hr)	R3(2)/P (Ci/hr*Mwe)
2/10/85 14:15	100	1.118E-03	2.987E-03			
2/20/85 8:36	0	4.002E-04	2.259E-03	7.565E-01	7.280E-01	8.545E-04
4/18/85 19:15	97.8	9.899E-04	2.758E-03			
4/26/85 21:27	0	5.402E-04	2.098E-03	7.606E-01	6.760E-01	8.112E-04
9/9/85 17:40	98	1.570E-03	6.447E-03		· · · · ·	
9/16/85 12:38	0	3.581E-03	9.193E-03	1.426E+00	2.962E+00	3.547E-03
5/9/86 18:00	84.7	5.962E-03	2.049E-02			
5/17/86 3:15	0	2.488E-02	3.635E-02	1.774E+00	1.174E+01	1.627E-02
End Cycle 5						
1/11/87 19:55	98.8	3.472E-03	6.812E-03			
1/12/87 3:46	0	2.080E-02	2.447E-02	3.592E+00	7.884E+00	9.366E-03
2/1/87 19:25	100	1.950E-03	5.229E-03			
2/8/87 12:00	0	3.828E-02	4.276E-02	8.177E+00	1.376E+01	1.615E-02
4/19/87 16:33	99.5	1.606E-03	4.956E-03			0.0075.00
4/25/87 1:50	0	5.863E-02	7.000E-02	1.413E+01	2.261E+01	2.66/E-02
End Cycle 6						
6/5/88 17:38	99.7	1.983E-03	3.602E-03			4.5405.00
6/11/88 13:10	0	3.856E-03	4.054E-03	1.125E+00	1.308E+00	1.540E-03
5/16/89 17:55	89	1.139E-03	3.060E-03			0.0005.00
5/18/89 4:37	0	1.071E-02	1.644E-02	5.372E+00	5.284E+00	0.9095-03
End Cycle 7						
1/16/90 18:47	100	2.134E-04	1.003E-03		4 0505 04	2 2005 04
1/19/90 20:45		1.494E-04	6.035E-04	6.016E-01	1.9205-01	2.2095-04
3/25/90 17:31	99.4	1.885E-04	9.169E-04		2 0205 01	2 3955-04
3/30/90 18:00		1.656E-04	6.252E-04	0.0192-01	2.0202-01	2.3050-04
7/8/90 16:50	100	7.359E-04	1.814E-03	6.0145+00	2 5255+00	A 127E 02
7/14/90 2:00		9.461E-03	1.091E-02	0.0142700	3.525E+00	4.1372-03
10/5/90 17:57	88	1.41/E-04		4 7065+01	2 5745+01	3 051E-02
10/0/90 0:35		0.724E-02	2 3415-02	4.7002+01	2.5742.01	0.0012-02
12/20/90 16:23	80.5	1.108E-03	2.3412-00	1 181E+01	8 895 =+00	1 060E-02
12/26/90 14:25		2.3002-02	2.7042-02	1.1012.01	0.0352.00	
End Cycle 6	100	1 2245 04	5 8455-04	1		
9/1//91 11:40		1.2.34E-04	8 1155-04	1 388F+00	2 615E-01	3 069E-04
8/10/81 7.45		1.4665-04	6 130E-04		2.0102.01	
10/17/81 10.50		2 6695-04	6 430E-04	1 0495+00	2 070E-01	2.430E-04
10/22/91 0.5		4 140E-04	1 276E-0			
10/0/92 9.0		1 283E-02	1.270E 0	1.398E+01	5,751E+00	7.500E-03
End Cycle 9	1	1.2002 01				
10/12/93 9:30	996	3.303E-04	1.095E-03	3	-	
10/12/03 18:15	3 C	5.711F-02	6.701E-0	6.121E+01	2.165E+01	2.551E-02
5/5/94 8-2	5 100	7.571E-04	2.145E-0	3		
5/7/94 11:00		1.682E-01	1.969E-0	9.182E+0*	6.358E+01	7.463E-02
7/19/94 9:4	5 100	8.411E-04	1 2.994E-0	3		
7/19/94 19:3	5 0	2.862E-02	2 4.167E-02	2 1.392E+0 ⁴	1.340E+0	1 1.573E-02

Sample Date & Time	% Power	1-131	DEI-131	DEI-131 SPIKE	R3(2) (Ci/hr)	R3(2)/P (Ci/hr*Mwe)
	<u> </u>					
End Cycle 10						
8/17/95 8:50	99.7	1.005E-03	3.288E-03			
8/19/95 3:20	0	6.157E-02	7.705E-02	2.343E+01	2.482E+01	2.922E-02
12/14/95 7:57	100	1.523E-03	4.624E-03			
12/19/95 1:00	0	7.817E-02	9.539E-02	2.063E+01	3.089E+01	3.625E-02
End Cycle 11						
5/30/96 9:46	99.8	3.503E-04	1.601E-03			
6/1/96 1:15	0	3.735E-03	5.674E-03	3.544E+00	1.828E+00	2.150E-03
8/1/96 9:25	100	4.642E-04	1.873E-03			
8/5/96 8:53	0	6.474E-04	1.661E-03	8.865E-01	5.337E-01	6.264E-04
3/12/97 10:31	99.5	5.709E-04	2.466E-03			
3/19/97 8:55	0	4.155E-02	5.299E-02	2.149E+01	1.707E+01	2.013E-02
End Cycle 12			T			
1/21/99 9:12	2 100	3.839E-04	1.635E-03)		
1/23/99 13:38	3 0	1.699E-03	2.926E-03	1.790E+00	9.471E-01	1.112E-03
4/8/99 10:35	100	4.021E-04	1.676E-03)		
4/13/99 5:45	5 0	1.027E-03	1.450E-03	8.652E-01	4.669E-01	5.480E-04
9/2/99 9:42	2 100	6.608E-04	2.439E-03)		
9/6/99 19:56	i 0	3.083E-02	3.993E-02	1.637E+01	1.288E+01	1.512E-02
End Cycle 13	1	1			1	

Table 1Evaluation of BVPS Unit 1 lodine Release Rate Data
(Continued)

ATTACHMENT E

Beaver Valley Power Station, Unit No. 1 License Amendment Request No. 284

Safety Analysis of the Control Room, EAB and LPZ Doses from a Main Steam Line Break Outside of Containment at BVPS Unit 1 with Increased Primary-to-Secondary Leakage

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Subje and L CNM	ect: Safety Analysis of the Commo PZ Doses from a Main Steam Line T at U1 with Increased Primary-to-	on Control Room EAB Break Outside of Secondary Leakage	ERS-SFL-95-008	PAGE 1 OF 76
Refe	rence HPM RP/RIP EPP	T/S <u>3/4.4.5</u>	EM	DCP_
Revie	ew Category		10 CFR 50.59	Unit 1 Unit 2
		Not Required	Required	
Purp This EAB maxi perfo	ose: calculation package documents ar and at the LPZ, following a MSLB mum allowable primary-to-seconda prmed in support of a license amen	analysis of the postula outside CNMT at Unit 1 ary leakage in the faulte adment request for alter	ated dose in the common i, with the objective of o ed steam generator. The nate tube plugging crite	on CR, at the determining the his analysis eria (APC).
NOTE autho in the	E: This calculation package documents the rity for any revision in a structure, system, plant licensing basis. The data and/or co it concurrence from Radiological Enginee	e evaluation described above , or component; nor changes inclusions of this package sh ring.	b. This package DOES NOT in procedures, tests and ex all not be extended to other	, in itself, provide periments describe purposes without
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	by 5-15-00 Call 5-15-00 Call 5 18 00	Changed assumed RCS dose equivalent iodine induced leak rate from plume and filter shine	activity limit from 0.3: 131; revised the max 3.0 to 5.5 gpm; remove analyses; eliminated do	5 to 0.20 µCi/g imum accident- d sensitivity and uble-counting of
	app ASC ARAD 6/2/00	T.S. primary-to-second contribution to the pre-a	ary leakage and of the T accident spike concentration	S RCS activity
E	by limit sur S/15/94, chki chki	Revised to include revised RCS to S West Jutes parame	ORIGEN based su /E masses , revised ters , revised conce	eri terms, eri CR arrant radine
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	by See previous cover sheet for chk	Checklist	⊠ input Data □ D ☑ Results	ata Sheets lustrations
	revisions 0 - 4 signatures app	I Methodology	⊠ References Ø P ↓ □ C	ontouts ode Listings
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DISCUSSION

General

This calculation determines control room operator, exclusion area boundary (EAB) and low population zone (LPZ) radiation doses following a main steam line break design basis accident (MSLB DBA) at BVPS Unit 1. Doses for the whole body (effective dose equivalent – EDE), the thyroid (committed dose equivalent – CDE) and the skin (skin dose equivalent – SDE) are calculated. The plant parameters and assumptions used herein are consistent with the plant design basis, and they provide results that define the upper bound of the accident dose consequences. As a design basis calculation, this is not intended to show what the expected doses would be, but rather what they might be if the plant is operated at "worst case" limits (operating at the NRC License limits) and using "worst case" accident conditions. The combination of circumstances that would result in the associated maximum dose is unlikely to occur.

This revision of the MSLB radiological analysis was prompted by a need to increase the allowable accident induced primary-to-secondary leak rate. This became necessary after the Westinghouse analysis of projected end of cycle leak rate produced a Unit 1, Cycle 14 value higher than that analyzed in the previous revision of this calculation. Without compensatory actions, this higher projected leak rate will result in analyzed accident doses that exceed regulatory criteria. Consequently, this analysis is being revised using assumed reactor coolant system (RCS) radioactivity upper limits of 0.20 μ Ci/g steady state and 12 μ Ci/g transient dose equivalent iodine 131. These are lowered from the previous limits of 0.35 μ Ci/g and 21 μ Ci/g, respectively. All other parameters, assumptions and methodologies used in this revision remain unchanged.

Main Steam Line Break Accident

This DBA is described in the Unit 1 UFSAR¹ and NUREG 0800 Chapter 15, Section 15.1.5². Additionally, because BVPS Unit 1 has implemented steam generator alternative repair criteria (ARC), NRC Generic Letter 95-05³ also influences the accident scenario.

The MSLB accident begins with a rupture of one of the three main steam lines that carry steam from the steam generators to the turbine. The break location is assumed to be in the turbine building, because using this as the release point will result in the lowest amount of atmospheric dispersion as the plume travels to the control room ventilation system intake. Because of the relatively longer distances, offsite doses are not influenced by the release location. Consequently, the bounding break location is strongly influenced by release point atmospheric dispersion factor with respect to the control room ventilation system intake. Normally, any steam release in the turbine building would be prevented by closure of the main steam line isolation valve, located in the main steam valve room just outside of the reactor containment building. However, there is only one isolation valve per line and this is assumed to remain open as the single active component failure for this accident.

The line break discussed above represents the most significant radioactivity release pathway. The liquid contents of the associated steam generator will flash to steam, releasing all of the radioactive iodine and noble gas contained therein. Additionally, an assumed existing primary to secondary leak (at the Technical Specification⁴ limit allowable leakage rate) plus additional leakage induced by the accident transient, will continually release radioactivity via the break until the primary system pressure has been reduced to atmospheric pressure.

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Another analyzed release pathway of much less radiological significance is the steam release via the two intact steam generators. Because AC power is assumed to be unavailable, the condenser steam dump valves will remain closed. Because of this, plant heat must be removed by releasing steam through the main steam safety or atmospheric steam dump valves. This release will continue until the RCS has been cooled to the point where the residual heat removal system (RHRS) can be placed in service. Upon the steam line break and reactor trip, the steam valves will open. This is assumed to cause an immediate release of the steam generators steam content and the radioactivity contained therein. Until the RHRS is placed in service, the steam release will continue, releasing a portion of the radioactive iodine that was initially contained in the steam generator liquid, and radioactive noble gas and iodine released into the generators due to assumed, existing primary to secondary leaks (at the Technical Specification⁴ limit allowable leakage rate). Because of the possibility that the water level in the steam generators may drop below the level of the tubes for a brief period, all of the iodine contained in the primary system leakage is assumed to flash with the steam and is released without any credit for retention in the steam generator liquid (partitioning factor of 1.0) until the water level can be restored.

The radiological source term for the MSLB accident consists of the noble gas and iodine contained in the RCS and in the steam generators, both assumed to be at the Technical Specification^{5,6} concentration limits. While no fuel failure is postulated to occur due to the transient, two different scenarios are analyzed which consist of additional iodine being released into the RCS (iodine spike) from existing fuel defects. First an analysis is performed assuming that a spike event has occurred prior to the MSLB. This pre-accident spike raises the RCS activity to the instantaneous limit of 12 μ Ci/g (proposed in this revision), at which time the accident occurs. The second scenario assumes the release of iodine from the fuel as a consequence of the transient. This coincident iodine spike results in a release of iodine into the RCS at a rate assumed to be 500 times that which would maintain the RCS concentration at the 48 hour limit of 0.20 μ Ci/g (proposed in this revision).

Calculation History

As part of the Unit 2 Licensing effort, SWEC performed calculations of the potential control room doses from DBAs at Unit 2^{7,8} and at Unit 1^{9,10}. These calculations became part of the licensing basis for BVPS-1 and 2 and have been documented in the UFSARs^{1,11}.

In 1994, Westinghouse performed analyses¹² to support the interim use of steam generator tube plugging limits based on voltage indications. These analyses included re-analysis of the offsite consequences of a postulated main steam line break during which a degraded tube leaks at rates higher than technical specification limits. Based on these analyses, Westinghouse postulated that a 6.6 gpm leakage could be tolerated and not exceed EAB thyroid dose of 30 rem. Based on correlation analyses it was determined that the potential 95% / 95% leakage rate associated with a 2.0 volt indication was much lower than 6.6 gpm providing reasonable margin of safety. In the licensing action, the NRC authorized use of a 1 volt criterion¹³ for cycle 11. While offsite doses were evaluated in the Westinghouse report, control room doses were not.

In August 1995, the NRC issued Generic Letter 95-05³, Voltage-Based Repair Criteria for Westinghouse Steam Generator Tubes Affected by Outside Diameter Stress Corrosion Cracking. The generic letter specified that the accident leak rate acceptability needed to assess the offsite and control room doses. License amendment requests for these alternate plugging criteria must meet the guidance of the generic letter. Revision 0 (October 1995) analyzed the postulated control room doses at the projected accident leakage rate in support of a license amendment request for cycle 12 and beyond. Since then the calculation has been revised as follows:

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Revision 1 (December 1996) - The source term was calculated based on DE-I-131 values of 0.5 and 0.35 uCi/gm (1.0 uCi/gm in Rev. 0). New short term X/Q values calculated in ERS-SFL-96-021¹⁴ were used. The EAB and LPZ doses were calculated. The DE-I-131 used in Revision 0 was based on the dose conversion factors of TID1484421¹⁵. Revision 1 uses isotopic concentrations developed using the ICRP 26/30 based, EPA Federal Guidance Report No. 11¹⁶ dose conversion factors.

Revision 2 (February 1997) - Corrected typo on LPZ table.

Revision 3 (January 1998) - Revised control room ventilation parameters, and RCS and steam generator mass values. Appendices added to address concurrent lodine spiking, and RCS and steam generator mass values, respectively.

Revision 4 (March 1998) - Revised RCS density value used. A sensitivity analysis of the effect of RCS and steam generator water and steam mass was completed and included.

Revision 5 (June 1999) was performed in response to Condition Report 972390¹⁷ (Corrective Action 972390-2). The requirement for verification of parameters and assumptions imposed by this condition report resulted in substantial changes to this calculation. New source terms were calculated based on revised calculations of core inventory and 1% failed fuel concentrations performed by SWEC^{18,19}. The calculation of concurrent iodine spike appearance rates was revised. Specifically the radioactivity transfer rate constant used in the calculation was revised to include the total RCS Technical Specification leakage (identified + unidentified + primary to secondary leakage), max letdown (purification) flow rate, and max purification efficiency. This revision completely supercedes the previous revision. In addition, the control room dose from control room filter shine and plume shine were calculated.

This Revision (Revision 6) was performed to evaluate the doses resulting from a Main Steam Line Break (MSLB) event assuming that the RCS activity concentration limits are reduced to 0.20 μ Cl/g (48 hour) and dose equivalent I-131. Associated with this is a revised, commensurately higher assumed primary-to-secondary leakage rate in the faulted steam generator. This is in keeping with the purpose of the analysis, that is, to use the highest leakage rate while maintaining doses within all applicable limits. Two slight over-conservatisms are removed: 1) allowable steam generator primary-to-secondary leakage was previously double counted in the concurrent iodine spike calculation, and 2) the maximum transient RCS activity concentration had the 48 hour maximum concentration added to it for the dose calculations. These changes in assumptions have a very small affect on the results. The sensitivity analyses are removed from the calculation package. These are still performed and maintained on file; however, only the bounding case is documented herein. Because the plume and filter shine dose for the control room operator are not included as part of the current design basis assumptions, and the dose contribution from these sources is small, this part of the calculation (added in the last revision) is not carried forward in this revision.

METHODOLOGY

Overall Methodology

The analyses in this revision use version 1.0a of the TRAILS_PC (for Transport of Radioactive mAterial In Linear Systems), PC version documented in ERS-SFL-96-004²⁰. This version is the same as that used in the revisions 1 - 4 analyses with the exception that the 1.0a version calculates the control room, EAB and LPZ doses in a single computer run. This analysis contains no methodologies that have not been previously used in BVPA Unit 1 DBA analyses and reviewed by the NRC.

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Main Steam Line Break Release Modeling

The radioactivity releases from this accident are addressed in a series of cases. The results from applicable cases are summed to obtain the total postulated dose. The release cases are (see Attachment 1):

- FRP: Release from <u>Faulted</u> steam generator, <u>Rupture</u> leakage, <u>Pre-incident</u> RCS iodine spike activity. Release rate from steam generator equal to release rate from RCS. No hold-up or iodine decontamination credited. Eight hour release. Noble gas and iodine considered.
- FRC: Release from <u>Faulted</u> steam generator, <u>Rupture</u> leakage, <u>Concurrent</u> RCS iodine spike activity plus T/S equilibrium activity. Release rate from steam generator equal to release rate from RCS. No hold-up or iodine decontamination credited. Eight hour release. Noble gas and iodine considered.
- ITN: Release from Intact steam generators, <u>Technical Specification limit leakage</u>, RCS <u>Noble</u> gas activity. Release rate from steam generator equal to release rate from RCS. No holdup credited. Eight hour release. Noble gas considered.
- ITP: Release from Intact steam generators, <u>I</u>echnical Specification limit leakage, <u>Pre-incident</u> lodine spike RCS activity. Release rate from steam generator equal to release rate from RCS. Eight hour release. No hold-up credited. However, release rate reduced by factor of 100 to reflect iodine partitioning after one hour.
- Note: Partitioning credit is appropriate whenever the steam generator level is such that the tube leak location is submerged. In this event, the level in the intact steam generators will initially drop, but is assumed to be restored within one hour. See Assumption 1.8 below.
- ITC: Release from Intact steam generators, Technical Specification limit leakage, Concurrent iodine spike plus T/S equilibrium RCS activity. Release rate from steam generator equal to release rate from RCS. Eight hour release. No hold-up credited. However, release rate reduced by factor of 100 to reflect iodine partitioning after one hour.

See note above under ITP

- FLI: Release from Eaulted steam generator, Liquid jodine activity initially present in steam generator. Release rate based on release of 99.9999% of pre-accident activity in the liquid phase in 30 minutes.
- Note: The 30 minute assumption is based on the assumption used in the original and all prior analyses. The exponential release model used front-loads the activity release, thus, the assumption will be retained as it is sufficiently conservative.
- ILI: Release from Intact steam generators, Liquid Iodine activity initially present in steam generator. Release rate based on steaming rate of steam generator. Hold-up is modeled. Release rate reduced by a factor of 100 to reflect iodine partitioning.
- Note: This partitioning is not affected by steam generator level since the activity was dispersed in the liquid prior to the event. Case ITP / ITC / ITN address leakage after the start of the event.
- ASA: Release from <u>All</u> steam generators, <u>Steam</u> space activity initially present in steam generators, pre-incident steam generator activity, <u>All</u> nuclides. Instantaneous puff release (99.9999% in 1 second.).

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For the pre-incident iodine spike cases FTP and ITP, a transient dose equivalent iodine-131 activity of 12 μ Ci/gm will be used (in this revision) to obtain the pre-incident activities for the five iodine nuclides.

For the co-incident lodine spike cases FTC and ITC, the iodine appearance rates are assumed equal to 500 times the iodine appearance rate that yields an operating steady-state 0.20 μ Cl/gm dose equivalent lodine-131 concentration. The lodine spike is additive to the postulated, existing iodine and noble gas equilibrium concentrations at the assumed steady-state concentration. At four hours post accident, the co-incident spike ceases (modeled by dividing lodine appearance rates by 500). This conservative assumption is retained from previous revisions.

For the ITN case, the noble gas concentrations associated with the 0.20 μ Ci/gm dose equivalent lodine-131 RCS equilibrium concentration are used.

For the FLI and ILI cases, the iodine activities in the steam generator liquid phase associated with the 0.1 μ Cl/gm secondary equilibrium concentration dose equivalent iodine-131 Technical Specification limit are used. Noble gases are assumed to enter the steam phase immediately.

For the ASA case, the lodine activities in the steam phase associated with the 0.1 μ Cl/gm secondary equilibrium concentration DE I-131 Technical Specification limit are used. The noble gas activities associated with the primary 0.20 μ Cl/gm RCS equilibrium concentration DE I-131 are used.

Percent Power / Percent Steam Generator Tubes plugged Sensitivity Analysis

Dose from the MSLB accident is primarily dependent upon releases from the faulted steam generator (at the Technical Specification activity concentration limit) and the release of RCS through the faulted steam generator. The source terms for each of these are mass dependent, which is in turn both power level and percent of tubes plugged dependent. As power level changes the source release for one of these increases while the other decreases. This necessitates a sensitivity analysis to determine which combination of percent power and percent plugging results in the highest overall dose as the result of a MSLB accident. This may result in the use of a particular mass that is not bounding for a specific release case, but when used in conjunction with the other mass values is bounding for the total of all release cases. For example, a steam generator steam mass may be used that is not bounding for the total of all release cases.

In order to determine which combination of percent power and percent plugging (and their associated RCS and steam generator mass values) results in the highest dose, sets of source terms and radioactivity transfer rate constants were calculated for the following four cases: (1) 0% power, 0% plugging (2) 0% power, 30% plugging (3) 100% power, 0% plugging and (4) 100% power, 30% plugging. These cases were analyzed for control room thyroid CDE, the limiting dose quantity for the Unit 1 MSLB analysis.

The results of the sensitivity analysis performed for this revision produced the same conclusion as that done for the previous revision. The conditions of 0% power, 30% plugging, produce the bounding accident conditions, and are again used for the bounding conditions in the analysis. Only this combination of power and plugging is included in this calculation package, with the other combination analyses maintained on file.

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INPUT DATA AND ASSUMPTIONS

1.0 Assumptions

- 1.1 The analysis of the main steam line break (MSLB) is based on the guidance provided in Chapter 15.1.5 of Reference 2 supplemented by Reference 3.
- 1.2 There is no failed fuel for the MSLB.

The Unit 1 UFSAR shows that DNB is not exceeded for a MSLB. In accordance with Reference 2, no fuel damage need be assumed if DNB is not exceeded.

- 1.3 The MSLB occurs outside of containment releasing activity from the faulted and the intact steam generators.
- 1.4 The transport of radioactivity from the point of release to the control room intake or offsite receptor is assumed to be instantaneous.
- 1.5 The control room is isolated by manual operator action within 30 minutes.

The validity of this assumption was challenged by the Onsite Safety Committee obtained timing data during validation of Emergency Operating Procedure^{21,22} (EOP) changes related to that amendment. The results indicated that it would take 17 minutes for the operator to manual isolate the control room. This is well within the thirty minute period assumed. The margin is considered adequate to address uncertainty associated with the application of these results at Unit 1, and including the approximate 1.1 minute delay^{23,24,25,26} in equipment response due to loss of AC power and subsequent diesel start and sequencing. See Attachment 2.

