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ComEd

April 7, 2000

United States Nuclear Regulatory Commission
Attention: Document Control Desk
Washington, D.C. 20555

LaSalle County Station, Units 1 and 2
Facility Operating License Nos. NPF-11 and NPF-18
NRC Docket Nos. 50-373 and 50-374

Subject: Updated Final Safety Analysis Report (UFSAR)

Reference: D. M. Skay (U.S. NRC) letter to O. D. Kingsley (Commonwealth Edison (ComEd) Company), Issuance of Exemption to 10 CFR 50.71(e)(4) for Braidwood, Units 1 and 2; Byron, Units 1 and 2; Dresden, Units 2 and 3; LaSalle, Units 1 and 2; and Quad Cities, Units 1 and 2 (TAC NOS. MA5716, MA5717, MA5720, MA5721, MA5722, MA5723, MA5729, MA5730, MA5732, MA5733), dated July 27, 1999.

In accordance with the requirements of 10 CFR 50.71(e)(4), 50.59(b)(2), and the above reference, ComEd submits Revision 13 to the Updated Final Safety Analysis Report for the LaSalle County Station, and summaries of safety evaluations for activities evaluated in accordance with the requirements of 10 CFR 50.59.

Revision 13 reflects changes to the facility and procedures which were in effect as of October 8, 1999. Attachment A provides a brief summary of the changes incorporated into UFSAR Revision 13. Also, attached is an "Index of Changes" which explains UFSAR page removal and replacement instructions.

Attachment B provides summaries for tests and experiments not described in the safety analysis report, changes to the facility described in the safety analysis report, and changes to procedures described in the safety analysis report. These activities were evaluated in accordance with the requirements of 10 CFR 50.59, and were implemented in calendar years 1998 and 1999.

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Should you have any questions concerning this letter, please contact Mr. Frank A. Spangenberg, III, Regulatory Assurance Manager, at (815) 357-6761, extension 2383.

Respectfully,

Charles G. Pardee
Site Vice President
LaSalle County Station

Attachments

cc: Regional Administrator - NRC Region III
NRC Senior Resident Inspector - LaSalle County Station

Attachment A

Summary of Changes for UFSAR Revision 13 Update

UFSAR Update for Installation of Hot Tap Upstream of 2E12-F068A for Dewatering, Design Change Package (DCP) 9700149
The DCP installed a 4-inch drain connection to pipeline 2RH083AA-20" used for dewatering the piping to support repairs to the internals of residual heat removal (RHR) valve 2E12-F068A. UFSAR Drawing M-134 Sheet 2 (Core Standby Cooling System Equipment Cooling Water System) is revised to reflect the installation of the drain connection.

Revision to UFSAR Drawing M-100 Sheet 3, Control Rod Drive Hydraulic Piping
Drawing M-100 Sheet 3 is revised to incorporate editorial changes for clarification of equipment part numbers (EPNs) as a result of the plant labeling effort.

Revision to UFSAR Drawing M-146 Sheet 3, Control Rod Drive Hydraulic Piping
Drawing M-146 Sheet 3 is revised to incorporate editorial changes for clarification of equipment part numbers (EPNs).

Anderson/Greenwood 2" Double Block Valves 1E21-F331 and 1E21-F332, Desing Change Package (DCP) 9700374
The block valves located on the Low Pressure Core Spray (LPCS) pump suction line were replaced with a single valve assembly. This was done due to through-seat leakage and the Anderson/Greenwood double block valve being obsolete. A gate valve replaced the double block valve since it is less susceptible to becoming a crud trap. UFSAR drawing M-94, "LPCS" was revised to reflect this change.

Addition of Hole to Reactor Building Equipment Drain Line 1RF61AB-4" per Design Change Package 9700449
The DCP installed a 0.5" drain hole in the discharge piping associated with and immediately downstream of residual heat removal (RHR) system relief valve 1E12-F313B. Its purpose is to prevent water from accumulating in the discharge piping as such an accumulation may affect the setpoint of the relief valve.
UFSAR drawing M-91 Sheet 3 for the Unit 1 Reactor Building Equipment Drain system is revised to reflect the installation of the drain hole.

Replacement of Liquid Process Radiation Monitor Probe 1E12-N511 per Design Change Package 9700522
The DCP replaced the probe for monitoring the Division 2 residual heat removal (RHR) heat exchanger 1B service water discharge, the previous probe failed due to flow induced vibration. The replacement probe is designed similar to one utilized successfully in the reactor recirculation system. UFSAR drawing M-87 Sheet 1 is revised to reflect the probe replacement.

UFSAR Change to reflect Addition of Drain Connection to Pipeline 1RH83AA-20" per Design Change Package (DCP) 9700147
The DCP installed a 4" drain connection to pipeline 1RH83AA-20", which was used to dewater the piping to permit repairs to Residual Heat Removal (RHR) valve 1E12-F068A. UFSAR drawing M-87 Sheet 2 is revised to reflect the design change.

ECCS Suction Strainer Replacement per Design Change Package (DCP) 9600290
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 1 "A" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA).
The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Section 15.9.3.7 is not being revised as proposed in the DCP (see PIF L1997-07829). UFSAR drawing M-96 Sheet 2 for the Unit 1 RHR system is revised to reflect the strainer replacement.

Change to UFSAR Subsections 1.2.3.1.3 and 10.4.2.2 to Reflect Engineering Request (ER) 9704131
UFSAR Subsections 1.2.3.1.3 and 10.4.2.2 are revised to allow operation of the mechanical vacuum pump 1(2)OG02P following reactor shutdown in accordance with LaSalle General Procedure LGP-2-1, *Normal Unit Shutdown*. This is to allow main condenser vacuum to be maintained as long as possible following reactor shutdown to minimize condensate polisher resin breakdown caused by the combination of high dissolved oxygen (when vacuum is lost) and high condensate water temperature (right after shutdown).

Revision to UFSAR subsections 3.8.4.1.2 and 10.3.6.2
UFSAR subsections 3.8.4.1.2 and 10.3.6.2 are revised to achieve consistency with original design drawings M-9 (General Arrangement Ground Floor Plan) and M-806, Sheet 2 (Turbine Cycle Feedwater Heater Drain Piping).

3731609800016 UFSAR Update due to Addition of Hole to Reactor Building Equipment Drain Line 1RF61AA-4" per Design Change Package (DCP) 9700448
The DCP installed a 0.5" drain hole in the discharge piping associated with and immediately downstream of residual heat removal (RHR) relief valve 1E12-F313A. Its purpose is to prevent water from accumulating in the discharge piping as such an accumulation may affect the setpoint of the relief valve. UFSAR drawing M-91 Sheet 3 for the Unit 1 Reactor Building Equipment Drain system is revised to reflect the installation of the drain hole.

UFSAR Update due to Unit 2 Station Heat Supply Air Coils Replacement per Design Change Package (DCP) 9600548
The DCP replaced Unit 2 station heat supply air coils 2VT02AA and 2VT02AB in the ventilation supply of the turbine building and rerouting of some associated piping. The previous coils were freeze-damaged. The DCP installation allows for complete draining and venting of the coils and headers. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Update due to Addition of Drain Connection to Pipeline 1RH83BB for Dewatering 1E12-F068B, Design Change Package (DCP) 9700148
The DCP installed a 4-inch drain connection to pipeline 1RH83BB used for dewatering the piping to support repairs to the internals of residual heat removal (RHR) valve 1E12-F068B.
UFSAR Drawing M-87 Sheet 1 (Core Standby Cooling System Equipment Cooling Water System) is revised to reflect the installation of the drain connection.

UFSAR Update due to Unit 1 Station Heat Supply Air Coil Replacement per Design Change Package (DCP) 9600549
The DCP replaced Unit 1 station heat supply air coil 1VR02A in the ventilation supply of the reactor building and rerouting of some associated piping. The previous coil was freeze-damaged. The DCP installation allows for complete draining and venting of the coil and header. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Change due to Unit 0 Station Heat Supply Air Coil Replacement per Design Change Package (DCP) 9600551
The DCP replaced supply air coil 0VR03A in the ventilation supply of the Radwaste building and rerouting of some associated piping. The previous coil was freeze-damaged. The DCP installation allows for complete draining and venting of the coil and header. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Revision for End of Cycle Recirculation Pump Trip (EOC-RPT) Response Times

The EOC-RPT response times in UFSAR Subsections G.3.2.2.2.D.1 and G.5.1.3.1 are revised from 140 milliseconds (msec) to 190 msec. This is to achieve consistency with other UFSAR subsections, the Technical Specifications, and transient analyses reports submitted by General Electric and Siemens Power Corporation. UFSAR pages G.3.2-2 and G.5.1-2 are revised.

Revision to UFSAR Subsection 2.4.8.4
The description of the blowdown waterline in subsection 2.4.8.4 of the UFSAR is revised to achieve consistency with the generalized waterline description of UFSAR subsection 10.4.5.2.

Revision to UFSAR Subsection 7.3.9.2.1
UFSAR Section 7.3.9.2.1 is revised to indicate that containment spray is not required to be initiated on recombiner operation. Containment spray initiation is based on containment pressure and/or combustible levels of hydrogen /oxygen concentrations, as opposed to recombiner operation.
The containment spray mode does not have to be initiated if the recombiners are required for service. Suppression chamber spray initiation is required to prior to suppression chamber pressure reaching 8 psig. If suppression chamber pressure exceeds 8 psig, drywell spray is also initiated.

Revision to UFSAR Tables 9.4-1 (Sheet 1) and 9.4-3 due to revised Filter Pressure Drop
In conjunction with a change to an alternate supply air filter for use in the control room and the auxiliary electrical equipment room (AEER) HVAC systems, the filter pressure drop, clean (inches water) parameter as listed in UFSAR Tables 9.4-1 (Sheet 1) and 9.4-3 is increased from "0.35" to " < 0.8" inches water column for the control room and AEER HVAC systems (VC and VE, respectively). The increase in the rated pressure drop clean value was made in association with an upgrade to safety related rating for the supply air filter for use in the control room and AEER HVAC systems.

Revision to UFSAR Subsection 6.4.2.2
UFSAR Subsection 6.4.2.2 is revised to direct the reader to UFSAR Volume XI diagrams, as opposed to Figures 9.4-1 and 9.4-2. These two Figures don't exist in the UFSAR.

Revision to UFSAR Subsection 6.1.2 and Table 6.1-2 to incorporate FSAR Question 312.21 for clarity
Information from FSAR Question 312.21 is transferred to UFSAR subsection 6.1.2, Organic Materials, and UFSAR Table 6.1-2, Organic Materials Within the Primary Containment, to bring forward applicable information from the FSAR into the UFSAR. All exposed metal surfaces inside containment are not prime coated with an inorganic

zinc compound that has been fully qualified in accordance with ANSI standards. Some exposed metal surfaces inside containment are coated with coatings not qualified in accordance with ANSI standards N101.2, N101.4 and N512. These unqualified coatings have been previously identified and addressed in FSAR Question 312.21 and the NRC has issued an SER, NUREG-0519, Section 6.1.2, Organic Materials, approving the use of this unqualified coating.

UFSAR Revision due to Design Change Package (DCP) 9500324
The internals to High Pressure Core Spray (HPCS) check valve 1E22-F016 were removed. The valve was previously required to prevent draining of the cycled condensate storage tank (CST) in to the suppression pool. The valve is no longer required since the suction path from CST has been removed. UFSAR Drawing M-95 Sheet 1 is revised per ECN 001234M (Unit 1 HPCS) and Figure 6.3-1 (HPCS system process diagram) is revised.

UFSAR Update due to Emergency Core Cooling System (ECCS) Testable Check Valve 1E22-F005 Upgrade per Design Change Package (DCP) 8700286
The DCP accomplished the following on the high pressure core spray (HPCS) 1E22-F005 valve: replaced the valve stem packing to reduce valve shaft friction, removed the leakoff line, and replaced the associated limit switch. These activities were performed to minimize the likelihood of the valve failing to fully close following low flow testing. The changes to UFSAR subsection 5.2.5.2 and Figure 7.3-7 were previously incorporated by associated partial modifications. UFSAR Drawing M-95 Sheet 1 (Unit 1 HPCS) is accordingly revised.

Revision to UFSAR per Design Change Package (DCP) 9700390
The DCP replaced a portion of the Unit 1 Reactor Building Closed Cooling Water (RBCCW) heat exchange outlet Service Water (WS) system outlet header 1WS26B-20" from carbon steel to stainless steel. The replaced portion of piping was eroded due to severe cavitation and impingement. The replacement stainless steel piping is more resistant to cavitation and impingement.
UFSAR Drawing M-69 Sheet 1 (Unit 1 Service Water system) is accordingly revised.

Revision to UFSAR Subsection 6.4.1
The first sentence of the third paragraph of UFSAR Subsection 6.4.1.g is revised to reflect the availability of self-contained breathing air systems (air packs) dedicated for use by the fire brigade.

Revision to UFSAR Subsection 4.3.2.5.1.2
The current description in UFSAR 4.3.2.5.1.2 for control rod withdrawal sequences in the rod worth minimizer (RWM) power range, first paragraph, is incorrect per GE design

document NEDO – 21231, Banked Position Withdrawal Sequence, (BPWS), and contradicts the second paragraph of the section. UFSAR Subsection 4.3.2.5.1.2 is revised to reflect actual BPWS rules.

Revision to UFSAR Subsection 7.7.6.1.1
UFSAR Subsection 7.7.6.1.1 is revised to incorporate an exception to source range monitor (SRM) operability requirements during refueling operations, implemented per licensing amendments 32 and 18, for Unit 1 and 2, respectively.

UFSAR Revision reflect Cable Qualification to IEEE 383-1974
UFSAR subsections 8.3.1.4.2.2, 9.5.1.1.2, and H.1.1.1 presently imply that all cables at LaSalle, without exception, are qualified to IEEE 383-1974. These UFSAR subsections are revised to clarify the requirements for using cables that are qualified to IEEE 383-1974. Cables which do not interact with division or division associated cables, that are not routed in cable trays, that are routed in dedicated enclosed raceways and that present acceptable combustible loading (e.g., lighting and communications) do not require IEEE 383-1974 qualification.

Revision to UFSAR Subsection 9.4.4.3 and Table 9.4-14
The text "installation of redundant principal system components." of Subsection 9.4.4.3 at the top of page 9.4-31 is deleted since it is redundant to text at the bottom of page 9.4-30.
The second sentence in the COMMENTS section applicable to MALFUNCTION Fail closed for the flow control damper on main supply discussion of UFSAR Table 9.4-14 is deleted. The Turbine Building Ventilation System main supply dampers are normally open / fail open components, therefore, the "fail closed" malfunction would be an extremely rare failure mode. Shutting down supply fans with the exhaust fans in operation could result in ductwork damage.

Update to UFSAR Table 6.2-21 Sheet 14, Item 18
Note 18 of UFSAR Table 6.2-21 describes the TIP drive guide tube ball valve and shear valve isolation capabilities, and that the time period that the valves are opened is very limited. The note has a final statement that states "However, at the insistence of the NRC, these valves will be tested in accordance with the requirements of 10CFR50, Appendix J." This final statement is changed to indicate that the TIP ball valves are tested in accordance with 10CFR50, Appendix J and that the TIP shear valves are tested as specified in Technical Specification 4.6.3.5, which verifies continuity of the explosive charge and batch sampling testing of the explosive squib charges, with replacement of the explosive squib before expiration of the shelf-life and operating-life.

UFSAR Update to Appendix G, Reactor Recirculation System

UFSAR Appendix G was revised to resolve inconsistencies between the power to flow map in the UFSAR and station procedure LOA-RR-101/201, and, the power to flow map in the procedure LOA-RR-101/201 is not properly labeled for the low flow lines, nor is the source of the power to flow map referenced.
The change involved updating the power to flow map to be consistent with procedure LOA-RR-101/201. The maps in the UFSAR are considered reference only with the operational boundary of the power to flow map being defined by technical specifications and the Core Operating Limits Report (COLR).

Update to UFSAR Table 9.4-15
UFSAR Table 9.4-15, Diesel-Generator Facilities Ventilation System Equipment Parameters, is revised to specify the filter pressure drop for a dirty filter is 0.40 inches water in lieu of 0.35 inches water for ventilation supply filters 0VD01F, 1VD01F, 1VD02F, 2VD01F, and 2VD02F.
This proposed change reflects Sargent & Lundy (S&L) Design Criteria DC-VD-01-LS, dated 12/21/78, and Design Calculation VD-1C, dated 6/6/78, which specify the dirty filter pressure drop as being 0.40 inches of water.

Change to UFSAR Subsection 9.2.1.1.1.a.4
Engineering Request (ER) 9604121 identified that UFSAR Subsection 9.2.1.1.1.a.4 incorrectly states that system sizing is based upon a minimum 20 gpm flow of cooling water to the RHR pump seal coolers. Vendor Drawing (Spec J-2500) VPF- 2993-174-1 sheet 2 identifies that the shell side of the seal coolers (the CSCS-ECWS side of the exchanger) is designed for a flow of 9 gpm with a cooler water temperature of 80^0F. The maximum design temperature of the Ultimate Heat Sink (UHS) is 100^0F. Subsequent correspondence received from the seal cooler manufacturer provided a data sheet detailing that 12.5 gpm are required for a cooling water temperature of 100^0F (based upon 85% cleanliness). The change required for UFSAR Subsection 9.2.1.1.1.a.4 was identified and evaluated during the preparation of Design Change Packages (DCPs) 9800053 and 9800054. This change is not dependent upon installation of these DCPs.

UFSAR Revision to Incorporate Previously Approved Technical Specification revisions associated with the Main Steam Isolation Valve (MSIV) Limit Switch Setpoint Values
The original evaluation associated with the licensing amendment did not identify all of the required UFSAR changes. The proposed UFSAR changes will resolve discrepancies between the current Technical Specifications and the UFSAR, as well as discrepancies within the UFSAR (e.g., sections that incorporated the change and those sections that were missed).
The applicable sections of the UFSAR are revised to reflect the previously approved MSIV limit switch setpoint values (nominal, allowable and analytical) currently identified in the Technical Specifications. At the time the Technical Specifications were revised

not all applicable portions of the UFSAR affected by the change were identified and revised to incorporate the revised Technical Specification values.
The current Technical Specification scram setpoints are less than or equal to 8% closure trip and less than or equal to 12% closure allowable. The basis for these values is the 85% analytical value based on the General Electric (G. E.) reanalysis of the MSIV closure transient position scram. The affected UFSAR Sections and subsections are 5.4.5.2, 5.4.5.4, 7.2.2.4.6, 7.A.2.1.2, 15.0.8; 15.0.9 (new), 15.1.3.2, 15.1.3.3, 15.1.5, 15.2.4.1, 15.2.4.2, 15.2.4.3 and 15.2.10; Tables 7.2-1 and 7.3-4; Figure 7.2-7; and Table of Contents page 15.0-I.

Revision to UFSAR Drawings M-Index Sheet 4 and M-19
M-Index Sheet 4 (General Arrangement Index) and M-19 (General Arrangement Lake Screen House) are revised to reflect the as-built condition of the plant. Pumps and equipment being removed from drawing M-19 and M-Index Sheet 4 do not exist, and pumps that do exist in the plant are being added to these drawings.

Revision to UFSAR Subsection 2.4.13.2.2.3.2
UFSAR Subsection 2.4.13.2.2.3.2 is revised to specify that after completion of the ground water monitoring program specified in Section 6.3.3 of NUREG-0486 "Final Environmental Statement" (November 1978), the number of observation wells monitored and the frequency of monitoring will be performed as described in the plant surveillance program.

Revision to UFSAR Drawing M-80 Sheet 2
Drawing M-80 Sheet 2, Turbine Building Equipment Drains incorrectly showed the following: Drain lines 1ES47BA - 2" and 1ES47BB - 2" connected to drain header 1TEC4A - 8", they are actually connected to drain header 1TEC5A - 8";
Drain line 1TD01B - 2" connected to drain header 1TEC5A - 8", whereas it is connected to drain header 1TEC6A - 8"; and, the drawing did not properly reflect the sheet number on the drawing jump arrow on lines 1TD01B - 2" and 1TD02C - 2" by showing M-65 instead of M-65-1 as should have been the case. The drawing was revised to reflect actual field conditions.

UFSAR Table 6.2-21 Revision to reflect As-built Conditions
UFSAR Table 6.2-21 Sheet 6A is revised to reflect As-built Conditions for containment penetration I-8D. The restricting orifice referenced by the note does not exist in the plant. The note states that the applicable instrument lines are provided with flow restricting orifices, manual isolation valves, and excess flow check valves. The table is revised to match plant configuration, as the flow restricting orifice does not exist. Additionally, the valve number is corrected from 1&2VO061 to 1&2VQ061.

Revision to UFSAR Table 8.3-2 and Subsection 9.2.1.5
UFSAR Table 8.3-2 is revised to provide additional clarifying on the Division III diesel generator overcurrent and overcurrent with voltage restraint protective relaying. UFSAR Subsection 9.2.1.5 is revised to clarify that the diesel generator cooling water pumps are automatically started during the corresponding diesel generator start sequence.

UFSAR Revision associated with Procedure LTS-300-5, Revision 22
Changes incorporated to procedure LTS-300-5 Revision 22, LaSalle Station Primary Containment Leak Rate Testing Program, are associated with an Assessment of the Appendix J Program, Licensee Event Report (LER) 97-014-00, plant modifications associated with NRC Generic Letter 96-06, and other various issues. Corresponding revisions to UFSAR Section 6.2.6 involve editorial changes, administrative changes, acceptance criteria changes, new components added to program, physical containment penetration changes, and change in testing methodology, all of which reflect the changes to LTS-300-5.

UFSAR Revision Associated with Station Blackout Rule
The NRC issued a Supplemental Safety Evaluation of the LaSalle County Station Response to the Station Blackout Rule (TAC Nos. M98864 and M98865) dated December 4, 1997. This was in response to a clarification submitted by LaSalle Station to the NRC, dated May 28, 1997. UFSAR Sections 8.3, 15.9, and H.4 are revised to reflect the NRC accepted method for calculating battery capacity utilizing the minimum 5% remaining margin, and adjustment of the aging factor, if necessary, to maintain the margin.

UFSAR Revision to Reflect Operating Experience (OPEX) Program
UFSAR Appendix L Section L.12 is revised to reflect the company organization and philosophy changes resulted in revisions to site procedures previously referenced in FSAR Appendix L. Changes are also incorporated in LaSalle Administrative Procedure LAP-850-6 Revision 9, Processing of Operating Experience (OPEX) Information and Changes to Regulatory Rules. Use of this procedure serves to ensure that OPEX information is appropriately reviewed and disseminated as required by NUREG-0737.

Editorial Correction to UFSAR Subsection 10.4.4.5, Turbine Bypass System, Instrumentation Application
The text "8% of the NSSS rated" was replaced with "80 % of the rated bypass". This change concerns the typographical omission of the '0' on the original "8 %" wording, thus the new words reflect the correct designation of "80 %". Also, the words "NSSS rated" are being replaced with "rated bypass" to clarify the meaning, without changing the intent. The context of this UFSAR subsection refers to how the Turbine Bypass valves react to the closure of the Turbine Stop Valves (TSVs) and Turbine Closure Valves (TCVs), and thus the wording of the change is correct in referring to the "rated

bypass" steam flow. The Design Bases Information from GE (OPL-3), states that the "80 % of the rated bypass" is the correct wording.

Revision to UFSAR Sections 4.6.1, 7.2.2, and 7.7.6
The changes implement UFSAR improvements in response to Engineering Requests (ERs) 9701543, 9702560, 9703059, and 9704829. The revisions to UFSAR Subsections 4.6.1.1.1.1.1.c.3 (Safety Design Bases, CRD Drive Mechanical System), 7.2.2.4.10 (CRD Low Charging Pressure), and 7.7.6.2.2.b ((LPRM) Physical Arrangement) are editorial (i.e., typographical error corrections, clarifying information). The revision to UFSAR Subsection 7.7.6.4.2 for the Traversing Incore Probe (TIP) Physical Arrangement, requires a change to the description of the X-Y recorder used to record TIP data. The proposed change also clarifies the valve system described in the last paragraph referring to the physical arrangement of the TIP system.

Revision to UFSAR Appendix B to reflect Updating of the status of the Discussion of Compliance with Regulatory Guide (RG) 1.100, Revision 1
The Discussion of the Regulatory Guide (R.G.) in FSAR Appendix B was last changed in 1977, when LaSalle was beginning evaluations for equipment originally qualified to IEEE 344 - 1971 to show qualification to IEEE 344-1975. Although FSAR section 3.10 was updated, Appendix B concerning R.G. 1.100, Rev. 1, was not. This UFSAR change brings forward and updates LaSalle conformance to R.G. 1.100, Revision 1, per section 3.10 of the UFSAR and adds the requirement to qualify non like-for-like replacements or new components to the 1975 standard and R.B. 1.100, Revision 1. This puts the qualification requirements in the appropriate place rather than in only specific cases, such as indicated in Tables 7.1-2 through 7.1-8. This change makes the requirements more clear in Section 3.10, which is referenced by the Tables.

Editorial change to UFSAR Subsection 7.7.10.2.2
UFSAR Subsection 7.7.10.2.2 is revised by changing the cross-reference for radiation detectors from Subsection 7.6.2 to Subsection 7.7.14.1.

Editorial change to UFSAR Subsection 7.7.14.1.1.2
UFSAR Subsection 7.7.14.1.1.2 is revised by changing the word "charcoal" to "catalytic" in items a., b., and c.

Revision to UFSAR Subsection 9.4.5.3.e
UFSAR Subsection 9.4.5.3 and Table 9.4-20 were revised to clarify ECCS area temperature indication on the main control board. The change in this package supersedes a previously proposed change to Subsection 9.4.5.3.e. This change is to delete reference to fan shutdown.

Containment Penetration General Design Criteria Inconsistency
UFSAR Sections 6.2 and 9.3 are revised to eliminate an inconsistency between containment penetration General Design Criteria (GDC) and its description in the UFSAR. For the compressed gas systems in subsection 9.3.1.3, the reference to the lines penetrating primary containment is changed to clarify the station air system and drywell pneumatic system lines that penetrate primary containment are provided with containment isolation valves which meet the requirements as applicable of GDC 56 or 57 of Appendix A of 10CFR50, as described in section UFSAR 6.2. Subsection 6.2.4.2.2, the evaluation against GDC 56, is expanded to include a description of the containment penetration line isolation for the service air and clean condensate systems.

UFSAR Revision per Temporary Alteration (TALT) 1-0028-98
Reactor Water Cleanup (RWCU) may be required by Technical Specification 3/4.4.9.2 action statements to be OPERABLE as an alternate shutdown cooling system. Modifications to the leak detection isolation circuitry for the Unit 1 inboard and outboard RWCU isolation valves are to be installed per Design Change Package (DCP) 9700532. These valves must remain open to maintain the shutdown cooling function. This TALT assists in the implementation of DCP 9700532.
This temporary alteration prevents the RWCU inboard and outboard and isolation valves 1G33-F001 and 1G33-F004 from automatically isolating as a result of leak detection isolation signals from high differential flow, room high differential temperature, or loss of power to the leak detection heat exchanger room temperature/differential temperature logic circuit while this TALT was in place. UFSAR Subsection 7.6.2.2.6 is accordingly revised to discuss the continuous bypassing of the Reactor Water Cleanup System Leak Detection isolation trip functions during operational conditions when a unit is in cold shutdown, refuel, or defueled.
UFSAR Vol. XI Drawings M-155 Sheet 2, Leak Detection, and M-2097 Sheet 2, Reactor Water Cleanup System are temporarily marked to indicate the temporary alteration being in place defeating the leak detection isolations. These drawings are to be restored following removal of the temporary alteration.

UFSAR Change Associated with Procedure LTS-200-9, Revision 5, RHR Pump Seal Cooler Service Water Flowrate Test
UFSAR Subsection 9.2.1.2 is revised since the procedure may leave the seal cooler outlet valves throttled if necessary to remain within design flows, as opposed to the seal cooler outlet valves being fully open.
UFSAR Subsection 9.2.1.5 is revised to reflect that there are no flow elements installed in the discharge path of the residual heat removal (RHR) seal cooler outlet lines and Low Pressure Core Spray (LPCS) motor cooler lines.

UFSAR drawings M-87 sheets 1 and 2, and M-134 sheets 1 and 2 are to be revised since the procedure proposes to leave these valves throttled if necessary to remain within the vendor stated maximum flow limit, as opposed to the locked open position.

UFSAR Update per Design Change Package (DCP) 9700321
Previous lake monitoring instrumentation provided only local lake blowdown flow velocity measurement, and did not provide continuous lake level monitoring in the main control room as required by the UFSAR. The DCP provides for continuous lake level monitoring in the main control room as required by the UFSAR. UFSAR Subsections 2.4.8.4, 7.7.11.3 and 11.2.2.6 are revised to reflect the recording of blowdown flow in the Main Control Room. UFSAR Subsection 9.5.2.2.2 is revised to reflect the existence of the telemetry system.

UFSAR Change to Reflect Modification of the Unit 1 Condensate Polishing Demineralizer Panel Design Change Package (DCP) 9700071 (Modification M01-1-97-001)
The DCP removed the condensate polisher automatic regeneration mode of operation from Unit 1, in addition to removing the valve interlocks and permissives which control transfer between the condensate polishers (CP) and the tanks related to regeneration, to instead be controlled by manual operator action from the control panel. The DCP modified the transfer of resin from the cation/separation tank to the mix/storage tank. The Unit 1 regenerate cycle no longer includes the full chemical cleaning process. UFSAR Subsections 10.4.6.2, 10.4.6.3, 10.4.6.5, 11.2.1.7, 11.2.1.7.1, and 11.2.2.3 are revised to reflect that regeneration is no longer possible in Unit 1.

UFSAR Update due to Unit 1 Station Heat Supply Air Coils Replacement per Design Change Package (DCP) 9600547
The DCP replaced Unit 1 station heat supply air coils 1VT02AA and 1VT02AB in the ventilation supply of the turbine building and rerouting of some associated piping. The previous coils were freeze-damaged. The DCP installation allows for complete draining and venting of the coils and headers. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Update due to Unit 2 Station Heat Supply Air Coil Replacement per Design Change Package (DCP) 9600550
The DCP replaced Unit 2 station heat supply air coil 2VR02A in the ventilation supply of the reactor building and rerouting of some associated piping. The previous coil was freeze-damaged. The DCP installation allows for complete draining and venting of the coil and header. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Update to reflect as-built Tygon Tubing Diesel Generator Drain Lines

3/4" drain lines are connected to the air box of each diesel generator. The air box is a part of each generator's skid package. The installed 1" tygon tubing is mechanically connected to the 3/4" drain pipe off of the air box of each diesel engine. The other end of the tygon tube rests in the floor drain funnel opening. The connection provides a drain path for the accumulation of liquids from the engine air box. Drawing M-83 Sheets 1, 2, and 3 are revised per as-built Drawing Change Request (DCR) 980304.

UFSAR Update per Main Turbine and Reactor Feedwater Pumps Level 8 Trip Logic Control Modification, Design Change Package (DCP) 9600545
The DCP added an interlock from the Unit 1 Reactor Core Isolation Cooling (RCIC) Division 1 level 8 trip relay 1B21A-K705AX to Channel C trip logic of the main turbine / feedwater pumps trip. This change allows the RCIC Division 1 level 8 trip to actuate the 'C' channel main turbine / feedwater pumps level 8 trip. UFSAR Figure 7.7-5 and Subsection 7.7.4.2.1 are revised to reflect the DCP.

Editorial Changes to UFSAR Drawings
Editorial changes are incorporated in to the following UFSAR drawings: M-54 Sheet 1 Revision S, M-54 Sheet 2 Revision A, M-54 Sheet 3 Revision A, M-98 Sheet 2 Revision Q, M-99 Revision T, M-103 Sheet 12 Revision N, M-103 Sheet 24 Revision AC, and M-143 Sheet 2, Revision R.

LaSalle Unit 1 ECCS Suction Strainer Replacement per DCP 9700303
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 1 low-pressure core spray (LPCS) suction line in the suppression pool. The replacement strainer has increased surface area to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR drawing M-96 Sheet 2 for the Unit 1 RHR system is revised to reflect the strainer replacement.

Revision to UFSAR Subsection 9.5.4.3
The diesel generator fuel transfer pump alarm and low-level alarm setpoints specified for the Division 3 diesel generator are incorrect, as identified in PIF 97-3109 and evaluated in Operability Evaluation OE97082. The revision to UFSAR Subsection 9.5.4.3 not only corrects the error but also specifies only the required criteria, and not the result of the calculations or instrument setpoints specifics. The change applies to all five emergency diesel generators since the criteria is common to all diesel generator fuel oil systems.

Revision to UFSAR Subsection 9.3.5.2 to reflect as-built condition of the facility

UFSAR Subsection 9.3.5.2 is revised to reflect the as-built condition of the standby liquid control system (SBLC) on Unit 1 and Unit 2. The description of the ambient temperature in subsection 9.3.5.2 is expanded from '70 °F - 100 °F' to '65 °F to 104 °F'.
UFSAR Revision for VC/VE Temperature, Pressure and Humidity Limits
Design Change Packages (DCPs) 9600214 and 9600215 removed the humidification equipment from the Control Room and Auxiliary Electric Equipment Room ventilation systems (VC and VE, respectively). Not all resultant changes to the UFSAR were revised per the DCPs. The UFSAR changes consist of revising the minimum, normal and maximum temperature, pressure and relative humidity parameters for the Main Control Room (MCR) and the Auxiliary Electric Equipment Room (AEER); clarification of the normal operating pressure for the VC and VE systems when not in Emergency Makeup Mode; references to pressure ranges are made to be consistent with other UFSAR sections: added a discussion of the humidity restrictions for the recirculation filters on both VC and VE to clarify their revised design basis; reference to steam humidifiers are deleted; and consistent wording is maintained for the discussion of pressurization modes.
UFSAR Tables 3.11-24 and 3.11-25, and UFSAR Sections 6.4, 6.5, 7.3, 9.4.1.1, 9.4.1.2, and H.3.4 are accordingly revised.

Revision to UFSAR Subsection 8.3.1.1.3 per Design Change Package 9800039
An evaluation of the Reactor Protection System (RPS) Electrical Protection Assembly (EPA) overvoltage, undervoltage, and underfrequency setpoints was performed in calculation L-001678. This calculation recommends a change to the calibration settings of the RPS EPA overvoltage, undervoltage, and underfrequency trips to account for instrument inaccuracies including drift. DCP 9800039 doesn't physically change hardware, as it adjusts the desired calibration setting to account for instrument inaccuracies including drift. The revised calibration settings insure compliance with the Technical Specifications; and change neither the Technical Specification setpoints nor how they were established. The change to Subsection 8.3.1.1.3 insures that the setpoint requirement is maintained in accordance with the design and licensing basis currently specified in the UFSAR and the Technical Specifications.
The UFSAR change is applicable to both units 1 and 2.

Clarification to UFSAR Subsections 9.4.1.1.2.a and 9.4.1.2.2.a
UFSAR Subsections 9.4.1.1.2.a, Control Room HVAC, and 9.4.1.2.2.a, Auxiliary Electric Equipment Room (AEER) HVAC are revised to clarify the description of the purge discharge path via the Auxiliary Building equipment vent.

Revision to UFSAR Figure 15.2-12
The editorial change incorporates the revision of references to other UFSAR figures in UFSAR Figure 15.2-12, ADS/RHR Cooling Loops.

Revision to UFSAR Subsections 5.2.2.4.1 and 7.3.1.2.2.1
An editorial revision to UFSAR Subsections 5.2.2.4.1 and 7.3.1.2.2.1 was made to achieve consistency between the two subsections.

Revision to UFSAR Figure 13.5-1 per Design Change Package (DCP) 9700248
The DCP relocated Balance of Plant (BOP) computers from the main control room to the computer room, and Nuclear Steam Supply System (NSSS) printers were relocated from adjacent to the center desk in the control room to the top of the lower desk, which is also a part of the center desk. The design change is part of the Main Control Room enhancement program, which is a human factors effort. UFSAR Figure 13.5-1 is accordingly revised.

Correction of Discrepancies in UFSAR Subsections 9.2.8.2 and 9.2.8.5
Discrepancies in UFSAR Subsections 9.2.8.2 and 9.2.8.5 for the Turbine Building Closed Cooling Water (TBCCW) are corrected. The changes apply to the description of system flow and heat exchange capability, a change in TBCCW system leakage, correction to the UFSAR list of equipment to which TBCCW provides cooling water, and a change in TBCCW abnormal pressure and temperature indications.

Revision to UFSAR Figure 13.5-1 per Design Change Package (DCP) 9700528
The DCP added various cabinets in the main control room to store operating procedures, prints, block cases, emergency, self-contained air breathing apparatus, and miscellaneous parts as requested by the Operating Department. The cabinets are required to be stored in the main control room to maintain habitability. UFSAR Figure 13.5-1 is accordingly revised.

Editorial Revision to UFSAR Appendix H
Editorial revisions were made to tables in UFSAR Appendix H resulting from a review of the UFSAR Safe Shutdown Analysis. UFSAR Tables H.4-17, H.4-18, H.4-20, H.4-22, H.4-23, H.4-25, H.4-49, H.4-50, H.4-51, H.4-70, H.4-80, H.4-95, H.4-104 are revised to correct typographical errors.

Revision to UFSAR Subsection H.3.4.17 per Design Change Package (DCP) 8300039
The addition of Chemical Feed Stations on Unit 2 changed the number of floor drains in fire zone 4F2 (Unit 2 Division 1 Essential Switchgear Room), from two to one. To install the DCP, a core bore was required in the Unit 2 Division 1 Switchgear room. This core bore accidentally cored through an existing floor drain line. A supplemental engineering change notice (ECN) was issued to define how to cap both ends of the floor drain line. However, the number of floor drains in this room was specifically described in the UFSAR. UFSAR Subsection H.3.4.17 is revised to state that the description of zones 4F1 and 4F2 is similar, except that the Unit 2 zone only contains 1 floor drain.