1.6 Incoming air is uniformly distributed throughout the control room volume.

This is a conservative assumption in that the radiation monitors will alarm when the exposure rate from the cloud of gases adjacent to the monitor exceeds the setpoint. Assuming complete mixing reduces the concentration and monitor exposure rate, thereby delaying the isolation actuation.

1.7 Loss of power is assumed coincident with the control room isolation actuation.

This assumption differs from that at Unit 2, where, loss of power is assumed coincident with the accident. The Unit 1 assumption is more conservative. However, the Unit 2 assumption meets the requirements of §3.1.1.3 of the UFSAR that states that a loss of offsite power is assumed if the postulated event or its effects results in a reactor or turbine trip. This requirement implies a coincident loss of power. Historically, this analysis has been performed assuming unavailability of the condenser at T = 0 due to the loss of power. This is conservative with respect to Assumption 1.7.

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1.8 The level in the unaffected, intact steam generators is restored to greater than 5% narrow range within one hour.

In response to the rapid pressurization of the main steam line, main steam line isolation (<500 psig) will occur, pressurizer level will drop to below the safety injection actuation set point (1845 psig). When safety injection occurs, all three auxiliary feed water pumps will receive a start signal and will inject water into the steam generators. The EOP²¹ will have the operator isolate feed water to the faulted steam generator. However, the EOP²⁷ directs the operator to ensure that (1) the discharge MOVs for the intact generators are fully open, and (2) once level is restored, that the level is controlled between 5% and 50%. It is significant to note, that if the level is less than 5% in all intact steam generators and feed water flow is less than 350 gpm, a heat sink red path critical safety function terminus is declared and function restoration procedure FR-H.1²⁸ is entered. As long as the heat sink is in a red path, all operator attention is directed to restoring the heat sink. Simulator training scenarios responses indicate that the level is restored to greater than 5% within 30 minutes from completion of blow down of the faulted generator. It is therefore reasonable to assume that partitioning be credited after one hour from the start of the event. The doubling of the expected time to cover the tubes was done to provide additional margin for this qualitative conclusion.

The validity of this assumption was challenged by the OSC during review of the technical specification amendment request for Unit 2. The Procedures group obtained timing data during validation of Unit 2 EOP changes related to that amendment. The results indicated that it would take 43 minutes to restore level. This is well within the one hour period assumed. The margin is considered adequate to address uncertainty associated with the application of these results at Unit 1. See Attachment 2.

1.9 The EDE result provided by TRAILS is assumed to correspond to the whole body photon guideline in NUREG 0800, Section 6.4²⁹, the skin DE to whole body beta, and the thyroid.

In the review of Revision 0 to this calculation package, the NRC staff accepted the use of these revised dose quantities.

2.0 Input Data

2.1 Reactor Coolant System Radioactivity Concentrations

[30]

The concentrations used in this revision are calculated from the 1% failed fuel RCS liquid, steam generator liquid and steam generator steam activity concentrations^{18,19}, and assuming the following operating limits: 0.20 μ Ci/gm DE I-131 in primary liquid (RCS), 0.1 μ Ci/gm DE I-131 in secondary liquid (steam generator liquid) and 12 μ Ci/gm DE I-131 in primary liquid (RCS) during transient conditions.

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	[A]i 0.20	[A]i 0.10	[A]i 0.20 steam	[A]: 12
Radio-	RCS	S/G Liquid	S/G Steam	RCS
nuclide	(µCi/gm)	(µCi/gm)	(µCi/gm)	(µCi/gm)
Kr-83m	2.30E-02	•	3.69E-07	
Kr-85m	8.04E-02		1.08E-06	
Kr-85	8.44E+00		1.14E-04	
Kr-87	5.39E-02	,	7.28E-07	
Kr-88	1.51E-01		2.03E-06	
Kr-89	4.37E-03		5.88E-08	
Xe-131m	2.74E-01		3.69E-06	
Xe-133m	2.29E-01		3.10E-06	
Xe-133	1.69E+01		2.29E-04	
Xe-135m	5.23E-02		4.92E-06	
Xe-135	5.63E-01		8.21E-06	
Xe-137	1.08E-02		1.46E-07	
Xe-138	3.70E-02		4.98E-07	•
1-131	1.57E-01	8.38E-02	8.38E-04	9.40E+00
1-132	6.17E-02	1.35E-02	1.35E-04	3.70E+00
1-133	2.35E-01	9.13E-02	9.13E-04	1.41E+01
1-134	3.46E-02	1.76E-03	1.76E-05	2.08E+00
1-135	1.35E-01	3.19E-02	3.19E-04	8.11E+00

Noté: Steam generator steam concentration for noble gas is based on RCS concentration, primary-to-secondary leak rate and steam flow. Iodine concentration is based on steam generator liquid and 0.01 partitioning between the liquid and steam phases.

2.2	Concurrent Iodine Spike Rate (µCI/sec) - See Appendix 1		1	Calculateo
2.3	Concurrent lodine Spike Duration = 4 hours			1,10,31,32]
2.4	Technical Specification Primary-to-Second		[4]	
	150 gpd any one steam generator, 450 gpd	total for all three s	steam generators	
2.5	RCS Density @ 576.6 °F = 44.13 lb/ft ³			[31]
2.6	Primary Coolant Mass			[33]
	<u>Component</u> RCS excluding PZR, 30% plugging PRZ water @ 0% power RCS @ 0% power, 30% plugging	<u>Value</u> 7127 ft ³ 340 ft ³ 7467 ft ³	<u>x 44.13 lb/ft³ (3.145E5 lb) (1.500E4 lb) (3.295E5 lb)</u>	
2.7	Primary-to-Secondary Leakage Mass = 1 g	/cc	[As	sumption,34]

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2.8	Secondary Side Mass:		[33,35]
	<u>Component</u> Steam generator liquid @ Steam generator steam @	<u>Valu</u> 0% power, 30% plugging 14810 ≥ 0% power, 30% plugging 578	<u>ie +10%</u> 4 Ibm 162914 Ibm 31 Ibm 6359 Ibm
	Westinghouse ²⁹ are give applied in the bounding of calculation based on the in the calculation of radio It is also used in the sou For the ILI case changin proportional changes in source term. However, liquid mass increases to constant remains the sa maximum steam general accident analysis. The case only. For the AS calculate the source ter transfer rate constant. A subsequently the dose. mass is bounding for the	An with an associated uncertainty irection. The +10% values are listed following: The steam generator liquid pactivity transfer rate constant for the ince term calculation for the ILI and of the steam generator liquid mass in the radioactivity transfer rate const for the FLI case, increasing the st he source term but the radioactivity ame, resulting in increased dose. for Liquid mass is bounding for the steam generator steam mass is us A case, steam generator steam m rm, but is not used to calculate to as the mass increases so does the s . Therefore, the maximum steam g Unit 1 MSLB analysis.	(±10%) to be d for use in this id mass is used e ILI case only. the FLI cases. is offset by the tant and in the team generator ty transfer rate Therefore, the e Unit 1 MSLB sed in the ASA hass is used to the radioactivity source term and tenerator Steam
2.9	Iodine Partition Factors: See Assumption 1.8 for j	Faulted steam generator Intact steam generators Intact steam generators Intact steam generators Intact steam generators	= 1.0 [2,10,32] 0-1 hour = 1.0 after 1 hour = 0.01
2.10	Time to Isolate Faulted S	Steam Generator = 8 hours	· [1,10,31,32]
2.11	Steam Release from Fau	utted Steam Generator:	[Assumption,10,32]
	0 - 0.5 hours = all of the $0.5 - 8$ hours = mass for	liquid and steam mass initially prese total P-to-S leak rate	ent
2.12	Steam Release from Inte	act Steam Generators:	[10,31,32]
		0-2 hrs = 336,776 lb 2-8 hrs = 705,393 lb	
2.13	Offsite Breathing Rate ()-8 hours) = 3.47E-4 m ³ /sec	[36]
2.14	Accident χ/Q Values - O	ffsite (sec/m ³)	[14]
	Location 0-2	hrs <u>0-8 hrs</u>	•
	LPZ	6.04E-5	
	•••• •••••••••••••••••••••••••••••••••		

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Control Room Parameters

The control room design and operating parameters used in this calculation are consistent with the current analysis of record with the exception of the 20 minute delay for operator action to start the emergency pressurization fan. The BVPS control room consists of control areas for both Unit 1 and Unit 2. This common control room is served by a single bottled air emergency pressurization system and two filtered air, fan pressurized systems. Flow and filtration specifications for these two systems are identical; however there are two major differences. The first is that, because Unit 1 has only one fan, it is a single train system, whereas Unit 2 has two separate and independent trains. The second difference is that there is no pressurization fan auto-start function for the Unit 1 system. Unit 2 is not affected by this because Unit 2 Technical Specifications do not recognize the Unit 1 system (the two independent Unit 2 trains only are considered). Unit 1 Technical Specifications recognize both Unit 2 trains plus the Unit 1 train, requiring two of the three to avoid entering an action statement. Operating with one Unit 2 train and the Unit 1 train, and considering a Unit 2 train failure, only the Unit 1 train is expected to operate. Because this will require manual initiation, a delay for operator action is included in this analysis. The delay time and it's basis is provided below.

See Attachment 3 for a time line and summary of control room parameters assumed for this analysis.

2.15	Normal control room unfiltered air intake rate = 500 cfm	[10,31,32,37]
2.16	Time post-accident to initiate control room isolation = 30 minutes	[Attachment 2]
	Note: 30 minutes has been used in previous revisions of this calculation. See assumption 1.5, above.	
2.17	Control room emergency bottled air pressurization system (CREBAPS) operation T = 30 to 90 minutes	[38,39]
	Note: Design of this system is such that the control room will be maintained at 0.125" wc positive pressure (with respect to adjacent areas) for one hour. The minimal affect of radioactive material removal by CREBAS is conservatively not modeled in this analysis. System actuation is assumed to occur at 30 minutes, with any delay due to loss of AC power being well within the margin discussed in Assumption 1.5, above.	
2.18	Unfiltered air inleakage during CREBAPS/emergency pressurization fan operation = 10 cfm	[29]
	Assumed 10 CFM unfiltered inleakage is consistent with all BVPS DBA analyses whenever these systems are in operation.	
2.19	Delay between bottled air depletion and emergency pressurization fan manual start (20 minutes) T = 90 to 110 minutes	[Assumption,40]
	Note: NUREG 0800 Chapter 6.4 ²⁹ , III.3.d.(3).li provides "A substantial time delay should be assumed where manual isolation is assumed, e.g., 20 minutes for the purposes of dose calculations". Information provided in Reference 40 provides a delay time of 9 minutes, thus the 20 minute assumption is adequate.)))
2.20	Minimum air flow rate to maintain the control room at 0.125" wc positive pressure = 600 cfm	. [41]

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2.21	Unfiltered air inleakage b emergency	etween bottled pressurization	i air depletion and n fan manual start = 31	[A: 0 cfm	ssumption,29
	Note: NUREG 0800 Cha rate is assumed to be of pressurized to 0.125" wc 2.18.	apter 6.4, III.3. ne-half of the . This is addit	d.(2) provides that the l flow rate from the cont ional to the 10 cfm spe	base infiltration rol room when cified in datum	
2.22	Emergency pressurizatio	n fan filtered a	ir intake flow rate (max	limum) = 1030 cfi	m [38]
	Note: Maximum fan in maximum, bounding do previous revisions of the this revision.	take rate has ses based o calculation a	been demonstrated to n sensitivity analyses nd verified and mainta	o result in the conducted in ined on file for	
2.23	Control room emergency	pressurization	n system filter removal	efficiency:	[42]
	Nobi Iodin Iodir	e gas le (total) le (effective)	0% 95% 94 .1%	• .	-
	Note: The effective considering unfiltered inle	value is ca	iculated for TRAILSP	PC processing	
	$Efficiency = \frac{(0.95*1)}{(0.95*1)}$	Filtered.Flow	+ (0.0 * Unfiltered.F	low)	
	$Efficiency = \frac{(0.95*1)}{100}$	Filtered Flow Filtered Flow)+(0.0*Unfiltered.F +Unfiltered.Flow	low)	
	$Efficiency = \frac{(0.95*1)}{Efficiency}$	Filtered .Flow Filtered .Flow 930) + (0.0*10 930 + 10	$\frac{(0.0 + Unfiltered.F}{V + Unfiltered.Flow}$	Iow)	
2.24	$Efficiency = \frac{(0.95*1)}{Efficiency} = \frac{(0.95*1)}{10}$ Post release control room	Filtered.Flow Filtered.Flow 030) + (0.0*10 030 + 10 n purge start a	$\frac{(0.0 * Unfiltered.F}{(0.0 * Unfiltered.F}) + (0.0 * Unfiltered.Flow}$ + Unfiltered.Flow = 0.941 nd duration T = 8 to 8.5	<u>'low)</u> 5 hours	[22]
2.24 2.25	$Efficiency = \frac{(0.95*1)}{10}$ $Efficiency = \frac{(0.95*1)}{10}$ Post release control room Post release control room	Filtered.Flow Filtered.Flow (30) + (0.0*10 (30 + 10) n purge start a n purge flow ra	$\frac{(0.0 + Unfiltered.F}{(0.0 + Unfiltered.F}) + (0.0 + Unfiltered.Flow) + Unfiltered.Flow}$ = 0.941 nd duration T = 8 to 8.9 ate (minimum) = 28,000	<u>Tow)</u> 5 hours 9 cfm	[22] [22,43]
2.24 2.25	$Efficiency = \frac{(0.95*1)}{10}$ $Efficiency = \frac{(0.95*1)}{10}$ Post release control room Post release control room Note: Using the minimum material from the control maximum, bounding dos	Filtered.Flow Filtered.Flow 30) + (0.0*10 030 + 10 n purge start a n purge flow ra m purge flow ra m purge flow room after the	() + (0.0 * Unfiltered.F) () + Unfiltered.Flow () = 0.941 and duration T = 8 to 8.8 ate (minimum) = 28,000 rate minimizes remova e release has ended an	Tow) 5 hours 9 cfm 1 of radioactive nd provides the	[22] [22,43]
2.24 2.25 2.26	Efficiency = $\frac{(0.95*1)}{10}$ Efficiency = $\frac{(0.95*1)}{10}$ Post release control room Post release control room Note: Using the minimum material from the control maximum, bounding dos Post control room purge	Filtered.Flow Filtered.Flow (30) + (0.0*10) (30) + 10 (30) + 10 (3	$\frac{(0.0 * Unfiltered.F}{(0.0 * Unfiltered.F}) + (0.0 * Unfiltered.Flow) + Unfiltered.Flow = 0.941 and duration T = 8 to 8.9 ate (minimum) = 28,000 rate minimizes remova the release has ended and flow rate = 500 cfm$	<u>low)</u> 5 hours 9 cfm 1 of radioactive nd provides the [10	[22] [22,43] ,22,31,32,37]
2.24 2.25 2.26	$Efficiency = \frac{(0.95*1)}{10}$ $Efficiency = \frac{(0.95*1)}{10}$ Post release control room Post release control room Note: Using the minimum material from the control maximum, bounding dos Post control room purge	Filtered.Flow Filtered.Flow 30) + (0.0*10 030 + 10 n purge start a n purge flow ra m purge flow ra m purge flow room after the es.	$\frac{(0.0 + Unfiltered.F}{(0.0 + Unfiltered.F}) + (0.0 + Unfiltered.Flow)$ $\frac{(0.0 + Unfiltered.Flow)}{(0.0 + 0.941)} = 0.941$ and duration T = 8 to 8.5 ate (minimum) = 28,000 rate minimizes remova the release has ended at flow rate = 500 cfm	<u>low)</u> 5 hours 6 cfm 1 of radioactive nd provides the [10	[22] [22,43] ,22,31,32,37]
2.24 2.25 2.26	$Efficiency = \frac{(0.95*1)}{(0.95*1)}$ $Efficiency = \frac{(0.95*1)}{10}$ Post release control room Post release control room Note: Using the minimum material from the control maximum, bounding dos Post control room purge	Filtered.Flow Filtered.Flow (30) + (0.0 * 10) (30) + 10 (30) + 10	$\frac{(0.0 + Unfiltered.F}{(0.0 + Unfiltered.F}) + (0.0 + Unfiltered.Flow) + Unfiltered.Flow}$ $\frac{(0.0 + Unfiltered.Flow)}{(0.0 + 10^{-10})} = 0.941$ and duration T = 8 to 8.8 ate (minimum) = 28,000 rate minimizes remova the release has ended and flow rate = 500 cfm	<u>low)</u> 5 hours 9 cfm 1 of radioactive nd provides the [10	[22] [22,43] ,22,31,32,37]
2.24 2.25 2.26	$Efficiency = \frac{(0.95*1)}{10}$ $Efficiency = \frac{(0.95*1)}{10}$ Post release control room Post release control room Note: Using the minimum material from the control maximum, bounding dos Post control room purge	Filtered.Flow Filtered.Flow 30) + (0.0*10 30 + 10 n purge start a n purge flow ra m purge flow ra m purge flow room after the es.	() + (0.0 * Unfiltered.F) () + Unfiltered.Flow () = 0.941 and duration T = 8 to 8.9 () = 10.941 () = 10.941 $()$ = 10.941 () = 10.941 $()$ = 10.941 () = 10.941	<u>low)</u> 5 hours 6 cfm 1 of radioactive nd provides the [10	[22] [22,43] ,22,31,32,37]
2.24 2.25 2.26	$Efficiency = \frac{(0.95*1)}{10}$ $Efficiency = \frac{(0.95*1)}{10}$ Post release control room Post release control room Note: Using the minimum material from the control maximum, bounding dos Post control room purge	Filtered.Flow Filtered.Flow (30) + (0.0 * 10 (30) + 10 ((2) + (0.0 * Unfiltered.F) (2) + Unfiltered.Flow) (2) = 0.941 and duration T = 8 to 8.8 ate (minimum) = 28,000 rate minimizes remova the release has ended and flow rate = 500 cfm	<u>low)</u> 5 hours 9 cfm 1 of radioactive nd provides the [10	[22] [22,43] ,22,31,32,37]

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CALCULATION

All of the values calculated in this package for entry into TRAILSPC input files are calculated via an EXCEL spreadsheet and are rounded at the completion of the calculation. Specifically, during a calculation, all places are carried until the final number, and then the final number is rounded to the same number of significant figures as any number used in the calculation with the least number of significant figures. The number is then entered into the TRAILSPC input file. At the completion of the TRAILSPC runs and the summation of dose from various cases, the final result is also rounded to the number of significant figures of any input number with the least number of significant figures. Hence, reproduction of this calculation, without the same spreadsheet and protocol, may cause "rounding" differences.

1.0 Source Term: Technical Specification Limit DE I-131 Activity

Reference 30 provides the Technical Specification limit activity concentrations in uCi/gm, in the RCS primary, the secondary liquid, the secondary steam and in the RCS primary during a transient (Input Datum 2.1). For use in the calculation of isotopic release quantities and dose using TRAILSPC, these values must be expressed as total activity, in uCi. Total activity is the product of the Technical Specification limit DE I-131 concentration in uCi/gm and the applicable mass in gm. The following formulas were used to calculate activity for the bounding conditions of 0% reactor power, 30% steam generator plugging.

NOTE: The RCS mass value used in the calculation of the ITC and FRC cases does not include the pressurizer volume. The ITC and FRC cases include a concurrent iodine spike. Since the concurrent iodine spike occurs at the onset of the accident it is assumed that the pressurizer volume does not equilibrate with the RCS volume that includes the iodine spike. Therefore, the release rate is calculated using RCS volume less the pressurizer volume. However, the Technical Specification limit RCS activity is in equilibrium with the pressurizer volume. To offset the increase in Technical Specification limit RCS activity that will be released using the pressurizer less volume release rate, the activity is calculated with RCS mass less the pressurizer volume also.

NOTE: The steam generator liquid and steam mass values provided by Westinghouse³⁵ are given with an associated uncertainty (\pm 10%) to be applied in the bounding direction. The steam generator liquid and steam mass values used are the \pm 10% values as determined (and noted) below:

Ai 0.20	 [A]_{10.20} (uCl/gm) x RCS mass (lb) x 453.592 (gm/lb), Source Term for the ITN, ITC and FRC Case
Ai 0.10	= [A] _{10.10} (uCi/gm) x S/G liquid mass (ib) x 453.592 (gm/ib) = Source Term for ILI and FLI Cases
A _{i steam}	= [A] _{i steam} (uCl/gm) x S/G steam mass (lb) x 453.592 (gm/lb) = Source Term for ASA Case
A _{i 12}	= [A] _{I 12} (uCl/gm) x RCS mass (ib) x 453.592 (gm/lb) = Source Term for FRP and ITP Cases

The results for the bounding case is summarized in the table below:

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		FRC	ILI		FRP
	ITN	ITC	FLI	ASA	ITP
	Ai 0.20	Ai 0.20	Ai 0.10	Ai 0.20 steam	Ai 12
	TS	TS	TS	TS	TS Transient
Radio-	RCS	RCS	S/G Liquid	S/G Steam	RCS
nuclide	(uCi)	(uCi)	(uCi)	(uCi)	(uCi)
<r-83m< td=""><td>3.44E+06</td><td>3.28E+06</td><td></td><td>1.06E+00</td><td>3.44E+06</td></r-83m<>	3.44E+06	3.28E+06		1.06E+00	3.44E+06
<r-85m< td=""><td>1.20E+07</td><td>1.15E+07</td><td></td><td>3.11E+00</td><td>1.20E+07</td></r-85m<>	1.20E+07	1.15E+07		3.11E+00	1.20E+07
<r-85< td=""><td>1.26E+09</td><td>1.20E+09</td><td></td><td>3.29E+02</td><td>1.26E+09</td></r-85<>	1.26E+09	1.20E+09		3.29E+02	1.26E+09
<r-87< td=""><td>8.06E+06</td><td>7.69E+06</td><td></td><td>2.10E+00</td><td>8.06E+06</td></r-87<>	8.06E+06	7.69E+06		2.10E+00	8.06E+06
<r-88< td=""><td>2.25E+07</td><td>2.15E+07</td><td></td><td>5.84E+00</td><td>2.25E+07</td></r-88<>	2.25E+07	2.15E+07		5.84E+00	2.25E+07
Kr-89	6.54E+05	6.24E+05		1.70E-01	6.54E+05
Xe-131M	4.09E+07	3.90E+07		1.06E+01	4.09E+07
Xe-133M	3.42E+07	3.26E+07		8.93E+00	3.42E+07
Xe-133	2.53E+09	2.42E+09		6.60E+02	2.53E+09
Xe-135M	7.82E+06	7.47E+06		1.42E+01	7.82E+06
Xe-135	8.42E+07	8.03E+07		2.37E+01	8.42E+07
Xe-137	1.61E+06	1.54E+06	1	4.20E-01	1.61E+06
Xe-138	5.53E+06	5.27E+06		1.44E+00	5.53E+06
1-131		2.23E+07	6.19E+06	2.42E+03	1.40E+09
-132		8.81E+06	9.95E+05	3.89E+02	5.54E+08
1-133		3.35E+07	6.74E+06	2.63E+03	2.10E+09
1-134		4.93E+06	1.30E+05	5.09E+01	3.10E+08
1-135		1.93E+07	2.35E+06	9.19E+02	1.21E+09

Source Term: DE I-131 0.20 µCi/g, 0% power, 30% plugging

2.0 Activity Transfer (Release) Rate Constants (λ)

The conversion of water volume to mass will assume a density of 1.000 gm/cm³ (standard temperature and pressure)^{34,44}. The density of RCS at operating temperature and pressure is closer to 0.72 gm/cm³. However, as water is released the density increases rapidly towards 1.000 gm/cm³ as the water chills. Also, primary to secondary leak rate is routinely measured at a density approaching 1.000 gm/cm³. A density gradient also exists for steam generator liquid between 1.000 gm/cm³ is bounding for all intermediate values of density that may occur once an accident is initiated.

The transfer rate constants (λ) are calculated by dividing the release mass flow rate (F) by the compartment total mass (M) with appropriate unit conversion.

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2.1 FRP, FRC

Release rate based on rupture primary-to-secondary leak rate. Total leak rate includes accident induced plus allowable pre-accident leakage as permitted by facility Technical Specifications. The results for the bounding case of 0% power, 30% plugging are listed in the tables below.

NOTE: For the FRC case the RCS mass values used exclude pressurizer volume since in the first 4 hours post accident, when the concurrent iodine spike occurs, the pressurizer volume is assumed to not equilibrate with the remaining RCS volume.

FRC Release Rate Constant:

$$\lambda = \frac{(5.5 \text{ gal}/\min + (150 \text{ gal}/d / 1440 \min/d))^* 3785.3 \text{ cc}/\text{gal}^* 1 \text{ g/cc}}{(7127 \text{ ft}^3 * 44.13 \text{ lbm}/\text{ft}^3)^* 453.592 \text{ g/lbm}^* 60 \text{ s/min}} = 2.478E - 06 \text{ s}^{-1}$$

FRP Release Rate Constant:

$$\lambda = \frac{(5.5 \text{ gal/min} + (150 \text{ gal/d} / 1440 \text{ min/d})) * 3785.3 \text{ cc/gal} * 1 \text{ g/cc}}{(7467 \text{ ft}^3 * 44.13 \text{ lbm/ft}^3) * 453.592 \text{ g/lbm} * 60 \text{ s/min}} = 2.365E - 06 \text{ s}^{-1}$$

2.2 ITN, ITP and ITC

The ITN release rate is based on Technical Specification primary-to-secondary leak rate in the 2 intact steam generators. The ITP release rate is equal to the ITN radioactivity transfer rate constant for the first hour. After the first hour, the ITP release rate is reduced by a factor of 100 to account for partitioning. The ITC is calculated the same way as the ITP and ITN radioactivity transfer rate constants with the exception of the RCS mass value used. The RCS mass value used excludes pressurizer volume since in the first 4 hours post accident, when the concurrent lodine spike occurs, the pressurizer volume will not equilibrate with the remaining RCS volume. After the first hour, the ITC release rate is reduced by a factor of 100 to account for partitioning.

NOTE: Since the release rate represents 2 steam generators $(2 \times 150 \text{ gal/day} = 300 \text{ gal/day})$, the source term need not be multiplied by 2 in TRAILSPC.

ITN and ITP (ITP 0-1 hour only) release rate constant:

$$\lambda = \frac{300 \text{ gal/d} * 3785.3 \text{ cc/gal} * 1 \text{ g/cc}}{(7467 \text{ ft}^3 * 44.13 \text{ lbm/ft}^3) * 453.592 \text{ g/lbm} * 86400 \text{ s/min}} = 8.794E - 08 \text{ s}^{-1}$$

 $\lambda = 8.794E - 08 s^{-1} * 0.01 = 8.794E - 10 s^{-1}$ ITP only, after one hour.

ITC release rate constant:

$$\lambda = \frac{300 \text{ gal/d} * 3785.3 \text{ cc/gal} * 1 \text{ g/cc}}{(7127 \text{ ft}^3 * 44.13 \text{ lbm/ ft}^3) * 453.592 \text{ g/lbm} * 86400 \text{ s/min}} = 9.213E - 08 \text{ s}^{-1}$$

 $\lambda = 9.213E - 08 s^{-1} * 0.01 = 9.213E - 10 s^{-1}$ ITC after one hour.

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2.3 FLI

Release from the faulted steam generators of liquid activity initially in steam generators with hold-up credited. In order to model the release of the initial activity in 30 minutes, it is assumed that a reduction factor of 1E-6 represents 99.9999% of the activity. The radioactivity transfer rate constant is calculated as follows:

 $1E - 06 = e^{-\lambda \cdot 30 \min \cdot 60 s/\min}$

 $\lambda = 7.6753E - 03 s^{-1}$

2.4 ILI

Release rate for 2 intact steam generators of liquid activity initially present, with hold-up and partitioning credited. The steam release for 2 hours and 2-8 hours represents the release from both steam generators. In order to determine the release rate the steam mass is divided by the mass of two steam generators. Partitioning applies thus the multiplier of 0.01:

The steam generator mass value is the 0% power, 30% plugging liquid mass +10% as determined in the mass sensitivity analysis. The 0-2 hour value will be entered as the base value and the TRAILSPC XREM multiplier after 2 hours is the ratio of the 2-8 hr value over the 0-2 hr value. Since the release rate represents one steam generator, the source term is multiplied by 2 in the TRAILSPC input file to account for the release from 2 intact steam generators.

ILI rélease rate constant 0-2 hours:

$$\lambda = \frac{336776 \ lbm / (2 \ h * 3600 \ s / h)}{162914 \ lbm * 2} = 1.43555E - 06 \ s^{-1}$$

ILI release rate constant 2-8 hours:

$$\lambda = \frac{705393 \, lbm \, / \, (6 \, h * 3600 \, s \, / \, h)}{162914 \, lbm * 2} = 1.00228 E - 06 \, s^{-1}$$

XREM
$$(2-8 hours) = \frac{1.43555 E - 06 s^{-1}}{1.00228 E - 06 s^{-1}} = 0.698182$$

2.5 ASA

Release from all steam generators of steam activity (all radionuclides) initially in the steam generators. In order to model the release of 100 % of the initial activity in 1 second, it is assumed that a reduction factor of 1E-6 represents 99.9999 % of the activity. The radioactivity transfer rate constant is calculated as follows:

 $1E - 06 = e^{-\lambda + 1s}$

 $\lambda = 13.816 \ s^{-1}$

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RESULTS

The TRAILSPC input and output files are provided as Attachment 4, and the dose results summarized below.

Control Room Doses

Co-incident Snike

						on opino	
	Thyroid	External	Skin		Thyroid	External	Skin
ŕ	CDE	EDE	DE		CDE	EDE	DE
Case	(mrem)	(mrem)	(mrem)	Case	(mrem)	(mrem)	(mrem)
ASA	5.09E+00	1.63E-04	2.00E-03	ASA	5.09E+00	1.63E-04	2.00E-03
FLI	4.34E+03	1.38E-01	1.59E+00	FU	4.34E+03	1.38E-01	1.59E+00
ILI	3.97E+01	1.24E-03	1.61E-02	ILI	3.97E+01	1.24E-03	1.61E-02
ITN	0.00E+00	3.14E-03	3.10E-01	ITN	0.00E+00	3.14E-03	3.10E-01
ITC	9.14E+01	7.53E-03	7.06E-02	ITP	1.69E+02	8.76E-03	9.10E-02
FRC	2.48E+04	2.07E+00	3.26E+01	FRP	8.62E+03	5.25E-01	1.36E+01
Total:	2.93E+04	2.22E+00	3.46E+01	Total:	1.32E+04	6.76E-01	1.56E+01

EAB 0 - 2 hour Doses

Co-incident Spike

Thyroid Externat Skin Thyroid External Skin CDE EDE DE CDE EDE DE Case (mrem) (mrem) (mrem) Case (mrem) (mrem) (mrem) ASA 3.38E+00 2.57E-03 1.46E-03 ASA 3.38E+00 2.57E-03 1.46E-03 FLI 2.88E+03 2.16E+00 1.17E+00 FLI 2.88E+03 2.16E+00 1.17E+00 ILI 5.87E+01 4.07E-02 2.28E-02 **ILI** 5.87E+01 4.07E-02 2.28E-02 ITN 0.00E+00 1.68E-02 6.57E-02 ITN 0.00E+00 1.68E-02 6.57E-02 ITC 2.13E+02 5.36E-01 2.16E-01 ITP 2.22E+02 2.90E-01 1.37E-01 FRC 2.18E+04 5.12E+01 2.26E+01 FRP 1.16E+04 1.47E+01 8.65E+00 Total: 2.50E+04 5.40E+01 2.41E+01 Total: 1.48E+04 1.72E+01 1.00E+01

LPZ 0 - 30 days Doses

	Co-incid	ent Spike			Pre-incid	ent Spike	
	Thyroid	External	Skin		Thyroid	External	Skin
	CDE	EDE	DE		CDE	EDE	DE
Case	(mrem)	(mrem)	(mrem)	Case	(mrem)	(mrem)	(mrem)
ASA	1.96E-01	1.49E-04	8.45E-05	ASA	1.96E-01	1.49E-04	8.45E-05
FLI	1.67E+02	1.26E-01	6.78E-02	FLI	1.67E+02	1.26E-01	6.78E-02
ILI	1.02E+01	6.04E-03	3.61E-03	ILI	1.02E+01	6.04E-03	3.61E-03
ITN	0.00E+00	3.22E-03	1.47E-02	ITN	0.00E+00	3.22E-03	1.47E-02
ІТС	1.74E+01	3.86E-02	1.61E-02	ITP	1.36E+01	1.74E-02	8.30E-03
FRC	1.43E+04	2.25E+01	1.08E+01	FRP	2.55E+03	2.47E+00	1.68E+00
Total:	1.45E+04	2.27E+01	1.09E+01	Total:	2.74E+03	2.62E+00	1.77E+00

Pre-incident Spike

Pre-incident Snike

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CONCLUSION

The analysis documented herein has established that the maximum primary-to-secondary leak rate that could be tolerated during a MSLB outside of containment is 5.6042 gpm (5.5 gpm accident induced + 150 gpd Technical Specification limit) if the RCS specific activity is maintained less than 0.20 μ Ci/gm DE I-131. The control room dose is limiting.

Offsite doses are a small fraction of the applicable regulatory limits of 10 CFR 100.11^{45} of 300 rem thyroid and 25 rem whole body, and are less than the more restrictive guidance criteria in the Standard Review Plan² of 30 rem thyroid and 2.5 rem whole body. Control room operator doses are less than the 10 CFR 50⁴⁶ criteria of 5 rem whole body or its equivalent to any part of the body.

			RTL: n/a Form: RE 1.103-3 9/92					
BEAV POW	VER VALLEY ER STATION ealth Physics Department	ERS-SFL-95-008 Revision 6	Page 19					
REF	ERENCES							
1.	BVPS Unit 1 UFSAR, Chapter 14	, Section 14.2.5, Major Secondary S	ystem Pipe Rupture					
2.	USRNC, Standard Review Plan f Plants. NUREG 0800, Chapter 15	USRNC, Standard Review Plan for the Review of Safety Analysis Reports for Nuclear Power Plants. NUREG 0800, Chapter 15, Section 15.1.5, Revision 5; 1987						
3.	USNRC, Voltage-Based Repair C Outside Diameter Stress Corrosic	Criteria for Westinghouse Steam Gen on Cracking, Generic Letter 95-05	erator Tubes Affected by					
4.	BVPS Unit 1 Technical Specifica	tion 3/4.4.6.2, Operational Leakage						
5.	BVPS Unit 1 Technical Specifica	tion 3/4.4.8, Specific Activity						
6.	BVPS Unit 1 Technical Specifica	tion 3/4.7.1.4, Activity						
7.	SWEC, Control Room Habitabilit UR(B) 445, 1987	y Due to Design Basis Accident (exc	ept LOCA) at BVPS-2, 12241					
8.	SWEC, FSAR Section 15.6.5 - L 190, 1987	OCA Releases and Doses - Site and	Control Room. 12241 UR(B)					
9.	SWEC, Doses to the Combined	Control Room due to LOCA at BVPS	-1. 12241 UR(B) 450, 1987					
10	SWEC, Combined BV1-BV2 Cor LOCA) at BV1, 12241-UR(B)-45	ntrol Room Habitability Due to Design 6, 1987	a Basis Accidents (except					
11.	BVPS, Updated Final Safety Ana	alysis Report Unit 2, Chapter 15						
12.	Westinghouse, Beaver Valley Po Indications at Tube Support Plate	ower Station-1 Steam Generator Tub es, WCAP-14122, dtd 7/94	e Plugging Criteria for					
13.	USNRC, Beaver Valley Power S 334, February 1995	tation Unit No. 1 Amendment 184 to	Facility Operating License 50-					
14.	BVPS, RG1.145 Short-Term Acc 1986-1995 Observations. ERS-S	ident X/Q Values for EAB and LPZ, FL-96-021	Unit 1 and Unit 2, based on					
15.	DiNunno, J.J., etal, Calculation of Distance Factors for Power and Test Reactor Sites, USAEC TID 14844, 1962							
16.	USEPA, Limiting Values of Radi Factors for Inhalation, Submersi 020	onuclide Intake and Air Concentration on, and Ingestion, Federal Guidance	n and Dose Conversion Report No. 11, EPA-520/1-88-					
17.	BVPS, Control Room Pressuriza	tion Fan Flow Rate. Condition Repo	rt 972390, dtd 12/26/97					
18	SWEC Calculation Package 122 Enrichment) and Associated Equ	41/11700-UR(B)-478, Design Reactoulibrium Primary and Secondary Coc	or Core Inventory (3.96% Iant Activities for BVPS, 1999					
19	SWEC Calculation Package 122 Analyses —Composite Equilibriu Associated Design Primary and	241/11700-UR(B)-479, Radiological S Im Reactor Core Inventory (3.6% - 5 Secondary Coolant Activities for BVF	ource Terms for Accident % Initial Enrichment) and the PS, 1999					

			RTL: n/a Form: RE 1.103-3 9/92
BEAV POWI	'ER VALLEY ER STATION Patth Physics Department	ERS-SFL-95-008 Revision 6	Page 20
REF	ERENCES (cont)		
20.	BVPS Calculation Package ERS Linear Systems, PC Version v1.0	SFL 96 004, TRAILS_PC: Transport la, 2000	of Radioactive Material in
· 21.	BVPS Emergency Operating Pro	cedure, 1OM-53A.1.E-2 Faulted Stea	am Generator Isolation
22.	BVPS Unit 1 Operating Procedur Actuation/Recovery	e, 1/20M-44A.4A.A, Post Control Ro	om Habitability System
23.	BVPS Calculation Package ERS	-AJL-99-002, Generic Control Room	Modeling, 1999
24.	BVPS Licensing Requirements N	lanual, Table 3.2-1, Engineered Safe	ty Features Response Times
25.	BVPS Unit 1 Operating Manual C	DST 1.36.3	
26.	BVPS Unit 2 Operating Manual C	DST 2.36.3	•
27.	BVPS Emergency Operating Pro	cedure, 10M-53A.1.E-1, Loss of Rea	actor or Secondary Coolant
28.	BVPS Emergency Operating Pro	cedure, 10M-53A.1.FR-H.1, Respon	ise to Loss of Secondary Heat
29.	USRNC, Standard Review Plan Plants. NUREG 0800, Chapter 6	for the Review of Safety Analysis Re , Section 6.4, Revision 2; 1981	ports for Nuclear Power
30.	BVPS Calculation Package ERS Concentrations for RCS Liquid, S and 2, 2000	-AJL-99-007, Calculation of Technica Steam Generator Liquid and Steam C	al Specification Activity Senerator Steam for Units 1
31.	BVPS, Design basis accident pa 116252, dtd 08/01/98	rameter verification - Unit 1, BVPS -	Engineering Memorandum No.
32.	SWEC, Doses to the Combined UR(B)-448, 4/17/87	Control Room Due to a Main Steam	Line Break at BVPS-1, 12241-
33.	BVPS, Design basis accident pa 116251, dtd 12/04/98	rameter verification - Unit 2, BVPS -	Engineering Memorandum No.
34.	USNRC, Potential Inconsistency Steam Line Break Associated wi Repair Criteria, Information Noti	in the Assessment of the Radiologic ith the Implementation of Steam Gen ce 97-79	al Consequences of a Main erator Tube Voltage-Based
35.	DLC, Steam Generator Liquid an dtd 1/20/98 (Includes Westingho	nd Steam Masses, BVPS - Engineeri ouse Ltr NSD-SAE-ESI-98-027, dtd 1/	ng Memorandum No. 115783, /7/98)
36.	USNRC, Assumptions Used for Coolant Accident for Pressurized	Evaluating the Potential Radiological distribution of the sectors	Consequences of a Loss of 1.4, Revision 2; 1974
37.	BVPS Unit 2 UFSAR, Chapter 6 This UFSAR Section is applicab	Table 6.4.1, Control Room Envelope le to the Unit 1 (common) control roo	e Design Parameters (Note:)m)
38.	BVPS, Dilution Flow for Health I No. 115766, dtd 1/15/98	Physics Control Room Dose Calculat	ion, Engineering Memorandum

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REFERENCES (cont)

- 39. BVPS, CREBAPS Design Basis Testing, Engineering Memorandum No. 115735, dtd 1/14/98
- 40. BVPS, Unit 1 Start-Up of the Emergency Control Room Ventilation System, Engineering Memorandum No. 116523, dtd 8/20/98
- 41. BVPS, Minimum Air Flow to Maintain Control Room Pressurized to 1/8" wc, Engineering Memorandum No. 117830, dtd 4/15/99
- 42. BVPS Unit 1 Technical Specification 3/4.7.7, Control Room Emergency Habitability Systems
- 43. BVPS, Minimum Control Room Ventilation Fan Flow Rates, Engineering Memorandum No. 115712, dtd 1/5/98
- 44. EPRI, Review of Iodine Spike Data From PWR Power Plants in Relation to SGTR with MSLB, TR-103680, draft, December 1993
- 45. Title 10 Code of Federal Regulations, Part 100 §100.11, Determination of exclusion area, low population zone, and population center distance
- 46. Title 10 Code of Federal Regulations, Part 50, Appendix A, Criterion 19, Control Room







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EAVER VALLE OWER STATION Health Physics Depa	Y N rtment	E	RS-SFL-95-008 Revision 6	SFL-95-008 Page 25 vision 6 Attachment 2				
		D] Opera	ruquesae Light Company Nuclear Power Division bions Experience Departme	eat	·			
		1	MEMORANDUM					
TO:	S. F. LaVie		•					
LOCATION:	SOSB-4.	0						
DATE:	September 17,	1996						

SUBJECT: MSLB Control Room Isolation Timing Validation

In your memo of 7/3/96, you requested assistance in obtaining time-related data for support of the Unit 2 Alternate Plugging Criteria assumptions based on a EOP Simulator Validation. E-2, "Faulted Steam Generator Isolation" (IB/2) was validated on September 17, 1996 with the following results:

- The time from the reactor trip until CREBAPS was manually actuated was approximately 1000 seconds (~17 minutes)
- The time from the reactor trip until SG NR level was recovered to >5% in the unaffected SGs was
 approximately 2600 seconds (≈43 minutes)

The scenario run was for a 8 E+5 LBM/HR steam break (20%), outside CNMT on the B SG. This case is considered conservative since SLI was delayed which prolonged the SG blowdown and maximized the mass loss from the unaffected SGs. For larger breaks, reactor trip, safety injection and SLI occur almost simultaneously, and thus minimize unaffected SG blowdown. It should also be noted that the PO manually throttled total AFW flow to the unaffected SGs to about 365 GPM (per procedure) which is the minimum acceptable AFW flow to provide an adequate heat sink. This action extended SG refill time to its maximum limit. All other cases would be bounded by this feed flow value.

In conclusion, both objectives were met with considerable margin and appropriate conservative assumptions.

I will maintain the original data in the appropriate EOP history file. If you have any questions about this information, please call me at X4935.

CO/Img

cc:

G. E. Storolis R. M. Vento A. H. Brunner F. J. Schaffner M. P. Flynn T. W. Burns R. N. Ireland T. W. Bean J. T. Lebda T. M. McGhee L. G. Schad K. J. Winter

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TRAILSPC Input File For ASA	Case		
L1 ',10,1.0E-3,3.47E-4,1.0E-5,3	.47E-4,1.0,1.0E-3,3.47E-4,1,24	1,0,2	
'C1 ','not used ',0.0 ,0.0,0.0,0.0	(07 0836 2) [882737.11] (4/00)	
'C2 ','all S/Gs ',13.816,0.0,0.0,0.	0	. '	
'CR ',1.73E5 ,10.,10.,0.0,0.941,0).0		
'PRD',24*0.0			
"PRD",24"0.0 "INI" 4.0 ! ! 24*0.0			
'INI', 1.0, ,24 0.0 'INI', 3.0 'UCi', 1.06E0, 3, 11E0, 3, 20			
1.06E1.8.93E0.6.60E2.1.42E1.2	.37E1.4.20E-1.1.44E0	J,	
2.42E3,3.89E2,2.63E3,5.09E1,9	.19E2,5*0.0		
'INI',1.0,' ',24 * 0.0	•		
'TIM',1800.,5400.,6600.,7200.,14	1400.,28800.,30600.,86400.,3.	456E5,2.592E6	
'XPR',10"0.0 'XPR' 10*0.0			
'XPR'.50.0.1.0.31.0.3*104 2800	3*50		
'XRM',10*0.0	, 0 00 .		
'XRM',1.0,9*0.0			1
'XRM',50.0,1.0,31.0,3*104.,2800	.,3*50.		
'XRF',10*0.0			1
XRF,10"0.0 'XRF',3*0.0.2*1.0.4*0.0			
'XOOEB' 4*1 04 6*0 0			
'XBREB',4*1.0,6*0.0		•	
'XOQLZ',6*6.04,2*4.33,2.10,0.74	4	,	
'XBRLZ',10*1.0			
'XOQ',6*2.43,2*1.22,0.890,0.626			
000,01.0,0.0,0.4	,		

VER V VER S Health Phy			r N rtm	ent						E	:F	25)-	SI vis	L.	95 j	-0(8		Attac	l hm	Pag ent 4	je 4	1	02	8
				-																						
*** PROGENY INGROMTH ON ***	COMP: Control Room VOLUME: 1.730E+05 Cu.Ft.	0.000E+00 Kr-83m 0.000E+00 Kr-83m	0.000E+00 Kr-85	0.000E+00 Kr-87 0.000E+00 Kr-88	0.000E+00 Kr-89	0.000E+00 Xe-131m	0.000E+00 Xe-133m 0.000E+00 Xe-133	0.000E+00 Xe-135m	0.000E+00 Xe-135	U.UUUE+00 X=137 0 000E+00 X=138	0.000E+00 I-131	0.000E+00 I-132	0.000E+00 I-133	0.000E+00 I-134 0.000E+00 I-135	1.0005+00				•							
n Linear Systems, Vl.Oa A.in] (4/00)	COMP: all S/Gs	1.060E+00 Kr-83m uC1 3.110E+00 Kr-85m	3.290E+02 Kr-85	Z.IO0E+00 Kr-87 5.840E+00 kr-88	1.700E-01 Kr-89	1.060E+01 Xe-131m 0 030E+00 V-133-	0.23005400 XE-133m 6.6005402 Xe-133	1.420E+01 Xe-135m	2.370E+01 Xe-135 4 200E-01 Y-137	1.440E+00 Xe-138	2.420E+03 I-131	3.890E+02 I-132	2.630E+03 I-133	5.U9UE+UI I-134 9.190E+O2 I-135	3.0005+00			·								
ort of Radioactive Material 1 4 LPZ dose (SA Case 2) [sa2AS		0.000E+00 Kr-83m 0.000E+00 Kr-85m	0.000E+00 Kr-85 0 0005400 Kr-83	0.000E+00 Kr-88 0.000E+00 Kr-88	0.000E+00 Kr-89	0.000E+00 Xe-131m 0.000E+00 Xe-133m	0.000E+00 Xe-133	0.000E+00 Xe-135m	U.UUUE+0U X=-135 0.000E+00 X=-137	0.000E+00 Xe-138	0.000E+00 I-131	0.000E+00 I-132	0.000E+00 I-133 0 000E+00 I-134	0.000E+00 I-135	1.000E+00		•									
rrails_PC ∽ Transp Asa - for cr, eab		INITIAL:													ACT MULT (to uci):							•				