UFSAR change per Design Change Package (DCP) 9700599, Replacement of RHR Heat Exchanger Relief Valve 1E12-F313B
The DCP replaced the residual heat removal (RHR) B heat exchanger tube side relief valve 1E12-F313B in response to past setpoint test failures. The valve was also re-oriented to the vertical position, per current ASME requirements. UFSAR drawing M-91 Sheet 3, Reactor Building Equipment Drains, is revised to reflect the installation of DCP 9700599.

UFSAR Change per Design Change Package (DCP) 9700578, Relocation of pressure switches 1B21-N413A and C
The design change relocated pressure switches 1B21-N413A and C from pipe stand mounts to instrument rack 1H22-P026, where better instrument needle valves are available to minimize spiking caused instrument valve operations. This will aid in minimizing the incidence of scrams and/or engineered safety feature actuations resulting from pressure spiking associated with instrument valve operations. UFSAR drawing M-93 Sheet 5, Nuclear Boiler and Reactor Recirculating, is revised.

UFSAR Change per Design Change Package (DCP) 9700579, Relocation of pressure switches 1B21-N413B and D
The design change relocated pressure switches 1B21-N413B and D from pipe stand mounts to instrument rack 1H22-P027, where better instrument needle valves are available to minimize spiking caused instrument valve operations. This will aid in minimizing the incidence of scrams and/or engineered safety feature actuations resulting from pressure spiking associated with instrument valve operations. UFSAR drawing M-93 Sheet 4, Nuclear Boiler and Reactor Recirculating, is revised.

UFSAR change per Design Change Package (DCP) 9700598, Replacement of RHR Heat Exchanger Relief Valve 1E12-F313A
The DCP replaced the residual heat removal (RHR) A heat exchanger tube side relief valve 1E12-F313A in response to past setpoint test failures. The valve was also re-oriented to the vertical position, per current ASME requirements. UFSAR drawing M-91 Sheet 3, Reactor Building Equipment Drains, is revised to reflect the installation of DCP 9700598.

UFSAR Change per Engineering Request (ER) 9707835
UFSAR drawing M-69 sheet 2, Service Water, is revised per ER 9707835 to reflect the as-built condition of the plant. Correction of the valve omission will provide for better control of the valves.

UFSAR change per Engineering Request (ER) 9703090
UFSAR Drawings M-69 Sheet 1, Service Water, and M-125 Sheet 1, Service Water, are revised per Engineering Request (ER) 9703090 to reflect as-built conditions of the plant.

UFSAR Change per Engineering Request (ER) 9800832
USFAR drawing M-63 Sheet 4, Circulating Water System, is revised per Engineering Request 9800832 to delete a redundant detail from the drawing, reflecting the proper design specifications, in order to assure that future repairs are made with the correct materials.

UFSAR Change per Engineering Request (ER) 9707441
UFSAR drawing M-90 Sheet 2, Reactor Building Closed Cooling Water (RBCCW) System, is changed as a result of field walkdowns associated with the plant labeling effort. The drawing revision is a non-function change which reflects the relocation of an interconnection between the A and B reactor recirculation pump motor windings RBCCW outlet drain lines and the A and B reactor recirculation pump motor windings RBCCW outlet lines.

UFSAR Change Associated with Electrohydraulic Control System (EHC) Pressure Regulator Failure - Closed transient analysis
General Electric (GE) Service Information Letter (SIL) 614 states that plants must have specific evaluation of the pressure regulator failure - closed transient without a backup pressure regulator available to support operation without both pressure regulators available. LaSalle does not have such an analysis. The potentially restrictive core thermal limits such an analysis would impose makes performing such an analysis undesirable. Operation must accordingly be limited to meet the initial conditions assumed in the present Pressure Regulator Failure - Closed transient. This requires that both pressure regulators be available, to ensure that a single failure of one pressure regulator will result in operation of the backup regulator. UFSAR Subsections 7.7.5.2.2 and 15.2.1.1 are correspondingly revised.

Revision to UFSAR Section H.4
UFSAR Tables H.4-63, H.4-71, H.4-95, H.4-105, H.4-106, and H.4-107
are revised to rectify the typographical errors. These typographical errors were discovered while reviewing the tables for Safe Shutdown

Emergency Diesel Generator 1A Speed Sensor Replacement and UFSAR Update per Design Change Package (DCP) 9800003
The station's diesel generators have recently experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for

both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 0 emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch. UFSAR Section 1.7, Electrical, Control and Instrumentation drawings, is revised.

Revision to UFSAR Subsection 5.4.6.2.3
The reference to subsection 6.2.2 in the text of subsection 5.4.6.2.3 is revised to reference section 15.9. This change corrects the reference as it pertains to the operation of the Reactor Core Isolation Cooling (RCIC) during loss-of-offsite power.

UFSAR Revision to reflect Unit 1 Design Change Package (DCP) 9700402
The DCP installed 20" diameter valve 1VG023 on the Unit 1 standby gas (VG) treatment system (VG) primary containment suction piping in order to provide a method of isolating the standby gas treatment system from the primary containment vent/purge system during the purging/venting process. Installation of this design change provides over-pressurization protection in the event of a LOCA during the purging or venting of the drywell or the suppression chamber. UFSAR Tables 3.2-1 and 6.1-1, and UFSAR Subsections 6.5.1.5 and 6.5.1.6, and drawing M-89 are accordingly revised.

Generic Letter 96-06 Over-pressurization Protection for Primary Containment Piping, Design Change Package (DCP) 9700341
The DCP installed a thermal relief valve, 1E12-F460, on the residual heat removal (RHR) supply line between primary containment isolation system (PCIS) valves 1E12-F008 and 1E12-F009 (primary containment penetration M-7). The design change was installed to resolve overpressure concerns associated with NRC Generic Letter 96-06. UFSAR Table 5.2-6, Subsection 6.2.4.2.1, Tables 6.2-21and 6.2-28, Figure 6.2-31, and drawing M-96 Sheet 3 are revised to reflect the installation of the design change.

UFSAR Revision to reflect Unit 2 Design Change Package (DCP) 9700403
The DCP installed 20" diameter valve 2VG023 on the Unit 2 standby gas (VG) treatment system (VG) primary containment suction piping in order to provide a method of isolating the standby gas treatment system from the primary containment vent/purge system during the purging/venting process. Installation of this design change provides over-pressurization protection in the event of a LOCA during the purging or venting of the drywell or the suppression chamber. UFSAR Tables 3.2-1 and 6.1-1, and UFSAR Subsections 6.5.1.5 and 6.5.1.6, and drawing M-89 are accordingly revised.

Unit 1 Group IV Isolation Logic Power Supply Change to Direct Current (DC) per Design Change Package (DCP) 9500476

The DCP changed the power supply for logic relays that initiate Group IV isolation of ventilation dampers which provide secondary containment isolation to the Reactor Building Ventilation (VR) System as well as other Group IV isolation actions in the Reactor Building Purge (VQ) System and startup of the Standby Gas Treatment (VG) System of Unit 1. The power supply is changed from Reactor Protection System (RPS) Bus 120 Volt AC to 125 Volt DC, which prevents isolation of VR upon the loss of a single RPS bus.
This situation was a significant "work-around" for the operators at LaSalle. Changing of the power supplies for the Group IV logic relays to the 125 VDC system provides a more reliable power source for the logic relays than the RPS bus. The overall reliability of the plant is enhanced, unnecessary scrams and Group I isolations are prevented, and a significant "work-around" is cleared. The logic remains as de-energize-to-trip following installation of the DCP. UFSAR Subsection 7.3.2.2.1, Figure 7.3-10, and Tables 8.3-12 and 8.3-13 are revised.

Modification to Unit 1 Containment Leak Test Channels per Design Change Package (DCP) 9800041
The DCP removed eighteen leak test plugs for the leak test system around the Unit 1 safety relief valve (SRV) pipe support embedment plates at the containment wall above elevation 700' -0" in the Unit 1 suppression pool. The DCP also clarifies that all other test plugs in the suppression pool and the containment drywell may be permanently left in place. The leak-test channels were originally installed over containment liner welds so that these welds could be pressure tested to verify leak-tightness. Threaded plugs were installed in openings in these leak-test channels to facilitate this pressure testing. It was the intent of the original design that these plugs be removed after these local leakage tests were complete so that during future Containment Integrated Leak Rate Tests (CILRT), the liner welds would see the test pressures. The leak-test channels and plugs were not designed to act as the containment pressure boundary. Licensee Event Report (LER) 97-030 documents that the plugs were not removed as originally intended after the initial local leak rate tests. UFSAR Subsections 6.2.1.1.2 and 6.2.6.1 are revised.

Upgrade of Core Standby Cooling System Bypass Line and Valve 0E12-F300
The safety classification of the 54" Core Standby Cooling System - Equipment Cooling Water System (CSCS - ECWS) screen bypass supply pipe line 0RH01AA and valve (0E12-F300) to the service water intake tunnel was upgraded to "Safety Related". The 54-inch bypass line assures access to a continuous supply of water to the service water intake tunnel located in the lower level of the lake screen house, to cool various safety related equipment and equipment important to safety. The CSCS-ECWS also provides a source of emergency makeup water for fuel pool cooling and also provides containment flooding water for post-accident recovery. The pipe line and valve were originally classified as Pipe Class D, Non-Safety Related, Non-Seismic, and were recently upgraded to Class D, Seismic. Upon completion of the drawing change request (DCR) 960135 upgrade process, the subject pipe line and valve are classified

as Pipe Class D, Safety Related, Seismic Category I. UFSAR Table 3.2-1, and drawing M-87 Sheet 1 are revised.

Upgrade of the Public Address System and UFSAR Update per Design Change Package (DCP) 9700308
The DCP provides for permanent integration of the five zones into one plant-wide system for paging and party-line communications, and for extending the station's Public Address (PA) System to various outbuildings, which were outside the previous coverage areas. UFSAR Section 9.5.2 and Figure 9.5-2 are revised.

Correction of discrepancies in UFSAR Subsection 10.4.7.2
The capacities of the Turbine Driven Reactor Feed Pumps (TDRFPs) and the Motor Driven Reactor Feed Pumps (TDRFPs) in UFSAR Subsection 10.4.7.2 have been determined to be incorrect. The discussion in the UFSAR is revised to reflect the actual operating capacities of the TDRFPs and the MDRFPs.
The revision corrects a discrepancy between the stated and actual capacities of the above pumps, which was discovered during the 1997 System Functional Performance Review (SFPR). The change identifies the design target capacity of 68% for a TDRFP and deletes the incorrect design target capacity of 40% for a MDRFP. Additionally, the actual operational capability of 57% to 60% for a TDRFP and 30% to 32% for a MDRFP is listed to eliminate the inference that the unit is operated at 100% with a TDRFP and the MDRFP.

Revision to UFSAR description of the Containment Fill function provided by the Fuel Pool Emergency Makeup System
UFSAR Subsection 9.2.1.1.1.a.11 is revised to correct an ambiguous designation of the flow rate and the pump supplying it for the containment fill (flooding) function provided by each unit's fuel pool emergency makeup system. The flowrate is revised to a nominal value of 300 gpm, and the supplying pump is specified as being the unit's Division 2 fuel pool emergency makeup pump, 1(2)FC03PB.

UFSAR Revision to reflect Modification of Unit 1 Station Air Compressor Cooling Water Pressure Regulator and Relief Valves per Design Change Package (DCP) 9600322
The DCP increased the reliability of station air compressor 1SA01C by modifying the cooling water supply to the compressor's Inter/aftercooler and Oil Cooler. The bronze pressure regulator previously installed for 1WT087 was replaced with a cast iron pressure regulator. The regulator establishes a water supply pressure of 55 psig to the station air compressor inter/aftercooler.
Relief valve 1WT124 on the station air compressor inter/aftercooler cooling water supply line was replaced. The relief setpoint was increased from 65 psig to 75 psig, which reduces the chance of seat leakage during normal operating pressure. The associated discharge piping was reconfigured to reduce backpressure, as high backpressure on

the relief valve discharge may cause the relief valve to chug, damaging the seating surface of the relief valve. Relief valve 1WT125 on the station air compressor inter/aftercooler and oil cooler cooling water supply header was removed, as it is no longer required. UFSAR drawing M-67 Sheet 2, Turbine Building Closed Cooling Water, is correspondingly revised.

Update to UFSAR Drawings M-96 sheets 1 and 2, and M-142 Sheets 1 and 2
UFSAR drawings M-96 sheet 1 and 2 and M-142 sheet 1 are revised to reflect installed (as-built) conditions. Carbon steel piping is installed in portions of the system that were designed as stainless steel (and vice versa), and dissimilar welds (carbon to stainless) were not previously analyzed. A note was also added to drawings M-96 sheet s 1 and 2, and M-142 sheets 1 and 2 to reflect that SA-333 Grade 6 material may have been installed in the residual heat removal shutdown cooling lines during original construction. This has been evaluated as an acceptable alternate material per as-built drawing change request (DCR) 960156.

Self-Contained Breathing Apparatus (SCBA) Air Compressor Replacement per Design Change Package (DCP) 9600527
The DCP installed a new SCBA air compressor, 0FP35C, in the plant at the S and 29 lines in the Unit 2 Turbine Building, elevation 710'-6". The compressor serves to refill SCBA air bottles onsite, as opposed to sending them offsite. UFSAR drawings M-Index Sheet 2, M-9, and M-72 Sheet 4 are revised.

Revision to UFSAR Tables 6.2-21 and 6.3-5
The UFSAR description of the control circuits for the low pressure core spray (LPCS) pump suction valves 1(2)E21-F001 and the residual heat removal (RHR) pump suction valves 1(2)E12-F004A, B, and C do not agree with actual plant configuration. UFSAR Tables 6.2-21 and 6.3-5 indicate that these valves receive an auto-open signal following a LOCA. However, they do not receive any auto-actuation signal. Rather than having an auto-open circuit, these valves are operated by keylock switches in the control room and maintained in the open position. These valves are checked monthly per the Technical Specifications to ensure that they are maintained in the proper position. This UFSAR change brings the tabular description of the control circuits for these valves into agreement with actual plant configuration, descriptions in the UFSAR, ComEd responses to NRC questions, and GE design documents.

UFSAR Update to reflect Addition of Cooling Water Flow Gauges for Unit 1 Core Standby Cooling System (VY) Area Coolers per Design Change Package (DCP) 9700019
The DCP installed individual flow indication for coolers 1VY02A and 1VY03A, and combined flow indication for coolers 1VY01A, 1VY04A, and 1E21-C001. The addition of the flow indication allows for measurement of flow through the VY area coolers, which

was not previously monitored. UFSAR drawings M-87 Sheets 1 and 2 for the Unit 1 core standby cooling equipment cooling water system are revised.

UFSAR Update per Removal of Remote Indication Hardware from Division 1 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700487
DCP 9700487 removed remote indication hardware from Division 1 ECCS testable check valves 1E12-F041A, 1E12-F050A, and 1E21-F006. This was done to eliminate a recurring problem in which the valves fail to completely close. This is attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP increases the margin by reducing the frictional forces, thereby eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 9.3.1.2.2, Table 6.2-21, and drawings M-66 Sheet 2, M-94, and M-96 are revised.

Clarification to UFSAR Subsection 15.6.1.2
The operator response for a stuck open safety relief valve (SRV) in UFSAR Subsection 15.6.1.2 is indeterminate and confusing. UFSAR Subsection 15.6.1.2 is revised to clarify the actions to be taken in the event that a SRV can't be closed.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability of obtaining drywell and suppression pool atmosphere iodine and particulate samples for radionuclide analysis. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was made in anticipation that the information would be used by the core damage assessment methodology later approved for use by the NRC. The approved methodology does not require that these samples be obtained and analyzed. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability of obtaining a stripped gas sample from reactor coolant for radionuclide analysis. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was made in anticipation that the information would be used by the core damage assessment methodology later approved for use by the NRC. The approved methodology does not require that this sample be obtained and analyzed. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a dissolved oxygen analysis of reactor coolant. This

commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was intended to provide information on the corrosion potential of materials in contact with the reactor coolant under post accident conditions. The concentration level of concern for dissolved oxygen in reactor coolant is 0.1 parts per million (PPM) or greater. Under post accident conditions, the reactor coolant dissolved oxygen concentration will be greater than 0.1 PPM since there is no capability to remove dissolved oxygen from the coolant under shutdown conditions and the sources of water injected into the reactor system for makeup contain dissolved oxygen concentrations in excess of 4 PPM. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description. A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a dissolved hydrogen analysis of reactor coolant. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was intended to provide information on the possibility of forming a gaseous bubble in the reactor system that may prevent or reduce core cooling as well as to provide some information on the degree of core damage. The design of the LaSalle reactor systems precludes the possibility of forming gaseous bubbles under post-accident conditions that could inhibit core cooling. The core damage assessment methodology approved by the NRC does not require reactor coolant dissolved hydrogen analysis for the calculation. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a conductivity analysis of reactor coolant. This commitment was not required by NUREG-0737, Item II.B.3 or Regulatory Guide 1.97. The capability was intended to provide information on the corrosion potential of materials in contact with the reactor coolant under post-accident conditions. A review of the site's emergency operating procedures and generating station emergency plan shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a pH analysis of reactor coolant. This commitment was not required by NUREG-0737, Item II.B.3, but was described in Regulatory Guide 1.97. The capability was intended to provide information to facilitate the assessment of the potential inventory of activity available that could be released from the plant under post-accident conditions. Later NRC guidance does not require that a pH determination be made (NUREG-1228 and NUGEG-1465). A review of the site's emergency operating procedures and generating station emergency plan shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a chloride analysis of reactor coolant. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was intended to provide information on the corrosion potential of materials in

contact with reactor coolant under post-accident conditions. The primary method for performing a reactor coolant chloride analysis is an in-line analyzer. This analyzer will be retired and a laboratory method will be used instead to generate the reactor coolant chloride concentration data. UFSAR Section 11.5.5 is revised to change this commitment within the Post Accident Sampling program description.
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability of obtaining drywell equipment and floor drain sump samples for radionuclide and chemical analysis. This commitment was not required by NUREG-0737, Item II.B.3 but was described in Regulatory Guide 1.97. This commitment was made to facilitate core damage assessment calculations. Sampling containment sump is a PWR plant issue and does not apply to LaSalle since coolant leakage is collected in the suppression pool under post-accident loss of coolant conditions. A review of the site's core damage assessment procedure, emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Update per Removal of Remote Indication Hardware from Division 3 Emergency Core Cooling System (ECCS) Testable Check Valve, Design Change Package (DCP) 9700489
DCP 9700489 removed remote indication hardware from Division 3 ECCS testable check valve 1E22-F005. This was done to eliminate a recurring problem in which the valve failed to completely close. This is attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP increases the margin by reducing the frictional forces, thereby eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 9.3.1.2.2, Table 6.2-21, and drawings M-66 Sheet 2 and M-95 are revised.

Revision to UFSAR Table 9.3-1 and drawing M-99
Grab samples of the standby liquid control (SBLC) storage tank are gathered by dip sample in accordance with approved station procedure LCP-310-09. Sample pump 1C41-D303 was not installed as original equipment on either LaSalle unit, yet it is depicted on drawing M-99 (Unit 1 SBLC system). UFSAR Table 9.3-1 Sheet 5 indicates that one pump is required for the purpose of obtaining grab samples. If installed, the pump would serve no function that differs from the currently approved method of sampling. UFSAR Table 9.3-1 and drawing M-99 are revised to delete mention of the pump.

Deletion of Reference to UFSAR Section 15.B
UFSAR Subsection 15.1.1.3 is revised by deleting the reference to UFSAR Section 15.B. UFSAR Section 15.B was previously deleted.

UFSAR Update per Design Change Package (DCP) 9600356, Converting Main Condensate (MC) Drops to Cycled Condensate (CY) Drops
This design change converted portions of contaminated MC piping to a CY supply, abandoned in place and removed other portions, and provides a clean MC path to the chemistry sinks via the sample lines. UFSAR Drawing M-74, M-75 Sheets 1,2, and 3, and M-103 Sheet 26 are revised to show the portions of contaminated MC piping converted to a CY supply, the abandoned piping, and a clean MC path to the chemistry sinks via the sample lines.

Revision to UFSAR for Containment Monitoring Penetration Isolation
In order for the Post-LOCA H2/O2 system to be an extension of the primary containment, i.e., closed loop outside the containment, the High Radiation Sampling System (HRSS) Containment Air Sampling Isolation Valves 1(2)CM085, 1(2)CM086, 1(2)CM089, and 1(2)CM090 should have been considered containment isolation valves. These valves are designed to be ASME Class 2 and seismic Category I; however, these valves were not identified as containment isolation valves, were not specifically tested as containment isolation valves, and were not controlled as containment isolation valves. Administrative Technical Requirements Tables 3.6.3-1 and 3.6.3-2, UFSAR Table 6.2-21, Summary of Lines Penetrating the Primary Containment, and UFSAR Table 6.2-28, Primary Containment Isolation Valves, for penetrations I-35, I-47, & I-50, are revised to include High Radiation Sampling System (HRSS) Containment Air Sampling Isolation Valves 1(2)CM085, 1(2)CM086, 1(2)CM089, and 1(2)CM090.

UFSAR Update for the inclusion of a holdup volume in the pathway for unidentified leakage to reach the Drywell Floor Drain Sump (DWFDS)
The UFSAR didn't previously provide definitive information as to the potential of a holdup volume of water due to irregularities in the drywell floor and the effect on the design basis for the leakage detection system in the drywell. UFSAR Subsections 3.8.3.1.1 and 5.2.5.5.4 are revised for the reactor coolant pressure boundary leakage detection system to include the addition of holdup volume caused by the irregularities in the drywell floor.

Revision to UFSAR Table 9.3-1 and Drawing M-143 Sheet 1 to reflect as-built condition of the plant
UFSAR Table 9.3-1 Sheet 1, Process Sampling System (Reactor Building Samples), and drawing M-143 Sheet 1, Reactor Water Cleanup System, are revised reflect the as-built configuration of the subject sample line piping. These process-sampling lines include the reactor recirculation water sample line, the RWCU sample lines from each of the filter demineralizers, and the sample line off the discharge of the RWCU recirculation pumps.

Revision to UFSAR Subsection 7.5.3.c.4
UFSAR Subsection 7.5.3.c.4 is revised to reflect that safety relief valve position indication is actually powered by 125 VDC from Division I distribution panels 111Y (Unit 1) and 211Y (Unit 2). This was identified by the Design Basis Initiative project.

UFSAR Revision for Motor Operated Valve Thermal Overload Protection
UFSAR Section 6.3.2.2.13 is revised to reference UFSAR Table 6.3-9 for the HG valves and to add reference to Regulatory Guide 1.106, Revision 1.
UFSAR Table 6.3-9 was revised as follows:
Valves 1(2)G33-F001, 1(2)E12-F006A, and 1(2)E12-F011A are added to the table;
A clarification that Motor Operated Valves (MOVs) 1VQ037, 1VQ038, 2VQ037, and 2VQ038 have thermal overload bypass logic from both Unit 1 and Unit 2 was added to the table; Unit 1 and Unit 2 hydrogen recombiner (HG) MOVs were added to the table.
Main Steam Isolation Valve-Leakage Control System (MSIV-LCS) valves and 2E51-F091 were deleted from the table.
Table 6.3-9 was also reformatted to include the type of thermal overload bypass like Tech Spec Table 3.8.3.3-1, and to add allowance for no bypass for HG MOVs, as discussed in UFSAR subsection 6.3.2.2.13.
UFSAR Appendix B was revised by adding an update discussion on the applicability of Regulatory Guide 1.106, Revision 1.

Revision to UFSAR Sections 6.4, 6.5, 7.3.4, 7.3.8, 9.4.1, 9.4.10, 15.0.4, and 15.6.5 resulting from License Amendments
UFSAR Sections 6.4, 6.5, 7.3.4, 7.3.8, 9.4.1, 9.4.10, 15.0.4, and 15.6.5 were revised to reflect Technical Specification Amendments 125 and 126 for Unit 1, and 110 and 111 for Unit 2. These amendments established ventilation filter testing program technical specifications for the control room ventilation (VC), auxiliary electric equipment room (AEER) ventilation (VE), and standby gas treatment (VG) systems; and prohibited the simultaneous opening of the drywell and suppression chamber purge system (VQ) isolation valves.

UFSAR Revision for the Standby Gas Treatment (VG) System Charcoal Absorber High Temperature Alarm Setpoint
Design Basis documents for the standby gas treatment system either do not specify the charcoal absorber high temperature permissive alarm setpoint or else indicate a value of 310 °F. The alarm setpoint value of 250 °F in UFSAR Subsection 6.5.1.2.1.c.7 is revised to an alarm setpoint of 310 °F.

UFSAR Update to reflect Replacement of the Unit 1 Inboard MSIV Pilot Solenoid Valves
Design Change Packages (DCPs) 9500200, 9500201, 9500202, and 9500203 replaced the pilot solenoid valves of Unit 1 inboard Main Steam Isolation Valves (MSIVs) 1B21-F022A, B, C, and D. The previous ASCO model NP8323A20V valves (dual coil one per

MSIV) were replaced with Valcor model V70900-87 solenoid valves (single coil two per MSIV). The ASCO model NP8323A20V valve is no longer manufactured or supplied by ASCO. UFSAR Subsection 7.3.2.2.7 is revised, Figure 7.3-11 Sheet 1 is deleted, while Figure 7.3-11 Sheet 2 is redesignated as Figure 7.3-11 Sheet 1.

Revision to UFSAR discussion of the Reactor Mode Switch Bypass of the Charging Header Low Pressure Scram

UFSAR Section 7.2.2 is revised to add grammatical corrections and additional level of detail relevant to the operation of the control rod drive (CRD) charging header low pressure trip bypass test switches (1/2C11-S600A to D). These switches were part of the original design and installation of the low pressure trip circuit, but were not described well in the UFSAR. The existence of these test switches was implicit in the existing text, but it was not clearly stated.

UFSAR Figure 7.2-4 is revised to correct the normal position of the CRD low charging pressure scram bypass contacts from OPEN to CLOSED. This is an editorial correction of a typographical error. The text in the body of NUREG-0519 Supplement 7, the LaSalle UFSAR, and the LaSalle Technical Specification Bases make clear that the scram contacts are bypassed (i.e., bypass contacts CLOSED) during "normal" operation.

Revisions to UFSAR Subsections 6.5.1.2.1.C.7, 9.5.1.2.3, H.3.2.2, H.3.4.2, and H.3.5.33

UFSAR Subsections 6.5.1.2.1.C.7, 9.5.1.2.3, H.3.2.2, H.3.4.2, and H.3.5.33 state that the charcoal deluge valves are operated locally from the main control room board. The normally manual closed isolation valves upstream of the deluge valves, in all cases, require local actions to initiate water flow. The proposed change to the above UFSAR subsections clarifies the operation of the deluge valves to reflect manual operation of the charcoal deluge systems.

Editorial Revision to UFSAR Subsection 7.5.3.b.1

UFSAR Subsection 7.5.3.b.1 is revised to reflect that a separate power supply is furnished for the indicating lights for the valves 1(2)E12-F008. This is consistent with UFSAR subsections H.4.2.46.2 and H.4.2.47.2.

Revision to UFSAR Table 9.4-26

UFSAR Table 9.4-26 is revised to reflect that the Unit 2 supply air filters (area coolers) are a low efficiency type, the same as the Unit 1 filters.

UFSAR Revision for Control Room Ventilation System (VC) and Auxiliary Electric Equipment Room (AEER) Ventilation System (VE)

UFSAR Sections 6.4, 7.3, 9.4, and 9.5 are revised to reflect the proper operation of the VC/VE systems, correct grammatical errors, and clarify for consistency the discussion of VC and VE systems.

UFSAR Revision to Reflect Failure Modes of Turbine Building Ventilation Isolation Dampers
During a system functional performance review of the turbine building ventilation (VT) system, it was discovered that the above dampers would not close quickly enough to prevent overpressurization of the VT exhaust tunnel in the event of a main steam line break in the turbine building main steam line tunnel. UFSAR Section 9.4 is revised to reflect the failure modes of turbine building ventilation isolation dampers 1(2)VT079YA, 1(2)VT079YB, and 1(2)VT079YC.

UFSAR Revision to Reflect Design Change Package (DCP) 9500140
The DCP routed piping from the inlet of the plant chemical waste (WZ) evaporator to a vendor connection located in the Intermediate south storage area of the Radwaste truckbay in the Radwaste building. This DCP provides operational flexibility in the processing of floor drain/chemical drain water. Depending upon economics, it may be more advantageous to use state-of-the-art vendor skids to process waste instead of the currently installed evaporators. A return path is provided for processed water from the vendor skid to the WZ evaporator piping, which can be routed to the floor drain head tank or the floor drain collector, depending upon water quality. UFSAR Figure 11.2-1 is deleted, Sections 3.1, 9.3, 11.2, 11.4, and 11.5 are revised to reflect the option of using a vendor skid to process waste.

UFSAR Revision to reflect Minor Changes P01-1-91-542 and P01-2-91-538
Minor Changes P01-1-91-542 (Design Change Package [DCP] 9100290) and P01-2-91-538 (DCP 9100283) replaced the level instrumentation of the 1WX01TA, 1WX01TB, 2WX01TA, and 2WX01TB reactor water cleanup (RWCU) phase separator tanks. The original sonic type level indicating instruments in were replaced with thermal dispersion type level indicating instruments. A bubbler type level transmitter was also installed in the tanks. UFSAR Subsection 7.7.11.2.3 is accordingly revised.

UFSAR Revision Associated with Maximum Suppression Pool Temperature
License Amendments number 67 to Facility Operating License NPF-11 (Unit 1) and number 49 to Facility Operating License NPF-18 (Unit 2) approved raising of the maximum allowable technical specifications Limiting Condition for Operation (LCO) suppression pool temperature limit to 105 °F. The previous maximum allowable temperature was 100 °F. The NRC documented the acceptability of the new limit in the Safety Evaluation Report (SER) associated with the license amendments. UFSAR Sections 5.4, 6.0, 6.2, 15.0, 15.2, and 15.6 are revised to reflect the maximum allowable suppression pool temperature limit of 105 °F.

UFSAR Revision to reflect Design Change Package (DCP) 9500323
DCP 9500323 removed the precoatable elements of the Unit 2 equipment drain filters, and replaced them with non-precoatable filters. Filter precoat logic was also modified to accommodate non-precoating of filter elements. Non-precoatable filters provide comparable water quality, while minimizing the waste generated. UFSAR Sections 7.7, 11.2, 11.4, and 12.3 are revised.

UFSAR Revision to reflect the VC/VE Train B Electrical Demolition per Design Change Package (DCP) 9600215
DCP 9600215 demolished the humidification system (B train electrical portion) of Control Room (VC) and Auxiliary Electric Equipment Room ventilation (VE). Humidification system demolition was performed because the previous humidification units have been out of service for an extended period due to various system problems, and, the humidifiers and associated piping are not seismically supported, which is in direct conflict with the UFSAR which states that they are designed to meet II/I criteria. UFSAR Sections 6.4, 7.3, and 9.4 are revised.

Formalize the Design Basis for the Shad Net
The shad net provides no safety function and was introduced only to aid in the maintenance of existing plant system strainers and screens by preventing fish from entering plant components. The shad net has performed its intended function since installation in 1982, no formal evaluation was performed to update the UFSAR to include a description of the shad net. UFSAR Sections 2.5, 3.1, and 9.2 and Figure 2.5-59 are revised to include a discussion of the shad net.

UFSAR Revision for Cable Tray and Cable Tray Support System
UFSAR Subsection 3.7.3.16 is revised to reflect that the design includes consideration of LOCA and hydrodynamic loads as described in section 8.1.6.2 of Sargent and Lundy (S&L) calculation DC-SE-01-LS and sections 4.3.2 and 5.3.2 of the LaSalle Mark II Design Assessment Report (DAR).

Editorial Revisions to UFSAR
Editorial changes were made to the following UFSAR Sections for the purposes of consistency, clarification, and correction of typographical errors:
1.2, 3.1., 3.5, 4.1, 4.2, 4.3, 4.4, 4.6, 5.2, 6.2, 6.3, 6.B, 7.5, 7.7, 15.0, 15.1, 15.2, 15.3, 15.4, 15.5, 15.6, 15.A, and Appendix G.

Revision to UFSAR for 125 VDC Bus Ties

UFSAR Subsection 8.3.2.1.1 is revised to extend the use of the 125 VDC ESF Division 1, 2, and 3 bus ties to include battery charger failure, battery charger surveillance, and ground detection, and to reflect the battery testing is performed in accordance with IEEE 450-1980.

Resolution of Issues Involving Errors in UFSAR Containment Analysis
UFSAR Sections 5.4 and 6.2 describe the analytical results of a loss of coolant (LOCA) accident, e.g., recirculation line break or main steam line break within containment, and the specific assumptions used in both the original and 1988 GE containment analyses. The assumption that Feedwater flow instantaneously stops upon accident initiation, while being conservative with respect to peak cladding temperature (PCT) and accident blowdown, is not conservative for analysis of the suppression pool long term temperature. This analysis will be supplemented by including the injection of Feedwater, this will account for the additional mass and energy to the suppression pool and contribute to higher long term suppression pool temperatures. The suppression pool temperature limit in Technical Specification 3/4.6.2.1 was increased from 100°F to 105°F via Amendments 67 and 49, for Units 1 & 2 respectively, in 1988. General Electric provided the supporting calculations that concluded that the allowable temperature increase would have a negligible affect on the accident analyses. However, it was recently identified that two of the assumptions used in both the original and 1988 containment analyses were non-conservative when evaluating post-accident suppression pool temperature response. UFSAR Figure 5.4-5 and Section 6.2 are revised to resolve the Containment Analysis.

Revision to UFSAR Subsection 9.2.1.1.1.a.5
Test data obtained during performance of LaSalle Special Test (LST) procedure LST-97-183 in June 1998 to determine low pressure core spray (LPCS) Motor Cooler heat exchanger thermal heat transfer efficiency was utilized by General Electric (GE) to perform an updated baseline flow requirement using empirical data. The results of the GE heat transfer model indicated that the 4 gpm flowrate stated in UFSAR Section 9.2.1.1.1a.5 was overly conservative for LaSalle Station LPCS Motor Coolers, and that a value of 2 gpm is acceptable with the recommendation that the flow be periodically directly monitored to verify continued adequacy and absence of plugging. The new 2.0 gpm value will be the vendor recommended nominal value. Administratively, penalty factors consisting of Lake level affects and instrument tolerances will comprise the new value specified in procedures LTS-200-27 and LTS-200-10 for the LPCS Motor Cooler flowrate and will be variable based on test methodology utilized.
UFSAR Subsection 9.2.1.1.1.a.5 is revised from to reflect 2 gpm flow for the LPCS Motor Cooler.
Revising the flow balancing bands for Unit 1(2) loads listed in LTS-200-27/29 & LTS-200-10 to encompass the recommendations of Nuclear Design Information Transmittals (NDITs) #LS-0850 & 0854 resulted in the following flowrate changes:
0DG01A, 0 DG Cooling Water Cooler from 970 - 1030 to 1010 (± 20).
1(2)VY04A, NE Cubicle Area Cooler, from 240 - 280 to 240 (± 10)

1VY01A, NW Cubicle Area Cooler, from 190 - 260 to 200 (± 10)
2VY01A, NW Cubicle Area Cooler, from 190 - 230 to 200 (± 10)
1VY02A, SW Cubicle Area Cooler, from 200 - 220 to 185 (± 10)
1E22-S001, 1B DG Cooling Water Cooler from 840 - 860 to 880 (± 20)
1(2)E21-C001, LPCS Pump Motor Cooler from ≥ 4.7 to ≥ 2.8 by timed accumulation flow and Ultrasonics as information only.
Specified upper limit on 0 and 1B DG Cooling Water Cooler Pump Strainer of 300 gpm.

Procedure LTS-200-10 was revised to incorporate:
New LPCS motor cooler CSCS service water flowrate values.
Delete valve throttling repeatability Attachment since cooler is incapable of passing upper flow limit specified.

Of the changes to flowrate values, only the LPCS Motor Cooler Flowrate represents a change to the UFSAR, the others are considered Generic Letter (GL) 89-13 programmatic changes based on recent test data results and system performance trending.
Other administrative (non-intent) changes to LTS-200-27/29 and LTS-200-10, to aid in user performance.

Revision to UFSAR to Reflect Unit 1 Cycle 8 Core Operating Limits (L1C8 COLR) and Reload Transient Accident Analysis (RTAT)
1. Reanalysis of the pressurization transients (including transients analyzed with currently allowed Equipment Out Of Service (EOOS) modes) was required to support a change to the analytical value for the APRM flux scram from 122.4% to 124.2%. This analytical value change was necessary to ensure the APRM flux scram setpoint did not need to be lowered from its current value of 118% to meet the required difference between the setpoint and analytical value calculated under the changed ComEd setpoint methodology. These transient reanalysis have resulted in revised thermal limits, which have been included in the revised COLR.

2. Reanalysis of the pressurization transients (including EOOS modes) was also required to resolve an issue related to operation at less than rated pressure. The original GE transient analyses assumed the plant was at 1005 psig at 100% power, and at lower pressures at reduced power based on GE analytical modeling. ComEd discovered (PIF L1997-07035), and GE concurred, that operation at lower pressures than those modeled by GE are frequently seen at LaSalle during startup and other modes of operation (up to approximately 15# lower), and that this can be non-conservative for some transient analyses. In other words, the GE analytical assumptions for the plant's pressure vs. power operational characteristics were inaccurate. GE re-performed those transients such that they reflect actual plant operation.

3. An error in the generic TCV(s) slow closure EOOS analysis was discovered. The transient applicable to this EOOS condition was reanalyzed to ensure the core thermal limits are bounding. Revised thermal limits are included in the COLR.