*** PROGENY INGROWTH ON ***

	REMOVAL.		0 000F+00						*********		
NUC	Grn 1 PFI FD.		0.0002400	0 0002 00		1.382E+01	1/sec		1.000E+01	cfm	
NUC	Grn 2 REL ER.			0.0002+00			0.000E+00	INTA	KE REDUCT:	0.000E+00	
NUC	Grn 3 PFI FP.			0.00000000			0.000E+00	INTA	KE REDUCT:	9.410E-01	
	orb a ven evt		********	0.0006+00			0.000E+00	Inta	KE REDUCT:	0.000E+00	
MULT	'IPLIERS====>								*********	****	
step	TIME	XPR	XREM	XRF	XPR	XREM	XRF	XPR	XRFM	YRS	
1	1.800E+03	0.00	0.00	0.00	0.00	1.00	0.00	50.0	50.0	0.00	
2	5.400E+03	0.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	0.00	
3	6.600E+03	0.00	0.00	0.00	0.00	0.00	0.00	31.0	31 0	0.00	
4	7.200E+03	0.00	0.00	0.00	0.00	0.00	0.00	104	104	1 00	
5	1.440E+04	0.00	0.00	0.00	0.00	0.00	0.00	104	104	1.00	
6	2.880E+04	0.00	0.00	0.00	0.00	0.00	0.00	104	104.	1.00	
7	3.060E+04	0.00	0.00	0.00	0.00	0.00	0.00	2 8005+03	2 0005403	1.00	
8	8.640E+04	0.00	0.00	0.00	0.00	0.00	0.00	50 0	2.000ETU3	0.00	
9	3.456E+05	0.00	0.00	0.00	0.00	0 00	0.00	50.0	50.0	0.00	
10	2.592E+06	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00	
									50.0	0.00	
		C	ONTROL ROOM		EXCLUSI	on area bou	JNDARY	LOW PO	PULATION ZO	ME	
		X/Q	Breathing	Occupancy	X/Q	Breathi	lng	X/Q	Breathi	Ing	
		8/M3	s/M3 M3/s			M3/s		a/M3 M3/s			
		1.000E-03	3.470E-04	1.000E+00	1.000E	-03 3.470E-	-04	1.000E	-05 3.470E-	-04	
MULT: Step	IPLIERS > TIME,s									••	
1	1.800E+03	2.43	1.00	1.00	1.04	1.00		6.04	1 00		
2	5.400E+03	2.43	1.00	1.00	1.04	1.00		6.04	1.00		
3	6.600E+03	2.43	1.00	1.00	1.04	1 00		6.04	1.00		
4	7.200E+03	2.43	1.00	1.00	1 04	1 00		6.04	1.00		
5	1.440E+04	2.43	1.00	1 00	0.00	1.00		0.04	1.00		
6	2.8802+04	2.43	1 00	1 00	0.00	0.00		0.04	1.00		
7	3.0602+04	1.22	1 00	1 00	0.00	0.00	• •	6.04	1.00		
Â	8.6402+04	1 22	1 00	1 00	0.00	0.00		4.33	1.00		
ă	3.4565405	0 900 ···	1.00	1.00	0.00	0.00		4.33	1.00		
10	3 KOOPLAS	0.030	1.00	0.000	0.00	0.00		2.10	1.00		
10	2.3726700	V.020	1.00	0.400	0.00	0.00		0.744	1.00		

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ASA + for CR, EAB 4 LPZ dose (SA Case 2) [sa2ASA.in] (4/00)

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*** PROGENY INGROWTH ON ***

	not used	all S/Gs	AVERAGE	CONTROL ROOM
STEP TIME	UCI UCI-Sec	CURRENT INTEGRD uCi uCi-sec	RELEASED RELEASE •uCi uCi/sec	CURRENT CURRENT INTEGRD uCi uCi/cc uCi-sec
Kr-83m TOTALS	0.000E+00 0.000E+00	3.180E+00 2.302E-01	3.180E+00	0.000E+00 • 1.193E+01
Kr-85m INITIAL	0.000E+00	9.330E+00	9.330E+00	0.000E+00
Kr-85m Totals	0.000E+00	6.753E-01		5.174E+01
Kr-85 INITIAL	0.000E+00	9.870E+02	9.870E+02	0.000E+00
Kr-85 Totals	0.000E+00	7.144E+01		7.749E+03
Kr-87 INITIAL	0.000E+00	6.300E+00	6.300E+00	0.000E+00
Kr-87 Totals	0.000E+00	4.560E-01		1.878E+01
Kr-88 INITIAL	0.000E+00	1.752E+01	1.752E+01	0.000E+00
Kr-88 Totals	0.000E+00	1.268E+00		8.202E+01
Kr-89 INITIAL	0.000E+00	5.100E-01	5.0992-01	0.000E+00
Kr-89 Totals	0.000E+00	3.690E-02		7.909E-02
Xe-131m INITIAL	0.000E+00	3.180E+01	3.1802+01	0.000E+00
Xe-131m TOTALS	0.000E+00	2.302E+00		2.519E+02
Xe-133m INITIAL	0.000E+00	2.679E+01	2.679E+01	0.000E+00
Xe-133m TOTALS	0.000E+00	1.939E+00		2.574E+02
Xe-133 INITIAL	0.000E+00	1.980E+03	1.980E+03	0.000E+00
Xe-133 TOTALS	0.000E+00	1.433E+02		1.611E+04
Xe-135m INITIAL	0.000E+00	4.260E+01	4.262E+01	0.000E+00
Xe-135m TOTALS	0.000E+00	3.085E+00		. 2.593E+03
Xe-135 INITIAL	0.000E+00	7.110E+01	7.110E+01	0.000E+00
Xe-135 TOTALS	0.000E+00	5.146E+00		3.344E+03
Xe-137 INITIAL	0.000E+00	1.260E+00	1.260E+00	0.000E+00
Xe-137 TOTALS	0.000E+00	9.118E-02		2.364E-01
Xe-138 INITIAL	0.000E+00	4.320E+00	4.3202+00	0.000E+00
Xe-138 Totals	0.000E+00	3.127E-01		2.940E+00
I-131 Initial	0.000E+00	7.260E+03	7.2602+03	0.000E+00
I-131 Totals	0.000E+00	5.255E+02		5.649E+04

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ASA - for CR, EAB & LPZ dose (SA Case 2) [sa2ASA.in] (4/00) BEAVER VALLEY POWER STATION Health Physics Department

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	-			[(4/00)	***p	ROGENY INGROWTH ON ***	
STEP I-132 I-132	TIME INITIAL TOTALS	not used CURRENT : uCi : 0.000E+00 (INTEGRD WC1-sec D.000E+00	all S/Gs CURRENT uCi 1.167E+03	INTEGRD u C1-sec 8.447E+01	AVERAGE RELEASED RELEASE `uCi uCi/sec 1.167E+03	CURRENT CURRENT UC1 UC1/CC 0.000E+00	INTEGRD uCi-sec 4.950E+03
I-133 I-133	INITIAL TOTALS	0.000E+00 (0.000E+00	7.890E+03	5.711E+02	7.890E+03	0.000E+09	5.710E+04
I-134 I-134	initial Totals	0.000E+00 0	.000E+00	1.527E+02	1.105E+01	1.527E+02	0,0002+00	3.454E+02
I-135 I-135	INITIAL TOTALS	0.000E+00 0	.000E+00	2.757E+03	1.996E+02	2.757E+03	0.000E+00	1.696E+04

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ASA - for CR, EAB 4 LPZ dose (SA Case 2) [sa2ASA.in] (4/00)

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BEAVER VALLEY POWER STATION Health Physics Department

TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a ASA - for CR, EAB & LPZ dose (SA Case 2) [sa2ASA.in] (4/00) *** PROGENY INGROWTH ON *** - EXCLUSION AREA BOUNDARY ---- LOW POPULATION ZONE -------- CONTROL ROOM -----EDE SKIN-DE THY-CDE ÊDE SKIN-DE THY-CDE ED£ EDE RATE SKIN-DE THY-CDE DOSE DOSE DOSE DOSE DOSE · . DOSE DOSE DOSE RATE DOSE DOSE mrem Rren Mrem mrem mrem mrem mrem mrem/h mrem Kr-83m mrem TOTALS 4.92E-11 0.00E+00 0.00E+00 2.85E-12 0.00E+00 0.00E+00 1.82E-12 0.00E+00 0.00E+00 Kr-85m TOTALS 2.51E-07 4.96E-07 0.00E+00 1.46E-08 2.88E-08 0.00E+00 1.37E-08 5.40E-07 0.00E+00 Kr-85 TOTALS 3.65E-07 5.10E-05 0.00E+00 2.12E-08 2.96E-06 0.00E+00 2.83E-08 7.87E-05 0.00E+00 Kr-87 TOTALS 9.28E-07 2.20E-06 0.00E+00 5.39E-08 1.28E-07 0.00E+00 2.73E-08 1.29E-06 0.00E+00 Kr-88 TOTALS 6.53E-06 1.44E-06 0.00E+00 3.79E-07 8.35E-08 0.00E+00 3.01E-07 1.32E-06 0.00E+00 Kr-89 TOTALS 1.71E-07 1.86E-07 0.00E+00 9.92E-09 1.08E-08 0.00E+00 2.61E-10 5.65E-09 0.00E+00 Xe~131m TOTALS 4.49E-08 4.98E-07 0.00E+00 2.61E-09 2.89E-08 0.00E+00 3.51E-09 7.74E-07 0.00E+00 Xe-133m TOTALS 1.32E-07 8.75E-07 0.00E+00 7.64E-09 5.08E-08 0.00E+00 1.25E-08 1.65E-06 0.00E+00 Xe-133 TOTALS 1.15E-05 2.17E-05 0.00E+00 6.68E-07 1.26E-06 0.00E+00 9.23E-07 3.47E-05 0.00E+00 Xe-135m TOTALS 3.02E-06 9.59E-07 0.00E+00 1.75E-07 5.57E-08 0.00E+00 1.81E-06 1.15E-05 0.00E+00 Xe-135 TOTALS 2.94E-06 4.79E-06 0.00E+00 1.71E-07 2.78E-07 0.00E+00 1.36E-06 4.422-05 0.002+00 Xe-137 TOTALS 3.97E-08 6.01E-07 0.00E+00 2.30E-09 3.49E-08 0.00E+00 7.34E-11 2.21E-08 0.00E+00 Xe-138 TOTALS 8.92E-07 6.64E-07 0.00E+00 5.18E-08 3.86E-08 0.00E+00 5.99E-09 8.87E-08 0.00E+00 I-131 TOTALS 4.57E-04 2.41E-04 2.83E+00 2.66E-05 1.40E-05 1.64E-01 3.51E-05 3.68E-04 4.32E+00

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ASA - for CR, EAB & LPZ dose (SA Case 2) [sa2ASA.in] (4/00) *** PROGENY INGROWTH ON *** - EXCLUSION AREA BOUNDARY ---- LOW POPULATION ZONE ------ CONTROL ROOM ---EDE SKIN-DE THY-CDE EDE SKIN-DE THY-CDE EDE EDE RATE DOSE SKIN-DE DOSE DOSE DOSE DOSE DOSE . DOSE DOSE RATE mrem DOSE mrem mrem mrem mrem mrem I-132 mrem mrem/h mrem TOTALS 4.59E-04 1.36E-04 2.71E-03 2.66E-05 7.87E-06 1.58E-04 1.92E-05 1.13E-04 2.26E-03 I-133 TOTALS 7.98E-04 7.41E-04 5.13E-01 4.63E-05 4.30E-05 2.98E-02 5.69E-05 1.05E-03 7.28E-01 I-134 TOTALS 6.93E-05 2.28E-05 5.90E-05 4.02E-06 1.32E-06 3.42E-06 1.55E-06 1.01E-05 2.62E-05 I-135 TOTALS 7.58E-04 2.29E-04 3.11E-02 4.40E-05 1.33E-05 1.81E-03 4.60E-05 2.77E-04 3.76E-02 ALL NUCLIDES 0.5000 h 2.57E-03 1.46E-03 3.38E+00 1.49E-04 8.45E-05 1.96E-01 1.5000 h 0.00E+00 0.00E+00 0.00E+00 1.25E-05 4.90E-05 1.42E-04 3.32E-01 0.00E+00 0.00E+00 0.00E+00 1.8333 h 0.00E+00 0.00E+00 0.00E+00 4.66E-05 4.44E-05 5.41E-04 1.30E+00 0.00E+00 0.002+00 0.002+00 1.43E-05 4.16E-05 1.71E-04 4.22E-01 2.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 4.0000 h 0.00E+00 0.00E+00 0.00E+00 6.68E-06 3.86E-05 8.04E-05 2.01E-01

8.0000 h 0.00E+00 0.00E+00 0.00E+00

24.0000 h 0.00E+00 0.00E+00 0.00E+00

96.0000 h 0.00E+00 0.00E+00 0.00E+00

2.57E-03 1.46E-03 3.38E+00

0.00E+00

0.00E+00

8.5000 h 0.00E+00 0.00E+00

720.0000 h 0.00E+00 0.00E+00

TOTALS

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a

0.00E+00 0.00E+00 0.00E+00

0.002+00 0.002+00 0.002+00

1.49E-04 8.45E-05 1.96E-01

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BEAVER VALLEY POWER STATION Health Physics Department

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5.14E-05 1.62E-05 6.38E-04 1.65E+00

3.13E-05 3.05E-06 4.17E-04 1.17E+00

3.11E-07 2.32E-08 4.36E-06 1.30E-02

1.06E-07 9.53E-10 1.56E-06 5.14E-03

2.935-09 1.505-15 4.605-08 2.035-04

3.35E-15 0.00E+00 4.99E-14 3.70E-10

2.00E-03 5.09E+00

1.63E-04

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BEAVER VALLEY		ALL. ING FORM: RE 1.103-5	<u> 9/97</u>
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ricelul Physics Department	Revision 6	Attachment 4	
TRAILSPC Input File For FLIC	ase		
'L1 ',10,1.0E-3,3.47E-4,1.0E-5,3. 'FLI - for CR, EAB & LPZ Dose ('C1 ','not used ',0.0 ,0.0,0.0,0.0 'C2 ','faulted S/G ',7.6753E-3,0.0 'CR ',1.73E5 ,10.,10.,0.0,0.941,0 'PRD',24*0.0 'PRD',24*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,' ',24*0.0 'TIM',1800.,5400.,6600.,7200.,14 'XPR',10*0.0	47E-4,1.0,1.0E-3,3.47E-4,1,2 SA Case 2) [sa2FLI.in] (4/00) ,0.0,0.0 .0 E5,6.74E6,1.30E5,2.35E6,5*0. 400.,28800.,30600.,86400.,3.4	4,0,2 , 0 456E5,2.592E6	
'XPR',10*0.0 'XPR',50.0,1.0,31.0,3*104.,2800., 'XRM',10*0.0	3*50.	•	
'XRM'.6*1.0.4*0.0			
'XRM'.50.0.1.0.31.0.3*104 2800	2450		
'XRF'.10*0.0	3-50.		
'XRF'.10*0.0			
'XRF'.3*0.0 3*1 0 4*0 0	•		
'XOQEB'.4*1.04 6*0.0			
'XBREB'.4*1.0.6*0.0		•	
'XOQLZ',6*6.04,2*4 33 2 10 0 744			1
'XBRLZ', 10*1.0			
'XOQ',6*2.43,2*1,22,0,890,0,626			
'XBR',10*1.0			
'OCC',8*1.0,0.6,0.4			
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TRAILS_PC -- Transport of Radioactive Material in Linear Systems, V1.0a FLI - for CR, EAB 4 LPZ Dose (SA Case 2) [sa2FLI.in] (4/00) *** PROGENY INGROWTH ON *** COMP: not used COMP: faulted S/G COMP: Control Room VOLUME: 1.730E+05 Cu.Ft. INITIAL: 0.000E+00 I-131 6.190E+06 1-131 uCi 0.000E+00 I-131 0.000E+00 I-132 9.950E+05 I-132 0.000E+00 I-132 0.000E+00 I-133 6.740E+06 I-133 0.000E+00 I-133 0.000E+00 I-134 1.300E+05 I-134 0.000E+00 I-134 0.000E+00 I-135 2.350E+06 I-135 ACT MULT (to uCi): 0.000E+00 I-135 1.000E+00 1.000E+00 1.000E+00

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TRAILS PC -- Transport of Radioactive Material in Line FLI - for CR, EAB & LPZ Dose (SA Case 2) [sa2FLI.in]

XREM

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

----- CONTROL ROOM -----

M3/8 1.000E-03 3.470E-04 1.000E+00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

XPR

0.00

0.00

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0.00

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0.00

0.00

0.00

0.00

X/Q

a/M3

2.43

2.43

2.43

2.43

2.43

2.43

1.22

1.22

0.890

0.626

0.000E+00 1/sec

0.000E+00 0.000E+00

0.000E+00 _____

XRF

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

1.00

1.00 1.00

1.00

1.00 1.00

1.00

1.00

0.600

0.400

Breathing Occupancy

REMOVAL:

NUC Grp 1 REL FR:

NUC Grp 2 REL FR: NUC Grp 3 REL FR:

MULTIPLIERS===>> STEP TIME

1 1.800E+03

2 5.400E+03

6 2.880E+04

9 3.456E+05 10 2.592E+06

MULTIPLIERS----> STEP TIME, S 1 1.800E+03

2 5.400E+03

5 1.440E+04

6.600E+03

7.200E+03

2.880E+04

3.060E+04

8.640E+04

3.456E+05

10 2.592E+06

3

4

7

8

3

4

6 7

8

9

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6.600E+03

7.200E+03 5 1.440E+04

3.060E+04

8.640E+04

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TRAILS_PC FLI - for	Trans CR, EAB	port of Radi & LPZ Dose	oactive Mat (SA Case 2	terial in Line 2) [sa2FLI.in]	ear Systems, (4/00)	v1.0a	***PR(ogeny ingrowti	H ON ***	
STEP TIM	E	not used CURRENT uCi	INTEGRD u C1-se c	faulted S/G CURRENT uCi v 0.000E+00	INTEGRD uCi-sec	RELEASEI uCi	AVERAGE D RELEASE uCi/sec	CON CURRENT uC1 0.000E+00	CURRENT UCI/CC	INTEGRD uCi-sec
Xe-131m I Xe-131m	TOTALS	0.0005+00	0.000E+00	0.0002.00	7.759E+02	5.955E+0	00			3.250E+03
Xe-133m I Xe-133m	nitial Totals	0.000E+00	0.0002+00	0.000E+00	1.205E+04	9.249E+	01	0.000E+00		4.667E+04
Xe-133 I Xe-133	NITIAL TOTALS	0.0002+00	0.000E+00	0.000E+00	1.697E+05	1.303E+	03	0.000E+00		6.679E+05
Xe-135m I Xe-135m	INITIAL TOTALS	0.000E+00	0.000E+00	0.000E+00	4.492E+06	3.447E+	04	0.000E+00		2.201E+06
Xe-135 I Xe-135	INITIAL TOTALS	0.000E+00	0.000E+00	0.000E+00	7.117E+05	5.463E+	03	0.0002+00		2.479E+06
I-131 I I-131	INITIAL TOTALS	0.000E+00	0.000E+00	6.190E+06	8.064E+08	6.189E+	•06	0.000E+00		4.816E+07
I-132 1 I-132	INITIAL TOTALS	0.000E+00	0.000E+00	9,950E+05	1.282E+08	9.843E+	05	0.0002+00)	4.175E+06
I-133] I-133	initial Totals	0.000E+00	0.000E+00	6.740E+06	8.771E+08	6.732E+	+06	0.000E+00)	4.871E+07
I-134 I	INITIAL TOTALS	0.000E+00	0.000E+00	1.300E+05	1.647E+07	1.264E+	+05	0.000E+00		2.859E+05
I-135	INITIAL	0.0002+00	0.000E+00	2.350E+06	; 3.050E+08	2.34164	F06	0.0002+00)	1.440E+07

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TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a FLI - for CR, EAB & LPZ Dose (SA Case 2) (sa2FLI.in) (4/00) - EXCLUSION AREA BOUNDARY - --- LOW POPULATION ZONE ----EDE SKIN-DE THY-CDE EDE SKIN-DE THY-CDE

-- CONTROL ROOM -SKIN-DE THY-CDE EDE RATE EDE EDE SKIN-DE THY-CDE EDE DOSE DOSE RATE DOSE DOSE DOSE DOSE DOSE DOSE DOSE DOSE mrem mrem/h mrem mrem mrem mrem mrem mrem mrem mrem Xe-131m 9.98E-06 0.00E+00 4.53E-08 4.89E-10 5.42E-09 0.00E+00 8.41E-09 9.33E-08 0.00E+00 TOTALS Xe-133m 2.99E-04 0.00E+00 2.26E-06 2.64E-08 1.75E-07 0.00E+00 4.54E-07 3.02E-06 0.00E+00 TOTALS Xe-133 1.44E-03 0.00E+00 3.82E-05 4.39E-07 8.31E-07 0.00E+00 7.56E-06 1.43E-05 0.00E+00 TOTALS Xe-135m 9.72E-03 0.00E+00 1.54E-03 4.51E-05 0.00E+00 1.42E-04 2.44E-03 7.76E-04 0.00E+00 TOTALS Xe-135 3.28E-02 0.00E+00 1.01E-03 1.31E-05 2.14E-05 0.00E+00 2.268-04 3.688-04 0.008+00 TOTALS I-131 3.14E-01 3.68E+03 2.262-02 1.192-02 1.402+02 2.99E-02 3.90E-01 2.06E-01 2.41E+03 TOTALS I-132 9.52E-02 1.90E+00 1.62E-02 2.25E-02 6.64E-03 1.33E-01 3.87E-01 1.14E-01 2.29E+00 TOTALS I-133 8.98E-01 6.21E+02 4.86E-02 3.95E-02 3.67E-02 2.54E+01 6.01E-01 6.32E-01 4.37E+02 TOTALS I-134 8.36E-03 2.17E-02 1.28E-03 3.33E-03 1.09E-03 2.83E-03 5.73E-02 1.88E-02 4.88E-02 TOTALS I-135 2.35E-01 3.19E+01 3.91E-02 3.74E-02 1.13E-02 1.54E+00 6.44E-01 1.95E-01 2.64E+01 TOTALS ALL NUCLIDES 1.05E-02 4.12E-02 1.14E-01 2.83E+02 1.26E-01 6.78E-02 1.67E+02 0.5000 h 2.16E+00 1.17E+00 2.88E+03 3.93E-02 3.74E-02 4.34E-01 1.11E+03 6.59E-08 1.66E-04 1.20E-07 1.5000 h 2.06E-06 1.14E-06 2.86E-03 1.21E-02 3.51E-02 1.37E-01 3.60E+02 1.09E-19 6.24E-20 1.65E-16 1.8333 h 1.88E-18 1.07E-18 2.84E-15 3.26E-02 6.43E-02 1.71E+02 1.05E-23 6.07E-24 1.63E-20 5.63E-03 2.0000 h 1.81E-22 1.05E-22 2.80E-19 1.36E-02 5.10E-01 1.41E+03 1.05E-25 6.09E-26 1.64E-22 4.33E-02 4.0000 h 0.00E+00 0.00E+00 0.00E+00 3.31E-01 9.94E+02 2.64E-02 2.58E-03 0.00E+00 0.00E+00 8.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.96E-05 3.45E-03 1.11E+01 2.62E-04 0.00E+00 0.00E+00 0.00E+00 8.5000 h 0.00E+00 0.00E+00 0.00E+00 1.22E-03 4.39E+00 8.90E-05 8.02E-07 0.00E+00 0.00E+00 0.00E+00 24.0000 h 0.00E+00 0.00E+00 0.00E+00 2.47E-06 1.25E-12 3.48E-05 1.73E-01 0.00E+00 0.00E+00 0.00E+00 0.00E+00 96.0000 h 0.00E+00 0.00E+00 3.24E-11 3.15E-07 2.80E-12 0.00E+00 0.00E+00 0.00E+00 0.00E+00 720.0000 h 0.00E+00 0.00E+00 0.00E+00 1.59E+00 4.34E+03 1.38E-01 1.26E-01 6.78E-02 1.67E+02 2.16E+00 1.17E+00 2.88E+03 TOTALS