The Single Loop Operation flow dependent thermal limits have been modified based on reanalysis of the idle recirculation loop startup event for a revised minimum reactor recirculation flow control valve minimum position. UFSAR Sections 7.7 and 15.A are revised.

UFSAR Revision for Operation with Control Rod Drives with Higher Than Normal Withdrawal Speeds

There are occasions when the withdrawal rate of a control rod drive cannot be adjusted to be within the nominal band of 3.0 ± 20% inches per second via the speed controller on the appropriate directional control valve. The UFSAR presents control rod withdrawal rate (time) limits that reflect the Original Equipment Manufacturer's (OEMs) operational recommendations, 3.0 ± 20% inches per second. Recent evaluations have determined that the maximum control rod drive withdrawal rate may be safely increased to 5.14 inches per second when the Operating Limit Minimum Critical Power Ratio (MCPR) is based upon or exceeds the results of the Rod Withdrawal Error – at Power event analysis.

The maximum control rod withdrawal rate (or travel time) is increased from the 3.6 inches per second to a new maximum of 5.14 inches per second (28 seconds full-travel time) with an administrative constraint. UFSAR Sections 3.1, 4.6, and 15.4 are revised.

UFSAR Revision per Design Change Package (DCP) 9800150

Unit 1 initial start-up included a Mark II containment test to analyze hydrodynamic forces in the suppression pool during safety relief valve (SRV) actuation. Some instruments remain in the suppression pool, which are attached to the suppression pool liner, SRV discharge pipes and quenchers, drywell floor support columns, and drywell downcomers. The suppression pool test installations were to be removed at the earliest convenient opportunity. The instruments were installed prior to 1981, while the test was completed in 1983. The boxes on the drywell floor, the instruments in the suppression pool, and the cables between them are still installed. For maximum visibility for removal, the suppression pool should be drained, which has not occurred since that time. Per DCP 9800150 (Temporary Alteration 1-0069-98), the cables and instruments are to remain installed during plant operation through the remainder of the current Unit 1 fuel cycle until refuel outage L1R08, when they are scheduled to be removed. An engineering evaluation concluded that the original technical and licensing basis for continued operation with the instrumentation remaining installed in Unit 1 containment continues to be valid. UFSAR Sections 1.2, 6.1, and 6.2 are revised.

UFSAR Revision to reflect GE ARTS Analysis and Idle Loop Startup Analysis

UFSAR Subsection 6.B.3.1 is revised to reflect General Electric's APRM – Rod Block Technical Specification improvement program, and for abnormal startup of an idle reactor recirculation loop. The GE ARTS analysis was previously implemented for LaSalle. UFSAR Subsection 6.B.3.1 was not revised during the implementation. Much of the discussion that describes all two loop transients as bounding single loop operation (SLO) transients is changed due to the recently discovered limiting nature of the idle loop startup event.

UFSAR Revision Associated with Automatic Depressurization System (ADS) Logic Change

UFSAR Subsection 7.3.1.2.2.4 is revised to clarify that the manual ADS initiation circuits do not contain interlocks. Additionally, the last sentence of the first paragraph under "Manual Initiation (IEEE 279-1971 Paragraph 4.17)" in UFSAR Subsection 7.A.3.1.1.3 is deleted. The sentence to be deleted reads "The two switches have the a-c interlocks as a permissive." The changes correct wording associated with the manual ADS initiation circuits, and provides consistency with other UFSAR Sections and schematic drawings 1E-1(2)-4201AB and AH. Most of the UFSAR Sections affected by modifications 1-1-84-036 and 1-2-84-069 were revised at the time the modifications were implemented, but wording in Sections 7.3.1.2.2.4 and 7.A.3.1.1.3 was inadvertently missed. The current configuration of the ADS manual initiation circuits is consistent with the design intent and licensing basis approved by the NRC in License Amendments 29 and 27 for Units 1 and 2, respectively.

UFSAR Revision to reflect Design Change Packages 9700564, 9700565, 9700566, and 9700567

Two ventilation intake dampers on the 0, 1A, 1B, and 2A diesel generator (DG) ventilation equipment rooms were modified to include a warm weather manual bypass blade per DCPs 9700564, 9700565, 9700566, and 9700567, respectively. The bypass blades were installed to allow in-leakage of outside air into the DG rooms during the summer per original design. UFSAR Sections 9.4 and 9.5 and drawings M-1444, M-1445, and M-1447 are revised.

Revision to UFSAR Drawing M-69 Sheet 1 per Design Change Package (DCP) 9500360

The DCP replaced the Unit 1 6-inch primary containment ventilation chiller service water condenser Masoneilan control valve 1WS077A with a 10-inch Control Component Inc. (CCI) DRAG control valve. Noise, vibration, and downstream cavitation associated with the operation of the Masoneilan valve has caused erosion of the control valve body and the outlet piping. The CCI DRAG valve is designed to eliminate noise, vibration, and downstream cavitation such that erosion is minimized. UFSAR Drawing M-69 Sheet 1 for the Service Water System is accordingly revised.

Revision to UFSAR Section 9.4.10 for the Containment Purge and Vent (VQ) System
UFSAR Section 9.4.10 is revised to more accurately describe the Containment Purge and Vent (VQ) System. When the function and operating modes of the system was changed prior to initial plant startup, the SAR was not revised to reflect the changes. This change reflects the use of the system for containment purge during power operation, and identifies the potential failure of the VQ ductwork should a LOCA occur during containment purging operations at power.

Relocation of Certain Fire Protection Requirements from the Technical Specifications to the UFSAR
Unit 1 License Amendment 127 and Unit 2 License Amendment 112 relocated certain requirements of the Fire Protection program from the Technical Specifications to the UFSAR. The relocated Technical Specifications are 3/4.3.7.9, Fire Detection Instrumentation; 3/4.7.5, Fire Suppression Systems; 3/4.7.6, Fire Rated Assemblies; and 6.1.C.4, Fire Brigade Staffing. UFSAR Section 9.5 is revised.

UFSAR Change resulting from Design Change Package (DCP) 9700397, Turbine Building Supply Airflow Reduction for Turbine Building Negative Pressure
The DCP reduced the supply air to the Turbine Building to ensure a negative pressure is maintained by installing two recirculation dampers on the common supply header of the turbine building ventilation (VT) system supply fans 1VT01CA, 1VT01CB, and 1VT01CC. The dampers are installed in the supply air header before it penetrates the VT system supply air housing. UFSAR Sections 9.4, 11.3, and turbine building ventilation system drawings M-1459 sheets 1, 2, and 3 are revised.

UFSAR Revision per Design Change Package (DCP) 9600285, Elimination of Unit 1 Main Steam Isolation Valves Closure and Scram Functions of the Main Steam Line Radiation Monitors
The DCP improves unit availability by reducing spurious scrams and isolations caused by the Main Steam Line Radiation Monitors (MSLRMs). The original design function of the MSLRM was for detection/mitigation of consequences associated with fuel failure and the rod-drop design basis accident. The DCP consisted of the following: removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Protection System (RPS) Reactor Auto-Scram Trip logic circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Main Steam Line (MSL) Isolation and Drain Valve circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Water Sample Valve circuits and associated Normal/Test Selector Switches in Main Control Room (MCR) Panels, revising MSLRM's High and High-High alarm setpoints, rewiring MSLRM alarms per recommendation of ComEd Human Factors Group and Operations, rewiring computer digital inputs and outputs associated with the MSLRMs, revising off gas pre-treatment radiation monitor High and High-High alarm setpoints, and Add appropriate safety-related banana plugs per ComEd recommendation to one terminal at relays located in

the Main Control Room panels. UFSAR Sections 1.2, 7.1, 7.2, 7.3, 7.6, 7.7, 7.A, 11.5, and 15.2 are revised.

UFSAR Revision per Design Change Package (DCP) 9700350
The DCP revised the Control Room and Auxiliary Electric Equipment Room ventilation (VC and VE systems, respectively) manual purge control circuit for Train A, so that the following functional changes take place in the Purge Mode when smoke is detected in the control room:
Maximum outside air dampers 0VC08YA, 0VC53YA, 0VE05YA, and 0VE30YA close; Exhaust air dampers 0VC14YA and 0VE04YA close; and return air dampers 0VC10YA and 0VE03YA open. The DCP interlocks the outside smoke (ionization) detection system to the isolation dampers used during purging in order to achieve automatic realignment to pressurization mode upon detection of smoke in the outside air. UFSAR Drawing M-3443 Sheets 5, 18, and 24 are accordingly revised per ECN 001284E.

Revision to UFSAR Subsection 12.3.4.2 and Table 12.3-17 on Continuous Airborne Radioactivity Monitoring Instrumentation.
The specified flowrate for the Continuous Air Monitors (CAM) in UFSAR Section 12.3.4.2 is revised from "3 to 10 cfm" to "2 to 10 cfm", and Table 12.3-17 is revised to state that the CAM setpoints for the high radiation alarm are based on two times 100% power background. These changes provide consistency between continuous airborne radioactivity monitoring instrumentation and plant conditions.

UFSAR revisions per Design Change Package (DCP) 9200145 and Design Change Approval Letter Addendum #2 for ECN 001508M.
The DCP disconnected and capped the air supply to inlet valves for the "A" and "B" concentrator waste tanks to allow the valves to be maintained normally closed. The original administrative controls on the inlet valves were eliminated, the air supply to the valves disconnected and the air cylinders associated with each valve vented to ensure that the inlet valves remain closed as detailed in ECN 001508M. UFSAR Subsection 11.2.2.5.5 and drawing M-103 Sheet 14 are revised.

UFSAR Revision per Unit 1 Design Change Package (DCP) 9100236 Permanent Installation of Existing Transient Analysis Data System (TADS) Panel.
The TADS panel 1PA19J had been previously located in the AEER until it was identified that the panel was not seismically mounted (LER 97-027). The DCP permanently installed the TADS Panel 1PA19J and the associated nine (9) interconnection cables inside Unit 1 Auxiliary Electrical Equipment Room (AEER). UFSAR Figure H.4-1 is revised to show the location of the TADS panel 1PA19J in the AEER.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9500399 - CRD HCU Scram Air Pilot Solenoid Valves flexible air hose installed.
The original copper tubing between the Scram air header and the Scram solenoid pilot valves was replaced. The DCP installed flexible hoses in the air supply piping to the Control Rod Drive (CRD) Hydraulic Control Unit (HCU) SCRAM Air Pilot Solenoid Valves 1C11-D001-117 and 1C11-D011-118. The air supply stop valve (1C11-D001-116) was relocated closer to the air supply header (1RD52B-3/4"). UFSAR Appendix H Section H.3.2.6, Table H.3-2, and drawings M-100 Sheet 2 (ECN 000571M) and Sheet 3 (ECN 000571M) are revised accordingly

UFSAR revisions per Design Change Package (DCP) 9600528, Unit 1 Heater Bay Cooling Modification
The DCP modified the turbine building ventilation system to provide cooling to the area of the turbine valves' electro-hydraulic controls (EHC) in the turbine building low pressure heater bay. Two new 10,000 cfm vane axial fans (1VT14C and 1VT15C) were installed in the low pressure heater bay. Discharge ductwork from the fans was routed to the vicinity of the EHC controls for the turbine control valves, the turbine stop valves, and the main steam bypass valves to provide additional cooling air to reduce the temperature and thermal stratification in this area.

Revision 1 of the DCP approved the change in fan power supply location from MCC 133B-2 Compartments D3 and D6 to Compartments D3 and D2. UFSAR Table 9.4-13 and drawings M-INDEX Sheet 2, M-9 and M-1459 Sheet 2 are revised.

UFSAR revisions per Unit 1 Design Change Packages (DCPs) 9600216 and 9600217 - Changes to the Turbine Building Ventilation system to improve ventilation in the 1A/1B Turbine Driven Reactor Feedwater Pump (TDRFP) cubicle
The DCPs installed vane axial fans (1VT13CA and 1VT13CB) and associated ductwork over the existing floor openings in the Unit 1 'A' and 'B' TDRFP rooms to create a forced transfer of air from the pump room to the heater bay below. This change improved air circulation and heat removal capacity of the VT system in the TDRFP room and reduced the room temperature. The original safety evaluation was revised to address installation of backdraft dampers (1VT104Y and 1VT105Y) in the blowout panels (57 and 60) between the turbine operating deck and the pump room. Addendum 2 to DCP 9600216 and DCP 9600217 incorporated a revised safety evaluation into the DCP along with revising the ECN backup calculation list to reference additional calculations for the mounting of the backdraft dampers. The Addendum letter did not impact the previously identified UFSAR changes or necessitate additional UFSAR changes.
UFSAR subsections H.3.5.1, H.3.5.3, Table 9.4-13 and drawings M-INDEX Sheet 1, M-7, and M-1459 Sheet 2 are revised.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9600197 and Modification Approval Letter – Addendum No. 1 - Revised Reactor Water Level (RWL) Feedwater control selection circuitry.
The DCP 9600197 replaced two-position selector switch 1C34A-S001 in Main Control Board panel 1H13-P603 with a three-position selector switch and installed required wiring connections to provide one-out-of-three channel selection capability for RWL monitoring circuits. The DCP also removed local and remote channel selected and channel out of service indication and associated pushbutton switches, indicating lights, and fuses.
The changes identified in the addendum did not affect the conclusion of the original safety evaluation; however, a new safety evaluation was performed to identify additional UFSAR changes. UFSAR subsection 7.7.4.2, Figure 7.7-5 Sheet 1 and drawing 1E-1-4603AP (revised via ECN 000941E) are accordingly revised.

UFSAR revisions per Design Change Package (DCP) 9600090 - Chiller addition into Station Heat (SH) Recovery System for Turbine Building Ventilation cooling.
Chillers, pumps, instrumentation and associated piping were added to provide cooled glycol into the Turbine Building Ventilation (VT) and Reactor Building Ventilation (VR) system heating coils through the Station Heat Recovery system. This DCP provides an alternate cooling source to the original evaporative coolers, which have proven to be unreliable and difficult to maintain, and provides a more reliable cooling system with added heat removal capability.
UFSAR sections 6.2.3, 9.2.10, 9.4.2 and 9.4.4 are revised as a result of this DCP.

UFSAR revisions per Design Change Package (DCP) 9700594 - Main Control Room (MCR) and Auxiliary Electric Equipment Room (AEER) Penetration Seals (Addendum #8 and Engineering Change Notice (ECN) 001416S).
The original ECN and DCP provided alternate generic penetration sealing material and methods for the purpose of reducing air leakage from the outer envelopes of the MCR and AEER to adjacent areas. The volume of air leakage from the MCR and AEER is one of the contributing factors to the inability of the VC/VE systems to maintain their respective areas at the 1/8" water column (WC) positive pressure with respect to surrounding areas as required by the UFSAR. Addendum #8 to the Design Change Approval Letter was issued to provide clarification regarding alternate materials used for coating exiting gypsum cement floor penetration fire seals in response to Offsite Review Report No. 01-98-070.
UFSAR Section H.1.3 and Figure H.1-1 are revised to mention the option of coating the fire seals utilized at the top of concrete block walls in seismic structures with Vimasco 3IR cable coating air seal.

UFSAR revisions per Design Change Package (DCP) 9700551 - Reroute VE Ductwork from Computer Room to Units 1 & 2 Auxiliary Electric Equipment Room (AEER); (Addendum #2, Addendum #6, Addendum #8, Engineering Change Notices (ECNs)

001388H, 001392H, 001384E, and Supplemental Engineering Change Notice (ECN) 001392H-01 and 001392H-02).
The DCP created temporary access openings in the west wall of the duct chase near column 'R' and line '15' in the auxiliary building at floor elevations 768' and 749'. This allowed removal of the VE system supply and return air duct runs which service the computer room, along with their associated duct supports. New duct runs and duct supports from the existing VE supply and return ducting were installed to service Units 1 & 2 AEERs. Wall mounted and ceiling mounted lighting fixtures, emergency battery packs, a PA system horn with box, electrical conduits, fittings and associated supports were removed and relocated to facilitate the new duct installation. The temporary access openings in the duct chase were closed following completion of the construction work. This design provides new flow paths to serve both AEER and enhances the VE system in meeting its cooling and pressurization requirements for habitability and alleviates system performance problems.
Supplemental ECN 001392H-01 abandoned in place duct heaters 0VE03AA and 0VE03AB and disconnected the associated heater controls located in the section of duct that now serves the AEER.
With the extensive changes made to the VC/VE system, the system will balance and operate with flowrates that are different from the design flowrates given on the Piping & Instrument Diagrams (P&IDs). Therefore, calculated minimum and maximum flowrates supporting system requirements were established. Supplemental ECN 001392H-02 was issued to document the changes to the fan blade pitch settings for fans 0VE01CA/CB and 0VE02CA/CB to establish the design flowrates and the revised acceptance criteria for the modification testing. UFSAR Section 9.4.1.2 is revised to delete reference to the VE system supply and return interfacing with the computer room. UFSAR Drawing M-1443 Sheets 3 & 4 are revised to delete the return duct from the computer room to the VE return system. A new drawing (M-1467 Sheet 3) is added to the UFSAR to reflect that the supply duct from the VE supply to the computer room is deleted. The new flow path for the additional VE supply and return to both AEERs is added to these drawings. UFSAR Section 9.4.1.2.2, Table 9.4-3, and Drawing M-1443 Sheet 4 are revised to show 0VE03AA/AB are abandoned in place, and UFSAR Drawings M-1443 Sheets 1 through 4 are revised to include clarifying information on airflow rates for the VC/VE system duct segments to support system testing and balancing.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700532 - High Energy Line Break (HELB) Leak / Break Detection Modification.
The DCP modified the Leak Detection System for the Reactor Water Cleanup (RWCU), Reactor Core Isolation Cooling (RCIC), and the Residual Heat Removal (RHR) systems to resolve a concern identified with the original Leak Detection calculations (PIF L1997-04896 and LER 1-97-031-00). The modifications generally consisted of temperature sensor relocation, addition of temperature monitoring functions, and addition of a high flow monitor for HELB. An design change addendum was issued (addendum #3) to include the changes to the values and basis for the proposed RWCU pump suction high

flow that are described in the supplemental Technical Specification Amendment Request (OSR 98-204). The setpoint used in the instrument loop is 550gpm +/-2.0gpm. UFSAR Sections 1.2.2.6.6, 1.7, 3.1.2.2.4, 3.1.2.4.1, 5.2.5.1, 5.2.5.1.2, 5.2.5.2, 5.2.5.4, 5.2.5.5.4, 5.2.5.6, 5.4.7.3.1, 7.3.2, 7.4.1.2.6, 7.6.2.2.4, 7.6.2.2.5, 7.6.2.2.6, 15.9.3.4, H.3, Table 5.2-8, Table 7.3-2, Figure 7.3-7, and Drawings M-155 and M-2097 are revised accordingly.

UFSAR Revisions per Unit 1 Design Change Package (DCP) 9700519 and DCP 9700520 for Replacement of Limitorque Actuator and Motor on Motor Operated Valves 1G33-F001 and 1G33-F004
DCP 9700519 replaced the existing 15 ft-lb. SMB-0 actuator on Valve 1G33-F001 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed through containment penetration E-6 to provide power to the motor operated valve and the molded case circuit breakers (2) and thermal overload relay were replaced.
DCP 9700520 replaced the existing 15 ft-lb. SMB-0 actuator on Valve 1G33-F004 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed to provide power to the motor operated valve and the molded case circuit breaker and thermal overload relay were replaced.
UFSAR Table 6.2-28, Table H.4-14, Table H.4-17 and Table H.4-48 along with Unit 1 Administrative Technical Requirements (ATR) Table 3.6.3-1 are accordingly revised.

UFSAR revisions per Unit 1 & 2 Design Change Package (DCP) 9700504 for VC/VE "B" Train Condenser Bypass Damper – Snow Mitigation.
The original modification (DCP 9700504) provided a VC and VE (Train "B") refrigeration condenser unit fan recirculation flow path to allow continued condenser operation without opening the plenum door and preventing fan operation in an unstable region of the fan curve. Addendum #4 identified modification testing requirements for DCP 9700504. During testing activities, not all of the acceptance criteria were met. Calculation L-001992, "Minimum Airflow for the VC/VE Air Cooled Condensers," was performed to evaluate the minimum requirements for airflow through the condenser during the different tested conditions. The results were issued as Addendum #5 and the safety evaluation was revised to include the calculation as a reference and to reflect the minimum airflow rates to be used as acceptance criteria in the airflow testing.
UFSAR Sections 9.4.1.1.2c and 9.4.1.2.2c are revised.

UFSAR changes per Design Change Package (DCP) 9600214 Demolition of Train 'A' Electrical and Train 'A'/'B' Mechanical of the VC/VE Humidification System and Auxiliary Electric Equipment Room (VE) HVAC Systems
This DCP removed humidification equipment from the Control Room (VC) and Auxiliary Electric Equipment Room (VE) HVAC systems. The Mechanical portions of the 'A' & 'B' trains and the electrical portion of the 'A' Train were removed because the existing

humidification equipment, including the steam boilers, had been out of service for an extended period of time due to various system problems. Additionally, the humidifiers and associated piping were not seismically supported.
UFSAR Sections 6.4, 7.3.4, 9.4.1, Table 9.4-1, Table 9.4-3 and Drawings M-105 sheet 1, M-1443 Sheet 2, M-1443 Sheet 4, M-3443 Sheet 2, and M-3443 Sheet 21 are accordingly revised to reflect the removal of the VC and VE steam humidification equipment.

UFSAR Revision per Design Change Package (DCP) 9700351, "VC/VE Manual Purge Control Circuit Logic Change – 'Train B'."
The DCP revised the Control Room and Auxiliary Electric Equipment Room ventilation (VC and VE systems, respectively) manual purge control circuit for Train B, so that the following functional changes take place in the Purge Mode when smoke is detected in the outside air:
Maximum outside air dampers 0VC08YB, 0VC53YB, 0VE05YB, and 0VE30YB close; Exhaust air dampers 0VC14YB and 0VE04YB close; and return air dampers 0VC10YB and 0VE03YB open. The DCP interlocks the outside smoke (ionization) detection system to the isolation dampers used during purging in order to achieve automatic realignment to pressurization mode upon detection of smoke in the outside air.
UFSAR Drawing M-3443 Sheets 5, 18, and 24 are accordingly revised per ECN 001285E.

UFSAR Revisions per Unit 1 Design Change Package (DCP) 9700343, "Generic Letter (GL) 96-06 Overpressure Protection for Reactor Recirculation Containment Penetration M-36 Piping."
This DCP installed a ¾" diameter bypass line, including a check valve and a manual isolation globe valve, around the existing Inboard Containment Isolation Valve 1B33-F019 to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the bypass check valve will prevent potential over-pressurization during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event.
UFSAR Section 6.2.4.2.1, Table 3.2-1, Table 5.2-6 Sheet 2, Table 6.1-1, Table 6.2-21 Sheet 2A and 2B, Table 6.2-28 Sheet 1 and Drawing M-93 Sheet 2 are revised accordingly. UFSAR Figure 6.2-31 Sheet 10D (new figure) was added and Administrative Technical Requirements (ATR) Table 3.6.3-1 was revised.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700339, "Generic Letter (GL) 96-06 Overpressure Protection for Penetration Piping.
This DCP added two ¾" diameter relief valve assemblies between containment penetrations M-16 and M-17 and existing inboard containment isolation valves 1WR179 and 1WR180 to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the relief valves will prevent potential over-pressurization during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event.

UFSAR Section 6.2.4.2.2, Table 6.2-21 Sheets 1A and 1B, Table 6.2-28 Sheet 7, Figure 6.2-31 Sheet 2 and Drawing M-90 Sheet 2 were revised accordingly. Administrative Technical Requirements (ATR) Table 3.6.3-1 was revised.

UFSAR revision per Design Change Package (DCP) 9700461 - Removal of Unit 1 Main Steam Isolation Valve (MSIV) Closure Scram Bypass Pressure Switches.
This DCP disconnected and removed the existing MSIV closure bypass pressure switches 1B21-N020A, 1B21-N020B, 1B21-N0202C, and 1B21-N020D along with the associated tubing, valves and fittings from instrument racks 1H22-P004, 1H22-P027, 1H22-P005 and 1H22-P026 respectively. The cables between the instrument racks and the main control room (MCR) panels were de-terminated and left in place unassigned, and the associated terminal points in the MCR panels were jumpered.
UFSAR Sections 7.2.2.4.6, 7.A.2.1.2, 7.A.2.1.14, 7.A.3.2, 15.2.4, Figure 7.2-1 Sheets 2 and 3, and Drawings M-93 Sheet 4 and Sheet 5 are revised accordingly.

UFSAR Revisions per Unit 1 Design Change Package (DCP) 9400064 and Addendum – "Installation of Continuous Oxygen Monitor."
This DCP removed the existing drywell humidity monitoring system (trains A & B) and installed a new continuous oxygen monitoring system for sampling suppression chamber air and drywell air. The existing drywell sample line was reused. The existing return line to the suppression chamber was rerouted to a new containment penetration and will be used as a sample line to obtain the suppression chamber sample.
This design change installed a dedicated system to continuously monitor suppression chamber and drywell oxygen concentration and eliminated the use of the Post-LOCA containment monitoring system for drywell oxygen concentration monitoring during normal plant operation. The drywell humidity monitoring system was removed because it was not performing properly and there are no regulatory requirements for such a system.
UFSAR Section 1.7 and Tables 3.8-1 Sheet 6, and 6.2-21 Sheets 4C, 4D, 6A and 9A are revised accordingly by the DCP and an Addendum.

Revision to UFSAR Subsection 11.3.3 per Unit 1 Design Change Package (DCP) 9700530 – Modify VR Flow to the RT Pump / Valve Rooms.
The design change replaced the existing Reactor Water Cleanup (RWCU) pump room pneumatic controlled balancing dampers (1VR16Y, 1VR17Y, & 1VR18Y) with smaller manual controlled balancing dampers (1VR84Y, 1VR85Y, 1VR86Y, 1VR87Y, 1VR88Y, & 1VR89Y). The air regulators, temperature controllers, and actuators on the existing dampers were removed from the affected areas. The instrument air line to the regulators was cut and capped. The design change also installed and balanced new manual controlled balancing dampers (1VR80Y and 1VR81Y) in the associated ductwork outside of the RWCU pump rooms, along with balancing (adjusting) flow through existing manual controlled balancing dampers in several areas. Additionally, the duct to wall penetrations between the existing RWCU pump rooms were sealed.

The design change was made to revise the variable exhaust flow in the RWCU pump rooms to the revised new fixed flows. The installation of the additional new manual controlled balancing dampers and the balancing of the dampers in the associated valve and heat exchanger rooms assures proper flows throughout the area.
UFSAR Subsection 11.3.3 is revised to indicate the new ventilation system capacity of 110,800 scfm.

UFSAR revision to reflect Unit 1 Design Change Package (DCP) 9700130, Replacement of Unit 1 Loose Parts Monitoring System (LPMS)
The DCP removed the loose parts monitoring equipment from panel 1PA15J and replaced it with a new state-of-the- art data acquisition system manufactured by Siemens Power Corporation. The new equipment is designed to work with existing accelerometers and preamplifiers (charge converters), and the existing annunciator system and power supply. The previous LPMS did not conform to the configuration described in the SER and the response to FSAR Question 221.14. UFSAR Section 4.4.6 is revised by adding Section 4.4.6.1 to include a description of the installed upgraded LPMS configuration applicable to Unit 1.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700335 and DCP 9700336, "Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-25(M-26) and M-27(M-28)."
These DCPs installed ¾"x1" relief valves on the Primary Containment Penetrations M-25(M-26) and M-27(M-28) piping between the primary containment penetrations and the inboard isolation valves 1VP113A/B and 1VP114A/B to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the relief valves will prevent potential over-pressurization of the piping between the PCIS valves during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event.
UFSAR Section 6.2.4.2.2, Table 3.2-1, Table 6.2-21 Sheets 1C and 1D, Table 6.2-28 Sheet 7, Figure 6.2-31 (new figure) and Drawing M-86 Sheet 1 are revised accordingly. Administrative Technical Requirements (ATR) Table 3.6.3-1 is revised.

UFSAR revisions per Design Change Package (DCP) 9700310, "Auxiliary Electrical Equipment Room (AEER) Ventilation System – Return Air Isolation Damper Replacement."
This DCP replaced the existing AEER HVAC return fans' isolation dampers (0VE06YA and 0VE06YB) with new dampers. The new dampers were installed in the ductwork upstream of the AEER Return Air Fans 0VE02CA and 0VE02CB. The new dampers will enhance the performance and reliability of the VE system by improving the maintainability of the damper once installed. The existing dampers were left in place to serve as manual isolation dampers and assigned new EPN numbers (0VE66YA and 0VE66YB).
UFSAR Section 3.11.4.1, Table H.4-4, Table H.4-101 and Drawing M-1443 Sheet 3 are revised accordingly.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700302, "ECCS Suction Strainer Replacement Modification."
The DCP replaced the existing suction strainer on the RCIC suction line in the suppression pool with a larger capacity strainer to reduce pump Net Positive Suction Head loss due to accumulated strainer debris resulting from a design basis line break LOCA. The existing strainer was replaced to increase the surface area of the strainer and thus increase the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03.
UFSAR section 15.9.3.7 and Drawing M-101 Sheet 2 are revised to reflect the strainer replacement.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700419 – "Heater Drain Pump Minimum Flow Changes to Facilitate Idle Pump Warm-up."
The DCP added the controls necessary to utilize the Heater Drain (HD) pump minimum flow bypass line to facilitate warm-up of an idle HD pump by permitting a higher flow rate in the minimum flow line for a short time period upon pump start-up. The design change was implemented to reduce the potential loss of the unit (at high unit power) due to Feedwater heater string isolations and resulting transients in the Feedwater pump suction.
UFSAR Section 10.4.7.2, and Drawing M-61 Sheet 2 are revised accordingly.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800004, "Emergency Diesel Generator 1B Speed Sensor."
The station's diesel generators have recently experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 1B emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch.
UFSAR Section 1.7, Electrical, Control and Instrumentation drawings, is accordingly revised per DCP 9800004.

UFSAR revisions per Document Change Request (DCR) 980716
The reactor building evaporative coolers have never worked effectively, are high cost maintenance items, and have not been used for some time. The evaporative cooler spray pumps are currently controlled by Out Of Service (OOS) #960001935. UFSAR Sections 6.2.3.2, 9.4.2.1.2, 9.4.2.2, Table 9.4-5, and Drawing M-1455 Sheet 1 are revised.

UFSAR revisions per Design Change Package (DCP) 9800044, "Modification of the Control Room Toilet Exhaust Fan Ductwork."
This DCP changed the existing configuration for the Main Control Room (MCR) toilet exhaust air system from a direct exhaust that vents to the Turbine Building to a recirculation system with a filter that returns air to the toilet area. The current arrangement of VC system MCR toilet exhaust air ductwork interfaces with the Turbine Building which could allow steam to enter the MCR and affect its habitability during a main steam line break in the Turbine Building.
The existing wall grille in the Turbine Building and fire damper 0VC39Y was removed and discarded and the duct penetration opening filled with concrete grout. Duct sections were cut, removed and end caps were installed on the duct that was abandoned in place. The ducting from the MCR toilet exhaust fan (0VC06C) was rerouted above the toilet room drop ceiling to reenter the toilet room and terminate in a charcoal filter assembly. This DCP eliminated the interface between the MCR and the Turbine Building main floor.
UFSAR Sections 6.4.2.3, 6.5.1.1.2.c, 9.4.1.1.1.1.g, and 9.4.1.1.2.b are revised to delete the reference to providing makeup air for toilet exhaust. Drawing M-1443 Sheet 2 is revised to reflect the changes to the system.

UFSAR revisions per Document Change Request (DCR) 980529, "As-built Hose Racks per Engineering Request (ER) 9707865."
Nineteen (19) hose racks were installed on various concrete and masonry walls in the plant using expansion anchors (reference CHRON letters 123650 and 115241) as a method to promote good housekeeping and safety by providing a place to store miscellaneous hoses when not in use. Many of the affected walls serve as fire barriers and the new hose storage increased the combustible loading in zones identified in the UFSAR. The DCR was issued to revise the affected sections of the UFSAR.
UFSAR Appendix H.3 and Table H.3-2 are revised to reflect the additional combustible loads for each affected zone.

UFSAR revision per Design Change Packages (DCP) 9700058 and DCP 9700059, "Revise Logic & Wiring for VC System Radiation Monitors (Trains A & B).
These DCPs removed the electrical connection that existed between the two trip systems in train 'A'('B') located in Main Control Room Panel 0PM14J (0PM15J). Output contacts from relays 1(2)D18-K751A and 1(2)D18-K751B were wired in series to comprise Trip System 1. Output contacts from relays 1(2)D18-K751C and 1(2)D18-K751D were wired in series to comprise Trip System 2. The output contacts from both channels of a trip system must close in order to energize the isolation relay logic for a given train. The previous configuration did not meet single failure criteria and would prevent an isolation from being initiated when required (ref. LER 96-021-01).
UFSAR Sections 6.4.4, 7.3.4.3.11 and 9.4.1.1.3 are revised to reflect the design change.

UFSAR revision per Design Change Package (DCP) 9800148, "Abandoning Main Steam (MS) Supply to Radwaste Reboiler 1AS01B.
The DCP modified main steam line 1MS41A-3" by removing a section of pipe by cutting and capping it in two locations. This isolated the main steam supply to Unit 1 Radwaste Reboiler 1AS01B. This reboiler is no longer used and is slated for abandonment.
UFSAR pending change section 3.1.2.6.1 is revised to delete reference to evaporators (Unit 1 only) and UFSAR pending change 11.2.2.3 is revised to delete reference to evaporators/bypass and indicate the use of a vendor system to process liquid Radwaste (applicable to Unit 1 only).

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800139, "Replace 1B21-F569, Add Tee and Test Connection Assembly."
This DCP replaced existing isolation valve 1B21-F569 with a similar valve and added a test connection to provide an alternate method for testing the excess flow check valve 1B21-F571. A tee with two isolation valves and a cap was added between 1B21-F569 and 1B21-F571 to permit testing of 1B21-F571.
UFSAR Table 6.2-21 Sheet 1C was revised to reference new detail, Figure 6.2-31 (new sheet 10D) was added to show a new detail reflecting the addition of the tee valves and cap, and Drawing M-93 Sheet 5 was revised to add the tee and branch line with valves and cap.

UFSAR Drawing Revision per Design Change Package (DCP) 9600300 – Revise Reject Line High Pressure Alarm Circuit.
Spare limit switch "IO" contacts on condenser valve 1G33-F034 and Radwaste collector valve 1G33-F035 were wired to the alarm circuit of existing pressure switch 1G33-N014 to disable the high pressure alarm when both valves are closed. New cables were routed from the valve limit switches to local panel 1H22-P002 and the alarm circuit in local panel 1H22P002 was rewired to obtain the required logic.
UFSAR Drawing M-97 Sheet 1 is revised to include dashed lines to indicate an interlock between the high pressure alarm and the F034 and F035 valves.

UFSAR Revision to reflect Design Change Package (DCP) 9600147 – Condensate Booster (CB) Pump Minimum Flow Loop Upgrade Design.
The DCP replaced the existing modulating Condensate Booster pump minimum flow valve pneumatic control loop for each of the CB pumps 1CB01PA, 1CB01PB, 1CB01PC, and 1CB01PD with ON-OFF control using a flow transmitter, trip unit interlock and a Main Control Room switch. With the current system control in AUTO, excessive and rapid valve cycling occurs. The new design increases the operability and reliability of the CD/CB minimum flow control loop.
UFSAR Drawings M-58 Sheet 1 and M-59 are revised to reflect these changes.

UFSAR Revision to reflect Design Change Package (DCP) 9600091 – Cooling Water Tie Into Station Heating (SH) for Turbine Ventilation (VT) Cooling.
The DCP replaced an existing elbow associated with the VT Supply Coil Floor Drain piping (SH system) with a hydrolyzing port consisting of a tee, spool of pipe, and cap to provide a means for hydrolyzing the section of the Unit 1 VT Floor Drain piping from the floor drain to its tie in to the drain header.
UFSAR Drawing M-102 Sheet 11 is revised to identify the new hydrolyzing port on the VT Supply Coil Floor Drain pipe.

UFSAR Revision to reflect Drawing Change Request (DCR) #980441.
New P&ID drawings were created to depict each Reactor Recirculation (RR) Hydraulic Power Units (HPU), using symbols consistent with the standards used at LaSalle, and added EPNs. Currently, the P&IDs depict the HPUs as a box with a note on the drawing directing the reader to vendor drawings for details. Additionally, UFSAR sections are revised to reflect the correct Figure reference.
UFSAR Section G.5.2.3.4 is revised to reference Figure G.5.2-1; Section G.5.2.3.4.9.1 and G.5.2.3.4.9.2 are revised to reference Figure G.5.2-2 and Drawings M-93 Sheets 1 and 2 and M-139 Sheets 1 and 2 are revised to reflect the HPUs.

UFSAR changes per Unit 1 Design Change Package (DCP) 9800135, "Install New Support on the Cooling Water Lines to the LPCS Motor, Remove Thermowell and Associated Temperature Indicator on Line 1DG23A."
This DCP added two gang hang supports to the cooling water supply and return lines for the Low Pressure Core Spray (LPCS) motor and eliminated the thermowell 1TEW-DG032 and associated temperature indicator 1TI-DG032 on line 1DG23A. One gang hang support was added to prevent an overstress condition on the pipes coming out of the LPCS motor (reference PIF L1998-03710). The other gang hang support was added to prevent an overstress condition on 1" carbon steel supply and return lines (reference PIF L1998-03806). The thermowell was removed to eliminate the flow obstruction it presented.
UFSAR sections 9.2.1.5, 7.3.3.3.1, and drawing M-87 Sheet 2 are revised to reflect the changes.