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TRAILSPC Input File For ILI Ca	ase	
'L1 ',10,1.0E-3,3.47E-4,1.0E-5,3 'ILI - for CR, EAB & LPZ dose ('C1 ','not used ',0.0,0.0,0.0,0.0 'C2 ','intact S/Gs ',1.43555E-6,0 'CR ',1.73E5,10.,10.,0.0,0.941,0 'PRD',24*0.0 'PRD',24*0.0 'INI',1.0,' ',24*0.0 'INI',2.0,'uCi',14*0.0,6.19E6,9.95 'INI',1.0,' ',24*0.0 'TIM',1800.,5400.,6600.,7200.,1 'XPR',10*0.0	9.47E-4,1.0,1.0E-3,3.47E-4,1,2 SA Case 2) [sa2ILI.in] (4/00) ' .0,0.0,0.0 0.0 5E5,6.74E6,1.30E5,2.35E6,5*0 4400.,28800.,30600.,86400.,3	4,0,2).0).456E5,2.592E6
'XPR',10*0.0 'XPR',50.0,1.0,31.0,3*104.,2800).,3*50.	•
'XRM',10*0.0 'XRM',4*1.0,2*0.698182,4*0.0 'XRM',50.0,1.0,31.0,3*104.,280 'XRF',10*0.0	0.,3*50.	
'XRF',10'0.0' 'XRF',3*0.0,3*1.0,4*0.0 'XOQEB',4*1.04,6*0.0 'XBREB',4*1.0,6*0.0		
'XOQLZ',6*6.04,2*4.33,2.10,0.7 'XBRLZ',10*1.0 'XOQ',6*2.43,2*1.22,0.890,0.62 'XBR',10*1.0 'OCC',8*1.0,0.6,0.4	44	-

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, V1.0a *** PROGENY INGROWTH ON *** COMP: Control Room COMP: intact S/Gs COMP: not used VOLUME: 1.730E+05 Cu.Ft. 6.190E+06 I-131 uCi 0.000E+00 I-131 INITIAL: 0.000E+00 I-131 9.950E+05 I-132 0.000E+00 I-132 0.000E+00 I-132 0.000E+00 I-133 6.740E+06 I-133 0.000E+00 I-133 0.000E+00 I-134 0.000E+00 I-134 1.300E+05 I-134 0.000E+00 I-135 2.350E+06 I-135 0.000E+00 I-135 1.000E+00 2.000E+00 ACT MULT (to uCi): 1.000E+00

ILI - for CR, EAB & LPZ dose (SA Case 2) [sa2ILI.in] (4/00)

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	PEMOVAL.		0.000E+0	0 1/sec		1.436E-0	6 1/sec		1.000E+01	cfm
	In 1 REL FR:		•••••	0.000E+00			0.000E+00	INTA	TE REDUCT:	0.000E+00
	m 2 REL FR:			0.000E+00			0.000E+00	INTA	TE REDUCT:	9.410E-0
NUC G	irp 3 REL FR:			0.000E+00			0.000E+00	INTA	RE REDUCT:	0.000E+00
MULTI	PLIERS===>		*********							
STEP	TIME	XPR	XREM	XRE	XPR	XREM	XRF	XPR	XREM	XRF
1	1.800E+03	0.00	0.00	0.00	0.00	1.00	0.00	50.0	50.0	0.00
2	5.400E+03	0.00	0.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00
3	6.600E+03	0.00	0.00	0.00	0.00	1.00	0.00	31.0	31.0	0.00
4	7.200E+03	0.00	0.00	0.00	0.00	1.00	0.00	104.	104.	1.00
5	1.440E+04	0.00	0.00	0.00	0.00	0.698	0.00	104.	104.	1.00
6	2.880E+04	0.00	0.00	0.00	0.00	0.698	0.00	104.	104.	1.00
7	3.0602+04	0.00	0.00	0.00	0.00	0.00	0.00	2.800E+03	2.800E+03	0.00
8	8.640E+04	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
9.	3.456E+05	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
10	2.592E+06	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
		C	ONTROL ROC	M	EXCLUS	ION AREA B	OUNDARY	LOW PO	PULATION Z	ONE
		x/o	Breathing	Occupancy	X/Q	Breat	hing	X/Q	Breath	ing
		s/M3	M3/s	•••	s/M	3 M3/	8	a/M3	M3/s	
		1.000E-03	3.4708-04	1.0005+00	1.000	E-03 3.470	E-04	1.000E	-05 3.470E	-04
(ULT)	PLIERS===>									
TEP	TIME.s									
1	1.800E+03	2.43	1.00	1.00	1.0	4 1.0	0	6.04	1.00	
2	5.400E+03	2.43	1.00	1.00	1.0	4 1.0	0	6.04	1.00	
3	6.600E+03	2.43	1.00	1.00	1.0	4 1.0	0	6.04	1.00	
4	7.200E+03	2.43	1.00	1.00	1.0	4 1.0	0	6.04	1.00	
5	1.440E+04	2.43	1.00	1.00	0.0	0 0.0		6.04	1.00	
6	2.8802+04	2.43	1.00	1.00	0.0	0 0.0	0	6.04	1.00	
7	3.060E+04	1.22	1.00	1.00	0.0	0 0.0	0	4.33	1.00	
8	8.640E+04	1.22	1.00	1.00	0.0	0 0.0	00	4.33	1.00	
9	3.456E+05	0.890	1.00	0.600	0.0	0 0.0	00	2.10	1.00	
· 10	2.592E+06	0.626	1.00	0.400	. 0.0	0 0.0	00	0.744	1.00	

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ILI - for CR, EAB 4 LPZ dose (SA Case 2) [sa2ILI.in] (4/00)

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*** PROGENY INGROWTH ON ***

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*** PROGENY INGROWTH ON ***

STEP TIME	not used CURRENT INTEGRD uCi uCi-sec	intact S/Gs CURRENT INTEGRD uCi uCi-sec	AVERAGE ' Released Release uci uci/sec	CURRENT CURRENT INTEGRD UCI UCI/CC UCI-Sec
Xe-131m INITIAL Xe-131m TOTALS	0.000E+00 0.000E+00	0.000E+00 8.137E+10	3.759E+01	2.670E+02
Xe-133m INITIAL	0.000E+00	0.000E+00	5.270E+02	0.000E+00
Xe-133m TOTALS	0.000E+00	4.062E+10		3.696E+03
Xe-133 INITIAL	0.000E+00	0.000E+00	7.579E+03	0.000E+00
Xe-133 TOTALS	0.000E+00	1.378E+12		5.365E+04
Xe-135m INITIAL	0.000E+00	0.000E+00	1.625E+04	0.000E+00
Xe-135m TOTALS	0.000E+00	2.601E+10		3.323E+04
Xe-135 INITIAL	0.000E+00	0.000E+00	2.600E+04	0.000E+00
Xe-135 TOTALS	0.000E+00	1.565E+11		1.717E+05
I-131 INITIAL	0.000E+00	1.238E+07	3.8462+05	0.000E+00
I-131 TOTALS	0.000E+00	1.112E+13		4.436E+05
I–132 INITIAL	0.000E+00	1.990E+06	2.608E+04	0.000E+00
I–132 TOTALS	0.000E+00	2.346E+10		2.865E+04
I–133 INITIAL	0.000E+00	1.348E+07	3.7652+05	0.000E+00
I–133 TOTALS	0.000E+00	1.416E+12		4.329E+05
I-134 INITIAL	0.000E+00	2.600E+05	1.583E+03	0.000E+00
I-134 TOTALS	0.000E+00	1.177E+09		1.479E+03
I-135 INITIAL	0.000E+00	4.700E+06	1.0362+05	. 0.000E+00
I-135 TOTALS	0.000E+00	1.578E+11		1.182E+05

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ILI - for CR, EAB & LPZ dose (SA Case 2) [sa2ILI.in] (4/00)

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*** PROGENY INGROWTH ON *** ILI - for CR, EAB & LPZ dose (SA Case 2) [sa2ILI.in] (4/00) - EXCLUSION AREA BOUNDARY ---- LOW POPULATION ZONE -------- CONTROL ROOM ----SKIN-DE THY-CDE EDE EDE RATE SKIN-DE THY-CDE EDE SKIN-DE THY-CDE EDE DOSE DOSE DOSE DOSE DOSE RATE DOSÉ DOSE DOSE DOSE DOSE mrem/h mrem mrem mrem mrem mrem mrem mrem mrem mrem Xe-131m 3.72E-09 8.20E-07 0.00E+00 3.08E-09 3.42E-08 0.00E+00 4.75E-09 5.27E-08 0.00E+00 TOTALS Xe-133m 1.79E-07 2.37E-05 0.00E+00 1.50E-07 9.99E-07 0.00E+00 TOTALS 2.50E-07 1.66E-06 0.00E+00 Xe-133 1.16E-04 0.00E+00 3.07E-06 TOTALS 4.19E-06 7.92E-06 0.00E+00 2.56E-06 4.83E-06 0.00E+00 Xe-135m 0.00E+00 6.68E-05 2.12E-05 0.00E+00 2.32E-05 1.47E-04 TOTALS 4.21E-04 1.34E-04 0.00E+00 Xe-135 2.27E-03 0.00E+00 6.24E-05 1.02E-04 0.00E+00 7.00E-05 1.28E-04 2.09E-04 0.00E+00 TOTALS I-131 2.89E-03 3.39E+01 1.41E-03 7.42E-04 8.71E+00 2.76E-04 7.99E-03 4.21E-03 4.94E+01 TOTALS I-132 6.53E-04 1.31E-02 1.11E-04 5.95E-04 1.76E-04 3.52E-03 TOTALS 6.04E-03 1.79E-03 3.57E-02 I-133 7.98E-03 5.52E+00 1.36E-02 1.26E-02 8.71E+00 2.21E-03 2.05E-03 1.42E+00 4.32E-04 TOTALS I-134 6.62E-06 4.33E-05 1.12E-04 4.17E-05 1.37E-05 3.55E-05 TOTALS 6.10E-04 2.00E-04 5.19E-04 I-135 1.93E-03 2.62E-01 1.66E-03 5.01E-04 6.80E-02 3.21E-04 TOTALS 1.20E-02 3.63E-03 4.93E-01 ALL NUCLIDES 5.33E-05 2.09E-04 5.81E-04 1.46E+00 6.36E-04 3.46E-04 8.61E-01 0.5000 h 1.09E-02 5.95E-03 1.48E+01 2.03E-04 1.97E-04 2.26E-03 5.82E+00 1.5000 h 2.03E-02 1.14E-02 2.93E+01 1.18E-03 6.61E-04 1.70E+00 7.682-05 2.632-04 8.772-04 2.332+00 3.69E-04 2.12E-04 5.63E-01 1.8333 h 6.36E-03 3.65E-03 9.69E+00 4.302-05 2.542-04 4.962-04 1.322+00 1.81E-04 1.04E-04 2.80E-01 2.0000 h 3.11E-03 1.80E-03 4.83E+00 3.94E-04 1.55E-04 4.83E-03 1.26E+01 1.39E-03 8.30E-04 2.32E+00 4.0000 h 0.00E+00 0.00E+00 0.00E+00 4.60E-04 9.28E-05 6.80E-03 1.57E+01 2.29E-03 1.46E-03 4.47E+00 8.0000 h 0.00E+00 0.00E+00 0.00E+00 9.402-06 6.962-07 1.542-04 3.242-01 0.00E+00 0.00E+00 0.00E+00 8.5000 h 0.00E+00 0.00E+00 0.00E+00 3.082-06 2.622-08 5.112-05 1.282-01 24.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 7.902-08 3,762-14 1.252-06 5.052-03 0.00E+00 0.00E+00 0.00E+00 96.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.03E-12 9.20E-09 8.38E-14 720.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.61E-02 3.97E+01 6.04E-03 3.61E-03 1.02E+01 1.24E-03 TOTALS 4.07E-02 2.28E-02 5.87E+01

TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a

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TRAILSPC Input File For ITN C	ase	
'L1',10,1E-3,3.47E-4,1.0E-5,3.4 'ITN - for CR, EAB & LPZ dose ('C1 ','not used ',0.0,0.0,0.0,0.0 'C2 ','intact S/G ',8.794E-8,0.0,0 'CR ',1.73E5,10,10,0.0,0.941,0 'PRD',24*0.0 'PRD',24*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,' ',24*0.0 'TIM',1800.,5400.,6600.,7200.,1 'XPR',10*0.0 'XPR',10*0.0 'XPR',10*0.0 'XPR',50.0,1.0,31.0,3*104.,2800 'XRM',6*1.0,4*0.0 'XRM',6*1.0,4*0.0 'XRF',10*0.0 'XRF',10*0.0 'XRF',10*0.0 'XRF',10*0.0 'XRF',10*0.0 'XRF',10*0.0 'XRF',10*0.0 'XCQ',4*1.04,6*0.0 'XOQ',6*6.04,2*4.33,2.10,0.744 'XBR',10*1.0 'XOQ',6*2.43,2*1.22,0.890,0.624 'XBR',10*1.0 'OCC',8*1.0,0.6,0.4	7E-4,1.0,1.0E-3,3.47E-4,1,24, SA Case 2) [sa2ITN.in] (4/00) 0,0.0 0,0 26E9,8.06E6,2.25E7,6.54E5,0 1.61E6,5.53E6,10*0.0 4400.,28800.,30600.,86400.,3 0.,3*50. 0.,3*50.	0,2 .0,4.09E7, .456E5,2.592E6
	۲.	

*** PROGENY INGROWTH ON ***

	COMP: not used	COMP: intact S/G	COMP: Control Room VOLUME: 1.730E+05 Cu.Ft.		
INITIAL: ACT MULT (to uCi):	0.000E+00 Kr-83m 0.000E+00 Kr-85m 0.000E+00 Kr-85 0.000E+00 Kr-87 0.000E+00 Kr-88 0.000E+00 Kr-89 0.000E+00 Xe-131m 0.000E+00 Xe-133m 0.000E+00 Xe-135m 0.000E+00 Xe-135 0.000E+00 Xe-137 0.000E+00 Xe-138 1.000E+00	3.440E+06 Kr-83m uC1 1.200E+07 Kr-85m 1.260E+09 Kr-85 8.060E+06 Kr-87 2.250E+07 Kr-88 6.540E+05 Kr-89 4.090E+07 Xe-131m 3.420E+07 Xe-133m 2.530E+09 Xe-133 7.820E+06 Xe-135m 8.420E+07 Xe-135 1.610E+06 Xe-137 5.530E+06 Xe-138 1.000E+00	0.000E+00 Kr-83m 0.000E+00 Kr-83m 0.000E+00 Kr-85m 0.000E+00 Kr-87 0.000E+00 Kr-87 0.000E+00 Kr-89 0.000E+00 Xe-131m 0.000E+00 Xe-133m 0.000E+00 Xe-135m 0.000E+00 Xe-135 0.000E+00 Xe-137 0.000E+00 Xe-138 1.000E+00		

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, V1.0a ITN - for CR, EAB & LPZ dose (SA Case 2) [sa2ITN.in] (4/00)

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BEAVER VALLEY

8.794E-08 1/sec 1.000E+01 cfm **REMOVAL:** 0.000E+00 1/sec INTAKE REDUCT: 0.000E+00 NUC Grp 1 REL FR: 0.000E+00 0.000E+00 0.000E+00 0.000E+00 INTAKE REDUCT: 9.410E-01 NUC Grp 2 REL FR: NUC Grp 3 REL FR: 0.000E+00 0.000E+00 INTAKE REDUCT: 0.000E+00 ____ MULTIPLIERS===> STEP TIME XRF XPR XREM XRF XPR XREM XRF XPR XREM 50.0 0.00 1 1.800E+03 0.00 0.00 0.00 0.00 1.00 0.00 50.0 0.00 1.00 0.00 1.00 1.00 0.00 2 5.400E+03 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.00 31.0 31.0 3 6.600E+03 0.00 4 7.200E+03 0.00 0.00 0.00 0.00 1.00 0.00 104. 104. 1.00 0.00 104. 104. 1.00 5 1.440E+04 0.00 0.00 0.00 0.00 1.00 104. 1.00 6 2.880E+04 0.00 0.00 0.00 0.00 1.00 0.00 104. 2.800E+03 2.800E+03 0.00 0.00 0.00 0.00 0.00 0.00 7 3.060E+04 0.00 50.0 0.00 0.00 0.00 0.00 0.00 0.00 50.0 8 8.640E+04 0.00 0.00 0.00 50.0 50.0 0.00 9 3.456E+05 0.00 0.00 0.00 0.00 50.0 0.00 50.0 10 2.592E+06 0.00 0.00 0.00 0.00 0.00 0.00 --- EXCLUSION AREA BOUNDARY ------ LOW POPULATION ZONE -------- CONTROL ROOM -----X/Q Breathing X/Q Breathing X/Q Breathing Occupancy M3/8 s/M3 M3/s s/M3 M3/s s/M3 1.000E-05 3.470E-04 1.0002-03 3.4702-04 1.000E-03 3.470E-04 1.000E+00 MULTIPLIERS====> STEP TIME, s 1 1.800E+03 6.04 1.00 2.43 1.00 1.00 1.04 1.00 2.43 1.04 1.00 6.04 1.00 2 5.400E+03 1.00 1.00 6.04 1.00 6.600E+03 2.43 1.00 1.00 1.04 1.00 3 4 7.200E+03 2.43 1.00 1.00 1.04 1.00 6.04 1.00 1.00 6.04 5 1.440E+04 2.43 1.00 1.00 0.00 0.00 6.04 1.00 6 2.880E+04 2.43 1.00 1.00 0.00 0.00 1.00 3.060E+04 1.22 1.00 1.00 0.00 0.00 4.33 7 1.00 8.640E+04 1.22 1.00 1.00 0.00 0.00 4.33 8 0.600 0.00 0.00 2.10 1.00 9 3.456E+05 0.890 1.00 1.00 10 2.592E+06 0.626 0.400 0.00 0.00 0.744 1.00

TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a ITN - for CR. EAB 4 LPZ dose (SA Case 2) [sa2ITN.in] (4/00) ***PROGENY INGROWTH ON ***

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of Radioactive Material in Linear Systems, v1.0a ----

ITN - fo	or CR, EAS	3 & LPZ dose	(SA Case 2)	[sa2ITN.in] (4/00)	***PR	OGENY INGROWTH ON ***	
STEP TI Kr-83m Kr-83m	ime Initial Totals	not used CURRENT uCi 0.000E+00	INTEGRD uCi-sec 0.000E+00	intact S/G CURRENT INTEGRD uCi uCi-sec 3.440E+06 3.267E+10	AVERAGE RELEASED RELEASE uC1 uC1/sec 2.734E+03	CURRENT CURRENT . UC1 UC1/CC 0.000E+00	INTEGRD uCi-sec 8.828E+03
Kr-85m Kr-85m	INITIAL TOTALS	0.000E+00	0.000E+00	1.200E+07 2.788E+11	1.741E+04	0.000E+00	8.421E+04
Kr-85 Kr-85	INITIAL TOTALS	0.000E+00	0.000E+00	1.260E+09 3.249E+15	3.187E+06	0.000E+00	2.020E+07
Kr-87 Kr-87	INITIAL TOTALS	0.000E+00	0.0002+00	8.060E+06 5.320E+10	4.619E+03	0.000E+00	1.119E+04
Kr-88 Kr-88	INITIAL TOTALS	0.000E+00	0.000E+00	2.250E+07 3.315E+11	2.502E+04	0.000E+00	1.030E+05
Kr-89 Kr-89	INITIAL TOTALS	0.000E+00	0.000E+00	6.540E+05 1.789E+08	1.573E+01	0.000E+00	2.437E+00
Xe-131m Xe-131m	INITIAL TOTALS	0.000E+00	0.000E+00	4.090E+07 4.981E+13	1.025E+05	0.000E+00	6.467E+05
Xe-133m Xe-133m	INITIAL TOTALS	0.000E+00	0.000E+00	3.420E+07 9.313E+12	8.210E+04	0.0002+00	5.087E+05
Xe-133 Xe-133	INITIAL TOTALS	0.000E+00	0.0002+00	2.530E+09 1.628E+15	6.263E+06	0.000E+00	3.932E+07
Xe-135m Xe-135m	INITIAL TOTALS	0.000E+00	0.000E+00	7.820E+06 1.040E+10	9.142E+02	0.000E+00	5.171E+02
Xe-135 Xe-135	Initial Totals	0.0002+00	0.000E+00	8.420E+07 3.987E+12	1.600E+05	0.0002+00	8.889E+05
Xe-137 Xe-137	INITIAL TOTALS	0.000E+00	0.000E+00	1.610E+06 5.338E+08	4.694E+01	0.0002+00	8.770E+00
Xe-138 Xe-138	INITIAL TOTALS	0.000E+0	0.000E+00	5.530E+06 6.763E+09	5.948E+02	0.0002+00	3.189E+02

TRAILS PC -- Transport of Radioactive Material in Linear Systems, vl.Oa *** PROGENY INGROWTH ON *** ITN - for CR, EAB & LPZ dose (SA Case 2) [sa2ITN.in] (4/00) --- LOW POPULATION ZONE -------- CONTROL ROOM ----- EXCLUSION AREA BOUNDARY -SKIN-DE THY-CDE EDE SKIN-DE THY-CDE EDE EDE RATE SKIN-DE THY-CDE EDE DOSE RATE DOSE DOSE DOSE DOSE DOSE DOSE DOSE DOSE DOSE mrem mrem mrem mrem mrem mrem nrem mrem/h mrem mrem Kr-83m 0.00E+00 0.00E+00 2.36E-08 0.00E+00 0.00E+00 2.45E-09 0.00E+00 0.00E+00 1.35E-09 TOTALS Kr-85m 8.79E-04 0.00E+00 TOTALS 1.76E-04 3.47E-04 0.00E+00 2.72E-05 5.38E-05 0.00E+00 2.24E-05 Kr-85 TOTALS 2,95E-04 4,12E-02 0.00E+00 6.84E-05 9.57E-03 0.00E+00 7.37E-05 2.05E-01 0.00E+00 Kr-87 4.58E-04 1.09E-03 0.00E+00 3,95E-05 9.38E-05 0.00E+00 1.63E-05 7.68E-04 0.00E+00 TOTALS Kr-88 0.00E+00 3.79E-04 1.66E-03 0.00E+00 TOTALS 4.202-03 9.252-04 0.002+00 5.42E-04 1.19E-04 Kr-89 5.27E-06 5.73E-06 0.00E+00 3.06E-07 3.33E-07 0.00E+00 8.05E-09 1.74E-07 0.00E+00 TOTALS Xe-131m 1.99E-03 0.00E+00 8.41E-06 9.32E-05 0.00E+00 9.01E-06 TOTALS 3.65E-05 4.04E-04 0.00E+00 Xe-133m 2.46E-05 3.26E-03 0.00E+00 TOTALS 1.05E-04 6.97E-04 0.00E+00 2.34E-05 1.56E-04 0.00E+00 Xe-133 9.25E-03 1.75E-02 0.00E+00 2.11E-03 3.99E-03 0.00E+00 2.25E-03 8.47E-02 0.00E+00 TOTALS . . Xe-135m 2.28E-06 0.00E+00 3.61E-07 TOTALS 6.44E-05 2.05E-05 0.00E+00 3.76E-06 1.19E-06 0.00E+00 Xe-135 3.62E-04 1.17E-02 0.00E+00 TOTALS 2.05E-03 3.34E-03 0.00E+00 3.84E-04 6.25E-04 0.00E+00 Xe-137 2.72E-09 8.21E-07 0.00E+00 TOTALS 1.48E-06 2.24E-05 0.00E+00 8.58E-08 1.30E-06 0.00E+00 Xe-138 9.62E-06 0.00E+00 7.14E-06 5.31E-06 0.00E+00 6.50E-07 1.23E-04 9.12E-05 0.00E+00 TOTALS

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TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a ITN - for CR, EAB & LPZ dose (SA Case 2) [sa2ITN.in] (4/00)

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*** PROGENY INGROWTH ON ***

	- EXCLUSI EDE DOSE mrem	ON AREA BO SKIN-DE DOSE mrem	UNDARY - THY-CDE DOSE mrem	LON EDE Dose mrem	POPULATION SKIN-DE DOSE mrem	ZONE THY-CDE DOSE mrem	EDE DOSE mrem	CONTRO EDE RATE DOSE RATE mrem/h	L ROOM SKIN-DE DOSE mrem	THY-CDE DOSE mrem
ALL NUCLIDES										
0.5000 h	4.595-03	1.67E-02	0.00E+00	2.66E-04	9.72E-04	0.00E+00	2.21E-05	8.59E-05	1.64E-03	0.00E+00
1 5000 h	8.305-03	3.28E-02	0.00E+00	4.82E-04	1.90E-03	0.00E+00	8.26E-05	8.02E-05	6.48E-03	0.00E+00
1 9333 h	2.605-03	1.085-02	0.00E+00	1.51E-04	6.27E-04	0.00E+00	3.12E-05	1.07E-04	2.58E-03	0.00E+00
2 0000 h	1 275-03	5.375-03	0.005+00	7.40E-05	3.12E-04	0.00E+00	2.16E-05	1.52E-04	1.81E-03	0.00E+00
2.0000 h	1.276-00	0.005+00	0.005+00	8 245-04	3.70E-03	0.00E+00	6.66E-04	4.728-04	6.05E-02	0.00E+00
4.0000 h	0.002+00	0.005+00	0.000,000	1 428-03	7 205-03	0 006+00	2.23E-03	6.14E-04	2.28E-01	0.00E+00
8.0000 n	0.002+00	0.002+00		1.426-03	0 005+00	0.005+00	6.25E-05	4.708-06	6.63E-03	0.00E+00
8.5000 h	0.00E+00	0.005+00	0.000+00	0.0000000		0.000+00	2 305-05	2 525-07	2.668-03	0.00E+00
24.0000 h	0.002+00	0.00E+00	0.00E+00	0.000+00	0.00E+00	0.002700	2.302-03	2.J26-07	1 118-04	0.005+00
96.0000 h	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	8.305-07	0.246-13	1.115-04	0.005+00
720.0000 h	0.00E+00	0.00E+00	0.00E+00	0.002+00	0.00E+00	0.00E+00	1.40E-12	0.00E+00	2.53E-10	0.005+00
TOTALS	1.68E-02	6.57E-02	0.00E+00	3.22E-03	1.47E-02	0.00E+00	3.14E-03		3.10E-01	0.00E+00

RTL: n/a Form: RE 1.103-3 9/92

BEAVER VALLEY		
POWER STATION	ERS-SFL-95-008	Page 50
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TRAILSPC Input File For ITC C	ase	
'L1 ',11,1.0E-3,3.47E-4,1.0E-5,3. 'ITC - for CR, EAB & LPZ dose ('C1 ','not used ',0.0,0.0,0.0,0.0 'C2 ','intact S/G ',9.213E-8,0.0,0. 'CR ',1.73E5 ,10.,10.,0.0,0.941,0	.47E-4,1.0,1.0E-3,3.47E-4,1,24 SA Case 2) [sa2ITC.in] (4/00) ' .0,0.0).0	4,0,2
'PRD',24*0.0 'PRD',14*0.0,6.59E5,6.41E5,1.1	3E6.7.11E5.8.52E5,5*0.0	•
'INI',1.0,' ',24*0.0		-
'INI',1.0,'uCi',14*0.0,2.23E7,8.81 'INI'.1.0.' '.24*0.0	E6,3.35E7,4.93E6,1.93E7,5"0	.0
'TIM',1800.,3600.,5400.,6600.,72 'XPR',11*0.0	200.,14400.,28800.,30600.,864	400.,3.456E5,2.592E6
'XPR',6*1.0,.002,4*0.0	·	
XPR',50.0,2*1.0,31.0,3*104.,280)0.,3*50 .	
'XRM'.2*1.0.5*0.01.4*0.0		
'XRM',50.0,2*1.0,31.0,3*104.,28	00.,3*50.	
'XRF',11*0.0		
XRF 1100		· · · ·
'XOQEB',5*1.04,6*0.0		•
'XBREB',5*1.0,6*0.0	· ·	•
XOQLZ',7*6.04,2*4.33,2.10,0.74	14	
XOQ'.7*2.43.2*1.22,0.890,0.626	5	
'XBR',11*1.0		
'OCC',9*1.0,0.6,0.4		

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TRAILS_PC -- Transport of Radioactive Material in Linear Systems, V1.0a ITC - for CR, EAB & LPZ dose (SA Case 2) [sa2ITC.in] (4/00)

*** PROGENY INGROWTH ON ***

	COMP: not used	COMP: intact S/G	COMP: Control Room VOLUME: 1.730E+05 Cu.Ft.
INITIAL:	0.000E+00 I-131 0.000E+00 I-132 0.000E+00 I-133 0.000E+00 I-134 0.000E+00 I-135 1.000E+00	2.230E+07 I-131 uC1 8.810E+06 I-132 3.350E+07 1-133 4.930E+06 I-134 1.930E+07 I-135 1.000E+00	0.000E+00 I-131 0.000E+00 I-132 0.000E+00 I-133 0.000E+00 I-134 0.000E+00 I-135 1.000E+00
PRODUCTION, uCi/s:	0.000E+00 I-131 0.000E+00 I-132 0.000E+00 I-133 0.000E+00 I-134 0.000E+00 I-135	6.590E+05 I-131 6.410E+05 I-132 1.130E+06 I-133 7.110E+05 I-134 8.520E+05 I-135	INTAKE: 1.000E+01 CFM

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BEAVER VALLEY POWER STATION Health Physics Department

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	REMOVAL:		0.000E+00	1/sec		9.213E-08	l/sec		1.000E+01	cím
NUC	Gro 1 REL FR:			0.000E+00			0.000E+00	INTA	KE REDUCT:	0.000E+00
NUC	Grp 2 REL FR:			0.000E+00			0.000E+00	INTA	KE REDUCT:	9.410E-01
NUC	Grp 3 REL FR:			0.000E+00		,	0.000E+00	INTA	KE REDUCT:	0.000E+00
HULT	IPLIERS====>									
STEP	TIME	XPR	XREM	XRF	XPR	XREM	XRF	XPR	XREM	XRF
1	1.800E+03	0.00	0.00	0.00	1.00	1.00	0.00	50.0	50.0	0.00
2	3.600E+03	0.00	0.00	0.00	1.00	1.00	0.00	1.00	1.00	0.00
3	5.400E+03	0.00	0.00	0.00	1.00	1.000E-02	0.00	1.00	1.00	0.00
- 4	6.600E+03	0.00	0.00	0.00	1.00	1.000E-02	0.00	31.0	31.0	0.00
5	7.200E+03	0.00	0.00	0.00	1.00	1.000E-02	0.00	104.	104.	1.00
6	1.440E+04	0.00	0.00	0.00	1.00	1.000E-02	0.00	104.	104.	1.00
7	2.880E+04	0.00	0.00	0.00	2.000E-03	1.000E-02	0.00	104.	104.	1.00
8	3.060E+04	0.00	0.00	0.00	0.00	0.00	0.00	2.800E+03	2.800E+03	0.00
9	8.640E+04	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
10	3.456E+05	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
11	2.592E+06	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
		C	CONTROL ROOM	*******	EXCLUSION AREA BOUNDARY			LOW POPULATION ZONE		
		X/Q 8/M3	Breathing (M3/s	Occupancy	X/Q s/M3	Breath M3/s	ing	X/Q s/M3	Breath: M3/s	lng
		1.000E-03	3.470E-04	1.000E+00	1.000E	-03 3.470E	-04	1.000E	-05 3.470E	-04
MULT	IPLIERS===>									
STEP	TIME, s	•								
1	1.800E+03	2.43	1.00	1.00	1.04	1.00		6.04	1.00	
2	3.600E+03	2.43	1.00	1.00	1.04	1.00		6.04	1.00	
3	5.400E+03	2.43	1.00	1.00	1.04	1.00		6.04	1.00	
4	6.600E+03	2.43	1.00	1.00	1.04	1.00		6.04	1.00	
5	7.200E+03	2.43	1.00	1.00	1.04	1.00		6.04	1.00	
6	1.440E+04	2.43	1.00	1.00	0.00	0.00	I	6.04	1.00	
7	2.880E+04	2.43	1.00	1.00	0.00	0.00	I Contraction of the second	6.04	1.00	
8	3.060E+04	1.22	1.00	1.00	0.00	0.00	I	4.33	1.00	
. 9	8.6402+04	1.22	1.00	1.00	. 0.00	0.00	I	4.33	1.00	
10	3.456E+05	0.890	1.00	0.600	0.00	0.00	i i i i i i i i i i i i i i i i i i i	2.10	1.00	
11	2.592E+06	0.626	1.00	0.400	0.00	0.00	1	0.744	1.00	

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ITC - for CR, EAB & LPZ dose (SA Case 2) [sa2ITC.in] (4/00)

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*** PROGENY INGROWTH ON ***

RTL: 10/18 Form: RE 1.103-3 9/92

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Attachment 4

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BEAVER VALLEY

ITC - for CR, EAB	4 LPZ dose (SA Case 2) [sa2]	ITC.in] (4/0	0)	*** PROGENY INGROWTH ON ***				
STEP TIME Xe-131m INITIAL	not used CURRENT I uC1 u 0.000E+00	intac INTEGRD CU IC1-sec u 0.0	ct S/G RRENT INTE Ci uCi-s D00E+00	GRD RELEAS ec aCi	AVERAGE ED RELEASE uC1/sec	CURRENT CURRENT UCI UCI/CC 0.000E+00	INTEGRD uC1-sec		
Xe-131m TOTALS	0	.000E+00	6.45	2E+13 1.903E	+01		1.620E+02		
Xe-133m INITIAL Xe-133m TOTALS	0.000E+00 0	0.0	000E+00 5.08	2E+13 4.336E	+02	0.000E+00	3.613E+03		
Xe-133 INITIAL Xe-133 TOTALS	0.000E+00 0	0.0 0.000E+00	000E+00 1.72	3E+15 6.194E	+03	0.000E+00	5.206E+04		
Xe-135m INITIAL Xe-135m TOTALS	0.000E+00 0	0.().000E+00	000E+00 6.97	4E+13 7.064E	+04	0.000E+00	1.773E+05		
Xe-135 INITIAL Xe-135 TOTALS	0.000E+00 0	0.0 0.000E+00	000E+00 4.22	7E+14 5.046E	+04	0.000E+00	3.948E+05		
I–131 INITIAL I–131 TOTALS	0.000E+00 0	2.2 0.000E+00	230E+07 8.82	7E+15 5.837E	+05	0.000E+00	9.237E+05		
I-132 INITIAL I-132 TOTALS	0.000E+00 0	8.0 0.000E+00	B10E+06 1.10	6E+14 4.300E	+05	0.000E+00	4.419E+05		
I-133 INITIAL I-133 TOTALS	0.000E+00 0	3.3 0.000E+00	350E+07 1.76	5E+15 9.647E	+05	0.0002+00	1.454E+06		
I-134 INITIAL I-134 TOTALS	0.000E+00 0	4.9 .000E+00	930E+06 4.67	3E+13 3.719E	+05	0.000E+00	2.334E+05		
I-135 INITIAL I-135 TOTALS	0.000E+00 0	1.9 0.000E+00	930E+07 4.22	7E+14 6.725E	+05 · ·	0.000E+00	9.060E+05		

TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a

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BEAVER VALLEY POWER STATION Health Physics Department

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***Pro	JENY INGROW	TH ON ***		BEAVER POWER : Health F	
				Ξ°ς <	
EDE Dose mrem	EDE RATE DOSE RATE mrem/h	L ROOM SKIN-DE DOSE mrem	THY-CDE DOSE mrem	 ALLE	
2.26E-09		4.98E-07	0.00E+00		
1.75E-07		2.31E-05	0.00E+00		
2.98E-06		1.12E-04	0.00E+00		
1.24E-04		7.83E-04	0.00E+00	ш	
1.61E-04		5.22E-03	0.00E+00	RS-	
5.74E-04		6.02E-03	7.07E+01	SFL	
1.71E-03		1.01E-02	2.02E-01	95	
1.45E-03		2.68E-02	1.85E+01	-008	
1.04E-03		6.83E-03	1.77E-02	~	
2.46E-03		1.48E-02	2.01E+00	Attach	
6.51E-04 1.20E-03	2.50E-03 2.30E-03	5.22E-03 9.82E-03	5.17E+00 1.05E+01	Pag ment 4	RTL: 1
1.07E-03	2.01E-03	9.13E-03	1.07E+01	- Q	۲ ا
6.43E-04	1.85E-03	5.63E-03	7.05E+00	*	-
2.95E-04	1.69E-03	2.62E-03	3.40E+00		3
z.15E-03	6.62E-04	2.03E-02	2.88E+01		Ħ
1.49E-03	2.22E-04	1.75E-02	2.53E+01		권
2.24E-05	1.63E-06	3.10E-04	4.00E-01		E
0,4924U0 1 208-07	1.33E-U8	9.81E-05	1.56E-01	, 15 , 15, 1	
4.952-1/	3.375-14	2.125+UD 1 25P-12	3.9/E-U3 1 058-00		μ
7.538+03	VIVETUV	7.06E-02	9.148401		هٽ ا
		· • • • • • • • • • • • • •			26/6

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, vl.Oa ITC - for CR, EAB & LPZ dose (SA Case 2) [sa2ITC.in] (4/00) - EXCLUSION AREA BOUNDARY ---- LOW POPULATION ZONE ---EDE

EDE

DOSE

THY-CDE

DOSE

SKIN-DE

DOSE

DOSE

mren	nrem	mrem	mrem	mrem	mrem	mrem	mrem/h	mrem
5.40E-09	5.99E-08	0.00E+00	1.56E-09	1.73E-08	0,00E+00	2.26E-09		4.98E-0
4.54E-07	3.02E-06	0.00E+00	1.24E-07	8.22E-07	0.00E+00	1.75E-07		2.31E-0
7.57E-06	1.43E-05	0.00E+00	2.09E-06	3.95E-06	0.00E+00	2.98E-06		1.12E-0
3.15E-03	1.00E-03	0.00E+00	2.90E-04	9.23E-05	0.00E+00	1.24E-04		7.83E-0
5.02E-04	8.19E-04	0.00E+00	1.21E-04	1.97E-04	0.00E+00	1.61E-04		5.22E-0
2.60E-02	1.37E-02	1.61E+02	2.14E-03	1.13E-03	1.32E+01	5.74E-04		6.02E-0
1.41E-01	4.17E-02	8.34E-01	9.81E-03	2.90E-03	5.805-02	1.71E-03		1.01E-0
7.06E-02	6.55E-02	4.53E+01	5.67E-03	5.26E-03	3.64E+00	1.45E-03		2.68E-0
1.54 E-0 1	5.07E-02	1.31E-01	9.80E-03	3.22E-03	8.34E-03	1.04E-03		6.83E-0
1.41E-01	4.26E-02	5.78E+00	1.07E-02	3.25E-03	4.41E-01	2.46E-03		1.48E-0

SKIN-DE

DOSE

THY-CDE

• DOSE

ALL NUCLIDES

Xe-131m TOTALS Xe-133m TOTALS Xe~133 TOTALS Xe-135m TOTALS Xe-135 TOTALS I-131 TOTALS I-132 TOTALS I-133 TOTALS I-134 TOTALS I-135 TOTALS

.0.5000 h 1.39E-01 5.53E-02 5.27E+01 8.06E-03 3:21E-03 3.06E+00 6.51E-04 2.50E-03 5. 1.0000 h 3.84E-01 1.55E-01 1.54E+02 2.23E-02 9.00E-03 8.94E+00 1.20E-03 2.30E-03 9. 1.5000 h 5.95E-03 2.44E-03 2.54E+00 3.46E-04 1.42E-04 1.48E-01 1.07E-03 2.01E-03 9. 1.8333 h 5.01E-03 2.08E-03 2.25E+00 2.91E-04 1.21E-04 1.31E-01 6.43E-04 1.85E-03 5. 2.0000 h 2.80E-03 1.17E-03 1.29E+00 1.62E-04 6.79E-05 7.50E-02 2.95E-04 1.69E-03 2. 4.0000 h 0.00E+00 0.00E+00 0.00E+00 2.69E-03 1.17E-03 1.40E+00 2.15E-03 6.62E-04 2. 8.0000 h 0.00E+00 0.00E+00 0.00E+00 4.74E-03 2.34E-03 3.61E+00 1.49E-03 2.22E-04 1. 8.5000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 2.24E-05 1.63E-06 3. 24.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 6,49E-06 4.53E-08 9. 96.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.298-07 4.498-14 2. 720.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 9.95E-14 0.00E+00 1.: 5.36E-01 2.16E-01 2.13E+02 TOTALS 3.86E-02 1.61E-02 1.74E+01 7.53E-03 7.

RTL: n/a Form: RE 1.103-3 9/92

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TRAILSPC Input File For ITP C	ase	
'L1 ',11,1.0E-3,3.47E-4,1.0E-5,3 'ITP - for CR, EAB & LPZ dose ('C1 ','not used ',0.0,0.0,0.0,0.0 'C2 ','intact S/G ',8.794E-8,0.0,0 'CR ',1.73E5,10.,10.,0.0,0.941,0 'PRD',24*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,' ',24*0.0 'TIM',1800.,3600.,5400.,6600.,72 'XPR',11*0.0 'XPR',11*0.0 'XPR',11*0.0 'XPR',50.0,2*1.0,31.0,3*104.,28 'XRM',11*0.0 'XRM',2*1.0,5*0.01,4*0.0 'XRM',50.0,2*1.0,31.0,3*104.,28 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XRF',11*0.0 'XCQEB',5*1.0,4*0.0 'XOQLZ',7*6.04,2*4.33,2.10,0.74 'XBRLZ',11*1.0 'XOQ',7*2.43,2*1.22,0.890,0.620	.47E-4,1.0,1.0E-3,3.47E-4,1,2 SA Case 2) [sa2ITP.in] (4/00) .0,0.0).0 HE8,2.10E9,3.10E8,1.21E9,5*0 200.,14400.,28800.,30600.,86 00.,3*50. 00.,3*50.	4,0,2 0.0 400.,3.456E5,2.592E6
'OCC',9*1.0,0.6,0.4		

COMP: intact S/G COMP: Control Room COMP: not used VOLUME: 1.730E+05 Cu.Ft. _____ 0.000E+00 I-131 1.400E+09 I-131 uCi INITIAL: 0.000E+00 I-131 0.000E+00 I-132 0.000E+00 I-132 5.540E+08 I-132 2.100E+09 I-133 0.000E+00 I-133 0.000E+00 I-133 3.100E+08 I-134 0.000E+00 I-134 0.000E+00 I-134 0.000E+00 I-135 0.000E+00 I-135 1.210E+09 I-135 1.000E+00 1.000E+00 ACT MULT (to uCi): 1.000E+00

TRAILS PC -- Transport of Radioactive Material in Linear Systems, V1.0a ITP - for CR, EAB 4 LPZ dose (SA Case 2) [sa2ITP.in] (4/00) *** PROGENY INGROWTH ON *** BEAVER VALLEY POWER STATION Health Physics Department

RTL: n/a Form: RE 1.103-3 9/92

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Revision 6

TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a ITP - for CR, EAB & LPZ dose (SA Case 2) [sa2ITP.in] (4/00) *** PROGENY INGROWTH ON *** 8.794E-08 1/sec 1.000E+01 cfm 0.000E+00 1/sec REMOVAL: NUC GFD 1 REL FR: 0.000E+00 0.000E+00 INTAKE REDUCT: 0.000E+00 0.000E+00 0.000E+00 INTAKE REDUCT: 9.410E-01 NUC Gro 2 REL FR: NUC Grp 3 REL FR: 0.000E+00 0.000E+00 INTAKE REDUCT: 0.000E+00 MULTIPLIERS===> STEP TIME XPR XREM XRF XPR XREM XRF XPR XREM XRF 0.00 1.00 0.00 50.0 50.0 0.00 0.00 0.00 1 1.800E+03 0.00 0.00 0.00 1.00 0.00 1.00 1.00 0.00 2 3.600E+03 0.00 0.00 1.000E-02 1.00 0.00 5.400E+03 0.00 0.00 0.00 0.00 0.00 1.00 3 1.000E-02 0.00 6.600E+03 0.00 0.00 0.00 0.00 0.00 31.0 31.0 4 5 7.200E+03 0.00 0.00 0.00 0.00 1.000E-02 0.00 104. 104. 1.00 0.00 104. 104. 1.00 6 1.440E+04 0.00 0.00 0.00 1.000E-02 0.00 1.00 0.00 0.00 1.000E-02 0.00 104. 104. 7 2.880E+04 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0,00 2.800E+03 2.800E+03 3.060E+04 8 50.0 50.0 0.00 0.00 0.00 0.00 9 8.640E+04 0.00 0.00 0.00 0.00 0.00 0.00 50.0 50.0 0.00 10 3.456E+05 0.00 0.00 0.00 50.0 50.0 0.00 11 2.592E+06 0.00 0.00 0.00 0.00 0.00 0.00 --- EXCLUSION AREA BOUNDARY ------ LOW POPULATION ZONE ----CONTROL ROOM -----_____ X/Q Breathing X/Q Breathing X/Q Breathing Occupancy s/M3 M3/s a/M3 M3/s s/M3 M3/s 1.000E-03 3.470E-04 1.000E+00 1.000E-03 3.470E-04 1.000E+05 3.470E-04 MULTIPLIERS== STEP TIME, s 1.00 1.00 6.04 1 1.800E+03 2.43 1.00 1.00 1.04 6.04 1.00 2 3.600E+03 2.43 1.00 1.00 1.04 1.00 6.04 1.00 3 5.400E+03 1.00 1,04 1.00 2.43 1.00 1.00 6.04 1.00 4 6.600E+03 2.43 1.00 1.00 1.04 7.200E+03 1.00 1.04 1.00 6.04 1.00 5 2.43 1.00 1.00 0.00 0.00 6.04 6 1.440E+04 2.43 1.00 1.00 6.04 1.00 2.43 1.00 1.00 0.00 0.00 7 2.880E+04 1.00 0.00 0.00 4.33 1.00 3.060E+04 1.22 1.00 8 4.33 1.00 8.640E+04 1.22 1.00 1.00 0.00 0.00 9 2.10 1.00 10 3.456E+05 0.890 1.00 0.600 . 0.00 0.00 0.744 1.00 11 2.592E+06 0.626 1.00 0.400 0.00 0.00

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Attachment 4

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POWER EAVER Health Physics Department R VALLEY *** PROGENY INGROWTH ON *** -----CONTROL ROOM------AVERAGE intact S/G INTEGRD RELEASED RELEASE CURRENT CURRENT CURRENT INTEGRD uCi-sec uC1 uCi/cc uCi-sec ùCi uCi/sec uCi 0.000E+00 0.000E+00 1.534E+02 9.498E+12 9.530E+00 0.000E+00 0.000E+00 0.000E+00 3.010E+03 6.531E+12 1.945E+02 0.000E+00 0.000E+00 0.000E+00 4.320E+04 2.766E+03 2.215E+14 0.000E+00 0.000E+00 0.000E+00 1.917E+05 4.267E+04 6.852E+12 0.000E+00 ERS-SFL-95-008 0.000E+00 0.000E+00 2.573E+05 4.153E+13 1.829E+04 0.000E+00 **Revision 6** 0.000E+00 1.400E+09 1.771E+06 1.297E+15 4.729E+05 0.000E+00 0.000E+00 5.540E+08 3.525E+05 6.616E+12 1.552E+05 0.000E+00 0.000E+00 2.100E+09 2.450E+06 2.268E+14 6.939E+05 0.000E+00 0.000E+00 3.100E+08 9.307E+04 1.411E+12 6.838E+04 0.000E+00 0.000E+00 1.210E+09 1.177E+06 Attachment 4 4.153E+13 3.807E+05 0.000E+00 Page

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a ITP - for CR, EAB & LPZ dose (SA Case 2) [sa2ITP.in] (4/00)