UFSAR Changes per Design Change Package (DCP) 9500483 – Install Filter in 1FW01KA/B Turbine Driven Reactor Feed Pump (TDRFP).
This DCP added in-line filters to the high pressure control and hydraulic oil piping just before the TDRFP turbine controllers. One duplex filter was added to each TDRFP 1FW01KA & B. This new filtration system will trap particles that could affect the hydraulic operation of the turbine speed controller and the turbine drive trip spool. Additionally, new differential pressure indicators were added outside the TDRFP room walls to minimize dose to personnel. Revision 1 of the safety evaluation removed the 'Hold' for calculation L-001430 and L-001509 and removed the requirement to simulate a 12 psid pressure across the on-line filter during the filter swap test.

UFSAR Section 9.5.1 and Drawings M-INDEX Sheet 1 and M-7 are revised to reflect this change.

Revision to UFSAR Drawing M-69 Sheet 1 per Design Change Package (DCP) 9500363
The DCP replaced the Unit 1 6-inch primary containment ventilation chiller service water condenser Masoneilan control valve 1WS077B with a 10-inch Control Component Inc. (CCI) DRAG control valve. Noise, vibration, and downstream cavitation associated with the operation of the Masoneilan valve has caused erosion of the control valve body and the outlet piping. The CCI DRAG valve is designed to eliminate noise, vibration, and downstream cavitation such that erosion is minimized. UFSAR Drawing M-69 Sheet 1 for the Service Water System is accordingly revised. (Reference NTS 373-160-98-00148 (DCP 9500360) for same USFAR Drawing Change)

UFSAR Drawing M-86 Sheet 1 revised per Design Change Package (DCP) 9500283 – Primary Containment Chilled Water (VP) System Hold up & Expansion Tank Water Level Control/Alarm Design Change.
The DCP revised the High/Low level alarm, and the automatic makeup Start/Stop setpoints for the VP system expansion tanks (1VP01TA/TB). The high level alarm switch ((1LSH-VP071) on the 8-inch vent line of the holdup tank (1VP02T) was raised higher on the vent line and the setpoint revised accordingly. A new drain-back line was installed from the holdup tank vent pipe to the vent pipe of the 'B' expansion tank along with a new support to stabilize the holdup tank vent line. This design change eliminates unnecessary drawing of clean condensate water through the makeup lines to the VP expansion tanks.
UFSAR Drawing M-86 Sheet 1 is revised to incorporate the changes discussed.

Unit 1 & 2 Design Change Package (DCP) 9700314 for VC/VE "A" Train Condenser Bypass Damper – Snow Mitigation (Design Change Approval Letter Addendum #4), and UFSAR revisions.
The original modification provided a VC and VE (Train "A") refrigeration condenser unit fan recirculation flow path to allow continued condenser operation without opening the plenum door and preventing fan operation in an unstable region of the fan curve. Addendum #4 identifies performance of an additional calculation (L-001925) to verify the acceptability of the negative static pressure within the condensing unit due to potential snow/ice blockage across the coils. The calculation determined that the coil and support members for the condensing units are adequate for the differential pressure load of approximately 9 inches of water, maximum ice load of 1 inch thickness over 80% of the coil area and seismic effects. There was no physical work associated with this addendum. UFSAR Sections 9.4.1.1.2c and 9.4.1.2.2c are revised.

Editorial Revision to UFSAR Subsection 6.2.4.2.3
The ending text of UFSAR Subsection 6.2.4.2.3 was inadvertently deleted during the preparation of the UFSAR Revision 11 update. The UFSAR contains an incomplete discussion of Subsection 6.2.4.2.3 (Evaluation against General Design Criterion (GDC) 57). This change restores the original text.

Revision to UFSAR drawing per Design Change Package (DCP) 9700056 – "Repair / Replacement of Degraded Duct Sections of VE."
This DCP replaced two damaged sections of ductwork between HVAC hangers S-521 and S-519 (col. 10/row L, elev. 786'-6"), replaced a buckled horizontal wye duct fitting upstream of dampers 0VE06YA and OVE06YB and replaced duct sections on the discharge side of fan 0VE02CA. The DCP also replaced damaged sections of ductwork located above elev. 786'-6" in the Auxiliary Building and repaired sections of HVAC ductwork on the VE system along with other miscellaneous repairs.
UFSAR Drawing M-1443 Sheet 4 is revised to reflect the changes.

Revision to UFSAR drawing per Design Change Package (DCP) 9700316 – "Replacement of Double Block Valve 1B33-F021/F022."
This DCP replaced the existing Anderson/Greenwood stainless steel double block valve (1B33-F021/F022) with two low carbon content stainless steel Y-Pattern globe valves installed in series. The design change was performed because the existing double block valve leaked by its seats with the pipe end cap removed and the Anderson/Greenwood valve is obsolete and parts are no longer available to repair it.
UFSAR Drawing M-93 Sheet 2 is revised to change the drawing from the existing double block valve to two Y-Pattern globe valves.

Revisions to UFSAR drawings per Design Change Package (DCP) 9700069 – "Replacement of Continuous Air Monitors 1PL15J &1PL75J (Phase I)."
This DCP completed the preliminary work to support replacement of the existing Continuous Air Monitor panels 1PL15J and 1PL75J in the future. New manual isolation valves were installed in the inlet sample line, return sample line for panel 1PL75J, and return sample line for panel 1PL15J. Portions of stainless steel piping from the new isolation valves to the panels were replaced with stainless steel tubing. Two new grab sample stations for each panel were installed and existing manual equipment isolating valves were relocated to a higher elevation.
UFSAR Drawing M-156 Sheet 4 is revised to show the new isolation valves, new grab sample stations and tubing.

Revision to UFSAR drawings per Design Change Package (DCP) 9700075 – "Modify 16A/B High Pressure Heater Tube Side Relief Valves."
This DCP replaced the Unit 1 High Pressure Feedwater Heater tube side relief valves (1DV002A and 1DV0002B). These relief valves were replaced with new relief valves

that meet the requirements of ASME Section VIII and are UV stamped. The existing inlet and outlet piping of the relief valves was modified to fit the new relief valves. The original valves were not UV stamped as required by ASME Section VIII.
UFSAR Drawing M-62 Sheet 1 is revised to reflect the new line numbers for the relief valve inlet piping, and to show the new pipe flanges at the relief valve inlets.

Revision to UFSAR drawings per Design Change Package (DCP) 9700078 – "Modify all Unit 1 Low Pressure Feedwater Heater Tube Side Relief Valves."
This DCP replaced the Unit 1 Low Pressure Feedwater Heater tube side relief valves (1DV003A/B/C, 1DV0004A/BC, 1DV007A/B/C, 1DV009A/B/C and 1DV012A/B/C). These relief valves were replaced with new relief valves that meet the requirements of ASME Section VIII and are UV stamped. The existing inlet and outlet piping of the relief valves was modified to fit the new relief valves. The original valves were not UV stamped as required by ASME Section VIII.
UFSAR Drawing M-62 Sheet 2, Sheet 3, and Sheet 4 are revised to reflect the new line numbers for the relief valve inlet piping, and to show the new pipe flanges at the relief valve inlets.

Revision to UFSAR drawings per Design Change Packages (DCPs) 9700031 and 9700032 – "Replacement of Backdraft Dampers 1(2)VX09Y, 1(2)VX11Y and 1(2)VX53Y."
(Note: This safety evaluation is for DCPs 9700031 (Unit 1) and 9700032 (Unit 2).)
These DCPs replaced the existing Switchgear Ventilation System (VX) backdraft dampers 1(2)VX09Y, 1(2)VX11Y and 1(2)VX53Y with seismically qualified dampers with aluminum blades that will actuate at a lower differential pressure than the existing backdraft dampers. The new backdraft dampers will help to lower the pressure in the switchgear room. The change will improve the ability of the Auxiliary Electric Equipment Room (AEER) Ventilation System (VE) to maintain a positive pressure of 1/8" water column in the AEER.
UFSAR Drawings M-1462 and M-1463 are revised to remove the locked open (L.O.) designation after dampers 1(2)VX09Y, 1(2)VX11Y and 1(2)VX53Y.

Revision to UFSAR drawings per Design Change Package (DCP) 9700040 – "Replacement of Relief Valve 1CB004A with a Newer Model Valve."
This DCP replaced the existing 1CB004A (Consolidated/Dresser model 1970C) relief valve with a new relief valve (Consolidated/Dresser model 1996C) because the existing valve was leaking and could not be repaired. The original model is no longer in production and the manufacture recommended the replacement model. The new valve was flanged in for ease of future removal and testing.
UFSAR Drawing M-59 is revised to reflect the as-installed configuration.

Revision to UFSAR Drawing per Design Change Package (DCP) 9600532 – "1WS043 Control Valve Replacement."
This DCP replaced and relocated the existing carbon steel Generator Hydrogen Coolers Service Water Control Valve (1WS043) [Masoneilan control valve] with a stainless steel Fisher-Rosemount Vee-Ball control valve with a noise attenuator ball. Upstream isolation valve (1WS042) was also relocated and downstream isolation valve (1WS044) was replaced with a flanged end butterfly valve. The carbon steel piping between 1WS043 and 1WS044 was replaced with stainless steel pipe. The changes were made to minimize the cavitation erosion damage problem previously experienced.
UFSAR Drawing M-69 Sheet 2 is revised to reflect the new control valve and the downstream piping as stainless steel.

Revision to UFSAR drawing per Design Change Package (DCP) 9700030 – "Removal of Non-Safety Related/Non-Seismic Ductwork in the Main Security Control Center (MSCC)."
This DCP removed the non-safety related/non-seismic ductwork physically associated with the Control Room HVAC system (VC) and with the spot cooler previously installed in the MSCC. The interconnections to the safety related ductwork were restored to the as-designed condition. This equipment is no longer required for present plant configuration. The removal of the non-safety related ductwork associated with the spot cooler will restore the VC system duct to the original design configuration.
UFSAR Drawing M-1443 Sheet 2 is revised to reflect the plant configuration of the MSCC return air being ducted to the VC return.

UFSAR changes per Design Change Package (DCP) 9600525 – "Installation of New Microwave Tower / Meteorological Monitors."
The DCP installed a replacement microwave / meteorology tower, a shelter (pre-fabricated building), support equipment, and replacement meteorological instruments on the tower and / or in the shelter, outside the security fence. The replacement tower complies with the siting criteria of Regulatory Guide 1.23 and ANSI/ANS 2.5 (1984). The previous tower did not comply as it was located too close to the New Service Building, causing the 10 meter wind speed and direction data to be inaccurate.
UFSAR Figures 2.1-3, 2.1-4, 8.2-2, and 9.5-1 Sheet 1 and Section 2.3.3.1 are revised to reflect the installation of the new tower.
UFSAR Drawing Revision per Design Change Package (DCP) 9600411 – "IN System Primary Containment Isolation Valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN075 Operator Upgrades." (Reference ECN 000995M and ECN 000995M-01.)
The DCP increased the supply air pressure setting and bench set values, 2) inverted the actuator upper and lower casings, 3) replaced the actuator adjusting screw with a longer screw, 4) installed spacer washers onto the bolts retaining the upper actuator casing and spring barrel, 5) replaced the original Grafoil packing with Teflon based packing and 6) increased design differential pressure specifications (1IN001A/B) and decreased design differential pressure specifications (1IN017, 074,075). For 1IN017, 1IN074, and 1IN075, the existing 420 lb/in actuator spring was replaced with an 840

lb/in actuator spring, and the existing 0-40 psig air regulator was replaced with a 0-100 psig air regulator.
This DCP also replaced the existing supports with improved (stronger) supports for the pneumatic supply piping to the regulators associated with valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN075. New air regulator support brackets were installed for 1IN074. The new supports were upgraded to improve their adequacy under dynamic conditions and reduce the air supply tubing loads.
UFSAR Drawing M-66 Sheets 1 and 3 are revised to delete the air regulator setpoints for valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN975.

Editorial Revision to UFSAR drawing M-87 Sheet 2
UFSAR drawing M-87 Sheet 2 is revised to correct a directional arrow typo on (at drawing coordinates) A-3.5 from "FORM 1VY02A" to "FROM 1VY02A and to correct a typo at drawing coordinates F-7 from "1E12-F330"0" " to "1E12-F330D".

Revision to UFSAR drawing per Design Change Package (DCP) 9700368 – Install Isolation Valve between FC Demineralizers and SA System.
The DCP relocated the existing orifice 0FE-FC001 from downstream of check valve 0FC035 to downstream of check valve 0SA048. Existing check valve 0FC035 and isolation valve 0FC034 were relocated such that isolation valve 0FC034 is downstream of check valve 0FC035. Valve 0FC034 was replaced with a new ball valve and an additional isolation valve (0FC038) was installed downstream of 0FC034. A drip leg, consisting of a drip isolation valve (0FC039) and a new line 1FCC1A-3/4" was added between 0FC034 and 0FC038. A pressure indicator (0PI-FC009), a shut-off valve (0FC039) and an instrument line 1FCC2A-1/2" were added to the drip leg.
UFSAR Drawing M-98 Sheet 2 was revised to reflect the changes.

Revision to UFSAR drawings per Unit 1 Design Change Package (DCP) 9700507 – "Permanent Installation of the Unit 1 Heater Bay Cameras."
This DCP replaced the nine (9) existing cameras in the Unit 1 Heater Bay with permanently installed cameras and added one new camera in the Condenser Pit. The permanently installed cameras are cooled by forced air supplied by a skid mounted compressor assembly (1CQ013) and will allow visual inspection of Heater Bay components with the Unit at power without exposing personnel to high dose rates.
Revision 1 to the safety evaluation was prepared to consider the pending UFSAR changes (373-160-98-00038) that were approved subsequent to the preparation of Revision 0. These changes were similar to those proposed by Revision 0, and therefore were eliminated from the safety evaluation.
UFSAR Drawings M-Index and M-8 are revised accordingly.

UFSAR drawing revision per Design Change Package (DCP) 9700422 – Addition of Low Point Drains in Service Water Piping

This DCP added low point drain lines with manual valve and pipe cap to Unit 1 Turbine Building Service Water supply lines 1WS09A-14" (Turbine Oil Cooler Supply Header) and 1WS11A-20" (Stator Cooling Unit and Generator Hydrogen Cooler Unit Supply Header). These low point drain lines were added to allow draining of the piping during extended system lay-up to prevent corrosion damage to the piping due to stagnant water conditions.
UFSAR Drawing M-69 Sheet 2 is revised to show the addition of the drain line assemblies.

UFSAR changes per Design Change Package (DCP) 9700208 – Reactor Water Cleanup (RT) System Recirculation Pumps and Return to Hot Suction.
This DCP restored the "hot suction" configuration of the Unit 1 RT system, as originally designed by General Electric, by replacing / reworking piping and associated valving. The design change installed the Reactor Water Cleanup pumps upstream of the system heat exchangers and routed the piping from outside the primary containment to the pump suction bypassing the heat exchangers. The pump discharge was routed to the system heat exchangers. The DCP replaced the three existing non-safety related 50% capacity RT System recirculation pumps with two new 100% capacity pumps.
UFSAR Sections 1.7, 7.3.2.2.3.8, and 7.7.1.2.1, Tables 5.4-1, 8.1-2, 8.1-9, 8.3-1 Sheet 2, 12.3-16 Sheet 1, Figures 4.6-5, 4.6-6, 5.4-6 Sheet 1 and Sheet 2, 5.4-8, 12.3-1 Sheet 4, 12.3-2 Sheet 4, 12.3-4 Sheet 2, and H.2-1 Sheet 3 and Drawings M-Index Sheet 1, M-7, M-74, M-90 Sheet 3, M-91 Sheets 2 and 6, M-97 Sheet 1, M-100 Sheet 1, M-104 Sheet 1, and M-2097 are revised accordingly.

Revision to UFSAR drawings per Design Change Package (DCP) 9700605 – "Relocate VC Train B Outside Air Intake to Return Fan Suction."
This DCP relocated the outside air intake connection in the VC system Train "B" from its present connection point (suction of the supply fan) to the suction of the return fan. The work included relocation of dampers 0VC04YB, 0VC06YB and 0VC70YB, rerouting existing ductwork, removal of existing hanger (973-S), installation of new hangers, and removal of an air flow monitor (0FE-VC037). This change ensures sufficient air is drawn into the system during normal and emergency modes of operation for Main Control Room pressurization and enhances the overall VC system airflow.
UFSAR Drawings M-1443 Sheet 1 and M-3443 Sheets 1, 3, 4, 5, 6 and 17 are revised to reflect the changes.

Revision to UFSAR drawings per Design Change Package (DCP) 9700604 – "Relocate VC Train A Outside Air Intake to Return Fan Suction."
This DCP relocated the outside air intake connection in the VC system Train "A" from its present connection point (suction of the supply fan) to the suction of the return fan. The work included relocation of dampers 0VC04YA, 0VC06YA and 0VC70YA, rerouting existing ductwork, removal of existing hangers (942-S/943-S), installation of new hangers, and removal of an air flow monitor (0FE-VC032). This change ensures

sufficient air is drawn into the system during normal and emergency modes of operation for Main Control Room pressurization and enhances the overall VC system airflow. UFSAR Drawings M-1443 Sheet 1 and M-3443 Sheets 1, 3, 4, 5, 6 and 17 are revised to reflect the changes.

Revision to UFSAR drawing per Design Change Package (DCP) 9700469 – Seal Weld Cap/Nipple to Class I Requirements (Loop A) and Design Change Package (DCP) 9700529 – Seal Weld Cap/Nipple to Class I Requirements (Loop B).
This DCP replaced the existing Class D reducer, pipe nipple (1RR17CA and 1RR17BB) and threaded cap of the Reactor Recirculation System drain line with Class A reducer, pipe nipple and welded cap. The piping was insulated due to the change in pipe class. These changes allow the Reactor Recirculation System's pressure boundary and the ASME code classification boundary to be extended from valves 1B33-F052A and 1B33-F052B to the Class A pipe nipple and cap.
UFSAR Drawing M-93 Sheet 1 and Sheet 2 are revised to reflect this change.

Revision to UFSAR Drawing per Design Change Package (DCP) 9700358 – Upgrade (0HY01J) Hydrogen Control Panel & Relief Valve (0HY005)
This DCP added a union downstream of relief valve 0HY005, between the valve and the vent line to allow easier removal of the valve for maintenance and bench testing. Additionally P&ID M-78 Sheet 1, a vendor drawing and the vendor Bill of Material were revised to reflect the as-built condition of the control panel which included adding two needle valves, several unions and relief valve vent caps not shown on the original design drawings.
UFSAR Drawing M-78 Sheet 1 is revised accordingly.

UFSAR Drawing revision per Design Change Package (DCP) 9700353 – Relocate 1EH07B Sensing Line to Electrohydraulic Control (EHC) Header Manifold.
This DCP relocated 1EH07B sensing line from EH-13 tee instrument cluster to the main header so that pressure switch 1PS-EH007B would be less susceptible to pressure fluctuations during testing.
UFSAR Drawing M-55 Sheet 10 is revised to reflect this change.

UFSAR Drawing revisions per Design Change Package (DCP) 9700352 – VC and VE Systems Air Conditioning Unit Prefilters Differential Pressure (DP) Switch Setpoint Revision.
This DCP changed the setpoints of differential pressure (DP) switches 0PDS-VC024, 0PDS-VC026, 0PDS-VC064 and 0PDS-VC066 for the Main Control Room air conditioning units and 0PDS-VE024 and 0PDS-VE064 for the Auxiliary Electric Equipment Room air conditioning units. The range springs in the existing DP switches were replaced, and the switches were recalibrated to a new setpoint. The setpoints

were revised in order to be consistent with the Pressure Drop Calculations, the Vendor recommendations and the UFSAR.
UFSAR Drawing M-3443 Sheet 9, Sheet 10 and Sheet 27 are revised to remove the setpoint values of the referenced DP switches and of other instruments shown on the drawing.

UFSAR drawing revisions per Drawing Change Request (DCR) 980435.
The EPNs for the Reactor Water Clean Up (RWCU) System Regenerative and Non-Regenerative Heat Exchangers were changed by adding an additional numerical identifier. The RWCU Heat exchangers for each unit consist of three regenerative and two non-regenerative heat exchanger sets. Each set of regenerative and non-regenerative heat exchangers were identified as a whole by a single EPN [1(2)G33-B001A(B) for regenerative, and 1(2)G33-B002A(B) for non-regenerative]. The Unit 1 and 2, A and B RWCU regenerative heat exchangers are now identified as 1(2)G33-B001A(B)-1, 1(2)G33-B001A(B)-2, and 1(2)G33-B001A(B)-3. The Unit 1 and 2, A and B RWCU non-regenerative heat exchangers are now identified as 1(2)G33-B002A(B)-1 and 1(2)G33-B002A(B)-2. Additionally, a correction was made to revise the line number for the "B" RWCU regenerative heat exchanger tube side outlet piping from "1RT05DB" to "1RT03AB"
UFSAR drawings M-91 Sheet 2, M-97 Sheet 1, M-137 Sheet 2 and M-143 Sheet 1 are revised accordingly.

Editorial Changes to UFSAR drawing M-75 Sheets 1 – 4 per Drawing Change Request (DCR) 980045.
Notes were added to UFSAR Drawing M-75 Sheet 1, 2, 3 and 4 to reference new drawing M-75 Sheet 5. The new drawing contains the new EPNs for the manual and check valves associated with the MC drops. The existing legend on M-75 Sheet 1 provides the detail as to what type of valve or valves are provided for each MC drop. The notes were added for clarification as to where the EPNs are located. M-75 Sheet 5 will not be added to the UFSAR since it does not contain any pertinent design basis information that could affect the licensing basis.
UFSAR Drawing M-75 Sheet 1, Sheet 2, Sheet 3 and Sheet 4 are revised accordingly.

Revise UFSAR drawing per Drawing Change Request (DCR) 980691.
This DCR revised UFSAR drawing M-69 Sheet 2 to correct the specified line size for 0WS89A. The line was field verified to be 1 ½" rather than ½" as shown on the drawing. UFSAR Drawing M-69 Sheet 2 is revised to show the as-built condition in the plant.

Revise UFSAR drawing per Drawing Change Request (DCR) 980640.
This DCR revised UFSAR Drawing M-134 Sheet 1 to reflect that the 2B Fuel Pool Emergency Makeup Pump Discharge Pressure Gauge Sensing Line is connected between the discharge check valve (2FC044B) and the discharge isolation valve

(2FC045B), and not upstream of the discharge check valve (2FC044B) as originally shown.
UFSAR drawing M-134 Sheet 1 is revised to correct the drawing to reflect how the line is connected in the plant.

Revise UFSAR Drawings per Drawing Change Request (DCR) 980634.
The DCR revised UFSAR Drawings M-101 Sheet 1 and M-147 Sheet 1 by assigning EPNs to existing components and corrected the nomenclature on instrument 1E51-R904 (Barometric Condenser Water Temperature) from pressure indicator (PI) to temperature indicator (TI). These changes were determined to be editorial and correction of a typographical error.
UFSAR Drawings M-101 Sheet 1 and M-147 Sheet 1 are revised accordingly.

UFSAR drawings M-67 Sheets 1, 2, and 3, M-91 Sheet 3, M-124 Sheet 2 and M-137 Sheet 3 revised per Drawing Change Request (DCR) 980591.
The DCR revised the UFSAR drawings to reflect the as-built configuration and current design of the Turbine Building Closed Cooling Water (TBCCW) System (WT), the Reactor Building Closed Cooling Water (RBCCW) System (WR) and the Reactor Building Equipment Drains (RE). The current drawings did not reflect the actual field configuration of the systems and were not in agreement with the Electronic Work Control System (EWCS).
UFSAR drawings M-67 Sheets 1, 2, and 3, M-91 Sheet 3, M-124 Sheet 2 and M-137 Sheet 3 are revised accordingly.

Revision to UFSAR Drawings M-94 and 1E-1-4601AB per Design Change Request (DCR) 980504.
These drawings are revised to incorporate the nameplate nomenclature on panel 1H13-P601 for the Overload Bypass Hand Switch associated with valve 1E21-F001, and to correct the EPN for the LPCS Minimum Flow Bypass Valve Hand Switch on the P&ID. The changes are editorial and are as-built configuration changes based on the LPCS system walkdown.

3731609800225 Revision to UFSAR Drawing M-83 Sheet 1 per Drawing Change Request (DCR) 980515.
The DCR documents two existing (as-built) configurations of piping and pipe fittings on the 1DG01S Standby Diesel Generator Starting Air Compressor Skid. The first change required is to show the field verified configuration of ½" diameter piping of the vendor furnished drain line from the 1DG03MA Moisture Separator in lieu of ¾" diameter. The second configuration change shows the material grade of the approximately 4-inch long pipe spool of 1-1/2" piping between valves 1DG049A(B) and 1DG050A(B) as carbon steel, ASTM A-106 Grade B in lieu of Grade C.
UFSAR Drawing M-83 Sheet 1 is revised accordingly.

3731609800226 Revise UFSAR drawings per Drawing Change Request (DCR) 980706.
This DCR revised design documents that incorrectly described the current plant configuration and were in disagreement with other design documents that correctly described the plant configuration. Drawing M-1461 Sheet 1 is revised to add the correct panel reference to control switches 0HS-VW038A, 0HS-VW039B and 0HS-VW038C. Drawing M-1461 Sheet 2 is revised to correct the nomenclature used to describe four cubicles served by Radwaste Ventilation, to add a missing EPN for a damper and to correctly depict a damper as a fire damper versus a standard damper.
UFSAR Drawings M-1461 Sheets 1 and 2 are revised accordingly.

3731609800227 Revision to UFSAR drawings per Design Change Request (DCR) 980523.
The UFSAR drawings for the Instrument Air (IA) and Service Air (SA) Systems are revised to reflect the as-built configuration of the system. The as-built changes are implemented to update the drawings to resolve Operator Work Around (OWA) #224 and various PIFs.
UFSAR Drawings M-82 Sheets 1, 2, 3, 4 and 6, M-92 Sheet 1 and M-56 Sheet 1 are revised to reflect the as-built configuration of the IA/SA system.

3731609800228 Revision to UFSAR drawing M-55 Sheet 10 per Design Change Request (DCR) 980501.
As a result of the EHC Functional Walkdown (ER #9801496), UFSAR drawing M-55 Sheet 10 requires revision to document the as-found field configuration of the Unit 1 Turbine EHC system (as-built). The existing drawing in the UFSAR is functionally incorrect and requires revision to reflect the installed configuration.

Revision to UFSAR drawings per Design Change Package (DCP) 9800146 – "Replace Turbine Building Closed Cooling Water (TBCCW) Heat Exchanger Flow Control Valve 1WS029."
This DCP replaced the existing TBCCW Heat Exchanger Flow Control Valve 1WS029, which was a Masoneilan model 37-20521 AOV, with a Masoneilan model 37-41612 AOV with anti-cavitation trim. The replacement was necessary because the existing valve had cavitation damage and was obsolete. In addition the DCP replaced the existing filter/regulator, revised the bench set values, revised the pressure regulator setpoint and permitted field re-routing of the air tubing and supports to accommodate the new valve assembly.
UFSAR Drawing M-69 Sheet 2 is revised to accurately show the pneumatic supply and control lines.

Revision to UFSAR Drawings M-90 Sheet 2 and M-115 Sheets 1 and 2 per Design Change Request (DCR) 980693.
The UFSAR drawings are revised to reflect as-built changes for components in the Reactor Building Closed Cooling Water (RBCCW) System associated with the Reactor Building process sample sink and sample coolers.
UFSAR Drawings M-90 Sheet 2 and M-115 Sheets 1 and 2 are revised accordingly.

Revision to UFSAR drawings M-91 Sheet 3 and M-137 Sheet 3
UFSAR drawings M-91 Sheet 3 and M-137 Sheet 3 are revised to switch line numbers and valve equipment part numbers to provide consistency in the numbering and labeling of the drain lines and drain valves associated with the A and B heat exchangers of the Unit 1 and 2 residual heat removal (RHR) systems.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800134 – "Install High Point Vents on the Cooling Water Lines to the LPCS Motor Cooler."
This DCP added two vent valves each in Low Pressure Core Spray Motor Cooler Supply and Return Lines 1DG22A-1 ½" and 1DG23A -1 ½" to allow these loops to be vented. No vents were installed previously. UFSAR Drawing M-87 Sheet 2 is revised accordingly.

Revision to UFSAR drawings per Design Change Package (DCP) 9800078 – "Reinstate 11 and 12 Feedwater Heater Normal Drain and Emergency Spill Valve Alarms."
This DCP reinstated the normal drain valve closed and emergency spill valve open alarms for Feedwater Heaters 11 and 12, and removed the emergency spill valve level solenoid valves, associated stop valves and level switches, which were previously abandoned in place. The spill and drain valves for the 11 and 12 heaters were modified under DCP 9700287, permitting throttling capability to maintain heater level. This design change (9800078) restored the control room annunicators that were previously removed by modification M01-1-89-014.
UFSAR Drawings M-61 Sheets 3 and 4 are revised to show the deletion of the solenoid valves.

Revision to UFSAR drawings per Design Change Package (DCP) 9800074 – "Replacement of Outlet Throttle Valve 1DG020 for N.W. Area Cubicle Cooler (1VY01A)."
The DCP replaced the existing 4-inch 1DG020 globe valve, downstream of VY cooler 1VY01A, with a 3-inch globe valve. A portion of the existing 4-inch piping was replaced with reducing fittings to fit-up the new valve with the existing piping. The existing valve had deteriorated and was replaced with a smaller valve to increase the pressure drop to facilitate flow balancing.
UFSAR Drawing M-87 Sheets 2 and 3 are revised to show the smaller valve and associated reducers.

UFSAR revision per Design Change Package (DCP) 9800133 – "Install New Isolation Valves on the Cooling Water Lines to the LPCS Motors."
This DCP added inlet and outlet isolation valves to the Unit 1 and 2 Low Pressure Core Spray Motor Cooler Inlet and Outlet lines 1DG22A –1 ½", 1DG23A – 1 ½", 2DG22A – 1 ½" and 2DG23A – 1 ½". Installation of these additional piping isolation valves allow future pipe maintenance or replacement without having to take the entire Division 1 Diesel Generator Cooling Water System out-of-service.
UFSAR Drawings M-87 Sheet 2 and M-134 Sheet 2 are revised accordingly.

Revision to UFSAR drawings per Design Change Package (DCP) 9800059 – "Addition of Supports to Pipe Line 1HD37AA-1½" and 1HD37AB-1½"."
This DCP added one new pipe support each on lines 1HD37AA-1½" and 1HD37AB-1½", which brings the pipe stress into conformance with Code allowables. The DCP also provided for as-built routing of the pipe and existing supports.
UFSAR Drawing M-61 Sheet 3 and Sheet 4 are revised to reflect the as-built line size from ¾" to 1½".

UFSAR revisions per Design Change Package (DCP) 9700512 – "Flow Control Valve (FCV) Position Setpoint for Reactor Recirculation (RR) Pump Upshift."
This DCP revised the flow control valve (FCV) position setpoint for FCV 1B33-F060A/B limit switches. The FCV position limit switches (1B33-N039A/B) setpoint was changed to 20% open with a tolerance of +/-1.0% of FCV position. This change was required to increase the valve position when the RR pumps are transferred from low to high speed to reduce the possibility of FCV sticking.
UFSAR Sections 15.4.4, 15.4.10, G.2.1.1.1, G.2.1.2.2.1.3, G.2.2.4, and G.2.2.5, Figures 15.4-10 and G.2.3-1, Drawings M-93 Sheets 1 and 2, 1E-1-4205AF, 1E-1-4205AR, 1E-1-4205BA, and 1E-1-4205BB are revised accordingly.

UFSAR drawing revision per Unit 1 Design Change Package (DCP) 9800109 – "1E12-F549 Division 2 RHR-WS Keep Fill Pressure Regulating Valve Setpoint / Range Change."
This design change revised the setpoint for the self-contained pressure regulator (1E12-F459) in the RHR Service Water (RHR-WS) cross-tie from 50 psig to 20 psig. The setting change required replacement of the pressure regulator spring and a revision to the system pressure specified in operating procedure LOP-RH-Q1.
A Validation of Previously Performed Safety Evaluations and Screenings (Exhibit H) was performed using the safety evaluation for DCPs 9600195 and 9600198 that installed the Division 2 RHR-WS keep fill system and valve 1E12-F459. This design change revised the setting of 1E12-F459 but did not change the function. The previous safety evaluation evaluated the addition of the Division 2 cross-tie between RHR-WS and WS, which included 1E12-F459. It was determined that the previous safety evaluation adequately evaluated the safety implications of the proposed change to the

pressure regulator (1E12-F459) setpoint. UFSAR Drawing M-87 Sheet 1 is revised to delete the setpoint from the drawing.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800112, "VR System Exhaust Plenum Overpressure Protection Damper Due to High Energy Line Break (HELB) in Main Steam Tunnel (MST)."
This DCP installed a new relief damper (1VR90Y) in the VR system between 1VR05YB and the VR plenum wall to prevent a failure of the plenum following a postulated Main Steam Line Break in the Main Steam Tunnel. Stiffeners were added to the existing transition piece to allow for the addition of the relief damper. Additional supports were added to support all the added loads due to the modified duct, associated stiffeners and the relief damper.
UFSAR Section 9.4 is revised to include descriptions of the safety and design bases and operation of the new pressure relief damper 1VR90Y. Drawing M-1455 Sheet 1 is revised to reflect the addition of the new pressure relief damper.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800073 – "Loss of Coolant Accident (LOCA) / Purge Analysis."
This DCP analyzed and modified the VQ piping system as a result of postulating a LOCA during containment purge. During investigation of LER 97-005, it was discovered that in the event of a LOCA coincident with containment purging, the VQ ductwork could potentially rupture and VQ piping downstream of the VQ Containment Isolation Valve could experience temperature increases beyond the originally analyzed conditions.
As a result of the VQ piping analysis, two VQ pipe supports (1VQ02-1035X and 1VQ02-1040X) were removed to control piping stresses under thermal conditions resulting from the postulated LOCA during purging evolutions. A local temperature gauge (0TI-VQ010) was added in the Auxiliary Building to provide local ambient temperature indication.
In addition to analyzing the VQ piping system, an analysis to evaluate the environmental impact on equipment and radiological impact on the onsite and offsite personnel by the VQ ductwork rupture and resultant steam release that occurs as a result of the postulated LOCA was performed. This analysis determined that a new harsh environmental zone (designated H10) must be created, requiring a change to the UFSAR. UFSAR Section 3.11.1 is revised, and Figure 3.11-6 sheets 1 and 2 are added.

Revision to UFSAR Table H.4-78
Design Change Package (DCP) 9600115 installed instrumentation cable 1HP297 between Diesel Generator (DG)-1B panels 1H22-P028 and 1E22-P301B in the Division 3 DG room. The DCP did not identify this cable as a safe shutdown cable. UFSAR Table H.4-78, "Safe Shutdown Equipment Located in Fire Zone 7B1", is appropriately revised.

Revision to UFSAR Table H.4 - 56
UFSAR Table H.4 - 56 Sheet 4 (Safe Shutdown Equipment located in Fire Subzone 4D2) is revised to correct a typographical error. Cable number 2RA293 is corrected to 2RH293. The letter designation of the cable signifies the system, and there is no RA system. The Sargent & Lundy Interactive Cable Engineering (SLICE) report identifies cable 2RH293 as a safe shutdown cable. The report also indicates that the cable is routed through fire zone 4D2. This typographic error was discovered while resolving discrepancies for the cable 2RA293 and other cables. A review of the pending changes has revealed that this typographic error has been not accounted for.

Revision to UFSAR Appendix H Tables
UFSAR Tables H.4-67 (Safe shutdown equipment located in fire zone 4FI - Division 1 ESF Switchgear Room) and H.4-68 (Safe shutdown equipment located in fire zone 4F2 - Division 1 ESF Switchgear Room) are revised to achieve consistency with design bases drawings. In Table H.4-67, cable 1DC012 is replaced with cables 1DC128, 1DC129, 1DC130, 1DC131, 1DC132, 1DC133, 1DC134, and 1DC135. In Table H.4-68 cable 2DC050 is deleted, and cable 2DC012 is replaced with cables 2DC128, 2DC129, 2DC130, 2DC131, 2DC132, 2DC133, 2DC134, 2DC135.

The following cables are deleted from the associated UFSAR Tables.
Cable 1NBE44 from Table H.4-14 (Safe shutdown cables located in the fire subzone 2E-2).
Cables 1NBE45 and 46 from Table H.4-13 (Safe shutdown cables located in the fire subzone 2E-1).
Cable 2NBE44 from Table H.4-16 (Safe shutdown cables located in the fire subzone 3E-2).
Cables 2NBE45 and 46 from Table H.4-15 (Safe shutdown cables located in the fire subzone 3E-1).

The safe shutdown cables listed in UFSAR Tables H.4-67 and H.4-68 did not agree with previous design bases drawings.

Cable 1DC012 was replaced with cables 1DC128, 1DC129, 1DC130, 1DC131, 1DC132, 1DC133, 1DC134, 1DC135 per modification M01-1-88-001, which replaced the Unit 1 250VDC Division 1 battery (1DC01E).

The Unit 2 250VDC Division 1 battery (2DC01E) was replaced under modification M01-2-88-001, replacing cable 2DC012 with cables 2DC128, 2DC129, 2DC130, 2DC131, 2DC132, 2DC133, 2DC134, 2DC135.

Modification M01-2-88-004 replaced the Unit 2 125VDC Division 1 battery (2DC07E), deleting cable 2DC050.

The above modifications were installed in the early 90's and all are operable. The associated omitted the revision to the Safe Shutdown sections of the UFSAR.

Cables 1NBE44, 45, 46, and 2NBE44, 45, 46 were added to UFSAR Appendix H in the UFSAR Revision 7 1991 update. These cables are deleted as they were never installed as part of modifications M01-1-87-097 and M01-2-87-085, or any other plant modifications, as the cable numbers were reserved for these modifications. The removal of these cables corrects the UFSAR tables to agree with design bases.