INTEGRD

uCi-sec

not used

CURRENT

uCi

0.000E+00

STEP TIME

Xe-131m INITIAL

Xe-131m TOTALS

Xe-133m INITIAL

Xe-133m TOTALS

Xe-133 INITIAL

Xe-135m INITIAL

Xe-135m TOTALS

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TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a ITP - for CR, EAB & LPZ dose (SA Case 2) [sa2ITP.in] (4/00) *** PROGENY INGROWTH ON *** --- LOW POPULATION ZONE -------- CONTROL ROOM ---- EXCLUSION AREA BOUNDARY -EDE RATE SKIN-DE THY-CDE EDE SKIN-DE THY-CDE EDE SKIN-DE THY-CDE EDE DOSE DOSE DOSE DOSE DOSE DOSE DOSE RATE DOSE DOSE DOSE mrem/h MLGW mrem mrem mrem area mren mrem mrem mrem Xe-131m 7.82E-10 8.67E-09 0.00E+00 4.71E-07 0.00E+00 2.14E-09 TOTALS 8.55E-09 9.48E-08 0.00E+00 Xe-133m 1.93E-05 0.00E+00 TOTALS 6.28E-07 4.18E+06 0.00E+00 5.55E-08 3.69E-07 0.00E+00 1.46E-07 Xe-133 9.31E-05 0.00E+00 9.33E-07 1.76E-06 0.00E+00 2.47E-06 TOTALS 1.05E-05 1.98E-05 0.00E+00 Xe-135m 8.47E-04 0.00E+00 1.34E-04 2.85E-03 9.07E-04 0.00E+00 1.75E-04 5.58E-05 0.00E+00 TOTALS Xe-135 3.40E-03 0.00E+00 4.39E-05 7.15E-05 0.00E+00 1.05E-04 TOTALS 5.37E-04 8.75E-04 0.00E+00 1-131 1.15E-02 1.35E+02 1.73E-03 9.12E-04 1.07E+01 1.10E-03 TOTALS 2.81E-02 1.48E-02 1.74E+02 I-132 1.37E-03 8.04E-03 1.61E-01 3.54E-03 1.05E-03 2.09E-02 TOTALS 5.99E-02 1.77E-02 3.54E-01 I-133 4.51E-02 3.12E+01 2.44E-03 4.08E-03 3.78E-03 2.62E+00 6.67E-02 6.20E-02 4.29E+01 TOTALS I-134 4.16E-04 2.72E-03 7.05E-03 1.80E-03 5.92E-04 1.53E-03 TOTALS 3.09E-02 1.02E-02 2.63E-02 I-135 3.19E-03 1.92E-02 2.61E+00 TOTALS 1.01E-01 3.05E-02 4.14E+00 6.08E-03 1.84E-03 2.50E-01 ALL NUCLIDES 7.21E-04 2.80E-03 6.74E-03 1.08E+01 8.72E-03 4.05E-03 6.39E+00 0.5000 h 1.50E-01 6.99E-02 1.10E+02 1.36E-03 2.63E-03 1.29E-02 2.14E+01 1.0000 h 1.37E-01 6.59E-02 1.09E+02 7.98E-03 3.83E-03 6.35E+00 7.37E-05 3.64E-05 6.31E-02 1.26E-03 2.43E-03 1.24E-02 2.15E+01 6.27E-04 1.09E+00 1.5000 h 1.27E-03 7.79E-04 2.25E-03 7.83E-03 1.40E+01 4.63E-05 2.34E-05 4.19E-02 1.8333 h 7.97E-04 4.02E-04 7.21E-01 3.66E-03 6.68E+00 2.24E-05 1.14E-05 2.09E-02 3.60E-04 2.07E-03 2.0000 h 3.85E-04 1.97E-04 3.60E-01 2.38E-04 1.28E-04 2.48E-01 2.692-03 8.222-04 2.86E-02 5.50E+01 4.0000 h 0.00E+00 0.00E+00 0.00E+00 1.86E-02 3.94E+01 1.57E-03 1.55E-04 0.00E+00 0.00E+00 3.68E-04 2.19E-04 4.80E-01 8.0000 h 0.00E+00 1.58E-05 1.17E-06 2.05E-04 4.54E-01 0.002+00 0.002+00 0.002+00 0.00E+00 8.5000 h 0.00E+00 0.00E+00 4.06E-08 6.99E-05 1.78E-01 5.05E-06 24.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.21E-07 5.08E-14 1.80E-06 6.90E-03 0.00E+00 96.0000 h 0.00E+00 0.00E+00 1.36E-12 1.23E-08 1.13E-13 0.00E+00 0.00E+00 0.00E+00 0.00E+00 720.0000 h 0.00E+00 0.00E+00 0.00E+00 9.10E-02 1.69E+02 8.76E-03 2.90E-01 1.37E-01 2.22E+02 1.74E-02 8.30E-03 1.36E+01 TOTALS

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BEAVER VALLEY	ERS-SEL-95-008	Page 60					
Health Bhyrier Danatmant		Attachment A					
TRAILSPC Input File For FRC	Case	- Autominion -					
'L1 ',10,1.0E-3,3.47E-4,1.0E-5,3 'FRC - for CR, EAB & LPZ dose 'C1 ','not used ',0.0,0.0,0.0,0.0 'C2 ','Affected S/G ',2.478E-6,0. 'CR ',1.73E5,10.,10.,0.0,0.941,0 'PRD',24*0.0 'PRD' 14*0 0 6 59E5 6 41E5 1 1	1.47E-4,1.0,1.0E-3,3.47E-4,1,2 (SA Case 2) [sa2FRC55.in] (4 0,0.0,0.0).0	24,0,2 4/00) '					
'PRD',14*0.0,6.59E5,6.41E5,1.13E6,7.11E5,8.52E5,5*0.0 'INI',1.0,' ',24*0.0 'INI',1.0,'uCi',3.28E6,1.15E7,1.20E9,7.69E6,2.15E7,6.24E5,0.0,3.90E7, 3.26E7,2.42E9,7.47E6,8.03E7,1.54E6,5.27E6,2.23E7,8.81E6,3.35E7,4.93E6, 1.93E7,5*0.0 'INI' 1.0'' 24*0.0							
'TIM',1800.,5400.,6600.,7200.,1 'XPR',10*0.0 'XPR',5*1.0,.002,4*0.0 'XPR',50.0,1.0,31.0,3*104.,2800 'XRM',10*0.0	4400.,28800.,30600.,86400.,3).,3*50.	3.456E5,2.592E6					
'XRM',6*1.0,4*0.0 'XRM',50.0,1.0,31.0,3*104.,280 'XRF',10*0.0 'XRF',10*0.0 'XRF',3*0.0,3*1.0,4*0.0	0.,3*50.						
'XOQEB',4*1.04,6*0.0 'XBREB',4*1.0,6*0.0 'XOQLZ',6*6.04,2*4.33,2.10,0.7 'XBRLZ',10*1.0 'XOO' 6*2,43,2*1,22,0,890,0,62	44						
'XBR',10*1.0 'OCC',8*1.0,0.6,0.4							

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*** PROGENY INGROWTH ON ***

	COMP: not used	COMP: Affected S/G	COMP: Control Room VOLUME: 1.730E+05 Cu.Ft.
INITIAL:	0.000E+00 Kr-83m	3.280E+06 Kr-83m uCi	0.000E+00 Kr-83m
	0.000E+00 Kr-85m	1.150E+07 Kr-85m	0.000E+00 Kr-85m
	0.000E+00 Kr-85	1.200E+09 Kr-85	0.000E+00 Kr-85
	0.000E+00 Kr-87	7.690E+06 Kr-87	0.000E+00 Kr-87
	0.000E+00 Kr-88	2.150E+07 Kr-88	0.000E+00 Kr-88
	0.000E+00 Kr-89	6.240E+05 Kr-89	0.000E+00 Kr-89
	0.000E+00 Xe-131m	3.900E+07 Xe-131m	0.000E+00 Xe-131m
	0.000E+00 Xe-133m	3.260E+07 Xe-133m	0.000E+00 Xe-133m
	0.000E+00 Xe-133	2.420E+09 Xe-133	0.000E+00 Xe-133
	0.000E+00 Xe-135m	7.470E+06 Xe-135m	0.000E+00 Xe-135m
	0.000E+00 Xe-135	8.030E+07 Xe-135	0.000E+00 Xe-135
	0.000E+00 Xe-137	1.540E+06 Xe-137	0.000E+00 Xe-137
	0.000E+00 Xe-138	5.270E+06 Xe-138	0.000E+00 Xe-138
	0.000E+00 I-131	2.230E+07 I-131	0.000E+00 I-131
	0.000E+00 I-132	8.810E+06 I-132	0.000E+00 I-132
	0.000E+00 I-133	3.350E+07 I-133	0.000E+00 T-133
	0.000E+00 I-134	4.930E+06 I-134	0.000E+00 T-134
	0.000E+00 I-135	1.930E+07 I-135	0.000E+00 I-135
ACT MULT (to uCi):	1.000E+00	1.000E+00	1.000E+00
PRODUCTION, uCi/s:	0.000E+00 I-131	6.590E+05 I-131	INTAKE: 1.000E+01 CFM
	0.000E+00 I-132	6.410E+05 I-132	
	0.000E+00 I-133	1.130E+06 I-133	•
	0.000E+00 I-134	7.110E+05 I-134	
	0.000E+00 I+135	8.520E+05 T-135	

TRAILS_PC -- Transport of Radioactive Material in Linear Systems, V1.0a FRC - for CR, EAB 4 LPZ dose (SA Case 2) [sa2FRC55.in] (4/00)

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BEAVER VALLEY POWER STATION Health Physics Department

2.478E-06 1/sec 1.000E+01 cfm **REMOVAL:** 0.000E+00 1/sec 0.000E+00 INTAKE REDUCT: 0.000E+00 NUC Gro 1 REL FR: 0.000E+00 0.000E+00 0.000E+00 INTAKE REDUCT: 9.410E-01 NUC Grp 2 REL FR: INTAKE REDUCT: 0.000E+00 0.000E+00 0.000E+00 NUC Grp 3 REL FR: MULTIPLIERS===> XREM XRF STEP TIME XPR XREM XRF XPR XREM XRF XPR 1.00 0.00 50.0 50.0 0.00 0.00 0.00 1.00 1 1.800E+03 0.00 1.00 0.00 1.00 1.00 0.00 0.00 1.00 2 5.400E+03 0.00 0.00 0.00 0.00 1.00 1.00 0.00 31.0 31.0 0.00 3 6.600E+03 0.00 104. 1.00 104. 1.00 4 7.200E+03 0.00 0.00 0.00 1.00 0.00 104. 5 1.440E+04 0.00 0.00 0.00 1.00 1.00 0.00 104. 1.00 104. 0.00 0.00 0.00 2.000E-03 1.00 0.00 104. 1.00 6 2.880E+04 2.800E+03 2.800E+03 0.00 0.00 0.00 0.00 7 3.060E+04 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 50.0 50.0 0.00 8.640E+04 50.0 50.0 0.00 3.456E+05 0.00 0.00 0.00 0.00 0.00 0.00 50.0 50.0 0.00 10 2.592E+06 0.00 0.00 . 0.00 0.00 0.00 0.00 --- EXCLUSION AREA BOUNDARY ------ LOW POPULATION ZONE -------- CONTROL ROOM -----X/Q Breathing X/0 X/Q Breathing Occupancy Breathing M3/a s/M3 M3/a #/M3 M3/s s/M3 1.000E-05 3.470E-04 1.000E-03 3.470E-04 1.000E+00 1.000E-03 3.470E-04 MULTIPLIERS====> STEP TIME, s 1.00 1 1.800E+03 1.00 1.04 1.00 6.04 2.43 1.00 1.00 1.04 1.00 6.04 1.00 2 5.400E+03 2.43 1.00 1.00 6.04 1.00 6.600E+03 2.43 1.00 1.00 1.04 1.00 4 7.200E+03 2.43 1.00 1.00 1.04 1.00 6.04 0.00 6.04 1.00 5 1.440E+04 2.43 1.00 1.00 0.00 0.00 0.00 6.04 1.00 2.43 1.00 1.00 6 2.880E+04

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TRAILS PC -- Transport of Radioactive Material in Linear Systems, v1.0a FRC - for CR, EAB & LPZ dose (SA Case 2) [sa2FRC55.in] (4/00)

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7 3.060E+04

10 2.592E+06

8.640E+04

3.456E+05

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*** PROGENY INGROWTH ON ***

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*** PROGENY INGROWTH ON ***

	not used	Affected S/G	AVERAGE	CONTROL ROOM
STEP TIME	CURRENT INTEGRD uCi uCi-sec	CURRENT INTEGRD UCI UCI-sec	RELEASED RELEASE	CURRENT CURRENT INTEGRD uC1 uC1/cc uC1-sec
Kr-83m INITIAL	0.000E+00	3.280E+06		0.000E+00
Kr-83m TOTALS	0.000E+00	3.049E+10	7.208E+04	2.316E+05
Kr-85m INITIAL	0.000E+00	1.150E+07		0.000E+00
Kr-85m TOTALS	0.000E+00	2.569E+11	4.576E+05	2.206E+06
Kr-85 INITIAL	0.000E+00	1.200E+09		0.000E+00
Kr-85 TOTALS	0.000E+00	2.890E+15	8.265E+07	5.233E+08
Kr-87 INITIAL	0.000E+00	7.690E+06		0.000E+00
Kr-87 TOTALS	0.000E+00	4.998E+10	1.224E+05	2.951E+05
Kr-88 INITIAL	0.000E+00	2.150E+07	6 6000+06	0.000E+00
KI-00 TOTALS	0.0000+00	3.0/46411	0.3805403	2.0972400
Kr-89 INITIAL	0.000E+00	6.240E+05	4 0078+00	0.000E+00
KI-09 101AD3	0.0002700	1./002400	9.22/6402	0.3472401
Xe-131m INITIAL	0.000E+00	3.900E+07	2.7015+06	0.0002+00
	0.0000.00	110001124	2	201048-01
Xe-133m INITIAL Xe-133m TOTALS	0.000E+00 0.000E+00	3.260E+07 5.650E+13	3.034E+06	0.000E+00 1.914E+07
Xe-133 INITIAL Xe-133 TOTALS	0,000E+00 0,000E+00	2.420E+09 3.090E+15	1.761E+08	0.000E+00 1.109E+09
Xe-135m INITIAL Xe-135m TOTALS	0.000E+00 0.000E+00	7.470E+06 6.698E+13	7.427E+07	0.000E+00 1.248E+08
Xe-135 INITIAL Xe-135 TOTALS	0.000E+00 0.000E+00	8.030E+07 4.052E+14	1.0592+08	0.000E+00 6.586E+08
•				
Xe-137 INITIAL Xe-137 TOTALS	0.000E+00 0.000E+00	1.540E+06 5.101E+08	1.264E+03	0.000E+00 2.362E+02
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Xe-138 INITIAL Xe-138 TOTALS	0.000E+00 0.000E+00	5.270E+06 6.426E+09	1.5922+04	0.000E+00 8.548E+03
	0.0005100		a. J/am. V1	
I-131 INITIAL	0.0002+00	2.230E+07 8 373E+16	4 9052408	0.000E+00 2.531E+08
T-121 101409	0.0005400	0.3/35413	1.3036 TU0	L.JIL+VO

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TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a FRC - for CR, EAB 4 LPZ dose (SA Case 2) [sa2FRC55.in] (4/00)

*** PROGENY INGROWTH ON ***

STEP	TIME	not used CURRENT INTEGRD uCi uCi-sec	Affected S/G CURRENT INTEGRD uCi uCi-sec	AVERAGE Released Release ùCi uCi/sec	CURRENT CURRENT INTEGRD UC1 UC1/CC UC1-sec
I-132	INITIAL	0.000E+00	8.810E+06		0.000E+00
I-132	TOTALS	0.000E+00	1.079E+14	2.2195+08	8.881E+07
I-133	INITIAL	0.000E+00	3.350E+07		0.000E+00
I-133	TOTALS	0.000E+00	1.682E+15	7.687E+08	3.856E+08
I-134	INITIAL	0.000E+00	4.930E+06		0.000E+00
I-134	TOTALS	0.000E+00	4.622E+13	1.130E+08	3.242E+07
I-135	INITIAL	0.000E+00	1.930E+07		0.0000+00
I-135	TOTALS	0.000E+00	4.065E+14	4.730E+08	2.224E+08

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$e_{RC} = 101$	CR, LAB & LPZ dose (SA Case 2) [SazirC55.1n] (4/00)							***PROGENI INGROWTH ON		
	- E	XCLUSI	ON AREA BO	UNDARY -	LOW P	OPULATION	ZONE		CONTROL	ROOM
	E	DE	SKIN-DE	THY-CDE	ËDE	SKIN-DE	THY-CDE	ÊDE	EDE RATE	SKIN-DE
	D	OSE	DOSE	DOSE	DOSE	DOSE	DOSE	DOSE	DOSE RATE	DOSE
	m	rem	mrøm	mrøm	mrem	mrem	mrem	nren	mrem/h	miem
Kr-83m										
FOTALS	6.2	9E-07	0.00E+00	0.00E+00	6.47E-08	0.00E+00	·0.00E+00	3,53E-08		0.00E+00
Kr-85m										
TOTALS	4.7	1E-03	9.30E-03	0.00E+00	7.16E-04	1.41E-03	0.00E+00	5.86E-04		2.30E-02
Kr-85										
TOTALS	7.8	5E-03	1.10E+00	0.00E+00	1.78E-03	2.48E-01	0.00E+00	1.91E-03		5.31E+00
Kr-87								•		
FOTALS	1.2	2E-02	2.90E-02	0.00E+00	1.05E-03	2.48E-03	0.00E+00	4.29E-04		2.02E-02
Kr-88										
TOTALS	1.1	2E-01	2.47E-02	0.00E+00	1.42E-02	3.14E-03	0.00E+00	9.91E-03		4.34E-02
Kr-89				•						
Totals	1.4	2E-04	1.54E-04	0.00E+00	8.23E-06	8.94E-06	0.00E+00	2.16E-07		4.68E-06
Ke-131m										
TOTALS	9.7	3E-04	1.08E-02	0.00E+00	2.22E-04	2.46E-03	0.00E+00	2.37E-04		5.24E-02
Ke-133m										
TOTALS	2.8	8E-03	1.92E-02	0.00E+00	8.65E-04	5.75E-03	0.00E+00	9.27E-04		1.23E-01

5.94E-02 1.12E-01 0.00E+00

3.05E-01 9.71E-02 0.00E+00

2.54E-01 4.14E-01 0.00E+00

2.31E-06 3.50E-05 0.00E+00

1.91E-04 1.42E-04 0.00E+00

1.79E+00 9.47E-01 1.11E+04

TRAILS PC -- Transport of Radioactive Material in Linear Systems, vl.Oa

2.49E-01 4.70E-01 0.00E+00

4.22E-01 1.34E-01 0.00E+00

1.53E-01 2.49E-01 0.00E+00

3.98E-05 6.03E-04 0.00E+00

3.28E-03 2.44E-03 0.00E+00

2.67E+00 1.41E+00 1.65E+04

Xe-133 TOTALS

Xe-135m

TOTALS

Xe-135

TOTALS

Xe-137 TOTALS

Xe-138 TOTALS

I-131 TOTALS

6.35E-02

8.71E-02

2.68E-01

7.34E-08

1.74E-05

1.57E-01

.

THY-CDE DOSE mrem 0.00E+00

0.00E+00

0.00E+00

0.00E+00

0.00E+00

0.00E+00

0.00E+00

0.00E+00

2.39E+00 0.00E+00

5.51E-01 0.00E+00

8.70E+00 0.00E+00

2.21E-05 0.00E+00

2.58E-04 0.00E+00

1.65E+00 1.94E+04

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POWER STATION BEAVER VALLEY Health Physics Department

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TRAILS_PC - FRC - for	- Transport CR, EAB & I	: of Radioa LPZ dose (S	ctive Mater A Case 2) (rial in Linear [sa2FRC55.in]	Systems, (4/00)	vl. 0a	***PROG	ENY INGROW	TH ON ***	
	- EXCLUSI	ON AREA BO	UNDARY -	LON P	OPULATION	ZONE	یک شده طب علیه مید بود بود خت متد	CONTRO	L ROOM	
	EDE DOSE	SKIN-DE DOSE	THY-CDE DOSE	EDE DOSE	SKIN-DE DOSE	THY-CDE DOSE	EDE DOSÉ	EDE RATE DOSE RATE	SKIN-DE DOSE	THY-CDE DOSE
	mrem	mrøm	mrem	mrem	nrem	mrem	nren	mrem/h	mrem	mrem
I-132										
TOTALS	1.33E+01	3.94E+00	7.896+01	5.06E+00	1.50E+00	3,00E+01	3.44E-01		2.02E+00	4.05E+01
I-133		•								
TOTALS	7.19E+00	6.68E+00	4.62E+03	4.51E+00	4.19E+00	2.90E+03	3.85E-01		7.10E+00	4.92E+03
I-134									1	
TOTALS	1.30E+01	4.27E+00	1.11E+01	2.98E+00	9.79E-01	2.54E+00	1.45E-01		9.49E-01	2.46E+00
1-135										
TOTALS	1.41E+01	4.25E+00	5.77E+02	7.562+00	2.29E+00	3.10E+02	6.03E-01		3.63E+00	4.93E+02
	~		· -							
ALL NUCLIDE	3 958+00	1 036+00	1 425403	2 245-01	1 125-01	9 225401	1 815-02	6 95F-02	1 845-01	1 395402
1 5000 h	2 648+01	1.952400	1.42E+03	1 635+00	6 718-01	6.22E+01 6.35E+02	£ 52E-02	6 20F-02	7 005-01	5.875+02
1 0333 h	1 355401	5 955100	6 01E+03	7 825-01	3 405-01	3 495+02	4 665-02	2 158-01	4.585-01	4.535+02
2 0000 h	7 495400	3 265+00	3 445403	4 358-01	1 905-01	2.005+02	3.595-02	2.168-01	3.505-01	3.50E+02
4.0000 h	0.005+00	0.002+00	0.005+00	7.185+00	3.198+00	3.706+03	5.17E-01	2.905-01	6.55E+00	5.50E+03
8 0000 h	0.005+00	0.005+00	0.002+00	1.24E+01	6.28E+00	9.385+03	1.346+00	3.65E-01	2.346+01	1.71E+04
8.5000 h	0.005+00	0.005+00	0.005+00	0.005+00	0.005+00	0.000+00	3.675-02	2.64E-03	6.99E-01	5.01E+02
24.0000 h	0.000+00	0.000+00	0.005+00	0.00E+00	0.00E+00	0.002+00	1.04E-02	7.10E-05	2.30E-01	1.95E+02
96.0000 h	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	2.036-04	7.31E-11	6.06E-03	7.44E+00
720.0000 h	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	1.62E-10	0.00E+00	8.13E-09	1.30E-05
TOTALS	5.12E+01	2.26E+01	2.18E+04	2.25E+01	1.08E+01	1.43E+04	2.07E+00		3.26E+01	2.48E+04

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BEAVER VALLEY POWER STATION Health Physics Department

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BEAVER VALLEY		
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TRAILSPC Input File For FRP	Case	
'L1 ',10,1.0E-3,3.47E-4,1.0E-5,3	.47E-4,1.0,1.0E-3,3.47E-4,1,2	4,0,2
'FRP - for CR, EAB & LPZ Dose	(SA Case 2) [SA2FRP55.in] (4	i/00) '
'C1 ','not used ',0.0,0.0,0.0,0.0		
'C2 ','Affected S/G ',2.365E-6,0.	0,0.0,0.0	
	.0	
'INI' 1 0 'UCI' 3 44E6 1 20E7 1 3	06F9 8 06F6 2 25F7 6 54F5 0	0 4 09F7
3 42F7 2 53F9 7 82F6 8 42F7 1	61F6 5 53F6 1 40F9 5 54F8	2 10 59 3 10 58
1 21F9 5*0 0	1.0120,0.0020,1.4020,0.0120,	
'INI'.1.0.' '.24*0.0		
'TIM'.18005400660072001	44002880030600864003	.456E5,2.592E6
'XPR',10*0.0		
'XPR',10*0.0		: :
'XPR',50.0,1.0,31.0,3*104.,2800	.,3*50.	
'XRM',10*0.0		
'XRM',6*1.0,4*0.0		
'XRM',50.0,1.0,31.0,3*104.,280	0.,3*50.	
'XRF',10*0.0		
'XRF',10*0.0		
XRF',3"0.0,3"1.0,4"0.0		
XUUEB,4*1.04,6*0.0		
XON 7' 6*6 04 2*4 22 2 40 0 7	AA	
'XRRI 7' 10*1 0	••••	
'XOO' 6*2 43 2*1 22 0 890 0 62	6	
'XBR'.10*1.0	-	
'OCC'.8*1.0.0.6.0.4		
· · · · · · · · · · · · · · · · · · ·	•	