UFSAR Change associated with the Replacement of the Unit 1 RCIC Steam Line Drain Tap per Design Change Package (DCP) 9800227
The DCP reconfigured the Reactor Core Isolation Cooling (RCIC) Condensate Pot Level Control, Steam Trap, and Rupture Disks, to prevent repeated blowouts, which have occurred during RCIC fast start tests due to unanticipated water hammers or wet steam impingement on rupture disks. Rupture disks 1E51-D001 and 1E51-D002 were relocated from line 1RI12A-6" to 1RIA1A-6". UFSAR Drawing M-101 Sheet 1 (RCIC system) is revised.

Revision to UFSAR Sections 7.6.3 and 7.7.6
UFSAR subsections 7.6.3.2.2, 7.6.3.3.2, 7.7.6.1.2, 7.7.6.2.2, 7.7.6.3.2 and 7.7.6.4.2 are revised to provide needed flexibility in the application of new calibration techniques and station specific commitments to test and calibration procedures for the associated neutron monitoring systems, and to correct a spelling error in UFSAR subsection 7.7.6.1.3. The UFSAR previously stated that tests and calibrations are performed in accordance with procedures contained in system instruction manuals. Conversely, station procedures are used for test and calibration. These procedures are based on the recommended methods from the system instruction manual, industry standard techniques, and requirements specific to LaSalle. This revision corrects the overly restrictive UFSAR wording and brings it into compliance with Tech Spec requirements for specific stations procedures for these test and calibration activities.

Revision to UFSAR Drawing M-101 Sheet per Design Change Package (DCP) 9700180
DCP 9700180 replaced and rerouted the reactor core isolation cooling (RCIC) turbine condensation drain lines 1RI10B-3/4", 1RI10BA-3/4", 1RI10BB-3/4", 1RI14A-3/4", and 1RI96A-3/4", and installed a sight glass in the turbine condensation drain pot. The new stainless stell drain lines replace carbon steel lines. The use of stainless steel and the rerouting of the lines is intended to prevent low point condensation accumulation and subsequent rust formation. Stem packing leakoff line 1RI38B-3/4" from valve 1E51-F360 replaced and reconfigured to ensure that the pipe has continuous slope to the RCIC barometric condenser 1E51-C002 to minimize low point condensation accumulation. A new strainer and restricting orifice, 1E51-D319 and 1E51-D320, respectively, are added to drain line 1RI10B-3/4". UFSAR Drawing M-101 Sheet 1 (RCIC system) is revised.

Revision to UFSAR Section 13.1.1.3
UFSAR Subsection 13.1.1.3, Qualifications of Management and Technical Support Organization, defines the qualifications of support personnel (off-site ComEd personnel). Although historically accurate, this summary didn't reflect the present qualifications of support personnel. UFSAR Subsection 13.1.1.3 is revised to provide both a historical and a current perspective.

Revision to UFSAR Sections 9.4 and 9.5
DCPs 9700350 and 9700351 modified the Control Room and Auxiliary Electric Equipment Room ventilation (VC and VE systems, respectively) manual purge control circuit for Trains A and B to initiate automatic purge damper isolation upon detection of smoke in the outside air when the VC/VE system is aligned to purge the Control Room or Auxiliary Electric Equipment Room air (purge mode). UFSAR Subsections 9.4.1.1.1.1.d and 9.5.1.2.4 are revised, as the DCPs revised M-3443 sheets 5, 18, and 24. The changes to the above subsection are revised to be consistent with the DCPs and drawing changes.

Editorial Revision to UFSAR Sections 9.1, 9.2, 9.3, and 10.4
UFSAR Sections 9.1, 9.2, 9.3, and 10.4 are revised to correct chemistry conductivity units, to consistently document throughout the UFSAR that conductivity and pH measurements are corrected to 25 °C, and to correct typographical errors.

Revision to UFSAR Sections 1, 3, 4, 5, 6, 7, 9, and Appendix G
UFSAR sections 1, 3, 4, 5, 6, 7, 9, and Appendix G are updated to resolve discrepancies identified by Commonwealth Edison's Nuclear Fuel Management BWR Support Services.

Revision to UFSAR Subsection 7.8.2 for the Safety Parameter Display System (SPDS)
UFSAR subsection 7.8.2 is revised to reflect standardized Nuclear Utility Management Resources Council (NUMARC) emergency action levels (EAL) information previously approved in accordance with Regulatory Guide 1.101.

UFSAR Update per Removal of Remote Indication Hardware from Division 2 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700488
DCP 9700488 removed remote indication hardware from Unit 1 Division 2 ECCS testable check valves 1E12-F041B, 1E12-F041C, and 1E12-F050B. This was done to eliminate a recurring problem in which the valves fail to completely close. This is attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP increases the margin by reducing the frictional forces, thereby eliminating the problem.

UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 9.3.1.2.2, Table 6.2-21, and drawings M-66 Sheet 2 and M-96 are to be revised.

Revision to UFSAR Chapter 13, Section 13.2, Training
This revision to the UFSAR consists of the following:
The changes revise the UFSAR to the level of detail required by the Generic Letter 80-110 and Regulatory Guide 1.70. This revision modifies the description in the UFSAR of the following programs within the Training Department: 1) New Employee Orientation, 2) Nuclear General Employee Training, and 3) Replacement Training of Certain Specialties (Mechanical Maintenance, Electrical Maintenance, Instrument Maintenance, Radiation Protection Technicians, and Maintenance Supervisors).

"INPO" is replaced with "the National Academy for Nuclear Training" where applicable.

The revision also implements changes to the New Employee Orientation program to standardize this program across all ComEd sites, and removes the requirement for Staff (Non-Licensed) System Description training.

UFSAR Update for the inclusion of a holdup volume in the pathway for unidentified leakage to reach the Drywell Floor Drain Sump (DWFDS)
UFSAR Subsections 3.8.3.1.1 and 5.2.5.5.4 were revised for the reactor coolant pressure boundary leakage detection system to include the addition of holdup volume caused by the irregularities in the drywell floor. The UFSAR didn't previously provide definitive information as to the potential of a holdup volume of water due to irregularities in the drywell floor and the effect on the design basis for the leakage detection system in the drywell.

Revision to UFSAR Table 6.2-21
UFSAR Table 6.2-21 Sheets 2B and 10 are revised to reflect the correct location of remote manual switches 1(2)B33A-S800, S801, 802S, and S803 for the reactor recirculating flow control valve hydraulic power unit isolation valves 1(2)B33-F338A&B, F339A&B, F340A&B, F341A&B, F342A&B, F343A&B, F344A&B, and F345A&B are located in the auxiliary electric equipment room (AEER), rather than the main control room, and are capable of remote manual operation from there. Previously omitted data for valves 1(2)B33-F345A&B is added to Sheet 2B.

UFSAR Revision to reflect Installation of Rotary Variable Differential Transformer on the 1B33-F060A/B Valves per Design Change Package (DCP) 9600137
DCP 9600137 installed rotary variable differential transformers (RVDT) on the reactor recirculation (RR) flow control valves (FCV) 1B33-F060A and 1B33-F060B. The DCP also installed signal conditioning modules on the outputs from the RVDTs, and

upgraded the signal conditioning modules on the outputs of the existing linear variable differential transformers (LVDT). UFSAR Sections G.3.3 and G.5.2 are revised.

UFSAR change to reflect Chem-Nuclear Systems Procedure DM-OP-043-41314 Revision 1, Operating Procedure For CNS High Flow Dual Train System At LaSalle Station
The procedure provides instructions for the setup, operation, and removal of the CNS High Flow Dual Train System (HFDTS) at LaSalle Station. A portion of the vendor processing system is moved from the radwaste building truck bay to the south low level storage area. A redundant train was added to the vendor processing system. UFSAR Section 11.4 is revised to reflect system operation in the south low level storage area.

Revision to UFSAR Table 13.1-1
The UFSAR Table 13.1-1 title of Radiation Protection Manager is replaced with Health Physics Supervisor. The statement allowing that a technical person reporting to the Health Physics Supervisor may qualify for the position of Radiation Protection Manager is deleted. This change reflects the more restrictive requirements of Technical Specifications.

Revision to UFSAR Table 6.2-21
UFSAR Table 6.2-21 is revised to explicitly delete reference to LaSalle administrative procedure LAP-300-30, and to reflect the addition of monitoring to the scope of the check valve preventative maintenance program.

Clarification to UFSAR Subsection 12.1.1.3.k
Clarifying information was added to Subsection 12.1.1.3.k which associates survey requirements with automated monitors.

Revision to UFSAR for Installation of Unit 2 OPRM per Design Change Package (DCP) 9700502
DCP 9700502 installed a microprocessor based oscillating power range monitor (OPRM) system on Unit 2. The OPRM is intended to detect and suppress core oscillations that BWRs are susceptible to during high power – low coolant flow conditions. Once it is armed, the OPRM will function to automatically suppress oscillations. UFSAR Chapters 1, 3, 4, 7, and 15 are revised.

Revision to UFSAR Subsection 7.3.2.2.3.8
The package revises UFSAR subsection 7.3.2.2.3.8 to resolve conflicting changes proposed by DCP 9700532 (High Energy Line Break (HELB) Leak / Break Detection Modification) and DCP 9700208 (Reactor Water Cleanup System Recirculation Pumps and Return to Hot Suction). Index page 7.0-iii is also revised.

UFSAR revision per Unit 2 High Energy Line Break (HELB) Leak / Break Detection Modification, DCP 9700533
The DCP modified the Leak Detection System for the Reactor Water Cleanup (RWCU), Reactor Core Isolation Cooling (RCIC), and the Residual Heat Removal (RHR) systems of Unit 2 to resolve a concern identified with the original Leak Detection calculations. The modifications generally consisted of temperature sensor relocation, addition of temperature monitoring functions, and addition of a high flow monitor for HELB. UFSAR Subsections 5.2.5.1, 5.2.5.1.2, 5.2.5.5.4, 5.4.7.3.1, 7.3.2.2.3.8, 7.3.2.2.3.9, 7.3.2.2.3.10, 7.4.1.2.6, 7.6.2.2.4, 7.6.2.2.5, 7.6.2.2.6, 15.9.3.4, Table 5.2-8, Table 7.3-2, and Figure 7.3-7 are revised accordingly.

Revision to UFSAR Sections 6.5, 7.3, 9.5, and H.3
UFSAR Sections 6.5, 7.3, 9.5, and H.3 are revised to correct previously identified discrepancies relating to the description of the operation of the charcoal filter deluge system. These changes correct the UFSAR description to correspond with LaSalle operating procedure LOP-FP-05, Charcoal Filter Beds Manual Deluge Valve Reset Operation and Initiation.

UFSAR Revision per Removal of Remote Indication Hardware from Unit 2 Division 3 Emergency Core Cooling System (ECCS) Testable Check Valve, Design Change Package (DCP) 9700492
DCP 9700492 removed remote indication hardware from Unit 2 Division 3 ECCS testable check valve 2E22-F005, to eliminate a recurring problem in which the valve fails to completely close. This was attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves valve performance, increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 7.A.3.1.1.4, 9.3.1.2.2, and Table 6.2-21 Sheet 11 are revised.

UFSAR Revision Associated with Consolidation of Emergency Operations Facilities
Commonwealth Edison (ComEd) has consolidated its four near-site emergency operations facilities (EOFs) and corporate EOF into a single EOF. NRC approval of ComEd's proposed change is documented in NRC letter dated February 9, 1999 from Mr. Stuart Richards (NRC) to Mr. Oliver Kinsley (ComEd).
"Corporate Emergency Operations Facility (CEOF)," and "Backup Emergency Operations Facility (BEOF) (Zion only)," are correspondingly deleted in UFSAR Section 13.3. Additionally, and editorial change revises "Site Area Emergency" to "Site Emergency" in UFSAR Section 13.3

Revision to UFSAR Figure 7.3-7 per Design Change Package (DCP) 9500288
DCP 9500288 deleted the leak off line for reactor water cleanup (RWCU) suction stop valve 2G33-F102 from the valve to the pipe header 2REH9A-2", along with associated supports and in-line components. UFSAR Figure 7.3-7 Sheet 2 is revised to reflect the deletion of the leak off line.

UFSAR Revision per Design Change Packages (DCP) 9900041 and 9900042
DCPs 9900041 and 9900042 replaced the Relay House System 1 and System 2 125 VDC batteries, respectively. The previous batteries were 60 cell, 200 Ampere-hour batteries. The new batteries are 58 cell 270 Ampere-hour batteries. The original batteries were 25 years old and near the end of life. The new batteries improve the reliability of the control power supplied to the 345 kV switchyard breakers and the protective relay systems associated with the transmission lines. UFSAR Section 8.2.1.5 is revised.

UFSAR Revision to Reflect Compliance with NRC Bulletin 96-03
Previous installation of larger capacity passive strainer designs per Design Change Packages (DCPs) 9600290, 9700300, 9700301, 9700302, 9700303, and 9700304 for Unit 1, and DCPs 9600291, 9700543, 9700544, 9700545, 9700546, 9700547 for Unit 2 accomplished the necessary physical changes for implementing Option 1 of NRC Bulletin 96-03, "Potential Plugging of Emergency Core Cooling Suction Strainers by Debris in Boiling Water Reactors". The replacement strainers significantly increase the surface and flow area so as to improve the ECCS pumps' ability to maintain adequate Net Positive Suction Head (NPSH) during potential plugging from fibrous material and other debris transported into the Suppression Pool under LOCA conditions. The Bulletin requires BWR licensees to implement appropriate measures to ensure the capability of the ECCS to perform its safety functions following a LOCA. UFSAR Section 6.3.2.2.6 is revised to conform with Regulatory Guide 1.70 requirements, and ECCS pumps characteristic curves Figures 6.3-3, 6.3-6, and 6.3-9 are revised to incorporate the latest vendor information. The revisions to these Figures supersede changes to the same Figures previously proposed in the the applicable DCPs mentioned above.

Editorial Revision to UFSAR Subsection 7.7.1.2.2
UFSAR Subsection 7.7.1.2.2 is revised to correct the typographical error of "seal" to "seat".

Revision to UFSAR Sections 9.3 and H.3 to reflect Service Air Receivers Drain Trap Upgrades
Design Change Packages (DCPs) 9700311, 9700312, and 9700313 upgraded the service air receiver traps for Units 0, 1, and 2, respectively. The applicable equipment part numbers are 0SA01DA, 0SA03M, 1SA01DA, 1SA03M,

2SA01DA, and 2SA03M. The upgrades consisted of adding redundant isolation valves on the cross-tie on the receiver supply lines, swapping of the inlet and outlet ports on the air receiver to reflect the original vendor design, replacing the drap with a newer style trap, and modifying pipe supports to accommodate new piping loads. The DCPs enhance the reliability of the isolation valves, the train traps, and allows the receivers the operate as designed. UFSAR Section 9.3, Table H.3-2, and drawing M-82 sheet 1 are revised accordingly.

UFSAR Revision to Reflect Drilling of Vent Holes in RHR Valve 1E12-F027A
Design Change Package (DCP) 9400401 drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 1E12-F027A. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent hole also resolves the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installation satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

'UFSAR Revision to Reflect Drilling of Vent Holes in RHR Valve 1E12-F027B
Design Change Package (DCP) 9400402 drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 1E12-F027B. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent hole also resolves the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installation satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

Revision to UFSAR Figures 5.2-2 and 5.3-5
Figure 5.2-5 provides values for the top of active fuel water level indication. The value that is presented with respect to vessel zero is incorrect. For that value, the elevation of the physical top of active fuel was provided instead. The change corrects the top of active fuel elevation to correctly reflect the physical location of the instrumentation setpoint and corrects the instrumentation value to reflect actual plant description. A footnote is added that clarifies the difference between the top of active fuel instrumentation setpoint and the physical top of active fuel.
Figure 5.3-2 provides nominal reactor vessel water level elevations. The elevations for the recirculation outlet nozzle, the feedwater nozzle, top of active fuel (TAF), and bottom of active fuel (BAF) are incorrect. The change corrects the values and adds a footnote that specifies the differences between fuel zone instrumentation setpoints and physical fuel elevations.

Revision to UFSAR per Design Change Package (DCP) 9500477
The DCP changed the power supply for the Unit 2 Group IV isolation logic from the reactor protection system (RPS) AC to 125 VDC to prevent isolation of the reactor

building ventilation system upon loss of a single RPS bus. UFSAR subsection 7.3.2.2.1, Figure 7.3-10, and Table 8.3-13 are revised.

UFSAR Revision to reflect use of Microtherm Type Insulation
Pre-moulded non-hydrophobic Microtherm insulation enclosed in a 24-gauge stainless steel jacket was installed on lines 1NB09A-2", 1NB09B-1", 1NB88A-1", 1NB24A-2", 1NB24B-1", and 1MSC6AK-3/4". The insulation was used on the above reactor vessel water level and main stem flow sensing lines in the Unit 1 drywell to improve reactor vessel water level instrumentation reliability through increased thermal efficiency. The microtherm insulation was used instead of metallic reflective insulation (MRI). UFSAR subsections 6.2.3.1.3, 6.1.1.1, and Table 6.1-2 are revised.

ECCS Suction Strainer Replacement per Design Change Package (DCP) 9700547
The DCP replaced the high pressure core spray (HPCS) suppression pool suction strainer to increase the surface area with a larger capacity strainer to reduce pump net positive suction head. UFSAR subsections 15.9.3.7 and 15.9.5, and Figures 6.3-3, 6.3-6, and 6.3-9 are revised.

UFSAR Revision per Design Change Package (DCP) 9700453
The DCP replaced a previously existing two-position selector switch with a three-position selector switch to provide one-out-of-three channel selection capability among narrow range reactor water level channels 2C34-N004A, B, or C. UFSAR subsections 7.7.4.2.1, 7.7.4.2.2, and Figure 7.7-5 are revised.

UFSAR Revision per Design Change Package (DCP) 9600324 Installation of Above Ground Diesel and Gasoline Fuel Tanks per Design Change Package (DCP) 9600324
The DCP placed the original in ground Diesel Fuel Oil and Gasoline tanks out of service. Two new 2000-gallon capacity tanks were installed above ground about 370 feet East-Northeast (ENE) of the main access facility, inside the protected area. UFSAR subsections 2.2.3.1, 2.2.3.2, and 3.5.1.5 are revised.

UFSAR Revision per Design Change Package (DCP) 9600219
DCP 9600219, New Exhaust Fan and Vent Duct For the Unit 2 TDRFP Room B, installed vane axial fan 2VT13CB and ductwork over the existing floor opening in TDRFP room 2B to create a forced transfer of air from the pump room to the heater bay below. UFSAR Table 9.4-13, and subsections H.3.5.1 and H.3.5.3 are revised.

UFSAR Revision per Design Change Package (DCP) 9600218
DCP 9600218, New Exhaust Fan and Vent Duct For the Unit 2 TDRFP Room A, installed vane axial fan 2VT13CA and ductwork over the existing floor opening in

TDRFP room 2A to create a forced transfer of air from the pump room to the heater bay below. UFSAR Table 9.4-13, and subsections H.3.5.1 and H.3.5.3 are revised.

UFSAR Revision per Design Change Package (DCP) 9600284, Elimination of Unit 2 Main Steam Isolation Valves Closure and Scram Functions of the Main Steam Line Radiation Monitors
The DCP improves unit availability by reducing spurious scrams and isolations caused by the Main Steam Line Radiation Monitors (MSLRMs). The original design function of the MSLRM was for detection/mitigation of consequences associated with fuel failure and the rod-drop design basis accident. The DCP consisted of the following: removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Protection System (RPS) Reactor Auto-Scram Trip logic circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Main Steam Line (MSL) Isolation and Drain Valve circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Water Sample Valve circuits and associated Normal/Test Selector Switches in Main Control Room (MCR) Panels, revising MSLRM's High and High-High alarm setpoints, rewiring MSLRM alarms per recommendation of ComEd Human Factors Group and Operations, rewiring computer digital inputs and outputs associated with the MSLRMs, revising off gas pre-treatment radiation monitor High and High-High alarm setpoints, and Add appropriate safety-related banana plugs per ComEd recommendation to one terminal at relays located in the Main Control Room panels. UFSAR Sections 1.2, 7.1, 7.2, 7.3, 7.6, 7.7, 7.A, 11.5, 15.2, and 15.4 are revised.

ECCS Suction Strainer Replacement per Design Change Package (DCP) 9600291
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 "A" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. UFSAR subsections 15.9.3.7 and 15.9.5, and Figures 6.3-3, 6.3-6, and 6.3-9 are revised.

Revision to UFSAR Sections 3.4 and 3.11
UFSAR Subsections 3.4.1.1, 3.4.1.4, 3.11.1.4.2, and Figures 3.4-1 and 3.4-2 are revised to more accurately describe the actual design and flood protection measures at LaSalle. The changes concern results from an operability assessment and walkdowns. Various design basis deficiencies associated with the location of certain lake-connected piping relative to the condenser pit flood zone, and deficiencies discovered with the elevation of certain ventilation ducts associated with the core standby cooling system (CSCS) and equipment water cooling system (ECWS) pump room flood zone, are addressed by the UFSAR changes.

UFSAR Update per Main Turbine and Reactor Feedwater Pumps Level 8 Trip Logic Control Modification, Design Change Package (DCP) 9600546
The DCP added an interlock from the Reactor Core Isolation Cooling (RCIC) Division 1 level 8 trip relay 2B21A-K705AX to Channel C trip logic of the main turbine / feedwater pumps trip due to a variable leg instrument line break for channel B and C. UFSAR subsection 7.7.4.2.1 and Figure 7.7-5 are revised to reflect the DCP.

UFSAR Change per Design Change Package (DCP) 9600463, Deletion of Timer Interlock for Valve 2E12-F048B
DCP 9600463 changed the interlock that prevents closure of RHR heat exchanger bypass valve 2E12-F048B during a LOCA from a 10 minute interlock to a permissive interlock. This allows cooling of the RHR LPCI injection by the RHR heat exchanger immediately rather than wait 10 minutes. The control circuit was also modified such that thermal overloads are always bypassed whenever an accident signal is present. UFSAR subsection 7.3.1.2.4.6 is revised.

Unit 2 Division 2 Residual Heat Removal - Service Water Keep Fill Cross-Tie, Design Change Package (DCP) 9600198
The DCP added two cross-ties to Division 2 of the Unit 2 residual heat removal (RHR) - service water (WS) system to ensure that it is kept filled and pressurized. One cross-tie is from the service water system, the other is from the diesel generator cooling water (DGCW) system. The cross-tie from WS will keep the RHR-WS system filled during normal operation, while the cross-tie from the DGCW will keep it filled in the event of an accident, Loss of Offsite Power (LOOP), or seismic event. UFSAR Sections 7.3.3.3.1, 9.2.1.2, 9.2.1.5, 9.2.2, and 9.2.2.2 are revised to include a discussion of the keep fill for Unit 2 Division 2 RHR-WS, addressing an overview of the keep fill system, interfaces with DGCW, and alarm annunciation.

UFSAR Change per Design Change Package (DCP) 9600462, Deletion of Timer Interlock for Valve 2E12-F048A
DCP 9600462 changed the interlock that prevents closure of RHR heat exchanger bypass valve 2E12-F048A during a LOCA from a 10 minute interlock to a permissive interlock. This allows cooling of the RHR LPCI injection by the RHR heat exchanger immediately rather than wait 10 minutes. The control circuit was also modified such that thermal overloads are always bypassed whenever an accident signal is present. UFSAR subsection 7.3.1.2.4.6 is revised.

UFSAR Change per Design Change Package (DCP) 9800113, Addition of HELB Excess Flow Check Damper 2VR91Y to the VR Exhaust Duct
7The DCP installed High Energy Line Break (HELB) excess flow check damper 2VR91Y between secondary containment isolation damper 2VR05YB and pressure

relief damper 2VR90Y in the VR system ductwork located on elevation 786'-6" in the Auxiliary Building.
The new check damper, in conjunction with the downstream pressure relief damper, maintains the pressurization of the masonry exhaust plenum within acceptable limits following a postulated HELB in the Unit 2 main steam tunnel.
UFSAR Table 3.2-1, and sections 9.4.2.1.1, 9.4.2.3, 9.4.2.4, and Table 9.4-6 are revised.

UFSAR Revision due to Design Change Package (DCP) 9500325
The internals of high pressure core spray (HPCS) check valve 2E22-F016 were removed. The valve was previously required to prevent draining of the cycled condensate storage tank (CST) in to the suppression pool. The valve is no longer required since the CST has been separated (blank flanged) from the high pressure core spray system. UFSAR Figure 6.3-1 (HPCS system process diagram) and drawing M-141 are revised.

UFSAR revision per Unit 2 Design Change Package (DCP) 9800276 – Loss of Coolant Accident (LOCA) / Purge Analysis
This DCP analyzed and modified the VQ piping system as a result of postulating a LOCA during containment purge. During investigation of LER 97-005, it was discovered that in the event of a LOCA coincident with containment purging, the VQ ductwork could potentially rupture and VQ piping downstream of the VQ Containment Isolation Valve could experience temperature increases beyond the originally analyzed conditions. The required support modifications for Unit 2 were performed per this DCP following the completion of the thermal modes analysis for the Unit 2 VQ and VG piping, supports, and penetrations. UFSAR sections 3.0, 3.11.1.1, and Tables 3.11-28 and Table 3.11-29 are revised as a result of this design change.

UFSAR revision per High Energy Line Break (HELB) Re-analysis
The UFSAR is revised to reflect new environmental parameters following a HELB. The reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) HELB calculation initially was being revised as a result of design change packages (DCPs) 9700208 and 9700209, which return the RWCU system to hot suction. Review of the calculation led to the identification of non-conservatisms (Licensee Event Report 97-033). Corrective action modifications were subsequently implemented. The UFSAR changes revise the reactor building parameters and equipment qualification (EQ) zones. UFSAR Sections 3.0, 3.6, 3.11, Table 3.11-6, and Figure 3.11-1 Sheets 1, 2, 3, and 4 are revised.

UFSAR Update to Table 8.3-1
UFSAR Table 8.3-1, Load on 4160-Volt ESF Buses, identifies the coincidental loading on the 4160 volt ESF buses following a Loss Of Coolant Accident (LOCA) on Unit 1 and

a simultaneous Loss Of Offsite Power (LOOP) for both units. The table is revised to correct calculational errors, and to correct sum totals of the loads to reflect revised loads.

UFSAR Update for Lost Parts Analyses
UFSAR Subsection 4.2.3.13 and 4.2.5 are revised to reflect the new lost parts analysis from Siemens Power Corporation (SPC) and the latest revision to General Electric's lost parts document (NEDO-10174, Revision 1). The SPC analysis was performed in support of introducing the use of ATRIUM-9B fuel at LaSalle Station.

Revision to UFSAR for Installation of Unit 1 OPRM per Design Change Package (DCP) 9700500
DCP 9700501 installed a microprocessor based oscillating power range monitor (OPRM) system on Unit 1. The OPRM is intended to detect and suppress core oscillations that BWRs are susceptible to during high power – low coolant flow conditions. Once it is armed, the OPRM will function to automatically suppress oscillations. UFSAR Chapters 1, 3, 4, 7, and 15 are revised.

Editorial Revisions to UFSAR Section 7.3
Various parts of UFSAR Section 7.3 are editorially revised to correct the description associated with the Emergency Core Cooling System (ECCS).

UFSAR changes per Design Change Package (DCP) 9700209 – Unit 2 Reactor Water Cleanup (RT) System Recirculation Pumps and Return to Hot Suction.
The DCP restored the "hot suction" configuration of the Unit 2 RT system, as originally designed by General Electric, by replacing / reworking piping and associated valving. The design change installed the Reactor Water Cleanup pumps upstream of the system heat exchangers and routed the piping from outside the primary containment to the pump suction bypassing the heat exchangers. The pump discharge was routed to the system heat exchangers. The DCP replaced the three existing non-safety related 50% capacity RT System recirculation pumps with two new 100% capacity pumps. UFSAR Sections 1.7, 4.6.1.1.2.4.2, 5.4.8.2, 7.3.2.2.3.8, 7.7.1.2.1, and 9.2.3.2, Tables 5.4-1, 8.1-2, 8.1-10, 8.3-1 Sheet 2, 12.3-16 Sheet 1, Figures 4.6-5, 4.6-6, 5.4-6 Sheets 1, 2, and 3, 5.4-8, 8.3-4, 12.3-1 Sheet 4, 12.3-2 Sheet 4, 12.3-4 Sheet 2, and H.2-1 Sheet 3 are revised accordingly.

Revision to UFSAR Section 9.2 for the Core Standby Cooling System Equipment Cooling
Core Standby Cooling System (CSCS) equipment cooling flow rates, specifically those of the northwest, southwest, southeast, and northeast cubicle area cooling coils are

revised to reflect station efforts to re-balance the CSCS equipment cooling water system per the implementation of NRC Generic Letter 89-13.

Revision to UFSAR Table 6.2-21 and Figure 6.2-31
UFSAR Table 6.2-21 and Figure 6.2-31 are revised to reflect the correct valve arrangement and figure detail for containment penetration M-37. The revised UFSAR Figure 6.2-31 contains a new detail showing the configuration of the clean condensate (MC) system piping and valve drops inside the primary containment.

DCP 9700554, Replacement of 24/48 VDC lead-antimony batteries 1DC31E and 1DC32E with lead-calcium batteries
DCP 9700555 Replacement of 24/48 VDC lead-antimony batteries 1DC33E and 1DC34E with lead-calcium batteries
Inspections of the model DKR-13 24/48 VDC battery cells revealed damage due to swelling of the post seals, which cracked cells and deteriorated the plastic hold down nuts. These batteries provide power to the process radiation monitors and the SRM and IRM startup range neutron monitors. The DKR-13 batteries are no longer manufactured. Based upon the recommendation of the manufacturer, GNB Technologies, the DKR-13 batteries were replaced with GNB's lead-calcium model 2-MCX-5 batteries. UFSAR Section 8.3.2.1.1 is revised.

UFSAR Update per Main Turbine and Reactor Feedwater Pumps Level 8 Trip Logic Control Modification, Design Change Package (DCP) 9600546
The DCP added an interlock from the Unit 2 Reactor Core Isolation Cooling (RCIC) Division 1 level 8 trip relay 2B21A-K705AX to Channel C trip logic of the Main turbine / Feedwater pumps trip. This change allows the RCIC Division 1 level 8 trip to actuate the 'C' channel main turbine / feedwater pumps level 8 trip. UFSAR Figure 7.7-5 Sheet 1 and Subsection 7.7.4.2.1 are revised to reflect the DCP.

UFSAR Update per Installation of Test Tees for Excess Flow Check Valves per Design Change Package (DCP) 9800311
The DCP provides for an alternate method for testing Unit 2 excess flow check valves (EFCV) in the Nuclear Boiler (NB) system instrument lines.
Local leak rate testing (LLRT) is performed for the EFCVs during the Unit 2 nuclear boiler hydrostatic test, which consists of filling and pressuring the reactor pressure vessel. This often delays completion of the hydrostatic test, as valves which fail LLRT can't be certified as operable. The test tees are located between the manual isolation valve outside the primary containment penetration and the excess flow check valve (EFCV). The test tees, valves, and capped test connections provide a method of leak testing cxcess flow check valves with the upstream isolation valve closed, independent of the pressure vessel hydrostatic test. This will be the preferred method of testing, although leak testing during the hydrostatic test will remain an acceptable option.

UFSAR Table 3.2-1 sheet 2, Table 6.2-21 Sheet 1C, and Figures 6.2-31 Sheets 9 and 10 are revised. The proposed change for Figure 6.2-31 sheet 10D, detail (AE), which was previously issued per DCP 9800139, is deleted.

Revision to UFSAR per Design Change Package (DCP) 9100215
DCP 9100215 permanently installed Transient Analysis Data System (TADS) Panel 2PA19J and associated cables in a permanent location inside the Unit 2 Auxiliary Electrical Equipment Room (AEER). Previously, the TADS panel was rolled from a storage area and plugged into the Startrec panel as needed. UFSAR Figure H.4-2 is revised to reflect the resulting Unit 2 Auxiliary Electric Equipment Room layout.

Revision to UFSAR per Design Change Package (DCP) 9600120
DCP 9600120 removed the packing leakoff line from reactor recirculation (RR) suction valve 2B33-F023A. UFSAR Figure 7.3-7 Sheet 2 is revised.

UFSAR revision per Design Change Package (DCP) 9700462 - Removal of Unit 2 Main Steam Isolation Valve (MSIV) Closure Scram Bypass Pressure Switches
This DCP disconnected and removed the existing MSIV closure bypass pressure switches 2B21-N020A, 2B21-N020B, 2B21-N020C, and 2B21-N020D along with the associated tubing, valves and fittings from instrument racks 2H22-P004, 2H22-P027, 2H22-P005 and 2H22-P026 respectively. The cables between the instrument racks and the main control room (MCR) panels were de-terminated and left in place unassigned, and the associated terminal points in the MCR panels were jumpered. UFSAR Sections 7.2.2.4.6, 7.A.2.1.2, 7.A.2.1.14, 7.A.3.2, and 15.2.4 are revised.

UFSAR Change for Unit 2 Division 1 Core Standby Cooling System Local Flow Indicators and Motor Operated Valve Removal, Design Change Package (DCP) 9800320
The DCP installed two locally indicating flow elements (calibrated flow orifices) in Core Standby Cooling System (CSCS) supply and return lines. One was installed upstream of the low pressure core spray (LPCS) pump motor cooler, and the other was installed downstream of the northwest (NW) cubicle area cooler. Motor operated valve (MOV) 2DG035 was removed from the LPCS Pump Motor Cooler supply line and a flanged orifice installed. UFSAR Sections 9.2.1.2 and 9.2.1.5 are revised to reflect the new flow element on the inlet to the LPCS pump motor cooler.

Revision to UFSAR for Unit 2 P-Bypass Setpoint, Design Change Package (DCP) 9800068
DCP 9800068 revised the Unit 2 P-Bypass setpoint from less than or equal to 30% rated thermal power (RTP) to less than or equal to 25% RTP. Implementation of the revised setpoint is permitted per issuance of License Amendments number 114 to

Facility Operating License NPF-18 (Unit 2). The P-Bypass setpoint is the core thermal power below which the reactor protection system scram signals initiated by turbine stop valve (TSV) closure, turbine control valve (TCV) fast closure, and end-of-cycle reactor recirculation pump (EOC-RPT) trips are bypassed. LaSalle Unit 2 has approximately a 30% steam bypass capability. A scram on turbine control valve or turbine stop valve closure is not needed until 30% RTP is reached, as adequate bypass capacity is available. Reduction of this setpoint to 25% aids the plant transient response between 25% and 30% RTP. TCV / TSV fast closure and EOC-RPT pressure switches 2C71-N003A, 2C71-N003B, 2C71-N003C, and 2C71-N003D were replaced with Ashcroft B4 series pressure switches. UFSAR Sections 7.2, 7.A.2, 15.2, 15.3, G.3, and G.5 are revised.

Revision to UFSAR per Design Change Package (DCP) 9600121
DCP 9600121 removed the packing leakoff line from reactor recirculation (RR) suction valve 2B33-F023B. UFSAR Figure 7.3-7 Sheet 2, Table G.B.1-1 Sheet 1, drawings M-139 Sheet 2, M-157 Sheet 1, and M-2139 Sheet 9 are revised.

Modification to Unit 2 Containment Leak Test Channels per Design Change Package (DCP) 9800042
The DCP removed eighteen leak test plugs for the leak test system around the Unit 2 safety relief valve (SRV) pipe support embedment plates at the containment wall above elevation 700' -0" in the Unit 2 suppression pool. The DCP also clarifies that all other test plugs in the suppression pool and the containment drywell may be permanently left in place. The leak-test channels were originally installed over containment liner welds so that these welds could be pressure tested to verify leak-tightness. Threaded plugs were installed in openings in these leak-test channels to facilitate this pressure testing. It was the intent of the original design that these plugs be removed after these local leakage tests were complete so that during future Containment Integrated Leak Rate Tests (CILRT), the liner welds would see the test pressures. The leak-test channels and plugs were not designed to act as the containment pressure boundary. Licensee Event Report (LER) 97-030 documents that the plugs were not removed as originally intended after the initial local leak rate tests. UFSAR Subsections 6.2.1.1.2 and 6.2.6.1 are revised.

UFSAR revision to reflect Unit 2 Design Change Package (DCP) 9700131, Replacement of Unit 2 Loose Parts Monitoring System (LPMS)
The DCP removed the loose parts monitoring equipment from panel 2PA15J and replaced it with a new state-of-the-art data acquisition system manufactured by Siemens Power Corporation. The new equipment is designed to work with existing accelerometers and preamplifiers (charge converters), and the existing annunciator system and power supply. The previous LPMS did not conform to the configuration described in the SER and the response to FSAR Question 221.14. UFSAR Section

4.4.6.1 is revised to include a description of the installed upgraded LPMS configuration applicable to Unit 2.

UFSAR Change resulting from Design Change Package (DCP) 9700398, Turbine Building Supply Airflow Reduction for Turbine Building Negative Pressure
The DCP reduced the supply air to the Turbine Building to ensure a negative pressure is maintained by installing two recirculation dampers on the common supply header of the turbine building ventilation (VT) system supply fans 2VT01CA, 2VT01CB, and 2VT01CC. The dampers are installed in the supply air header before it penetrates the VT system supply air housing. UFSAR Sections 9.4 and 11.3 are revised.

UFSAR Change to Reflect Modification of the Unit 2 Condensate Polishing Demineralizer Panel Design Change Package (DCP) 9600572 (Modification M01-2-9600572)
The DCP removed the condensate polisher automatic regeneration mode of operation from Unit 2, in addition to removing the valve interlocks and permissives which control transfer between the condensate polishers (CP) and the tanks related to regeneration, to instead be controlled by manual operator action from the control panel. The DCP modified the transfer of resin from the cation/separation tank to the mix/storage tank. The Unit 2 regenerate cycle no longer includes the full chemical cleaning process. UFSAR Subsections 10.4.6.2, 10.4.6.3, 10.4.6.5, 11.2.1.7, 11.2.1.7.1, and 11.2.2.3 are revised to reflect that regeneration is no longer possible in Unit 2.

UFSAR Change per Design Change Package (DCP) 9500083, Implement Hydrogen Addition to Unit 2
The DCP upgraded process sample panels 2PL13J, 2PL14J, and 2PL40J in support of hydrogen water chemistry (HWC) addition to Unit 2. UFSAR Table 9.3-1 Sheets 1 and 2 are revised.

DCP 9700556, Replacement of 24/48 VDC lead-antimony batteries 2DC31E and 2DC32E with lead-calcium batteries
DCP 9700557 Replacement of 24/48 VDC lead-antimony batteries 2DC33E and 2DC34E with lead-calcium batteries
Inspections of the model DKR-13 24/48 VDC battery cells revealed damage due to swelling of the post seals, which cracked cells and deteriorated the plastic hold down nuts. These batteries provide power to the process radiation monitors and the SRM and IRM startup range neutron monitors. The DKR-13 batteries are no longer manufactured. Based upon the recommendation of the manufacturer, GNB Technologies, the DKR-13 batteries were replaced with GNB's lead-calcium model 2-MCX-5 batteries. UFSAR Section 8.3.2.1.1 is revised.

UFSAR Revision to reflect Design Change Package 9700568
DCP 9700568 installed a warm weather manual bypass blade in the two ventilation intake dampers of the 2B diesel generator (DG) ventilation equipment room. The bypass blade was installed to allow in-leakage of outside air into the DG room during the summer per original design. UFSAR Sections 9.4 and 9.5 are revised.

UFSAR Revision per Removal of Remote Indication Hardware from Unit 2 Division 1 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700490
DCP 9700490 removed remote indication hardware from Unit 2 Division 1 ECCS testable check valves 2E12-F041A, 2E12-F050A, and 2E21-F006, to eliminate a recurring problem in which the valves fail to completely close. This was attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves the performance of each valve, increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.2.2.3, 6.3.2.2.4, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.3.1, 7.3.1.2.4.1, 7.3.1.2.5, 7.A.3.1.1.1, 7.A.3.1.1.2, 9.3.1.2.2, and Table 6.2-21 Sheet 11 are revised.

Removal of Remote Indication Hardware from Unit 2 Division 2 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700491
DCP 9700491 removed remote indication hardware from Unit 2 Division 2 ECCS testable check valves 2E12-F041B, 2E12-F041C, and 2E12-F050B, to eliminate a recurring problem in which the valves fail to completely close. This was attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves the performance of each valve, increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.2.2.4, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.4.1, 7.3.1.2.5, 7.A.3.1.1.1, 9.3.1.2.2, and Table 6.2-21 Sheet 11 are revised.

UFSAR Revision to Reflect Unit 2 ECCS RHR B Suction Strainer Replacement, Design Change Package (DCP) 9700543
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 "B" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Figure 6.3-9 and Subsections 15.9.3.7 and 15.9.5 are revised.

UFSAR Revision to Reflect Unit 2 ECCS RHR C Suction Strainer Replacement, Design Change Package (DCP) 9700544
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 "C" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Figure 6.3-9 and Subsections 15.9.3.7 and 15.9.5 are revised.

UFSAR Revision to Reflect Unit 2 ECCS RCIC Suction Strainer Replacement, Design Change Package (DCP) 9700545
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 Reactor Core Isolation Cooling (RCIC) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Subsection 15.9.3.7 and 15.9.5 are revised.

UFSAR Revision to Reflect Unit 2 ECCS LPCS Suction Strainer Replacement, Design Change Package (DCP) 9700546
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 low pressure core spray (LPCS) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Figure 6.3-6 and Subsection 15.9.5 are revised.

Revision to UFSAR Section 5.4.7.2.2.3
Valve 2E51-F091 was physically removed from the reactor core isolation cooling (RCIC) System by design change package (DCP) 9500158, which was completed on 8/16/96. The safety evaluation associated with the DCP evaluated the removal of the valve from the system. The RCIC steam to RHR warmup valve, 2E51-F091, previously used in the Steam Condensing Mode of RHR, has been deleted since the steam condensing mode of RHR has been deleted from use at LaSalle.
DCP 9500158 revised UFSAR Tables 6.2-21 (Summary of Lines Penetrating the Primary Containment) and 6.2-28 (Primary Containment Isolation Valves) to reflect deletion of the 2E51-F091 valve. Valve 2E51-F091 was not deleted from the list of

Steam Condensing valves in UFSAR Section 5.4.7.2.2.3. UFSAR Section 5.4.7.2.2.3 is correspondingly revised to delete valve 2E51-F091.

Revision to UFSAR Appendix H
UFSAR Appendix H Subsection H.4.2.47.2 is not related to the suppression pool cooling path, as the valves described are not associated with a suppression pool cooling path. The only RHR loop A cables or equipment in fire subzone 4E2-1 necessary for safe shutdown is a flow indicator circuit. The revised discussion describes the indication available in lieu of a flow indicator.
Tables H.4-51 (Sheet 6 of 6), H.4-58 (sheet 5 of 5), H.4-65 (Sheet 4 of 5), H 4-68 (Sheet 6 of 6), H.4-70 (Sheet 7 of 7) and H.4-104 (Sheet 2 of 2) are revised to correct an erroneous cable number. Plant walkdowns and drawing reviews determined that an incorrect safe shutdown cable number is stated in the above Tables.

UFSAR Revision to Correct Section 15.2
The proposed change corrects turbine feedwater pump low condenser vacuum trip sepoint discrepancy and the time to trip discrepancy in the loss of condenser vacuum accident scenario in UFSAR Subsections 15.2.5 and 15.2.3.

Revision to UFSAR Subsection 12.5.3.2 for Dosimetry Collection
UFSAR Subsection 12.5.3.2 is revised to reflect the station practice of reading the thermoluminescent dosimeters (TLDs) on a quarterly frequency. The TLDs measure the amount of radiation received by individuals working at the station. TLDs were previously changed out on a monthly frequency. The UFSAR revision achieves consistency with ComEd's and industry practices. TLD collection permits recording each individual's permanent dose history. The annual exposure report is based on the information collected by the TLDs. Testing has demonstrated that TLDs will not indicate erroneous data due to the longer exposure time.

UFSAR Revision to reflect Installation of Manual Vacuum Breaker Downstream of Valve 1E12-F021 per Design Change Package (DCP) 9800345
The DCP installed a one-inch pipe with manual globe valves and a pipe cap downstream of the Unit 1 residual heat removal (RHR) C full flow test return line stop valve, 1E12-F021. This modification provides a convenient means of breaking vacuum and draining down the line following a full flow test to protect against water hammer. UFSAR Figure 6.2-31 sheet 7, Table 6.2-21, and Drawing M-96 sheet 3 are revised. A new sheet is added to Figure 6.2-31.

UFSAR Revision for Clarification of Corrosion Inhibitor and Glycol Concentration Requirements
UFSAR Subsections 9.2.3.2, 9.2.8.2, 9.2.10.2, 9.5.5.2, and Tables 9.2-1 and 9.2-2 are revised to clarify corrosion inhibitor requirements for the turbine building closed cooling

water (TBCCW), reactor building closed cooling water (RBCCW), and diesel generator closed cooling water systems, and to clarify station heat recovery glycol concentration requirements. The change provides sufficient latitude to allow alterations in closed cooling water system corrosion inhibitors based on corrosion conditions in the system. The specified minimum weight percentage of ethylene glycol concentration prevents freezing, while allowing some latitude for glycol concentrations to change as a result of normal system operations.

Revision to UFSAR Section 9.4.3.4.2.b and 9.4.3.4.2.c
UFSAR Sections 9.4.3.4.2.b and 9.4.3.4.2.c provide specific information that implies the operational configuration of the radwaste building supply and exhaust fans. This change deletes the nominal fan capacities and number of fans operated from these paragraphs. This change provides the flexibility operate the radwaste building supply and exhaust fans in the configuration required by plant conditions.

Revision to UFSAR Appendix L
UFSAR Appendix L item L.75 is revised to reflect that the description of the Technical Support Center (TSC), Operational Support Center, and Emergency Operations Facility are contained within the ComEd Offsite Dose Calculation Manual (ODCM).

UFSAR Revision for Drilling of Vent Hole in Valve 1E22-F012 per Design Change Package (DCP) 9800347
The DCP drilled a 1/4" vent hole in the upstream disc of valve 1E22-F012. The valve is the high pressure core spray (HPCS) high pressure pump minimum flow valve. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. Addition of the vent hole satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

UFSAR Revision per Design Change Package (DCP) 9700420, Heater Drain Pump Minimum Flow Changes to Facilitate Idle Pump Warm-up
Solenoid valves were added to the minimum flow bypass valves of the Unit 2 heater drain system (HD) pumps recirculation lines. This enables the valves to remain open for a period of time sufficient to allow recirculation of cold water in idle heater drain pumps upon startup of the idle pumps. Timer relays were added in the switchgear for the HD pumps to provide an adjustable timer permissive for energizing and deenergizing the solenoid valve. The pump discharge flow (differential pressure type) transmitters were replaced with flow transmitters that provide linear outputs, eliminating the need for square root extractors to modulate the DP type signal into a linear signal. Pressure breakdown devices in the minimum flow bypass line were replaced with straight pipe to allow for a greater flow of cold stagnant water back to the heater drain tank. UFSAR Section 10.4.7.2 is revised.

UFSAR Revision to Reflect Drilling of Vent Holes in RHR Valves 2E12-F027A and 2E12-F027B

DCP 9400404 drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 2E12-F027B, and DCP 9400405 drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 2E12-F027A. The holes were drilled on the side closest to the associated RHR heat exchanger. Each hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent holes also resolve the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installations satisfy a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

UFSAR Change for Installation of Bonnet Vent on Valve 2E51-F031, Design Change Package (DCP) 9600295

The DCP added a bonnet assembly to allow for a point of release of bonnet pressure in the event of a pressure locking condition of reactor core isolation cooling (RCIC) pump suppression pool suction isolation stop gate valve 2E51-F031 on pipeline 2RI17A-8". Gate valve 2E51-F031 was susceptible to pressure locking resulting from water accumulation in the bonnet area in conjunction with temperature and/or system pressure changes. Accumulated water in the bonnet may have prevented the valve from opening due to an increase in pressure in the bonnet resulting from temperature changes (increase) at the valve location or a drop in the process pipeline pressure while the trapped bonnet pressure remains high. The bonnet vent line provides a vent path to release the pressure in the bonnet to prevent pressure locking of the valve. The bonnet vent line satisfies a LaSalle commitment to Generic Letter 95-07 by providing a means to vent the bonnet. UFSAR Table 6.2-21 is revised.

UFSAR Revision per Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-26 and M-28, Design Change Package (DCP) 9700337

The DCP installed a ¾" diameter relief valve assembly on containment penetration M-26 and M-28 (VP Train B) piping between the respective inboard containment isolation valves 2VP113B and 2VP114B. The DCP was implemented to resolve overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. The addition of the relief valve prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the primary containment becomes isolated and experiences a pressure and temperature rise as a result of the accident. The water volume between the inboard isolation valves 2VP113B and 2VP114B and the respective outboard isolation valves, 2VP063B and 2VP053B, becomes trapped. The valve provides a relief path to prevent overpressurization of the piping and valves. UFSAR Table 6.2-21, 6.2-28, and Figure 6.2-31 are revised accordingly.

UFSAR Revision per Generic Letter 96-06 Overpressurization Protection for Unit 2 Primary Containment Piping, Design Change Package (DCP) 9700342
The DCP installed a ¾" diameter relief valve assembly between containment penetration M-7 and Inboard Containment Isolation valves 2E12-F009. This was done to resolve overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. The addition of the relief valve prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the Primary Containment becomes isolated and experiences a pressure and temperature rise as a result of the accident. The volume of water between the inboard containment isolation valve 2E12-F009 and outboard containment isolation valve 2E12-F008 containment isolation valve becomes trapped. As the temperature of the trapped water rises, without a relief path, the pipe and valves could become overpressurized. UFSAR Tables 5.2-6, 6.2-21, and 6.2-28, and Figure 6.2-31 are accordingly revised.

UFSAR Revision for Drilling of Vent Hole in Valve 2E22-F012 per Design Change Package (DCP) 9800346
The DCP drilled a 1/4" vent hole in the upstream disc of valve 2E22-F012. The valve is the high pressure core spray (HPCS) high pressure pump minimum flow valve. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. Addition of the vent hole satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

UFSAR Revision per Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-25 and M-27, Design Change Package (DCP) 9700338
The DCP installed a ¾" diameter relief valve assembly on containment penetration M-25 and M-27 (VP Train A) piping between the respective inboard containment isolation valves 2VP113A and 2VP114A. The DCP was implemented to resolve overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. The addition of the relief valve prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the primary containment becomes isolated and experiences a pressure and temperature rise as a result of the accident. The water volume between the inboard isolation valves 2VP113A and 2VP114A and the respective outboard isolation valves, 2VP063A and 2VP053A, becomes trapped. The valve provides a relief path to prevent overpressurization of the piping and valves. UFSAR Table 6.2-21, 6.2-28, and Figure 6.2-31 are accordingly revised.

UFSAR Revision to Reflect the Unit 2 Cycle 8 Reload Licensing Package
UFSAR Sections 1.2, 1.6, 3.1, 3.9, 4.0, 5.0, 4.1, 4.2, 4.3, 4.4, 5.2, 6.0, 6.3, 6.B, 6.3, 7.7, 10.4, 15.0, 15.1, 15.2, 15.3, 15.4, 15.5, 15.6, 15.7, 15.8, 15.A, G.3, and G.7 are revised for Unit 2 Cycle 8 operation. The changes reflect Unit 2 operation with fuel

manufactured by Siemens Power Corporation (SPC) and General Electric (GE). SPC Atrium 9B fuel and analytical methodologies are reflected in the changes.

UFSAR Revision Associated with Replacement of Internals and Removal of Stem Leakoff Line of Reactor Recirculation Isolation Valve 2B33-F023
Design Change Package (DCP) 9600121 installed a new valve bonnet, disc, and stem to reactor recirculation (RR) pump suction valve 2B33-F023B in accordance with vendor recommended upgrades. The revised stem provides a packing design with a single stack and no gland area. The stem leakoff line to the gland seal leakoff reservoir was accordingly removed. UFSAR Figure 7.3-7 and Table G.B.1-1 are revised.

UFSAR Revision per Replacement of Limitorque Actuator and Motor on Motor Operated Valve 2G33-F001
Design Change Package (DCP) 9700525 replaced the 15 ft-lb. SMB-0 actuator on valve 2G33-F001 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed to provide power to the motor operated valve and the molded case circuit breaker and thermal overload relay were replaced. The DCP asle drilled a vent hole in the upstream (reactor side) disc of valve 2G33-F001 to address NRC Generic Letter (GL) 96-06 concerns dealing with primary containment isolation valve arrangements that are susceptible to thermal overpressurization following a LOCA in the drywell. UFSAR Table 6.2-28, Table H.4-16, Table H.4-19, Table H.4-23 and Table H.4-49 are accordingly revised.

UFSAR Revision per Replacement of Limitorque Actuator and Motor on Motor Operated Valve 2G33-F004
Design Change Package (DCP) 9700526 replaced the 15 ft-lb. SMB-0 actuator on Valve 2G33-F004 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed to provide power to the motor operated valve and the molded case circuit breaker and thermal overload relay were replaced. UFSAR Table 6.2-28, Table H.4-16, Table H.4-19, Table H.4-23 and Table H.4-49 are accordingly revised.

UFSAR Revision per Replacement of Emergency Diesel Generator 2B Speed Sensor
The station's diesel generators have experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. Design Change Package 9800005 replaced and upgraded the speed sensor assembly of the 2B emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson

DG speed switch. UFSAR Section 1.7, Electrical, Control and Instrumentation drawings, is accordingly revised.

UFSAR Revision per Replacement of Diesel Generator 2B VAR Meter
Design Change package (DCP) 9600117 replaced the Diesel Generator (DG) 2B VAR meter and transducer. Due to failures of the DG VAR metering equipment and their obsolescence, the metering equipment was replaced to provide more reliable VAR indication with consistent ranges. UFSAR Table H.4-92 is accordingly revised.

UFSAR Revision per Replacement of Unit 1 Backup Overspeed
Design change package (DCP) 9800352 replaced a backup overspeed relay megacycler card in Unit 1 electrohydraulic control (EHC) system with a frequency/voltage circuit card. The original megacycler card is obsolete and is no longer available. An industry forced outage has been attributed to a failed megacycler card. The design change is an EHC system scram reduction effort. UFSAR Section 10.2 is revised.

UFSAR Revision per Installation of Emergency Battery Packs for Valves 2E12-F003, 2E12-F018B, and 2E12-F047B Design Change Package (DCP) 9700002
The DCP installed an emergency battery pack for valve 2E12-F003B, 2E12-F018B, and 2E12-F047B in order to illuminate the valve operators in accordance with 10CFR50 Appendix R requirements. The power for the battery pack is fed from 480-V motor control center (MCC) 234X-2, Compartment D2, through regular lighting cabinet (RLC) #216. UFSAR Tables H.4-3, H.4-30, and H.4-31 are revised.

UFSAR Revision per Generic Letter (GL) 96-06 Overpressure Protection for Reactor Recirculation Containment Penetration M-36 Piping, Unit 2 Design Change Package (DCP) 9700344
The DCP installed a ¾" diameter bypass line, including a check valve and a manual isolation globe valve, around Inboard Containment Isolation Valve 2B33-F019 to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the bypass check valve will prevent potential over-pressurization during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event. UFSAR Table 6.2-21, Table 6.2-28, and Figure 6.2-31 are revised.

UFSAR Revision per Generic Letter 96-06 Overpressure Protection for Reactor Building Closed Cooling Water Containment Penetrations, Unit 2 Design Change Package (DCP) 9700340
The DCP installed ¾" diameter relief valve assemblies between containment penetrations M-16 and M-17 and the associated inboard containment isolation valves 2WR179 and 2WR180, respectively. The DCP resolves overpressure protection

concerns as part of LaSalle's response to NRC Generic Letter 96-06. Adding the relief valves prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the Primary Containment becomes isolated and experience a pressure and temperature rise as a result of the accident. The volume of water between the inboard (2WR179 and 2WR180) and outboard (2WR029 and 2WR040) containment isolation valves becomes trapped. The relief valve provides a path to prevent overpressurization. UFSAR Table 6.2-21, 6.2-28 Sheet 7, and Figure 6.2-31 are revised accordingly.

Revision to UFSAR Chapter 11
UFSAR Section 11.2.2.2 is revised to reflect the use of ion exchange resins for floor drain processing. UFSAR Section 11.4 is revised to reflect the present strategy of using offsite vendors for compaction/incineration, and/or sorting of dry active waste (DAW). UFSAR Table 11.4-2 is revised to reflect present disposal volumes. These changes result from a corporate radiation protection self assessment.
LU1999-101 Revision to UFSAR per Design Change Package (DCP) 9600119
DCP 9600119 removed the packing leakoff line from reactor recirculation (RR) suction valve 1B33-F023B. UFSAR Figure 7.3-7 Sheet 2, Table G.B.1-1 Sheet 1, drawings M-93 sheet 2, M-155 Sheet 1, and M-2093 sheet 9 are revised.

Revision to UFSAR Subsection 7.2.2.10
UFSAR Subsection 7.2.2.10 indicated that the system response times of all trip channel sensors were verified during pre-operational testing. UFSAR Subsection 7.2.2.10 is revised to state that the response time testing was of those functions with times assumed in the accident analysis. This provides for agreement with Technical Specifications and aligns with actual pre-operational testing.

UFSAR Revision per Design Change Package (DCP) 9600156
The DCP upgraded reactor recirculation flow control valve 2B33-F060A and B position monitoring by providing redundant rotary variable differential transformer (RVDT) based valve position indication in addition to the linear variable differential transformer (LVDT) based valve position indication to be selectable by a selector switch, upgraded the (LVDT) based valve position indication instrumentation, and upgraded cable connections for linear velocity transducer (LVT) based flow control valve velocity fedback monitoring instrument loops. UFSAR Section G.5.2.3.4.11 is accordingly revised.
LU1999-105 Revision to UFSAR Drawings M-74 and M-127, and Subsection 9.2.7.3
Drawings M-74 Sheet 1 (Unit 1 Cycled Condensate Storage System) and M-127 Sheet 1 (Unit 2 Cycled Condensate Storage System) incorrectly show the ASME Code breaks and piping design tables for the high pressure core spray (HPCS) and reactor core isolation cooling (RCIC) cycled condensate storage tank suction lines. UFSAR subsection 9.2.7.3 is revised to clarify the correct extent of the seismic qualification for

the RCIC suction lines to the cycled condensate storage tanks and the method used for switchover to the suppression pool.

UFSAR Revision to reflect Unit 1 P-Bypass Setpoint Change, Design Change Package (DCP) 9800067
The DCP changed the Unit 1 P-bypass setpoint from $\leq$ 30% of reactor thermal power (RTP) to $\leq$25% of RTP. The P-bypass setpoint is the RTP level below which the reactor protection system scram signals initiate stop valve closure, turbine control valve fast closure, or end of cycle recirculation pump trip are bypassed. This change resolves difficulties associated with low power transient response analysis required at each fuel reload. The DCP incorporates Amendment 130 to facility license NPF-11, approved February 12, 1999. UFSAR Sections 6.B, 7.2, 7.A.2, 15.2, 15.3, G.3, and G.5 are revised.

UFSAR Revision to Chapter 9.1, Fuel Handling and Storage
UFSAR Chapter 9.1 was to revised to make the UFSAR consistent with the plant's operating license; Clarify that either pool may store new or spent fuel from either unit; Reflect that LaSalle has chosen to comply with 10CFR50.68(b), "Criticality Accident Requirements"; and corrected typographical errors.

Revision to UFSAR Section 7.6
UFSAR Subsection 7.6.2.2.4 is revised to state that there is one (as opposed to *two*) set of two differential pressure switches connected to measure the differential pressure created as steam flows past an elbow in the line so that the steam flow rate through it can be monitored.

Revision to UFSAR Chapter 9 and Volume X
The title for drawing M-82 is corrected in Chapter 9.0 Table of Contents for Drawings, changed to "Service Air System".
UFSAR Section 9.3.1.3 discusses the verification of design to a loss-of-pneumatic supply accident as a part of the preoperational test of the Drywell Pneumatic System. This section states that the Station Air System demonstration verifies that valves fail as designed on loss of air. This section refers the user to Table 14.2-72 of the FSAR for a listing of the valves. Table 14.2-72 of the FSAR does not include a listing of the valves which fail due to loss of air. The statement "as listed in Table 14.2-72 of the FSAR" is deleted from paragraph 6.
Drawing M-81-FD is added to Volume 10 of the UFSAR. The Drawing Index is revised as well. Drawing M-81 is referenced in the text section 9.3.1.2.1, but Drawing M-81-FD will be added in Volume 10 to provide a simple diagram of the Instrument Air System.

Change to UFSAR Section 7.7.4.2.2

The change deletes parenthetical information in a sentence in the "Interlock" subsection of UFSAR Section 7.7.4.2.2. The parenthetical information is misleading and it conflicts with information contained in UFSAR Section G.2.3.3.2.2. UFSAR Section 7.7.4.2.2 Equipment Design, Interlock subsection, first paragraph, second sentence is revised from "... recirculation flow is reduced (after a time delay) to within the power..." is changed to "... recirculation flow is reduced to within the power...".

Revision to UFSAR Section 7.7
UFSAR Subsections 7.7.2.2.3.3 and 7.7.2.2.3.4 were revised due to incomplete descriptions of the Source Range Monitor (SRM) rod block functions and bypasses. The change adds information to fully describe the interlocks involved in bypassing SRM rod blocks. This change corrects the descriptions in Subsections 7.7.2.2.3.3 and 7.7.2.2.3.4 to agree with Technical Specifications and actual plant design.

Revision to UFSAR Section 5.2.2.1.3
The change revises a sentence that conflicts with UFSAR Table 5.2-9 and Technical Specification 3.4.2.e. by eliminating incorrect text in Section 5.2.2.1.3. The sentence states, "Two of the valves are set at 1146 psig for other considerations." This sentence refers to the setpoint of the two safety relief valves that lift at the lowest pressure. The actual setpoint of the two safety relief valves that lift at the lowest pressure is 1150 psig. The 1150 psig setpoint is correctly listed in UFSAR Table 5.2-9 and Technical Specification 3.4.2.e. The contradiction occurred when the setpoint of the two Safety Relief Valves with the lowest opening pressure setpoint was changed from 1146 psig to 1150 psig. The setpoint change was implemented per license amendment numbers 28 and 15 for Unit 1 and 2, respectively. UFSAR Section 5.2.2.1.3 was not revised to reflect the setpoint change.

Revision to UFSAR Table 6.2-21
UFSAR Table 6.2-21 Sheet 4B is revised by adding reference to "Note (20)" in the remarks column for containment penetrations M-77 valve 1(2)E12-F088A, M-79 & M-84 valve 1(2)E12-F302, and M-79 & M-84 valve 1(2)E12-F088B. These valves are all leak tested in the reverse direction as are many other ECCS System Relief valves/Isolation valves which serve as primary containment isolation valves in water sealed ECCS Systems. Note (20), which discusses reverse direction testing, was inadvertently omitted from the remarks section of Table 6.2-21 for these components.

UFSAR Change for Turbine Stop Valve and Turbine Control Valve Closure Scram and EOC-RPT Bypass
This change clarifies the bypass interlock wording in the UFSAR consistent with the design and Technical Specifications. These changes to UFSAR Sections 6.B, 7.2, 7.A.2, 15.2, 15.3, G.3, and G.5 supplement those previously prepared for design

change packages (DCPs) 9800068 and 9800067. These DCPs implemented license amendment Nos. 130 and 114, for Units 1 and 2, respectively.

UFSAR Revision to reflect Revision to Reactor Protection System Surveillance Testing
UFSAR Subsection 7.2.2.10 is revised to provide an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. UFSAR 7.2.2.10 previously indicated that a logic trip occurs when a test signal is applied to an RPS channel. For the revised testing methodology, special test equipment is installed across the trip contacts in the RPS trip logic. This test equipment allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel. UFSAR Section 7.A.2 is revised to indicate that manual bypasses of the associated RPS instrument channels are indicated in the control room on the engineered safety features (ESF) status indication panel.

UFSAR Change to Chapter 9.4
Revised the "dirty" pressure drop of 0.35 inches water column for the diesel generator ventilation supply filters listed in Table 9.4-15 to 0.40 inches water column. The pressure drop was changed to agree with the Sargent & Lundy design criteria as specified in DC-VD-01-LS.
The description for the HPCS switchgear and pump room ventilation system in Section 9.4.5.1.2 is revised to state that the supply air fan induces filtered outside air. The previous description was incorrect.
The description of the truck bay exhaust fan and the statement pertaining to the designed Interim Radwaste Storage Facility (IRSF) operating pressure is deleted from Section 9.4.13.2. The IRSF truck bay exhaust fan is permanently disabled, and the IRSF design basis is described in section 9.4.13.1.

Revision to UFSAR Section 9.4.2
UFSAR Section 9.4.2.2.c is revised to reflect that the reactor building ventilation system filters are medium efficiency filters. This conforms with UFSAR Table 9.4-5.

Revision to UFSAR Sections 6.2 and 7.3
UFSAR Subsections 6.2.5.1.k, 6.2.5.2, 7.3.5.1.g, 7.3.5.2.2, 7.3.5.2.3, 7.3.5.2.5, 7.3.5.2.7, and 7.3.5.2.9 are revised to specify the correct control and monitoring locations for the operation of the hydrogen recombiner system. These revisions result in UFSAR descriptions that correctly reflect current hydrogen recombiner design.

Revision to UFSAR Sections 6.2 and 6.5
UFSAR Sections 6.2 and 6.5 are revised to clarify text as follows.

Clarifying information is added to Subsection 6.2.3.2 to indicate that the reactor building is designed to contain a negative interior pressure of 0.25 inch H_20 gauge. Subsection 6.2.4.2.4 is revised to clarify the containment vent and purge valve description.
Section 6.5.1.4.1.b.3 is revised by removing the statement that HEPA filter elements are tested by the USNRC QA station.
Section 6.5.1.6.f.4 is revised by removing the charcoal filter tray flanges and adds the statement that o-rings are used on the charcoal filter sample canister.

Revision to UFSAR Table 9.4-27
Table 9.4-27, Primary Containment HVAC System Failure Analysis, discusses the malfunction and resulting actions during two train operation. The table incorrectly lists an action which can not be accomplished. During two train operation, both Supply Fan Coil Units are operating. Therefore, if there is a failure in one supply air fan, there is not another supply air fan which may be started. In the description of Two Train Operation, Supply Air Fan in Fan-Coil Unit, the Comments column is revised by deleting the text "Operator starts the standby fan-coil unit if required."

Revision to UFSAR Section 12.3
UFSAR subsection 12.3.1.5.4 is revised by replacing "computer grade regulated voltage" in the last sentence of the first paragraph with "a reliable power source". This change to the UFSAR corrects the power source to the counting room from computer grade regulated voltage to reflect that the power supplied to the counting room is from a reliable source.

Revision to UFSAR Section 7.A.3.2
The UFSAR change reflects the revision to the method of testing the main steam line (MSL) isolation trip channels as described in UFSAR section 7.A.3.2. The UFSAR change allows the trip signal input to the MSL isolation logic to be bypassed to prevent a system trip during the calibration or functional testing of selected instrument channels. Previously, a logic trip would occur when a test signal is applied to an isolation instrument channel. To prevent a system trip, special test equipment is installed across the associated trip channel relay contact in the isolation trip logic. This test equipment allows the trip function of the instrument channel to be verified without tripping the associated logic circuit during the testing of the instrument channel. The purpose of this change is to incorporate SCRAM reduction test methodology.

Revision to UFSAR Appendix G
UFSAR Appendix G Subsection G.5.1.5 is revised to clarify the description of the reactor recirculation circuit breaker status indication in the closed position. This section incorrectly stated that the reactor recirculation pump motor circuit breaker status indications consist of two red pilot lights for breaker closed status indication. The

revision reflects the actual configuration consists of one blue light for the normal trip coil and one red light for the RPT trip coil.

Editorial Revision to UFSAR Section 6.B
The figure "Load Rejection with One Pump Operation" is returned to Section 6.B as Figure 6.B.4. This corrects an editorial error that was made during conversion from the FSAR to the UFSAR. Other figure numbers and references to figures in Section 6.B are correspondingly cleaned up. A review of the Section 6.B reflects that removal of the "Load Rejection with One Pump Operation" figure should not have occurred.

Revision to UFSAR Section 8.3
UFSAR Subsection 8.3.2.1.1 is revised as follows. In subparagraph a., "2% of total volume" supersedes "the explosion limit." In subparagraph b., "65°F minimum" is replaced with "maintain a minimum electrolyte temperature of 60°F for the 125VDC batteries and 65°F for the 250VDC batteries". The revision provides explicit values for the percentage of hydrogen concentration per volume allowed to accumulate in the battery rooms as recommended in ANSI/IEEE Standard 484-1987. This UFSAR change also defines the specific requirements for the minimum electrolyte temperature for 125 VDC and 250 VDC battery per calculation 4266/19D30.

Revision to UFSAR Chapters 9.1, 9.2, and 10.4
UFSAR Sections 9.1 and 9.2 are revised to reflect the raising of the maximum circulating water and service water inlet temperatures from 95 ^{0}F to 97 ^{0}F, and provide an update of the ultimate heat sink for worst case weather conditions. This is based upon calculation L-002456 Revision 0, LaSalle County Station Cooling Lake Performance.

Revision to UFSAR Figure 7.7-5
UFSAR Figure 7.7-5, Feedwater Control System diagram, was updated to reflect the as-built condition of the feedwater control system.

Revision to UFSAR for Condensate Tap Installation per Design Change Package 9900189
LaSalle Operating Procedure LOP-CY-02M Revision 6, Unit 2 Cycled Condensate Storage and Transfer Mechanical Checklist
A supply tap was installed on cycled condensate (CY) line 2CY67A in the turbine building. The tap consists of a piping tee, a 3 inch gate valve, and piping nipple with a threaded cap. The purpose of this installation is to provide a supply of water that may be used for maintenance activities requiring reactor grade water which is no radioactively clean. UFSAR sections 9.2.7 and 9.2.7.1.2 are revised to expand the CY system description.

Revision to UFSAR Figures 10.1-1 and 10.1-2
UFSAR Figure 10.1-1 is revised by adding a note that states the high pressure turbine modification for power uprate will change the heat balance and that a new heat balance will be provided following approval of the power uprate license amendment. UFSAR Figure 10.1-2 is revised by adding a note that states the heat balance is not current and will be changed when power uprate is approved.

Revision to UFSAR Section 7.4
UFSAR Subsection 7.4.1.2.1, Power Sources, is revised to incorporate the following editorial changes. Buses 221Y, 236Y-2, and 235X-1 in the text of are changed to 121(221)Y, 136(236)Y-2, and 135(235)X-1, respectively. This change clarifies the proper names.

Revision to UFSAR Chapters 9.1, 9.2, and 10.4
UFSAR Chapters 9.1, 9.2, and 10.4 are revised to reflect the raising of the maximum circulating water and service water inlet temperatures from 95 ^{0}F to 97 ^{0}F, and provide an update of the ultimate heat sink for worst case weather conditions. This is based upon calculation L-002456 Revision 0, LaSalle County Station Cooling Lake Performance.

UFSAR Revision to Reflect deletion of Tables 3.11-1 and 3.11-2
The original FSAR Table 3.11-1 contained a list of all Class 1E equipment located in the harsh and mild environmental zones of the plant and their location, EQ and seismic qualification references. Table 3.11-2 contained a list of all active mechanical equipment and their location, EQ and seismic qualification document references. The Tables were deleted from the UFSAR in Revision 3. This change deletes all references to previously deleted Tables 3.11-1 and 3.11-2 in UFSAR Sections 7.2, 7.3, 7.4, 7.5, 7.6, and 7.7. The references to these Tables are replaced by Section 3.11 where appropriate. UFSAR Section 3.11 provides the environmental design specifications for the mechanical and electrical equipment located in various plant areas. Additionally, the word "environemnt" is corrected to "environment" in Subsection 7.7.5.2.3.

Revision to UFSAR per Restoration of Unit 1 Jet Pump Number 9
During the LaSalle Unit 1 refuel outages numbers six and seven, L1R06 and L1R07, respectively, damage was observed on the inlet mixer wedge of jet pump number 9, the restrainer bracket pad, and associated set screws. Restoration of the jet pump per design change package (DCP) 9600289 consisted of two improved restrainer bracket wedge assemblies ("auxiliary wedges"), a replacement wedge for the inlet-mixer, and restoration of a smooth functional surface to the wedge interface pad on the restrainer bracket. UFSAR Sections 3.9, 4.1, 4.5, and G.4 are correspondingly revised.

Revision to UFSAR to Clarify Table 6.2-23
The change deletes reference to the test pressure (P_t) of 39.6 psig for Type A, B, and C leak rate testing from Table 6.2-23, Containment Leakage Testing, and inserts reference to Note 6. Note 6 correctly refers the reader to ANSI/ANS 56.8-1994 to determine the test pressure for Type A, B, and C tests. This change clarifies UFSAR Table 6.2-23.

Revision to UFSAR Section 7.6
UFSAR Subsection 7.6.2.2.4 is revised to state that there is one set (as opposed to *sets*) of two differential pressure switches connected to measure the differential pressure created as steam flows past an elbow in the line so that the steam flow rate through it can be monitored.

Revision to UFSAR Section 3.8 for Containment Grating
Design Change Package (DCP) 9900210 allows the containment grating at elevation 819'-8 3/4" to be aluminum, as opposed to steel, to facilitate its removal and installation during refuel outages. UFSAR Subsection 3.8.3.1.6 is accordingly revised.

Revision to UFSAR Section 7.4
UFSAR Subsection 7.4.2.2.9 is revised to eliminate the time required to retrieve and insert the keys into the standby liquid control system keylock switches before system initiation. The change reflects that the keys are maintained in the proper keylock switches, which expedites the initiation and subsequent injection when required.

Revision to UFSAR per Unit 1 Refuel Platform Upgrade
The Unit 1 refuel platform was upgraded per Design Change Package (DCP) 9600258. This was done to facilitate shorter refueling outages, increase the efficiency and reliability of the refuel platform, and to standardize the fuel handling hardware associate with Commonwealth Edison's boiling water reactor stations. UFSAR Sections 1.7 and 7.7.13 are revised.

Revision to UFSAR to Reflect Design Change Package 9900187
Design Change Package (DCP) 9900187, Removal of Old SRV Test Equipment, Valves, and Cables from Unit 1
Unit 1 initial startup included a Mark II containment test to analyze hydrodynamic forces in the suppression pool during safety relief valve (SRV) actuation. This DCP removes some of the test equipment and cables (including those in two downcomers), and abandon in place other equipment installed to support the initial SRV testing. This also closes temporary alteration (TALT) 1-0069-98.

The changes to UFSAR Sections 1.2, 6.1, and 6.2 previously proposed by DCP 9800150 are superseded in their entirety.

Revision to UFSAR Section 3.11
UFSAR Tables 3.11-21, 3.11-22, 3.11-26, and 3.11-27 are revised to correct radiation dose values in the associated environmental zones. These changes make the UFSAR and design documents consistent with each another.

UFSAR Revision for Removal of Original Meteorological Tower
Design change package 9600526 disassembled and removed the original meteorological tower and support buildings. The meteorological and communication equipment was moved to a new tower location outside the security fence. There is no further need for the original tower. UFSAR figures 2.1-3, 2.1-4, 2.4-6, 8.2-2, and 9.5-1 and subsection 8.3.3.2 and 9.5.1.2.3 are revised to reflect removal of the tower.