AVER VALLEY WER STATION Health Physics Department		ERS-SFL-95-008 Revision 6	Page (i68 Attachment 4
INGROWTH ON *** [P: Control Room 730E+05 Cu.Ft. 000E+00 Kr-83m 000E+00 Kr-85 000E+00 Kr-85	000E+00 KF-89 000E+00 KF-89 000E+00 Xe-133m 000E+00 Xe-133m 000E+00 Xe-135m 000E+00 Xe-135m	0008+00 Xe-133 0008+00 Xe-133 0008+00 I-131 0008+00 I-133 0008+00 I-135 0008+00	
+++ PROGENY 			•
<pre>1 in Linear Systems, V1.0a 2FRP55.in] (4/00) COMP: Affected S/G 3.440E+06 Kr-83m u0 1.200E+07 Kr-85m 1.260E+09 Kr-85 8.060E+06 Kr-87</pre>	2.2005407 KF-88 6.540E405 KF-89 4.090E407 Xe-131m 3.420E407 Xe-133m 2.530E409 Xe-133 7.820E407 Xe-135m 8.420E407 Xe-135m	1.6100000 Xe-133 5.5300000 Xe-137 5.540000 I-131 5.540000 I-133 3.100000 I-133 1.2100000 I-135 1.0000000 I-135	
<pre>stt of Radioactive Materia LPZ Dose (SA Case 2) [SA COMP: not used</pre>	0.0005+00 Kr-88 0.0005+00 Kr-89 0.0005+00 Xe-131m 0.0005+00 Xe-133m 0.0005+00 Xe-135m 0.0005+00 Xe-135m	0.0002+00 Xe-135 0.0002+00 Xe-137 0.0002+00 I-131 0.0002+00 I-133 0.0002+00 I-133 1.0002+00 I-135 1.0002+00 I-135	
MILS_PC Transpy RP - for CR, EAB (INITIAL:		CT MULT (to uCl):	

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*** PROGENY INGROWTH ON ***

	REMOVAL:		0.000E+0	0 1/sec		2.365E-0	06 1/sec		1.000E+01	cfm
NUC	Grp 1 REL FR:			0.000E+00			0.000E+00	INTA	KE REDUCT:	0.000E+00
NUC	Grp 2 REL FR:			0.000E+00			0.000E+00	INTA	KE REDUCT:	9.410E-01
NUC	Grp 3 REL FR:			0.000E+00		·	0.000E+00	Inta	KE REDUCT:	0.000E+00
MULT	IPLIERS>									
STEP	TIME	XPR	XREM	XRF	XPR	XREM	XRF	XPR	XREM	XRF
1	1.800E+03	0.00	0.00	0.00	0.00	1.00	0.00	50.0	50.0	0.00
2	5.400E+03	0.00	0.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00
3	6.600E+03	0.00	0.00	0.00	0.00	1.00	0.00	31.0	31.0	0.00
4	7.200E+03	0.00	0.00	0.00	0.00	1.00	0.00	104.	104.	1.00
5	1.4402+04	0.00	0.00	0.00	0.00	1.00	0.00	104.	104.	1.00
6	2.880E+04	0.00	0.00	0.00	0.00	1.00	0.00	104.	104.	1.00
7	3.060E+04	0.00	0.00	0.00	0.00	0.00	0.00	2.8005+03	2.8005+03	0.00
8	8.6402+04	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
9	3.456E+05	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
10	2.592E+06	0.00	0.00	0.00	0.00	0.00	0.00	50.0	50.0	0.00
	CONTROL ROOM		M	EXCLUSI	ON AREA E	OUNDARY	LON PO	PULATION 2	ONE	
		X/0	Breathing	Occupancy	X/0	Breat	hing	X/0	Breath	Ing
		8/M3	M3/s		s/M3	M3/	······	e/M3	M3/s	
		1.000E-0	3 3.470E-04	1.0002+00	1.0005	-03 3.470	- E-04	1.0005	-05 3.470E	-04
MULT	IPLIERS			110001.00	210002	00 01110		2.0001	00 011/00	~
STEP	TIME.s									
1	1.800E+03	2.43	1.00	1.00	1.04	1.0	0	6.04	1.00	
2	5.400E+03	2.43	1.00	1.00	1.04	1.0	0	6.04	1.00	
3	6.600E+03	2.43	1.00	1.00	1.04	1.0		6.04	1.00	
Ă	7.200E+03	2.43	1.00	1.00	1.04	1.0		6.04	1.00	
5	1.440E+04	2.43	1.00	1.00	0.00	0.0	0	6.04	1.00	
6	2.8802+04	2.43	1.00	1.00	0.00	0.0	· ·	6.04	1.00	
7	3.060E+04	1.22	1.00	1.00	0.00	0.0	0	4.33	1.00	
8	8.640E+04	1.22	1.00	1.00	0.00	0.0	0	4.33	1.00	
9	3.456E+05	0.890	1.00	0.600	0.00	0.0	0	2.10	1.00	
10	2.592E+06	0.626	1.00	0.400	0.00	0.0	0	0.744	1.00	

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TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a FRP - for CR, EAB 4 LPZ Dose (SA Case 2) [SA2FRP55.in] (4/00)

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RTL: n/a Form: RE 1.103-3 9/92

BEAVER VALLEY POWER STATION Health Physics Department
		not used		Affected S/	G		AVERAGE	CON	trol room	
		CURRENT	INTEGRD	CURRENT	INTEGRD	RELEASE	D RELEASE	CURRENT	CURRENT	INTEGRD
STEP TI	ME	uC1	uCi-sec	uCi	uCi-sec	uC1	uCi/sec	uCi	uCi/cc	uCi-sec
Kr-83m Kr-83m	INITIAL	0.000E+00	0 0008+00	3.4402+06	3 2015410	7 22154		0.00000000		2.320E+0
VI-0 Dia	IUIALS		0.0002700		5.2012110					210202.0
Kr-85m	INITIAL	0.000E+00		1.200E+07				0.000E+00		
Kr-85m	TOTALS		0.000E+00		2.686E+11	4.563E+	05			2.200E+0
K95	TNTPTAL	0 0008+00		1.2608409				0.0005+00		
Kr-85	TOTALS	0.0002100	0.000E+00	1.2002.07	3.044E+15	8.296E+	07			5.253E+0
						•				
Kr-87	INITIAL	0.000E+00		8.060E+06	6 0400110	1 00554	0.E	0.000E+00		2 0545+0
Kr-87	TOTALS		0.0005+00		3.2426+1U	1.22364	05			2.334670
Kr-88	INITIAL	0.000E+00		2.250E+07				0.000E+00		
K r-88	TOTALS		0.000E+00		3.222E+11	6.579E+	05			2.698E+0
Cr_90	TNTPTAT	0 0008+00		6 5405+05				0.0005+00		
(r-89	TOTALS	0.0001.00	0.000E+00	010101/05	1.788E+08	4.228E+	02	•••••		6.549E+0
Xe-131m	INITIAL	0,000E+00		4.090E+07	6 6668413	0 677P.	06	0.000E+00)	1 6995+0
K6-131W	TUTALS		0.0002700		3.3305413	2.0//24	00	x		1.0002+0
Ke-133m	INITIAL	0.000E+00		3.420E+07				0.000E+00	l -	
Ke-133m	TOTALS		0.000E+00		1.486E+13	2.322E+	06			1.452E+0
Ye-133	TNTTTAT	0 0005+00		2 5305+00				0.0002+00	1	
Ke-133	TOTALS	V. VVEFUU	0.000E+00	2 · C C C L T C S	1.734E+15	1.657E+	08			1.041E+0
					-					
Xe-135m	INITIAL	0.000E+00		7.820E+06	6 6468.10	0 6745.	A.C	0.000E+00	h	1 7028+0
ke-135M	TOTALS		U.UUUE+00		0.3405+12	8.0/JE+	00			1./02240
Xe-135	INITIAL	0.000E+00		8.420E+07				0.000E+00		
Xe-135	TOTALS		0.000E+00		4.276E+13	1.908E+	07			1.211E+0
w. 100	******			1 6108.00	•			0 0000400		
Ke-137 Ke-137	INITIAL TOTALS	0.0005+00	0.0002+00	1.0105+00	5.3336+08	1.26164	03	0.0005400	,	2.357E+0
	101100	•	4.000E.00			~				
Xe-138	INITIAL	0.000E+00		5.530E+06				0.000E+00)	
Xe-138	TOTALS		0.000E+00		6.744E+09	1.595E+	04			8.562E+0
*-131	THEFT	0 0008+00		1 4000+00				0 0008400		
1-131 T-131	TULLIVE	0.0002400	0.0002+00	1.4005409	1.213E+15	9,08864	07	V. VUVETUU		9.086E+0
*-*3*	101003		0.000ET00		~ • ~ ~ ~ ~ ~ ~ ~ ~ ~	2.000ST	v 7			

BEAVER VALLEY POWER STATION Health Physics Department

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RTL: n/a Form: RE 1.103-3 9/92

FRP - for CR, EAB 4 LPZ Dose (SA Case 2) [SA2FRP55.in] (4/00) *** PROGENY INGROWTH ON *** Affected S/G AVERAGE -----CONTROL ROOM-----not used CURRENT INTEGRD CURRENT INTEGRD RELEASED RELEASE CURRENT CURRENT INTEGRD STEP TIME uCi uC1-sec uCi uCi-sec 'uCi uCi/sec uCi uCi/cc uCi-sec 0.000E+00 5.540E+08 0.000E+00 I-132 INITIAL I-132 TOTALS 0.000E+00 6.451E+12 1.395E+07 1.376E+07 I-133 INITIAL 0.000E+00 2.100E+09 0.000E+00 2.137E+14 1.214E+08 I-133 TOTALS 0.000E+00 1.216E+08

INITIAL 0.000E+00 3.100E+08 0.000E+00 I-134 0.000E+00 1.396E+12 3.297E+06 2.942E+06 I-134 TOTALS 0.000E+00 I-135 INITIAL 1.210E+09 0.000E+00 3.968E+13 5.404E+07 TOTALS 0.000E+00 5.418E+07 I-135

TRAILS PC -- Transport of Radioactive Material in Linear Systems, vl.Oa

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Health Physics Department STATION VALLEY

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FRP - for CR, EAB & LPZ Dose (SA Case 2) [SA2FRP55.in] (4/00)						*** PROGENY INGROWTH ON ***			
	- EXCLUS EDE DOSE mrem	ION AREA BO Skin-de Dose Meem	UNDARY - THY-CDE DOSE mrem	LOW E EDE DOSE mrem	OPULATION SKIN-DE DOSE mrem	ZONE · THY-CDE · DOSE mrem	EDE DOSE mrem	CONTROL ROOM EDE RATE SKIN- DOSE RATE DOSI mrem/h mrem	-DE THY-CDE E DOSE mrem
Kr-83m TOTALS	6.30E-07	0.00E+00	0.00E+00	6.48E-08	0.00E+00	0.00E+00	3.54E-08	0.00E	+00 0.00E+00
Kr-85m Totals	4.69E-03	9.27E-03	0.00E+00	7.14E-04	1.41E-03	0.00E+00	5.84E-04	2.30E-	-02 0.00E+00
Kr-85 Totals	7.87E-03	1.10E+00	0.00E+00	1.78E-03	2.49E-01	0.00E+00	1.92 E- 03	5.33E-	+00 0.00E+00
Kr-87 Totals	1.22E-02	2.90E-02	0.002+00	1.05E-03	2.49E-03	0.00E+00	4.295-04	2.03E	-02 0.00E+00
Kr-88 Totals	1.12E-01	2.47E-02	0.00E+00	1.42E-02	3.14E-03	0.00E+00	9.92E-03	4.34E	-02 0.00E+00
Kr-89 Totals	1.42E-04	1.54E-04	0.00E+00	8.23E-06	8.94E-06	0.00E+00	2.16E-07	4.688	-06 0.00E+00
Xe-131m TOTALS	9.74E-04	1.08E-02	0.00E+00	2.20E-04	2.43E-03	0.00E+00	2.35E-04	5.19E·	-02 0.00E+00
Xe-133m TOTALS	2.86E-03	1.90E-02	0.00E+00	6.62E-04	4.40E-03	0.00E+00	7.03E-04	9.30E·	-02 0.00E+00
Xe-133 Totals	2.48E-01	4.68E-01	0.00E+00	5.59E-02	1.06E-01	0.00E+00	5.96E-02	2.24E	+00 0.002+00
Xe-135m Totals	1.80E-01	5.72E-02	0.00E+00	3.57E-02	1.13E-02	0.00E+00	1.192-02	7.52E	-02 0.00E+00
Xe-135 Totals	1.09E-01	1.77E-01	0.00E+00	4.58E-02	7.46E-02	0.00E+00	4.932-02	1.60E-	+00 0.00E+00
Xe-137 TOTALS	3.97E-05	6.01E-04	0.00E+00	2.31E-06	3.49E-05	0.00E+00	7.32E-08	2.21E	-05 0.00E+00
Xe-138 TOTALS	3.29E-03	2.44E-03	0.002+00	1.91E-04	1.42E-04	0.00E+00	1.74E-05	2.58E	-04 0.00E+00
I-131 TOTALS	1.48E+00	7.83E-01	9.18E+03	3.32E-01	1.75E-01	2.06E+03	5.64E-02	5.92E	-01 6.95E+03

Material in Linear Systems v1.0a

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TRAILS_PC -- Transport of Radioactive Material in Linear Systems, v1.0a FRP - for CR, EAB & LPZ Dose (SA Case 2) [SA2FRP55.in] (4/00) *** PROGENY INGROWTH ON *** - EXCLUSION AREA BOUNDARY ---- LOW POPULATION ZONE ------ CONTROL ROOM ---EDE SKIN-DE THY-CDE EDE SKIN-DE THY-CDE EDE EDE RATE SKIN-DE THY-CDE DOSE DOSE DOSE DOSE DOSE DOSE DOSE DOSE RATE DOSE DOSE mrem mrem mrem mren mrem mrem mrem mrem/h mrem mrem I-132 TOTALS 3.18E-01 9.41E-02 1.88E+00 2.76E+00 8.17E-01 1.63E+01 5.33E-02 3.14E-01 6.28E+00 I-133 TOTALS 3.47E+00 3.22E+00 2.23E+03 7.14E-01 6.63E-01 4.59E+02 1.21E-01 2.24E+00 1.55E+03 T-134 TOTALS 1.20E+00 3.93E-01 1.02E+00 8.69E-02 2.85E-02 7.39E-02 1.32E-02 8.61E-02 2.23E-01 I-135 TOTALS 5.07E+00 1.53E+00 2.08E+02 8.652-01 2.622-01 3.552+01 1.47E-01 8.82E-01 1.20E+02 ALL NUCLIDES 0.5000 h 4.15E+00 2.32E+00 2.95E+03 2.41E-01 1.35E-01 1.71E+02 1.99E-02 7.75E-02 2.25E-01 2.90E+02 1.5000 h 7.27E+00 4.30E+00 5.82E+03 4.23E-01 2.50E-01 3.38E+02 7.28E-02 6.87E-02 8.57E-01 1.16E+03 1.8333 h 2.18E+00 1.35E+00 1.91E+03 1.27E-01 7.86E-02 1.11E+02 2.65E-02 8.98E-02 3.27E-01 4.62E+02 2.0000 h 1.05E+00 6.64E-01 9.52E+02 6.12E-02 3.86E-02 5.53E+01 1.48E-02 8.75E-02 1.93E-01 2.62E+02 4.0000 h 0.00E+00 0.00E+00 0.00E+00 6.45E-01 4.32E-01 6.50E+02 1.51E-01 6.75E-02 3.12E+00 2.62E+03 8.0000 h 0.00E+00 0.00E+00 0.002+00 9.77E-01 7.44E-01 1.23E+03 2.33E-01 5.37E-02 8.54E+00 3.71E+03 8.5000 h 0.00E+00 0.00E+00 0.002+00 0.002+00 0.002+00 0.002+00 5.432-03 4.022-04 2.362-01 8.212+01 24.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.77E-03 1.53E-05 8.93E-02 3.22E+01 96.0000 h 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 4.69E-05 2.56E-11 3.30E-03 1.25E+00 720.0000 h 0.00E+00 0.00E+00 0.00E+00 0.002+00 0.002+00 0.002+00 5.71E-11 0.00E+00 6.77E-09 2.22E-06 TOTALS 1.47E+01 8.65E+00 1.16E+04 2.47E+00 1.68E+00 2.55E+03 5.25E-01 1.36E+01 8.62E+03

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U	nit 1 Concurrent Iodine Spike Addend	um	

This addendum is valid for total T.S. operational leakage (identified and unidentified leakage). Iodine DCFs are taken from Federal Guidance Report No 11. and are consistent with ICRP 26/30 methodology.

This addendum provides references, inputs, assumptions and calculation for the concurrent iodine spike postulated to occur coincident with certain design basis accidents (DBA). The analyst should ensure that the inputs and assumptions used herein are valid and applied in the limiting direction when used in any particular DBA analysis. The calculation is included below as an embedded EXCEL 95 spreadsheet. Any modification or change requires hand checking of the math as this spreadsheet is not subject to the SQA program of REAP 1.104. The methodology is identical to that of ERS-SFL-96-011 and -012. Significant changes were made to the RCS mass, RCS Tech. Spec. leak rate and letdown (purification) flow, and the final appearance rates are, therefore, changed.

Input Parameters/Assumptions:

RCS Tech. Spec. leakage____1 gpm unidentified leakage + 10 gpm identified leakage = 11 gpm (used 1 gm/cc for density conversion consistent with leak rate determination methodology) (ref. Unit 1 T. S. 3.4.6.2) NOTE: Includes T/S primary to secondary leakage.

RCS Mass_____ The RCS mass is calculated from the following component volumes provided in EM No.: 116251 and RCS Density @ 576.6 °F provided in EM No.: 116252.

RCS excluding PZR, 0% S/G plgd -	8099 fi ³	PZR water @ 100% power -	708 ft ³
RCS excluding PZR, 30% S/G plgd -	7127 ft ³	PZR water @ 0% power -	340 ft ³
Main RCS Density @ 576.6 °F -	44.13 lb/ ft ³		

Purification efficiency (PE)_____1 is used in this calculation. 0.9 was used previously based on a DF = 10 for iodine. (ref. Westinghouse letter DMW 4704, 1982 as used in SWEC 12241-UR(B)-224, and Unit 1 UFSAR Table 14B-5) Note: purification efficiency (PF) = 1 - 1/DF. The actual DF is much higher, possibly 1000 to 10000, which results in a PE = 0.999 to 0.9999. Since the actual DF is unknown, assuming the PE = 1 bounds the calculation.

Purification flow rate_____120 gpm is used to bound calculation (the maximum given in EM No.: 117705).

Iodine decay constants	I-131	9.9783E-7 sec ⁻¹
	I-132	8.3713E-5 sec ⁻¹
	I-133	9.2568E-6 sec ⁻¹
	· I-134	2.1963E-4 sec ⁻¹
	I-135	2.9129E-5 sec ⁻¹
	(re	f. ERS-SFL-93-018)

Formula for iodine loss constant____ $\lambda = (F^*E/M) + (L/M) + \lambda_{decay}$ (ref. EPRI Report, Review of Iodine Spike Data from PWR Power Plants in Relation to SGTR with MSLB, TR-103680)

Formula for iodine spike____Appearance rate = Equilibrium Concentration * M * λ (ref. EPRI Report, Review of Iodine Spike Data from PWR Power Plants in Relation to SGTR with MSLB, TR-103680



Concurrent Iodine Spike Appearance Rate = TS DE-I-131 x RCS Mass x λ_A

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POWER	SIAT	ION	ERS-S	FL-95-00	8	Page 76
Health	Physics D	Department	Revis	ion 6	Appe	ndix 1
		Concurrer	nt Iodine Spike A	opearance	Rate Calcu	lation
		Sensitivity	Analysis Case	2. 0% Powe	ar 30% S/G	Plad
				2.0/01 000		1.180
F	RCS Iodi	ne Concentratio	n (uCi/gm) @ 0.20	uCl/am Dos	e Equivalent i	odine 131:
			X	2	X	E
		Thyroid DCF *	Conversion		1% FF	1% FF iodine
		(Sv/Bq)	(mrem/uCi)/(Sv/Bq)	(mrem/uCi)	(uCi/am)	dose (mrem/am)
	I-131	2.92E-07	3.70E+09	1.08E+03	2.69E+00	2.91E+03
	l-132	1.74E-09	3.70E+09	6.44E+00	1.06E+00	6.82E+00
	l-133	4.86E-08	3.70E+09	1.80E+02	4.03E+00	7.25E+02
	l-134	2.88E-10	3.70E+09	1.07E+00	5.94E-01	6.33E-01
_	1-135	8.46E-09	3.70E+09	3.13E+01	2.32E+00	7.26E+01
						3.71E+03
-	ref. Fede	eral Guidance Re	port No. 11		1	E
					Iodine 131 D	CF @ 1% FF
				.*	(mrem/uCi)	DE I-131 (uCl/gm)
		•		3.71E+03	1.08E+03	3.435
				E	X	E
		1% Fr (00/000)	1% FF	DE I-131		RCS I @ 0.20
	1-121		DE 1-131 (UCI/gm)			DE-I131 (uCi/gm)
	1-131	2.092700	3.435	7.83E-01	0.20	1.57E-01
	1-132	1.002+00	3.433	3.092-01	0.20	6.17E-02
	1-134	4.03E+00 5 9/E-01	3.433	1.1/6+00	0.20	2.35E-01
	1-135	2 325+00	3.435	6 755 01	0.20	3.402-02
	1-100		3,433	0.752-01	0.20	1.352-01
L L	Joncurre	nt loaine Spike /	Appearance Rate:			•••••
l l		b leakage) =	_	F (purit flow r	rate) =	
	(anm)	X	E (and (and a)	(X	E
	(gpun) 11	(ynwyai) 3785 3	(907000) 4 16395±04	(gai/min)	(gm/gai)	. (gm/min)
	000	0100.0	4.10302+04	120	3705.3	4.54245+05
I^_	co mass	5, U% Power, 30%	s S/G piga =			E (purification
	/a3	Х //ь. /с.3.+		X	E	efficiency)
	(11)	(10/11)-		(gm/lbm)	(gm)	(-)
	Inter Dec	44.13 2 December of 570 9	3.30E+03	453.592	1.4947E+08	1
느		5 Density at 576	F (EM NO.:116252)		
N N	let lambd	a (all lambda's in	sec ⁻¹ , 60 sec/min)			
			+	+	E	
	• • • • •	=(F*E)/M	=L/M	Decay	Net Lambda	
	1-131	5.0651E-05	4.6430E-06	9.9783E-07	5.6291E-05	
	1-132	5.0651E-05	4.6430E-06	8.3713E-05	1.3901E-04	
	1-133	5.0651E-05	4.6430E-06	9.2568E-06	6.4550E-05	
	1-134	5.0651E-05	4.6430E-06	2.1963E-04	2.7492E-04	
	1-135	5.0651E-05	4.6430E-06	2.9129E-05	8.4423E-05	
A	ppearan	ce rate	X	X	E	E
		conc @ 0.20	М	net lambda	@ 0.20 uCl/gn	n RATE x 500
		(uCi/gm)	(gm)	(sec ⁻¹)	(uCi/sec)	(Ci/sec)
	1-131	1.57E-01	1.49E+08	5.6291E-05	1.3178E+03	6.59E-01
	I-132	6.17E-02	1.49E+08	1.3901E-04	1.2824E+03	6.41E-01
	1-133	2.35E-01	1.49E+08	6.4550E-05	2.2640E+03	1.13E+00
	I-134	3.46E-02	1.49E+08	2.7492E-04	1.4212E+03	7.11E-01
I	1-135	1.35E-01	1.49E+08	8.4423E-05	1.7046E+03	8 52E-01