Revision to UFSAR Subsection 7.6.2.2.7
Two paragraphs in UFSAR Subsection 7.6.2.2.7 are revised to correct the description of testing methodology for temperature switches and leak detection alarm units.

Revision to UFSAR Section 5.2
License amendments 134 and 119 for Unit 1 and 2, respectively, relocated Technical Specifications 3/4.4.4, Chemistry, to the UFSAR by reference to the Administrative Technical Requirements (ATR). "Technical Specifications" in Subsection 5.2.3.2.1 is revised to "Administrative Technical Requirements."

Revision to UFSAR for Discontinued Use of Rod Sequence Control System
UFSAR Section 3.1, Table 7.1-1, and Section 7.7 are revised to reflect the discontinued use of the Rod Sequence Control System (RSCS). The RSCS was designed to restrict rod movement to minimize the individual worth of control rods to mitigate the consequences of a Rod Drop Accident (RDA). The required use of RSCS was eliminated by license amendment 88 and 73 for Units 1 and 2, respectively (facility licenses NPF-11 and NPF-18). The need for these UFSAR changes was not previously identified when the license amendments were implemented.

UFSAR revision per Design Change Package (DCP) 9600529, Unit 2 Heater Bay Cooling Modification
The DCP modified the turbine building ventilation system to provide cooling to the area of the turbine valves' electro-hydraulic controls (EHC) in the turbine building low pressure heater bay. Two new 10,000 cfm vane axial fans (2VT14C and 2VT15C) were installed in the low pressure heater bay. Discharge ductwork from the fans was routed

to the vicinity of the EHC controls for the turbine control valves, the turbine stop valves, and the main steam bypass valves to provide additional cooling air to reduce the temperature and thermal stratification in this area. UFSAR Table 9.4-13 is revised.

Revision to Section 9.4 for Fuel Handling Accident Activity Detection
UFSAR Section 9.4.2.3 is revised to reflect the following. Potentially contaminated effluents rising from the surface of the fuel pools are drawn into the exhaust openings located above the water level. The radiation monitor trip in either the Unit 1 or Unit 2 pool exhaust ducts causes isolation of the reactor buildings and activates the standby gas treatment system. The size and length of the exhaust ducts from each pool are designed to ensure that the travel time of effluents from the radiation monitor to the isolation valve is a minimum of approximately 12.5 seconds, which is more than the closure time of the isolation valves (10 seconds).

Revision to UFSAR Table 5.4-1
UFSAR Table 5.4-1 is revised to match the nameplate design pressures of the reactor water cleanup (RWCU) system heat exchangers. The RWCU regenerative heat exchanger shell and tube design pressure is changed to 1425 psig, and the RWCU nonregenerative heat exchanger tube design pressure is changed to 1425 psig.

UFSAR Revision for Unit 1 Degraded Voltage Relay Setpoint Changes
UFSAR Section 8.2.3.3 is revised to change the setpoint for the Unit 1 second level undervoltage (degraded voltage) protection and to provide the lower and upper analytical limits for this parameter. The new values for the trip setpoint (3870 V), lower analytical limit (3814 V), and upper analytical limit (3900 V) are in conformance with Unit 1 Facility Operating License NPF-11 Amendment 135.
UFSAR Table 8.3-2 is revised to add the protective functions of the degraded voltage relay. The purpose of this table is to summarize the relay protection for ESF 4160-volt equipment, but it currently does not identify the protective functions provided by the degraded voltage relays. This change applies to both units.
Design Change Packages (DCPs) DCP's 9500018, 9500019, and 9500030 incorporated the degraded voltage relay setpoint changes for Unit 1 Divisions 1, 2, and 3. These DCPs were required to bring the degraded voltage protection circuit in compliance with the safety analysis report design bases requirements and GDC-17. LaSalle committed to implement the Unit 1 degraded voltage setpoint changes prior to startup from L1R08.

Revision to UFSAR to Reflect NobleChem Metal Compound Injection
The temporary Noblechem metal compound injection process allows for lower hydrogen water chemistry (HWC) hydrogen addition rates, while still achieving the electrochemical corrosion potential required of HWC. Benefits of lower hydrogen addition rates are lower operational dose rates from main steam line radiation, reduction

of administrative controls used to handle increased operating dose, decrease in personnel exposure during operation, and a reduction of localized shielding requirements. UFSAR Sections 5.2, 6.1, and 10.4 are revised to reflect NobleChem injection on Unit 1.

Disabling of Evaporative Cooler Spray Pumps
The Unit 1 and 2 reactor building evaporative cooler spray pumps 1VR01PA, 1VR01PB, 2VR01PA, and 2VR01PB are disabled. They have never worked effectively, are high cost maintenance items, and are not used. Revisions to UFSAR Section 6.2, 9.4, and Table 9.4-5 were previously proposed to reflect that the Unit 1 evaporative spray cooler pumps were out of service (OOS). UFSAR Section 6.2, 9.4, and Table 9.4-5 are revised to reflect that the evaporative cooler spray pumps on both units are out of service. UFSAR subsection 9.4.2.1.2 to its original text as it existed in UFSAR Revision 0.

UFSAR Revision to Reflect the Unit 1 Cycle 9 Reload Licensing Package
UFSAR Sections 1.2, 2.2, 3.9, 4.2, 4.3, 5.2, 6.2, 6.3, 6.B, 7.7, 9.1, 13.1, 15.0, 15.2, 15.4, 15.A are revised for Unit 1 Cycle 9 operation. The changes reflect Unit 1 operation with fuel manufactured by Siemens Power Corporation (SPC) and General Electric (GE). SPC Atrium 9B fuel and analytical methodologies are reflected in the changes.

Revision to UFSAR per Restoration of Unit 1 Jet Pump Number 9
Restoration of Unit 1 jet pump number 9 was accomplished per design change package (DCP) 9600289. An addendum to the DCP authorized qualification and installation of mock-up auxiliary wedges. UFSAR Section 4.5 is revised to reflect the materials of construction of the mock-up auxiliary wedges.

UFSAR Revision for Change to Procedure Described in UFSAR
Procedure LOP-WX-08, Establishing A URC Sludge Tank Transfer Loop, is revised to allow the capability of using the cycled condensate system (CY) pumps as an alternative to using the ultrasonic resin cleaner (URC) sludge recycle pumps to provide backflushing and recirculation. UFSAR Section 11.2.2.5.3 is revised.

Revision to UFSAR per Restoration of Unit 1 Jet Pump Number 9
Restoration of Unit 1 jet pump number 9 was accomplished per design change package (DCP) 9600289. An addendum to the DCP authorized the re-installation of temporary wedges, one on the vessel of jet pump number 5, and one on the shroud side of jet pump number 6. UFSAR Section 4.5 is revised to reflect the materials of construction due to the re-installation of the temporary wedges.

Revision to UFSAR for Procedure Preparation
Processes that are common to each of Commonwealth Edison's five operating stations are being controlled by generic corporate procedures. The corporate organization, with the assistance of each station, is preparing these generic documents. UFSAR Section 13.5.1.2 is revised to reflect the corporate involvement in the preparation of procedures.

Revision to UFSAR Section 9.1.3
The spent fuel pool normal maximum temperature limit of 120 °F in UFSAR Section 9.1.3 is revised to 140 °F. This limit is consistent with the allowable limit in NRC NUREG-0800, Standard Review Plan, Section 9.1.3. This proposed change supersedes a previously proposed change which restricted core offloads upon lake temperatures exceeding 95 °F. The alternate decay heat removal (ADHR) of Subsection 9.1.3.1.1 is revised to clarify the various potential lineups that may be used for the fuel pool cooling system during ADHR.

Change to UFSAR Table 5.2-3, and Figure 6.3-4, for the Low Pressure Core Spray System (LPCS)
UFSAR Table 5.2-3 and Figure 6.3-4 are revised to identify the design pressure for LPCS to be 550 psig as opposed to 475 psig. The proposed change to Figure 6.3-4 in this change package is superseded by that in change package LU1999-172.
LU1999-171 Revision to UFSAR Sections 15.9.3.7 and 15.9.5 for Net Positive Suction Head Requirements
UFSAR Sections 15.9.3.7 and 15.9.5 revised to update the net positive suction head available values and calculation reference of the reactor core isolation cooling (RCIC), high pressure core spray (HPCS), and residual heat removal (RHR) systems for station blackout.

Change to UFSAR Figure 6.3-4, Low Pressure Core Spray System (LPCS)
UFSAR Figure 6.3-4 is revised for the following: The design temperature for the Low Pressure Core Spray System (LPCS) is revised to 480 degrees Fahrenheit as opposed to the current value of 212 degrees Fahrenhet for locations 3 to 8 and 7 to 7.5; Deleted the "AO" from check valve 1(2)E21-F006 operator; Added Note 13 which states "Free swinging disc. The actuator is used for local leak rate testing only." Revised the LPCS design pressure to be 550 psig as opposed to the current value of 475 psig for figure locations 3 to 8.5, 4 to 4.5 , and 7 to 7.5. These changes to UFSAR Figure 6.3-4 supersede those proposed in UFSAR Change Package LU1999-170.

LU1999-174 Revision to UFSAR to reflect Compliance with Generic Letter 96-06
NRC Generic Letter (GL) 96-06, "Assurance of Equipment Operability and Containment Integrity During Design Basis Accident Conditions," includes a discussion of thermally induced overpressurization of isolated fluid filled piping sections inside primary containment. The overpressurization condition described in the GL applies to primary

containment penetrations M-49 and M-50. UFSAR Subsection 3.9.3.1.2.3 is revised to address overpressurization analysis of primary containment penetrations M-49 and M-50.

LU1999-177 Change to UFSAR Section 6.1 and 9.2 to reflect Use of Corrosion Inhibitors
UFSAR Subsections 6.1.1.2, Composition, Compatibility and Stability of Containment and Core Spray Coolants, 6.1.3, Post-Accident Chemistry, 9.2.3.2, Reactor Building Closed Cooling Water System description, 9.2.8.2, Turbine Building Closed Cooling Water, and 9.2.9.2, Primary Containment Chilled Water System description, are revised to state that limited quantities of corrosion inhibitors are present in these systems. The proposed change accurately reflects the condition of the plant in regard to the use of corrosion inhibitors, while not restricting the use of new, improved or alternate corrosion inhibitors that are evaluated to be acceptable for use at LaSalle.

LU1999-182 Editorial Change to UFSAR Section 9.4
UFSAR Subsections 9.4.10.1, 9.4.10.1.1, and 9.4.10.2, Containment Purge and Vent (VQ) System, are revised to resolve editorial discrepancies between previously existing changes, to accurately describe the containment purge and vent system.

LU2000-007 Revision to UFSAR Tables 7.3-5 and 7.7-4
Source Range Monitor (SRM) Retract Permissive and Downscale Trip Setpoint per Design Change Package 9700573
The SRM retract permissives didn't satisfy Technical Specifications Table 3.3.6-1, Trip Function 3.a. Note b, which states that the trip function of the SRM will be automatically bypassed if the detector count rate is greater than or equal to 100 counts per second (cps). This was documented in Licensee Event Report (LER) 97-011. Based upon General Electric (GE) calculations, design change package 9700573 revised the Unit 2 SRM retract permissive setpoints to 306 cps from 100 cps. The SRM downscale trip setpoints were also revised to 1.51 cps from 1.18 cps. UFSAR Tables 7.3-5 and 7.7-4 are revised.

LU2000-011 Revision to UFSAR to reflect deletion of the Unit 2 Main Steam Isolation Valve Leakage Control System
Unit 2 License Amendment Number 97 and the accompanying safety evaluation report approved the use of the main steam piping, drain lines, and main condenser as an alternate leakage treatment pathway for MSIV leakage and deletion of the MSIV-LCS. The Unit 2 main steam isolation valve (MSIV) leakage control system (LCS) was deleted per design change packages 9500168 and 9600092. UFSAR Sections 1.2, 1.7, 3.1, 6.0, 6.1, 6.2, 6.5, 6.7, 6.8, 10.3, 15.6, Appendix H, and Drawing Index are revised to reflect the deletion. Drawing M-116 Sheet was voided by design change package 9600092.

Revision to Clarify UFSAR 9.2.2.2
UFSAR 9.2.2.2 is revised to clarify that during startup or shutdown of one of the units, the service water pump combination can be adjusted such that the required number of main service water or jockey pumps is operating to meet that system's cooling requirements.

Revision to UFSAR 15.2.4.1 to reflect deletion of the high steam line radiation isolation of the Main Steam Isolation Valves
UFSAR 15.2.4.1 is revised reflect the deletion of the main steam line high radiation trip function by design change package (DCP) 9600284, elimination of unit 2 main steam isolation valves closure and scram functions of the main steam line radiation monitors. This section was missed by UFSAR changes previously proposed for DCP 9600284.

Revision to Drawing M-1465
Drawing M-1465 was revised to provide clarifying information for fire dampers 2VY12Y and 2VY13Y.

UFSAR Revision to Correct Miscellaneous Errors
The change package corrects many miscellaneous editorial changes, consisting of historical typographical errors in the text and word missuse, and data errors. UFSAR Table of Contents, Chapters 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 15, and Appendices B, G, H, J, and L are revised.

Attachment B

1998 Activities Evaluated in Accordance with 10 CFR 50.59

Revision to UFSAR Subsection 7.7.6.1.1
UFSAR Subsection 7.7.6.1.1 is revised to incorporate an exception to source range monitor (SRM) operability requirements during refueling operations, implemented per licensing amendments 32 and 18, for Unit 1 and 2, respectively.

Revision to UFSAR Section 13.2
UFSAR Section 13.2 is revised to update the description of the LaSalle County Station Training program.

UFSAR Revision to reflect Minor Changes P01-1-91-542 and P01-2-91-538
Minor Changes P01-1-91-542 (Design Change Package [DCP] 9100290) and P01-2-91-538 (DCP 9100283) replaced the level instrumentation of the 1WX01TA, 1WX01TB, 2WX01TA, and 2WX01TB reactor water cleanup (RWCU) phase separator tanks. The original sonic type level indicating instruments in were replaced with thermal dispersion type level indicating instruments. A bubbler type level transmitter was also installed in the tanks. UFSAR Subsection 7.7.11.2.3 is correspondingly revised.

UFSAR Revision to Reflect Design Change Package (DCP) 9500140
The DCP routed piping from the inlet of the plant chemical waste (WZ) evaporator to a vendor connection located in the Intermediate South storage area of the radwaste truck bay in the radwaste building. This DCP provides operational flexibility in the processing of floor drain/chemical drain water. Depending upon economics, it may be more advantageous to use state-of-the-art vendor skids to process waste instead of the currently installed evaporators. A return path is provided for processed water from the vendor skid to the WZ evaporator piping, which can be routed to the floor drain head tank or the floor drain collector, depending upon water quality. UFSAR Figure 11.2-1 in addition to sections 3.1, 9.3, 11.2, 11.4, and 11.5 is revised to reflect the option of using a vendor skid to process waste.

Removal of Stem Leakoff Line from Residual Heat Removal (RHR) Valve 1E12-F041B per Design Change Package (DCP) 8700289 (Partial Modification M01-1-87-098-4)
The DCP replaced the check valve component of Emergency Core Cooling System (ECCS) valve to improve valve operation, removed the leak detection system connection to the check valves which previously caused valve stem leakage to fall under more restrictive technical specification limits for unidentified leakage. The UFSAR change proposed for Subsection 5.2.5.2 and Figure 7.3-7 were incorporated in previous UFSAR updates associated with modifications M01-1-87-098-4 and M01-2-87-087-4.

Removal of Stem Leakoff Lines from Emergency Core Cooling System (ECCS) valves 1E12-F050B, 1E12-F009, 1B33-F067A, and 1B33-F067B
per Design Change Package (DCP) 8700292 (Partial Modification M01-1-87-098-7)
Modification Test Change
The DCP replaced the check valve components of the subject Emergency Core Cooling System (ECCS) valves to improve valve operation, removed the leak detection system connection to the check valves which previously caused valve stem leakage to fall under more restrictive technical specification limits for unidentified leakage. A revision to the modification test for DCP 8700292 included the deletion of a test steps that required partial stroke of valve 1E12-F050B, revised a test that allowed for the removal of additional leakoff line to valve 1E12-F050B, and revised a step to allow for a full stroke test of valve 1E12-F050B.

UFSAR Update due to Emergency Core Cooling System (ECCS) Testable Check Valve 1E22-F005 Upgrade per Design Change Package (DCP) 8700286
The DCP accomplished the following on the high pressure core spray (HPCS) 1E22-F005 valve: replaced the valve stem packing to reduce valve shaft friction, removed the leakoff line, and replaced the associated limit switch. These activities were performed to minimize the likelihood of the valve failing to fully close following low flow testing. The changes to UFSAR subsection 5.2.5.2 and Figure 7.3-7 were previously incorporated by associated partial modifications. UFSAR Drawing M-95 Sheet 1 (Unit 1 HPCS) is accordingly revised.

Replacement of the Unit 1 Inboard MSIV Pilot Solenoid Valves per Design Change Packages (DCPs) 9500200, 9500201, 9500202, and 9500203
The DCPs replaced the pilot solenoid valves of Unit 1 inboard Main Steam Isolation Valves (MSIVs) 1B21-F022A, B, C, and D. The previous ASCO model NP8323A20V valves (dual coil one per MSIV) were replaced with Valcor model V70900-87 solenoid valves (single coil two per MSIV). The ASCO model NP8323A20V valve is no longer manufactured or supplied by ASCO. UFSAR subsection 7.3.2.2.7 is revised, Figure 7.3-11 Sheet 1 is deleted, while Figure 7.3-11 Sheet 2 is re-designated as Figure 7.3-11 Sheet 1.

UFSAR Revision to reflect Design Change Package (DCP) 9500323
DCP 9500323 removed the protractible elements of the Unit 2 equipment drain filters, and replaced them with non-precoatable filters. Filter precoat logic was also modified to accommodate non-precoating of filter elements. Non-precoatable filters provide comparable water quality, while minimizing the waste generated. UFSAR Sections 7.7, 11.2, 11.4, and 12.3 are revised.

UFSAR Update for Modification of Unit 1 Station Air Compressor Cooling Water Pressure Regulator and Relief Valves per Design Change Package (DCP) 9600322
The DCP increased the reliability of station air compressor 1SA01C by modifying the cooling water supply to the compressor's Inter/aftercooler and Oil Cooler. The bronze pressure regulator previously installed for 1WT087 was replaced with a cast iron pressure regulator. The regulator establishes a water supply pressure of 55 psig to the station air compressor inter/aftercooler.
Relief valve 1WT124 on the station air compressor inter/aftercooler cooling water supply line was replaced. The relief setpoint was increased from 65psig to 75 psig, which reduces the chance of seat leakage during normal operating pressure. The associated discharge piping was reconfigured to reduce back-pressure, as high back-pressure on the relief valve discharge may cause the relief valve to chug, damaging the seating surface of the relief valve.
Relief valve 1WT125 on the station air compressor inter/aftercooler and oil cooler cooling water supply header was removed as it is no longer required. UFSAR drawing M-67 Sheet 2, Turbine Building Closed Cooling Water, is correspondingly revised.

Feedwater Isolation Valves 1B21-F065A and 1B21-F065B Feed Circuit Breaker Setpoint Change per Design Change Package (DCP) 9600349
The DCP changed the magnetic setpoint of feedwater isolation valves 1B21-F065A and 1B21-F065B. The circuit breaker was also replaced to accommodate the higher magnetic trip settings. This DCP provides a greater margin to prevent nuisance tripping during motor starting conditions.

Self-Contained Breathing Apparatus (SCBA) Air Compressor Replacement per Design Change Package (DCP) 9600527
The DCP installed a new SCBA air compressor, 0FP35C, in the plant at the S and 29 lines in the Unit 2 Turbine Building, elevation 710'-6". The compressor serves to refill SCBA air bottles onsite, as opposed to sending them offsite. UFSAR drawings M-Index Sheet 2, M-9, and M-72 Sheet 4 are revised.

UFSAR Update per Unit 1 Station Heat Supply Air Coils Replacement, Design Change Package (DCP) 9600547
The DCP replaced Unit ` station heat supply air coils 1VT02AA and 1VT02AB in the ventilation supply of the turbine building and rerouting of some associated piping. The previous coils were freeze-damaged. The DCP installation allows for complete draining and venting of the coils and headers. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Update Unit 2 Station Heat Supply Air Coil Replacement, Design Change Package (DCP) 9600550
The DCP replaced Unit 2 station heat supply air coil 2VR02A in the ventilation supply of the reactor building and rerouting of some associated piping. The previous coil was freeze-damaged. The DCP installation allows for complete draining and venting of the coil and header. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

UFSAR Update due to Unit 0 Station Heat Supply Air Coil Replacement per Design Change Package (DCP) 9600551
The DCP replaced supply air coil 0VR03A in the ventilation supply of the radwaste building and rerouting of some associated piping. The previous coil was freeze-damaged. The DCP installation allows for complete draining and venting of the coil and header. The DCP revises UFSAR Tables 9.4-5, 9.4-11, and 9.4-13.

Addition of Cooling Water Flow Gauges for Unit 1 Core Standby Cooling System (VY) Area Coolers, Design Change Package (DCP) 9700019
The DCP installed individual cooling water flow indicating gauges for coolers 1VY02A and 1VY03A, and combined flow indicating gauges for coolers 1VY01A, 1VY04A, and 1E21-C001. The addition of the flow indicating gauges allows for measurement of flow through the VY area coolers, which was not previously monitored. UFSAR drawings M-87 Sheets 1 and 2 for the Unit 1 core standby cooling equipment cooling water system are revised.

UFSAR Revision to reflect the VC/VE Train B Electrical Demolition per Design Change Package (DCP) 9600215
DCP 9600215 demolished the humidification system (B train electrical portion) of Control Room (VC) and Auxiliary Electric Equipment Room ventilation (VE). Humidification system demolition was performed because the previous humidification units have been out of service for an extended period due to various system problems, and, the humidifiers and associated piping are not seismically supported, which is in direct conflict with the UFSAR which states that they are designed to meet II/I criteria. UFSAR Sections 6.4, 7.3, and 9.4 are revised.

Design Change Package 9600545
Unit 1 Main Turbine and Reactor Feedwater Pumps Level 8 Trip Logic Control Modification
The DCP added an interlock from the Unit 1 Reactor Core Isolation Cooling (RCIC) Division 1 level 8 trip relay 1B21A-K705AX to Channel C trip logic of the Main turbine / Feedwater pumps trip. This change allows the RCIC Division 1 level 8 trip to actuate the 'C' channel main turbine / feedwater pumps level 8 trip. UFSAR Figure 7.7-5 Sheet 1 and Subsection 7.7.4.2.1 are revised to reflect the DCP.

Replacement of Valve Stem on the Unit 1 Motor Driven Reactor Feed Pump (MDRFP) Minimum Flow Valve per Design Change Package (DCP) 9700494
The DCP replaced the stainless steel stem of valve AOV-1FW008 with 718 Inconel material. The grafoil ring and guide bushing/spacers were replaced with metal guide ring and bushings. The valve stroke time was also increased to a range of 15 – 20 seconds. These measures are intended to reduce valve internal friction, improve wear resistance, and allow smoother operation.

Service water Pump Motor Inboard Bearing Thermocouple Connection per Design Change Package (DCP) 9800022
The DCP restored the original configuration by re-connecting the thermocouple extension wire associated with Service Water Pump 2A Motor Inboard Bearing Thermocouple 2TE-WS035B, and re-connected the lifted leads in junction box at the pump motor and on terminal block TB02 inside Input Termination cabinet AIT5.

Unit 1 CRD HCU SCRAM Air Pilot Solenoid Valves flexible hose installed per Design Change Package (DCP) 9500399 and UFSAR revisions.
The original copper tubing between the Scram air header and the Scram solenoid pilot valves was replaced. The DCP installed flexible hoses in the air supply piping to the Control Rod Drive (CRD) Hydraulic Control Unit (HCU) SCRAM Air Pilot Solenoid Valves 1C11-D001-117 and 1C11-D011-118. The air supply stop valve (1C11-D001-116) was relocated closer to the air supply header (1RD52B-3/4"). UFSAR Appendix H Section H.3.2.6, Table H.3-2, and drawings M-100 Sheet 2 and Sheet 3 are revised accordingly

Chiller addition into Station Heat (SH) Recovery System for Turbine Building Ventilation cooling per Design Change Package (DCP) 9600090 and UFSAR revisions.
Chillers, pumps, instrumentation and associated piping were added to provide cooled glycol into the Turbine Building Ventilation (VT) and Reactor Building Ventilation (VR) system heating coils through the Station Heat Recovery system. This DCP provides an alternate cooling source to the original evaporative coolers, which have proven to be unreliable and difficult to maintain, and provides a more reliable cooling system with

added heat removal capability. UFSAR sections 6.2.3, 9.2.10, 9.4.2 and 9.4.4 are revised as a result of this DCP.

UFSAR revision per Design Change Packages (DCP) 9700058, Revise Logic & Wiring for VC System Radiation Monitors (Train A)
This DCP removed the electrical connection that existed between the two trip systems in train 'A' located in Main Control Room Panel 0PM14J. Output contacts from relays 1D18-K751A and 1D18-K751B were wired in series to comprise Trip System 1. Output contacts from relays 1D18-K751C and 1D18-K751D were wired in series to comprise Trip System 2. The output contacts from both channels of a trip system must close in order to energize the isolation relay logic for a given train. The previous configuration did not meet single failure criteria and would prevent an isolation from being initiated when required (ref. LER 96-021-01).
UFSAR Sections 6.4.4, 7.3.4.3.11 and 9.4.1.1.3 are revised to reflect the design change.

UFSAR revision per Design Change Packages (DCP) 9700059, Revise Logic & Wiring for VC System Radiation Monitors (Train B)
This DCP removed the electrical connection that existed between the two trip systems in train 'B' located in Main Control Room Panel 0PM15J. Output contacts from relays 2D18-K751A and 2D18-K751B were wired in series to comprise Trip System 1. Output contacts from relays 2D18-K751C and 2D18-K751D were wired in series to comprise Trip System 2. The output contacts from both channels of a trip system must close in order to energize the isolation relay logic for a given train. The previous configuration did not meet single failure criteria and would prevent an isolation from being initiated when required (ref. LER 96-021-01).
UFSAR Sections 6.4.4, 7.3.4.3.11 and 9.4.1.1.3 are revised to reflect the design change.

UFSAR Revision to reflect Design Change Package (DCP) 9600091 – Cooling Water Tie Into Station Heating (SH) for Turbine Ventilation (VT) Cooling.
The DCP replaced an existing elbow associated with the VT Supply Coil Floor Drain piping (SH system) with a hydrolyzing port consisting of a tee, spool of pipe, and cap to provide a means for hydrolyzing the section of the Unit 1 VT Floor Drain piping from the floor drain to its tie in to the drain header.
UFSAR Drawing M-102 Sheet 11 is revised to identify the new hydrolyzing port on the VT Supply Coil Floor Drain pipe.
UFSAR Drawing Revision per Design Change Package (DCP) 9600411 –IN System Primary Containment Isolation Valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN075 Operator Upgrades.
The DCP increased the supply air pressure setting and bench set values, 2) inverted the actuator upper and lower casings, 3) replaced the actuator adjusting screw with a

longer screw, 4) installed spacer washers onto the bolts retaining the upper actuator casing and spring barrel, 5) replaced the original Grafoil packing with Teflon based packing and 6) increased design differential pressure specifications (1IN001A/B) and decreased design differential pressure specifications (1IN017, 074,075). For 1IN017, 1IN074, and 1IN075, replaced the existing 420 lb./in actuator spring with an 840 lb./in actuator spring, and replaced the existing 0-40 psig air regulator with a 0-100psig air regulator. (Reference ECN 000995M.)
UFSAR Drawing M-66 Sheets 1 and 3 are revised to delete the air regulator setpoints for valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN975.

UFSAR drawing revision per Unit 1 Design Change Package (DCP) 9800109 –1E12-F549 Division 2 RHR-WS Keep Fill Pressure Regulating Valve Setpoint / Range Change.
This design change revised the setpoint for the self-contained pressure regulator (1E12-F459) in the RHR Service Water (RHR-WS) cross-tie from 50 psig to 20 psig. The setting change required replacement of the pressure regulator spring and a revision to the system pressure specified in operating procedure LOP-RH-Q1.
This design change revised the setting of 1E12-F459 but did not change the function.
UFSAR Drawing M-87 Sheet 1 is revised to delete the setpoint from the drawing.

UFSAR Update due to Addition of Drain Connection to Pipeline 1RH83BB for Dewatering 1E12-F068B, Design Change Package (DCP) 9700148. The DCP installed a 4-inch drain connection to pipeline 1RH83BB used for dewatering the piping to support repairs to the internals of residual heat removal (RHR) valve 1E12-F068B.
UFSAR Drawing M-134 Sheet 1 (Core Standby Cooling System Equipment Cooling Water System) is revised to reflect the installation of the drain connection.

UFSAR Revision to reflect Design Change Package (DCP) 9600147 – Condensate Booster (CB) Pump Minimum Flow Loop Upgrade Design.
The DCP replaced the existing modulating Condensate Booster pump minimum flow valve pneumatic control loop for each of the CB pumps 1CB01PA, 1CB01PB, 1CB01PC, and 1CB01PD with ON-OFF control using a flow transmitter, trip unit interlock and a Main Control Room switch. With the current system control in AUTO, excessive and rapid valve cycling occurs. The new design increases the operability and reliability of the CD/CB minimum flow control loop.
UFSAR Drawings M-58 Sheet 1 and M-59 are revised to reflect these changes.

UFSAR changes per Design Change Package (DCP) 9600525 –Installation of New Microwave Tower / Meteorological Monitors.
The DCP installed a replacement microwave / meteorology tower, a shelter (pre-fabricated building), support equipment, and replacement meteorological instruments

on the tower and / or in the shelter, outside the security fence. The replacement tower complies with the siting criteria of Regulatory Guide 1.23 and ANSI/ANS 2.5 (1984). The previous tower did not comply as it was located too close to the New Service Building, causing the 10 meter wind speed and direction data to be inaccurate. UFSAR Figures 2.1-3, 2.1-4, 8.2-2, and 9.5-1 Sheet 1 and Section 2.3.3.1 are revised to reflect the installation of the new tower.

Removal of flow element straighteners (honeycomb) per Design Change Package (DCP) 9700096.
This DCP removed the air straighteners (honeycomb) from the flow elements in the VE system. The air straighteners were removed because they become clogged and/or damaged over time, and cannot be effectively cleaned or maintained due to lack of access. This condition resulted in an increased system supply and return pressure loss in the ductwork, leading to reduction in fan performance. The flow elements did not provide reliable flow measurement and were no longer used for airflow measurement.

Revision of the Thermal Overload Bypass of Residual Heat Removal (RHR) Motor Operated Valves per Design Change Package (DCP) 9700026
The DCP implemented the corrective actions identified in Licensee Event Report (LER) 96-022, Revision 0, for the thermal overload bypass logic of the Engineered Safety Features (ESF) Division 2 motor operated valves (MOVs). The control circuits of MOVs 1E12-F024B, 1E12-F027B, 1E12-F042B, and 1E12-F042C were modified to ensure that the thermal overloads are bypassed whenever a LOCA signal is present. The modified logic removed the interlock between the thermal overload bypass circuit and the manual override circuit, such that the thermal overload bypass logic is only interlocked with the high drywell pressure and low reactor level (i.e., LOCA) logic.

Removal of flow element straighteners (honeycomb) per Design Change Package (DCP) 9700094.
This DCP removed the air straighteners (honeycomb) from the flow elements in the VC system. The air straighteners were removed because they become clogged and/or damaged over time, and cannot be effectively cleaned or maintained due to lack of access. This condition resulted in an increased system supply and return pressure loss in the ductwork, leading to reduction in fan performance. The flow elements did not provide reliable flow measurement and were no longer used for airflow measurement.

LaSalle Unit 1 ECCS Suction Strainer Replacement per DCP 9700303
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 1 low pressure core spray (LPCS) suction line in the suppression pool. The replacement strainer has increased surface area to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak

or loss of coolant accident (LOCA). The strainer surface area is increased as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR drawing M-96 Sheet 2 for the Unit 1 RHR system is revised to reflect the strainer replacement.

Suppression pool strainer replacement per Design Change Package (DCP) 9700304
The DCP replaced the Unit 1 high pressure core spray (HPCS) suppression pool suction strainer to increase the surface area with a larger capacity strainer to reduce pump net positive suction head. UFSAR subsections 15.9.3.7 and 15.9.5, and Figures 6.3-3, 6.3-6, and 6.3-9 are revised.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700302, ECCS Suction Strainer Replacement Modification.
The DCP replaced the existing suction strainer on the RCIC suction line in the suppression pool with a larger capacity strainer to reduce pump Net Positive Suction Head loss due to accumulated strainer debris resulting from a design basis line break LOCA. The existing strainer was replaced to increase the surface area of the strainer and thus increase the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03.
UFSAR section 15.9.3.7 and Drawing M-101, Sheet 2 is revised to reflect the strainer replacement.

Installation of Lifting Beam to Remove 1VR02CA Fan Motor per Design Change Package (DCP) 9700365
Fan Motor 1VR02CA was removed for maintenance activities. In order to facilitate the lift and set rigging activity for the fan motor, an interfering diagonal brace for the motor support frame needed to be modified so that it could be expeditiously removed and replaced on temporary basis. A permanent rigging beam also needed to be installed to remove the motor or one floor plug at a time. The DCP provided details for adding a removable spliced connection to the diagonal brace and adding a new rigging beam.

Design Change Package (DCP) 9600411 –IN System Primary Containment Isolation Valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN075 Operator Upgrades. (Reference ECN 000995M-01)
This DCP replaced the existing supports with improved (stronger) supports for the pneumatic supply piping to the regulators associated with valves 1IN001A, 1IN001B, 1IN017, 1IN074, and 1IN075. New air regulator support brackets were installed for 1IN074. The new supports were upgraded to improve their adequacy under dynamic conditions and reduce the air supply tubing loads.

Demolition of Train 'A' Electrical and Train 'A'/'B' Mechanical of the VC/VE Humidification System per Design Change Package (DCP) 9600214 and UFSAR changes.
This DCP removed humidification equipment from the Control Room (VC) and Auxiliary Electric Equipment Room (VE) HVAC systems. The Mechanical portions of the 'A' & 'B' trains and the electrical portion of the 'A' Train were removed because the existing humidification equipment, including the steam boilers, had been out of service for an extended period of time due to various system problems. Additionally, the humidifiers and associated piping were not seismically supported.
UFSAR Sections 6.4, 7.3.4, 9.4.1, Table 9.4-1, Table 9.4-3 and Drawings M-105 sheet 1, M-1443 Sheet 2, M-1443 Sheet 4, M-3443 Sheet 2, and M-3443 Sheet 21are accordingly revised to reflect the removal of the VC and VE steam humidification equipment.

Replacement and Revision of Settings of Molded Case Circuit Breakers per Design Change Package (DCP) 9600346
The DCP replaced the molded case circuit breakers (MCCBs) and revised the magnetic trip setpoints for the motor operators of valves 1VG001, 1VG003, 1VQ035, 1VQ037, 1E12-F006B, and 1E51-F086. The DCP implements corrective actions identified in a root cause report addressing the tripping of several MCCBs during a response time test of the "0" Diesel Generator. The DCP provides a greater margin to ensure nuisance tripping does not occur during motor starting conditions.

UFSAR revisions per Design Change Package (DCP) 9700310, Auxiliary Electrical Equipment Room (AEER) Ventilation System – Return Air Isolation Damper Replacement.
This DCP replaced the existing AEER HVAC return fans' isolation dampers (0VE06YA and 0VE06YB) with new dampers. The new dampers were installed in the ductwork upstream of the AEER Return Air Fans 0VE02CA and 0VE02CB. The new dampers will enhance the performance and reliability of the VE system by improving the maintainability of the damper once installed. The existing dampers were left in place to serve as manual isolation dampers and assigned new EPN numbers (0VE66YA and 0VE66YB).
UFSAR Section 3.11.4.1, Table H.4-4, Table H.4-101 and Drawing M-1443 Sheet 3 are revised accordingly.

Drywell Equipment Drain System Valve 1RE035 Actuator Upgrade per Unit 1 Design Change Package (DCP) 9700047
This DCP upgraded the actuator of valve 1RE035 to ensure appropriate valve seat closing force to prevent internal valve and stem degradation. The actuator spring and actuator spring adjusting screw were replaced. Bench sets were revised to obtain the correct force from the diaphragm to the spring and the supply air regulator was adjusted

to compensate for the additional spring force, and two test taps in the air supply tubing to the actuator were installed.

Replacement of Continuous Air Monitors 1PL15J and 1PL75J (Phase I), Design Change Package (DCP) 9700069
This DCP completed the preliminary work to support replacement of continuous air (CAM) monitor panels 1PL15J and 1PL75J. New manual isolation valves were installed in the inlet sample line, return sample line for panel 1PL75J, and return sample line for panel 1PL15J. Portions of stainless steel piping from the new isolation valves to the panels were replaced with stainless steel tubing. Two new grab sample stations for each panel were installed and previously existing manual equipment isolating valves were relocated to a higher elevation. P&ID M-156 Sheet 4 is revised to show the new isolation valves, new grab sample stations and tubing.

Revision to UFSAR drawings per Design Change Package (DCP) 9700040 – Replacement of Relief Valve 1CB004A with a Newer Model Valve.
This DCP replaced the existing 1CB004A (Consolidated/Dresser model 1970C) relief valve with a new relief valve (Consolidated/Dresser model 1996C) because the existing valve was leaking and could not be repaired. The original model is no longer in production and the manufacture recommended the replacement model. The new valve was flanged in for ease of future removal and testing.
UFSAR Drawing M-59 is revised to reflect the as-installed configuration.

RE System Primary Containment Isolation Valves 1RF012 and 1RF013 actuator upgrades per Design Change Package (DCP) 9600407.
This DCP remounted the pilot solenoid valve for air operated valves 1RF012 and 1RF013 in the vertical and upright position to assure proper solenoid operation. The existing air supply regulators were replaced with air regulators having an integral relief valve and a new air regulator mounting bracket was installed to permit installation of the new air regulators without reworking the existing tubing. Two test taps were installed on the air supply line to the valve actuator to aid in diagnostic testing.

RE System Primary Containment Isolation Valves 1RE024, 1RE025, 1RE026 and 1RE029 actuator upgrades per Design Change Package (DCP) 9600408.
This DCP remounted the pilot solenoid valve for air operated 1RE024 and 1RE025 in the vertical and upright position to assure proper solenoid operation. The existing air supply regulators were replaced with air regulators having an integral relief valve and a new air regulator mounting bracket was installed to permit installation of the new air regulators without reworking the existing tubing. Two test taps were installed on the air supply line to the valve actuator to aid in diagnostic testing.

For 1RE026 and 1RE029, this DCP remounted the pilot solenoid valve in the vertical and upright position to assure proper solenoid operation. The existing actuator spring was replaced and new bench sets and air regulator setpoints were installed. The existing air supply regulators were replaced with air regulators having an integral relief valve and a new air regulator mounting bracket was installed to permit installation of the new air regulators without reworking the existing tubing. Two test taps were installed on the air supply line to the valve actuator to aid in diagnostic testing.

Modify mounting for Primary Containment Cooler Fans 1VP02CA/B per Unit 1 Design Change Package (DCP) 9600570
Vibration isolators installed for the primary containment cooler fans were not capable of carrying seismic loads. During an investigation it was noted that the housing itself was not qualified for the seismic loads resulting from the fan on its roof. This DCP installed new vibration isolators capable of transferring seismic loads from fans 1VP02CA/B and reinforced the VP housing so that it is acceptable for seismic loads resulting from the fan and its self-weight.

UFSAR Revision per Design Change Package (DCP) 9600285, Elimination of Main Steam Isolation Valves Closure and Scram Functions of the Main Steam Line Radiation Monitors
The DCP improves unit availability by reducing spurious scrams and isolations caused by the Main Steam Line Radiation Monitors (MSLRMs). The original design function of the MSLRM was for detection/mitigation of consequences associated with fuel failure and the rod-drop design basis accident. The DCP consisted of the following: removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Protection System (RPS) Reactor Auto-Scram Trip logic circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Main Steam Line (MSL) MSL Isolation and Drain Valve circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Water Sample Valve circuits and associated Normal/Test Selector Switches in Main Control Room (MCR) Panels, revising MSLRM's High and High-High alarm setpoints, rewiring MSLRM alarms per recommendation of ComEd Human Factors Group and Operations, rewiring computer digital inputs and outputs associated with the MSLRMs, revising off gas pre-treatment radiation monitor High and High-High alarm setpoints, and Add appropriate safety-related banana plugs per ComEd recommendation to one terminal at relays located in the Main Control Room panels. UFSAR Sections 1.2, 7.1, 7.2, 7.3, 7.6, 7.7, 7.A, 11.5, and 15.2 are revised.

Revision to UFSAR Subsection 9.5.4.3
The diesel generator fuel transfer pump alarm and low-level alarm setpoints specified for the Division 3 diesel generator were incorrect. The revision to UFSAR Subsection 9.5.4.3 not only corrected the error but also specifies only the required criteria, and not

the result of the calculations or instrument setpoints specifics. The change applies to all five emergency diesel generators since the criteria are common to all diesel generator fuel oil systems.

Partial installation of the Oscillation Power Range Monitors (OPRMs) enclosures and associated equipment replacements per Design Change Package (DCP) 9500040. This DCP constituted a partial installation of the OPRM system which included mounting the OPRM (1C51-K750A through H) metallic enclosures, wiring connections from the Local Power Ranger Monitor (LPRM) outputs to the OPRM inputs, and replacing any associated instrumentation to satisfy the functional, load and interface requirements of the OPRMs when they become operational.

Replacement of Offgas Preheater Flow Control Isolation Valve 1N62-F313B per Design Change Package (DCP)
The DCP replaced Offgas Preheater Flow Control Isolation Valve 1N62-F313B. The previous Edwards valve leaked past its seat, and would not isolate. The replacement valve is a similar type Edwards valve.

Unit 1 Design Change Package 9700065, Splice Local Power Range Monitor Cable
The Local Power Range Monitor (LPRM) cable shield for Cable 1NR229 was found broken under the reactor vessel. The Design Change Package removed the damaged LPRM Cable from the detector, and was then cut and spliced in a local junction box. The new replacement cable was spliced in the local junction box to the existing cable and routed within the existing conduit to the detector. This eliminates the potential for LPRM spikes due to noise that could be induction into the ground path.
Revision to UFSAR drawing per Design Change Package (DCP) 9700316 – Replacement of Double Block Valve 1B33-F021/F022.
This DCP replaced the existing Anderson/Greenwood stainless steel double block valve (1B33-F021/F022) with two low carbon content stainless steel Y-Pattern globe valves installed in series. The design change was performed because the existing double block valve leaked by its seats with the pipe end cap removed and the Anderson/Greenwood valve is obsolete and parts are no longer available to repair it. UFSAR Drawing M-93 Sheet 2 is revised to change the drawing from the existing double block valve to two Y-Pattern globe valves.

UFSAR Update to Appendix G, Reactor Recirculation System
UFSAR Appendix G was revised to resolve inconsistencies between the power to flow map in the UFSAR and station procedures LOA-RR-101/201, and, the power to flow map in the procedures LOA-RR-101/201 is not properly labeled for the low flow lines, nor is the source of the power to flow map referenced.

The change involved updating the power to flow map to be consistent with procedures LOA-RR-101/201. The maps in the UFSAR are considered reference only with the operational boundary of the power to flow map being defined by technical specifications and the Core Operating Limits Report (COLR).

Revision to UFSAR drawing per Design Change Package (DCP) 9700056 – Repair / Replacement of Degraded Duct Sections of VE.
This DCP replaced two damaged sections of ductwork between HVAC hangers S-521 and S-519 (col. 10/row L, elev. 786'-6"), replaced a buckled horizontal wye duct fitting upstream of dampers 0VE06YA and OVE06YB and replaced duct sections on the discharge side of fan 0VE02CA. The DCP also replaced damaged sections of ductwork located above elev. 786'-6" in the Auxiliary Building and repaired sections of HVAC ductwork on the VE system along with other miscellaneous repairs.
UFSAR Drawing M-1443 Sheet 4 is revised to reflect the changes.

Unit 1 Group IV Isolation Logic Power Supply Change to Direct Current (DC) per Design Change Package (DCP) 9500476
The DCP changed the power supply for logic relays that initiate Group IV isolation of those ventilation dampers which provide secondary containment isolation to the Reactor Building Ventilation (VR) System as well as other Group IV isolation actions in the Reactor Building Purge (VQ) System and startup of the Standby Gas Treatment (VG) System of Unit 1. The power supply is changed from Reactor Protection System (RPS) Bus 120 Volt AC to 125 Volt DC, which prevents isolation of VR upon the loss of a single RPS bus.
This situation was a significant "work-around" for the operators at LaSalle. Changing of the power supplies for the Group IV logic relays to the 125 VDC system provides a more reliable power source for the logic relays than the RPS bus. The overall reliability of the plant is enhanced, unnecessary scrams and Group I isolations are prevented, and a significant "work-around" is cleared. The logic remains as de-energize-to-trip following installation of the DCP. UFSAR Subsection 7.3.2.2.1, Figure 7.3-10, and Tables 8.3-12
and 8.3-13 are revised.

UFSAR Revision to reflect Installation of Rotary Variable Differential Transformer on the 1B33-F060A/B Valves per Design Change Package (DCP) 9600137
DCP 9600137 installed rotary variable differential transformers (RVDT) on the reactor recirculation (RR) flow control valves (FCV) 1B33-F060A and 1B33-F060B. The DCP also installed signal conditioning modules on the outputs from the RVDTs, and upgraded the signal conditioning modules on the outputs of the existing linear variable differential transformers (LVDT). UFSAR Sections G.3.3 and G.5.2 are revised.

Revision to UFSAR Drawing per Design Change Package (DCP) 9700358 – Upgrade (0HY01J) Hydrogen Control Panel & Relief Valve (0HY005)
This DCP added a union downstream of relief valve 0HY005, between the valve and the vent line to allow easier removal of the valve for maintenance and bench testing. Additionally P&ID M-78 Sheet 1, a vendor drawing and the vendor Bill of Material were revised to reflect the as-built condition of the control panel which included adding two needle valves, several unions and relief valve vent caps not shown on the original design drawings.
UFSAR Drawing M-78 Sheet 1 is revised accordingly.

UFSAR Drawing revisions per Design Change Package (DCP) 9700352 – VC and VE Systems Air Conditioning Unit Prefilters Differential Pressure (DP) Switch Setpoint Revision.
This DCP changed the setpoints of differential pressure (DP) switches 0PDS-VC024, 0PDS-VC026, 0PDS-VC064 and 0PDS-VC066 for the Main Control Room air conditioning units and 0PDS-VE024 and 0PDS-VE064 for the Auxiliary Electric Equipment Room air conditioning units. The range springs in the existing DP switches were replaced, and the switches were re-calibrated to a new setpoint. The setpoints were revised in order to be consistent with the Pressure Drop Calculations, the Vendor recommendations and the UFSAR.
UFSAR Drawing M-3443 Sheet 9, Sheet 10 and Sheet 27 are revised to remove the setpoint values of the referenced DP switches and of other instruments shown on the drawing.

Installation of Continuous Oxygen Monitor per Unit 1 Design Change Package (DCP) 9400064 and Addendum
This DCP removed the drywell humidity monitoring system (trains A & B) and installed a new continuous oxygen monitoring system for sampling suppression chamber air and drywell air. The drywell sample line was reused. The return line to the suppression chamber was rerouted to a new containment penetration and is to be used as a sample line to obtain the suppression chamber sample.
This design change installed a dedicated system to continuously monitor suppression chamber and drywell oxygen concentration and eliminated the use of the Post-LOCA containment monitoring system for drywell oxygen concentration monitoring during normal plant operation. The drywell humidity monitoring system was removed because it was not performing properly and there are no regulatory requirements for such a system.
UFSAR Section 1.7 and Tables 3.8-1 Sheet 6, and 6.2-21 Sheets 4C, 4D, 6A and 9A are revised accordingly.

UFSAR Revision per Design Change Package (DCP) 9500324

The internals to High Pressure Core Spray (HPCS) check valve 1E22-F016 were removed. The valve was previously required to prevent draining of the cycled condensate storage tank (CST) in to the suppression pool. The valve is no longer required since the suction path from the CST has been removed. UFSAR Drawing M-95 Sheet 1 is revised per ECN 001234M (Unit 1 HPCS) and Figure 6.3-1 (HPCS system process diagram) is revised.

Offgas Air Operated Valves Actuator Upgrades and Stem/Bellows Replacement per Design Change Package (DCP) 9700061
The DCP implemented new bench set and supply air set point values for valves 1N62-F019A/B/C/D, 1N62-F025A/B, 1N62-F042, 1N62-F047, 1N62-F049, 1N62-N057, and 1N62-F394. The DCP improves the reliability and performance of the valves without impacting the function of the actuators and system performance.

Insulation of LaSalle Unit 1 Main Steam Bypass Valve Tailpipes per Design Change Package (DCP) 9700379
Main steam bypass valve tailpipes 1MS33AA-12", 1MS33AB-12", 1MS33AC-12", 1MS33AD-12", 1MS33AE-12", 1MS33BA-18", 1MS33BB-18", 1MS33BC-18", 1MS33BD-18", and 1MS33BE-18" were not previously insulated. As part of the turbine bypass system, these lines are used to control reactor pressure during the reactor heat-up to rated pressure, while the turbine-generator is being brought to speed and synchronized, during power operation when the reactor steam generation exceeds the transient turbine steam requirements, and during reactor cool down.
A portion of the lines is routed under cable trays causing the trays to be aged at an unacceptable accelerated rate. The DCP added calcium silicate insulation with aluminum lagging on the lines to prolong the life of the cables, in addition to reduce the heat load on the turbine building ventilation system.

Installation of Emergency Battery Pack for Valve 1E12-F018B per Design Change Package (DCP) 9700001
The DCP installed an emergency battery pack for valve 1E12-F018B, in order to illuminate the valve operator in accordance with Appendix R requirements. The power for the battery pack is fed from 480-V motor control center (MCC) 134X-2, Compartment D2, through regular lighting cabinet (RLC) #116. One remote lighting fixture was installed with the battery pack.

Lake Blowdown Flow Valve Enhancements per Design Change Package (DCP) 9700186
The DCP enhanced the functionality of Lake Blowdown Flow Valve 0WL005 ("Howell-Bunger Valve"). During the winter months when freezing occurs, back-splashing water freezes on the valve operating mechanism (drive screws), inhibiting its movement. The

DCP minimizes the amount of back-splash and added an enclosure over the operating mechanism (drive screws) to eliminate this problem.

Security Computer Replacement Project per Design Change Package (DCP) 9500338
The DCP implemented phase I of the Security Computer system upgrade, to improve the reliability and maintainability of Security Computer Systems. This was part of a ComEd Corporate effort General Office (GO) Corporate Security commissioned the Information Systems (IS) group of ComEd to develop a low cost upgrade that renders all ComEd Nuclear Sites identical in Security Computer Hardware and Software. The ComEd Information Systems (IS) group developed a personal computer (PC) based Security Computer System design and software for replacing Security Computer Systems at all ComEd sites. The design objectives consisted of reliable system designed around standard PC based hardware, eliminating known inherent problems with existing systems, increased functionality, user friendly operator consoles, improved report capabilities and on-line history, improved card access time, provide for future expansion and requirements, and ability to install a new system with little or no down time.

Changes to the Turbine Building Ventilation system to improve ventilation in the 1A Turbine Driven Reactor Feedwater Pump (TDRFP) cubicle per Design Change Package (DCP) 9600216 and UFSAR revisions.
The DCP installed vane axial fan 1VT13CA and associated ductwork over the existing floor openings in the Unit 1 'A' TDRFP room to create a forced transfer of air from the pump room to the heater bay below to improve air circulation and heat removal capacity of the VT system in the TDRFP room and reduce the room temperature. UFSAR subsections H.3.5.1, H.3.5.3, Table 9.4-13 and drawings M-INDEX Sheet 1, M-7, and M-1459 Sheet 2 are revised.

Changes to the Turbine Building Ventilation system to improve ventilation in the 1B Turbine Driven Reactor Feedwater Pump (TDRFP) cubicle per Design Change Package (DCP) 9600217 and UFSAR revisions.
The DCP installed vane axial fan 1VT13CB and associated ductwork over the existing floor openings in the Unit 1 'B' TDRFP rooms to create a forced transfer of air from the pump room to the heater bay below to improve air circulation and heat removal capacity of the VT system in the TDRFP room and reduce the room temperature. UFSAR subsections H.3.5.1, H.3.5.3, Table 9.4-13 and drawings M-INDEX Sheet 1, M-7, and M-1459 Sheet 2 are revised.

Revision to UFSAR Figure 13.5-1 per Design Change Package (DCP) 9700248
The DCP relocated Balance of Plant (BOP) computers from the main control room to the computer room, and Nuclear Steam Supply System (NSSS) printers were relocated

from adjacent to the center desk in the control room to the top of the lower desk, which is also a part of the center desk. The design change is part of the Main Control Room enhancement program, which is a human factors effort. UFSAR Figure 13.5-1 is accordingly revised.

UFSAR changes per Design Change Package (DCP) 9700208 – Reactor Water Cleanup (RT) System Recirculation Pumps and Return to Hot Suction.
This DCP restored the "hot suction" configuration of the RT system, as originally designed by General Electric, by replacing / reworking piping and associated valving. The design change installed the Reactor Water Cleanup pumps upstream of the system heat exchangers and routed the piping from outside the primary containment to the pump suction bypassing the heat exchangers. The pump discharge was routed to the system heat exchangers. The DCP replaced the three existing non-safety related 50% capacity RT System recirculation pumps with two new 100% capacity pumps.
UFSAR Sections 1.7, 7.3.2.2.3.8, and 7.7.1.2.1, Tables 5.4-1, 8.1-2, 8.1-9, 8.3-1 Sheet 2, 12.3-16 Sheet 1, Figures 4.6-5, 4.6-6, 5.4-6 Sheet 1 and Sheet 2, 5.4-8, 12.3-1 Sheet 4, 12.3-2 Sheet 4, 12.3-4 Sheet 2, and H.2-1 Sheet 3 and Drawings M-Index Sheet 1, M-7, M-74, M-90 Sheet 3, M-91 Sheets 2 and 6, M-97 Sheet 1, M-100 Sheet 1, M-104 Sheet 1, and M-2097 are revised accordingly.

UFSAR Update per Design Change Package (DCP) 9700321
Previous lake monitoring instrumentation provided only local lake blowdown flow velocity measurement, and did not provide continuous lake level monitoring in the main control room as required by the UFSAR. The DCP provides for continuous lake level monitoring in the main control room as required by the UFSAR. UFSAR Subsections 2.4.8.4, 7.7.11.3 and 11.2.2.6 are revised to reflect the recording of blowdown flow in the Main Control Room. UFSAR Subsection 9.5.2.2.2is revised to reflect the existence of the telemetry system.

Revision to UFSAR drawings per Design Change Package (DCP) 9700031 – Replacement of Backdraft Dampers 1VX09Y, 1VX11Y and 1VX53Y.
This DCP replaced the existing Switchgear Ventilation System (VX) backdraft dampers 1VX09Y, 1VX11Y and 1VX53Y with seismically qualified dampers with aluminum blades that will actuate at a lower differential pressure than the existing backdraft dampers. The new backdraft dampers will help to lower the pressure in the switchgear room. The change will improve the ability of the Auxiliary Electric Equipment Room (AEER) Ventilation System (VE) to maintain a positive pressure of 1/8" water column in the AEER.
UFSAR Drawing M-1462 is revised to remove the locked open (L.O.) designation after dampers 1VX09Y, 1VX11Y and 1VX53Y.

Revision to UFSAR drawings per Design Change Package (DCP) 9700032 – Replacement of Backdraft Dampers 2VX09Y, 2VX11Y and 2VX53Y.
This DCP replaced the existing Switchgear Ventilation System (VX) backdraft dampers 2VX09Y, 2VX11Y and 2VX53Y with seismically qualified dampers with aluminum blades that will actuate at a lower differential pressure than the existing backdraft dampers. The new backdraft dampers will help to lower the pressure in the switchgear room. The change will improve the ability of the Auxiliary Electric Equipment Room (AEER) Ventilation System (VE) to maintain a positive pressure of 1/8" water column in the AEER.
UFSAR Drawing M-1463 is revised to remove the locked open (L.O.) designation after dampers 2VX09Y, 2VX11Y and 2VX53Y.

Revision to UFSAR drawing per Design Change Package (DCP) 9700030 – Removal of Non-Safety Related/Non-Seismic Ductwork in the Main Security Control Center (MSCC).
This DCP removed the non-safety related/non-seismic ductwork physically associated with the Control Room HVAC system (VC) and with the spot cooler previously installed in the MSCC. The interconnections to the safety related ductwork were restored to the as-designed condition. This equipment is no longer required for present plant configuration. The removal of the non-safety related ductwork associated with the spot cooler will restore the VC system duct to the original design configuration.
UFSAR Drawing M-1443 Sheet 2 is revised to reflect the plant configuration of the MSCC return air being ducted to the VC return.

Generic Letter (GL) 96-06 Overpressure Protection for Reactor Recirculation Containment Penetration M-36 Piping per Unit 1 Design Change Package (DCP) 9700343
This DCP installed a ¾" diameter bypass line, including a check valve and a manual isolation globe valve, around the existing Inboard Containment Isolation Valve 1B33-F019 to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the bypass check valve will prevent potential over-pressurization during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event.
UFSAR Section 6.2.4.2.1, Table 3.2-1, Table 5.2-6 Sheet 2, Table 6.1-1, Table 6.2-21 Sheet 2A and 2B, Table 6.2-28 Sheet 1 and Drawing M-93 Sheet 2 are revised accordingly. UFSAR Figure 6.2-31 Sheet 10D (new figure) was added and Administrative Technical Requirements (ATR) Table 3.6.3-1 was revised.

Heater Drain Pump Minimum Flow Changes to Facilitate Idle Pump Warm-up per Design Change Package (DCP) 9700419
The DCP added the controls necessary to utilize the Heater Drain (HD) pump minimum flow bypass line to facilitate warm-up of an idle HD pump by permitting a higher flow rate in the minimum flow line for a short time period upon pump start-up. The design

change was implemented to reduce the potential loss of the unit (at high unit power) due to feedwater heater string isolations and resulting transients in the feedwater pump suction. UFSAR Section 10.4.7.2 and Drawing M-61 Sheet 2 are revised.

Relocation of Unit 1 Electro-hydraulic Control (EHC) Pump Vent Lines, Design Change Package (DCP) 9700348
The DCP relocated the pump discharge vent lines associated with air bleed valves 1EH011 and 1EH012 from an area of high vibration to an area of low vibration. The relocation to area of low vibration is needed to resolve past tubing failures induced by vibration.

Upgrade of the Public Address System and UFSAR Update per Design Change Package (DCP) 9700308
The DCP provides for permanent integration of the five zones into one plant-wide system for paging and party-line communications, and for extending the station's Public Address (PA) System to various out-buildings, which were outside the previous coverage areas. UFSAR Section 9.5.2 and Figure 9.5-2 were revised.

UFSAR Drawing revision per Design Change Package (DCP) 9700353 – Relocate 1EH07B Sensing Line to Electrohydraulic Control (EHC) Header Manifold.
This DCP relocated 1EH07B sensing line from EH-13 tee instrument cluster to the main header so that pressure switch 1PS-EH007B would be less susceptible to pressure fluctuations during testing.
UFSAR Drawing M-55 Sheet 10 is revised to reflect this change.

UFSAR Change per Modification of the Unit 1 Condensate Polishing Demineralizer Panel, Design Change Package (DCP) 9700071 (Modification M01-1-97-001)
The DCP removed the condensate polisher automatic regeneration mode of operation from Unit 1, in addition to removing the valve interlocks and permissives which control transfer between the condensate polishers (CP) and the tanks related to regeneration, to instead be controlled by manual operator action from the control panel. The transfer of resin from the cation/separation tank to the mix/storage tank was modified. The Unit 1 regenerate cycle no longer includes the full chemical cleaning process. UFSAR Subsections 10.4.6.2, 10.4.6.3, 10.4.6.5, 11.2.1.7, 11.2.1.7.1, and 11.2.2.3 are revised to reflect that regeneration is no longer possible in Unit 1.

Changes to the Turbine Building Ventilation System to Provide Cooling to the Area of the Turbine Valves' Electro-Hydraulic Controls (EHC) in the Turbine Building Low Pressure Heater Bay per Design Change Package (DCP) 9600528 and UFSAR revisions.

The DCP installed two new 10,000 cfm vane axial fans (1VT14C and 1VT15C) in the low pressure heater bay. Discharge ductwork from the fans was routed to the vicinity of the EHC controls for the turbine control valves, the turbine stop valves, and the main steam bypass valves to provide additional cooling air to reduce the temperature and thermal stratification in this area.
Revision 1 of the DCP approved the change in fan power supply location from MCC 133B-2 Compartments D3 and D6 to Compartments D3 and D2. UFSAR Table 9.4-13 and drawings M-INDEX Sheet 2, M-9 and M-1459 Sheet 2 are revised.

Unit 1 Electro-Hydraulic Control Oil Trip Test Logic Setpoint Change per Design Change Package (DCP) 9600372
The DCP changed the time delay settings of two relays and installed a jumper in another relay of the main turbine trip reset circuits to provide more time to ensure that reset proceeds to completion when actuated.
Reactor Core Isolation Cooling (RCIC) Sight Flow Indicator Replacement per Design Change Package (DCP) 9500104
The DCP replaced Unit 1 RCIC high point vent flapper type sight flow indicator 1E51-D306 with a rotary wheel type sight flow indicator. Flow verification was difficult to perform with the previous flapper type sight flow indicator, and its horizontal configuration caused the hinged flapper to stick open.

UFSAR Revision per Design Change Package (DCP) 9700350.
DCP 9700350 revised the Control Room and Auxiliary Electric Equipment Room ventilation (VC and VE systems, respectively) manual purge control circuit for Train A, so that the following functional changes take place in the Purge Mode when smoke is detected in the control room:
Maximum outside air dampers 0VC08YA, 0VC53YA, 0VE05YA, and 0VE30YA close; Exhaust air dampers 0VC14YA and 0VE04YA close; and return air dampers 0VC10YA and 0VE03YA open. The DCP interlocks the outside smoke (ionization) detection system to the isolation dampers used during purging in order to achieve automatic realignment to pressurization mode upon detection of smoke in the outside air. UFSAR Drawing M-3443 Sheets 5, 18, and 24 are accordingly revised per ECN 001284E.

UFSAR Revision per Design Change Package (DCP) 9700351, VC/VE Manual Purge Control Circuit Logic Change – 'Train B'.
DCP 9700351 revised the Control Room and Auxiliary Electric Equipment Room ventilation (VC and VE systems, respectively) manual purge control circuit for Train B, so that the following functional changes take place in the Purge Mode when smoke is detected in the outside air:
Maximum outside air dampers 0VC08YB, 0VC53YB, 0VE05YB, and 0VE30YB close; Exhaust air dampers 0VC14YB and 0VE04YB close; and return air dampers 0VC10YB and 0VE03YB open. The DCP interlocks the outside smoke (ionization) detection

system to the isolation dampers used during purging in order to achieve automatic realignment to pressurization mode upon detection of smoke in the outside air. UFSAR Drawing M-3443 Sheets 5, 18, and 24 are accordingly revised per ECN 001285E.

Replacement of Unit 2 Reactor Building Closed Cooling Water system Outlet Header per Design Change Package (DCP) 9700390
The DCP replaced a portion of the Unit 1 Reactor Building Closed Cooling Water (RBCCW) heat exchange outlet Service Water (WS) system outlet header 1WS26B-20" from carbon steel to stainless steel. The replaced portion of piping was eroded due to severe cavitation and impingement. The replacement stainless steel piping is more resistant to cavitation and impingement. Drawing M-69 Sheet 1 (Unit 1 Service Water system) is accordingly revised.

Reroute VE Ductwork from Computer Room to Units 1 & 2 Auxiliary Electric Equipment Room (AEER) per Design Change Package (DCP) 9700551 (Addendum #2) and Engineering Change Notices (ECNs) 001388H, 001392H, and 001384E; and UFSAR revisions.
The DCP created temporary access openings in the west wall of the duct chase near column 'R' and line '15' in the auxiliary building at floor elevations 768' and 749' to allow removal of the VE system supply and return air duct runs that service the computer room along with their associated duct supports. New duct runs and duct supports from the existing VE supply and return ducting were installed to service Units 1 & 2 AEERs. Wall mounted and ceiling mounted lighting fixtures, emergency battery packs, a PA system horn with box, electrical conduits, fittings and associated supports were removed and relocated to facilitate the new duct installation. The temporary access openings in the duct chase were closed following completion of the construction work. This design provides new flow paths to serve both AEER and enhances the VE system in meeting its cooling and pressurization requirements for habitability and alleviates system performance problems.
UFSAR Section 9.4.1.2 is revised to delete reference to the VE system supply and return interfacing with the computer room. UFSAR Drawing M-1443 Sheets 3 & 4 are revised to delete the return duct from the computer room to the VE return system. A new drawing (M-1467 Sheet 3) is added to the UFSAR to reflect that the supply duct from the VE supply to the computer room is deleted. The new flow path for the additional VE supply and return to both AEERs is added to these drawings.

Source Range Monitor (SRM) Retract Permissive and Downscale Trip Setpoint per Design Change Package 9700572
The SRM retract permissives didn't satisfy Technical Specifications Table 3.3.6-1, Trip Function 3.a. Note b, which states that the trip function of the SRM will be automatically bypassed if the detector count rate is greater than or equal to 100 counts per second (cps). This was documented in Licensee Event Report (LER) 97-011. Based upon

General Electric (GE) calculations, the Unit 1 SRM retract permissive setpoints were revised to 306 cps from 100 cps. The SRM downscale trip setpoints were also revised to 1.51 cps from 1.18 cps. UFSAR Tables 7.3-5 and 7.7-4 are revised.

Revision to UFSAR drawing per Design Change Package (DCP) 9700469 – Seal Weld Cap/Nipple to Class I Requirements (Loop A).
This DCP replaced the existing Class D reducer, pipe nipple (1RR17CA) and threaded cap of the Reactor Recirculation System drain line with Class A reducer, pipe nipple and welded cap. The piping was insulated due to the change in pipe class. These changes allow the Reactor Recirculation System's pressure boundary and the ASME code classification boundary to be extended from valve 1B33-F052A to the Class A pipe nipple and cap.
Drawing M-93 Sheet 1 is revised to reflect this change.

Revision to UFSAR drawing per Design Change Package (DCP) 9700529 – Seal Weld Cap/Nipple to Class I Requirements (Loop B).
This DCP replaced the existing Class D reducer, pipe nipple (1RR17BB) and threaded cap of the Reactor Recirculation System drain line with Class A reducer, pipe nipple and welded cap. The piping was insulated due to the change in pipe class. These changes allow the Reactor Recirculation System's pressure boundary and the ASME code classification boundary to be extended from valve 1B33-F052B to the Class A pipe nipple and cap.
UFSAR Drawing M-93 Sheet 2 is revised to reflect this change.

Revise bench set and air supply pressure for Valve 1RE056 per Design Change Package (DCP) 9700425.
This DCP revised the bench set and air regulator setpoint for valve 1RE056, replaced the pressure regulator with one having a higher outlet pressure, and added two test tap connections in the air supply line to the actuator to facilitate diagnostic testing. The purpose of this change was to improve the reliability and to ensure proper performance of the valve without impacting the function of the valve actuator and system performance.

Revise bench set and air supply pressure for Valve 1RF021 per Design Change Package (DCP) 9700426.
This DCP revised the bench set and air regulator setpoint for valve 1RF021, replaced the pressure regulator with one having a higher outlet pressure, and added two test tap connections in the air supply line to the actuator to facilitate diagnostic testing. The purpose of this change was to improve the reliability and to ensure proper performance of the valve without impacting the function of the valve actuator and system performance.

Addition of Low Point Drains in Service Water Piping per Design Change Package (DCP) 9700422
This DCP added low point drain lines with a manual valve and pipe cap to Unit 1 Turbine Building Service Water supply lines 1WS09A-14" (Turbine Oil Cooler Supply Header) and 1WS11A-20" (Stator Cooling and Generator Hydrogen Cooler Units Supply Header). These low point drain lines were added to allow draining of the piping during extended system lay-up to prevent corrosion damage to the piping due to stagnant water conditions.
UFSAR Drawing M-69 Sheet 2 is revised to show the addition of the drain line assemblies.

Formalize the Design Basis for the Shad Net
The shad net provides no safety function and was introduced only to aid in the maintenance of existing plant system strainers and screens by preventing fish from entering plant components. The shad net has performed its intended function since installation in 1982, no formal evaluation was performed to update the UFSAR to include a description of the shad net. UFSAR Sections 2.5, 3.1, and 9.2 are revised to include a discussion of the shad net.

Unit 1 - Design Change Package (DCP) 9700518, Replacement of Valve Stem and Stem Nut on Motor Operated Valves 1G33-F001 and 1G33-F004
The DCP replaced the internals of valves 1G33-F001 and 1G33-F004 to support the installation of DCPs 9700519 and 9700520. These DCPs replaced each of the valve's Limitorque actuators.

Unit 1 - Design Change Package (DCP) 9700519 for Replacement of Limitorque Actuator and Motor on Motor Operated Valve 1G33-F001 and UFSAR Revisions. The DCP replaced the existing 15 ft-lb. SMB-0 actuator on Valve 1G33-F001 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed through containment penetration E-6 to provide power to the motor operated valve and the molded case circuit breakers (2) and thermal overload relay were replaced.
UFSAR Table 6.2-28, Table H.4-14, Table H.4-17 and Table H.4-48 along with Unit 1 Administrative Technical Requirements (ATR) Table 3.6.3-1 are accordingly revised.

Replacement of Limitorque Actuator and Motor on Motor Operated Valve 1G33-F004 per Design Change Package (DCP) 9700520
The DCP replaced the 15 ft-lb. SMB-0 actuator on Valve 1G33-F004 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than

10 seconds. A new three (3) conductor 6 AWG cable was installed to provide power to the motor operated valve and the molded case circuit breaker and thermal overload relay were replaced. UFSAR Table 6.2-28, Table H.4-14, Table H.4-17 and Table H.4-48 in addition to Unit 1 Administrative Technical Requirements (ATR) Table 3.6.3-1 are accordingly revised.

Unit 1 - Design Change Package (DCP) 9700518, Replacement of Valve Stem and Stem Nut on Motor Operated Valves 1G33-F001 and 1G33-F004
NRC Generic Letter (GL) 96-06 addresses primary containment isolation valve arrangements that are susceptible to thermal overpressurization following a LOCA in the drywell. The DCP drilled a vent hole in the reactor side of valve 1G33-F001 to address this concern.

Unit 1 Reactor Recirculation Hydraulic Power Unit (RR HPU) Containment Isolation Valve Switch and Cover Replacement per Design Change Package (DCP) 9700166.
This DCP affected sixteen (16) RR HPU Containment Isolation valves: 1B33-F338A/B, 1B33-F339A/B, 1B33-F340A/B, 1B33-F341A/B, 1B33-F342A/B, 1B33-F343A/B, 1B33-F344A/B, and 1B33-F345A/B
The modification replaced the steel housing on the solenoid and limit switches (top) of each valve with a two-piece design stainless steel housing. The previously existing assemblies of limit switch brackets, limit switches, and terminal blocks were replaced with new assemblies of limit switch brackets, limit switches, terminal blocks, and vernier adjustment devices for setting limit switch actuation positions. Additionally, cables from each of the valves to the first junction box was replaced with high-temperature cable. This modification was installed to resolve repeated position indication problems experienced by these valves.

Installation of Interposing Relays in Turbine Master Trip Solenoid Valves Test Circuits per Exempt Change E01-1-9600302 (Design Change Package 9600302)
General Electric Company (GE) Technical Information Letter (TIL) 1212 concerns the failure of the turbine master trip solenoid valves (MTSV) to reset at turbine reset or during MTSV testing. This has been attributed to inadequate voltage across the solenoid coil. The DCP installed a 24 VDC interposing relay in the test circuit of each MTSV. The functions of the MTSV turbine-generator electrical trips are maintained, as a valid electrical trip will de-energize both MTSV solenoids to trip the turbine-generator regardless of test status.

UFSAR Update per Design Change Package (DCP) 9600356, Converting Main Condensate (MC) Drops to Cycled Condensate (CY) Drops
The DCP converted portions of contaminated MC piping to a CY supply, abandoned in place and removed other portions, and provides a clean MC path to the chemistry sinks

via the sample lines. UFSAR Drawing M-74, M-75 Sheets 1,2, and 3, and M-103 Sheet 26 are revised to show the portions of contaminated MC piping converted to a CY supply, the abandoned piping, and a clean MC path to the chemistry sinks via the sample lines.

Revision to UFSAR Drawing M-69 Sheet 1 per Design Change Package (DCP) 9500360
The DCP replaced the Unit 1 6-inch primary containment ventilation chiller service water condenser Masoneilan control valve 1WS077A with a 10-inch Control Component Inc. (CCI) DRAG control valve. Noise, vibration, and downstream cavitation associated with the operation of the Masoneilan valve has caused erosion of the control valve body and the outlet piping. The CCI DRAG valve is designed to eliminate noise, vibration, and downstream cavitation such that erosion is minimized. UFSAR Drawing M-69 Sheet 1 for the Service Water System is accordingly revised.

Revision to UFSAR Drawing M-69 Sheet 1 per Design Change Package (DCP) 9500363
The DCP replaced the Unit 1 6-inch primary containment ventilation chiller service water condenser Masoneilan control valve 1WS077B with a 10-inch Control Component Inc. (CCI) DRAG control valve. Noise, vibration, and downstream cavitation associated with the operation of the Masoneilan valve has caused erosion of the control valve body and the outlet piping. The CCI DRAG valve is designed to eliminate noise, vibration, and downstream cavitation such that erosion is minimized. UFSAR Drawing M-69 Sheet 1 for the Service Water System is accordingly revised.

UFSAR Revision for End of Cycle Recirculation Pump Trip (EOC-RPT) Response Times
The EOC-RPT response times in UFSAR Subsections G.3.2.2.2.D.1 and G.5.1.3.1 are revised from 140 milliseconds (msec) to 190 msec. This is to achieve consistency with other UFSAR subsections, the Technical Specifications, and transient analysis reports submitted by General Electric and Siemens Power Corporation. UFSAR pages G.3.2-2 and G.5.1-2 are revised.

Revision to UFSAR Figure 13.5-1 per Design Change Package (DCP) 9700528
The DCP added various cabinets in the main control room to store operating procedures, prints, block cases, emergency, self-contained air breathing apparatus, and miscellaneous parts as requested by the Operating Department. The cabinets are required to be stored in the main control room to maintain habitability. UFSAR Figure 13.5-1 is accordingly revised.

Unit 1 Standby Gas System Overpressurization Protection per Design Change Package (DCP) 9700402 and UFSAR Revision
The DCP installed 20" diameter valve 1VG023 on the Unit 1 standby gas treatment system (VG) primary containment suction piping in order to provide a method of isolating the standby gas treatment system from the primary containment vent/purge system during the purging/venting process. Installation of this design change provides over-pressurization protection in the event of a LOCA during the purging or venting of the drywell or the suppression chamber. UFSAR Tables 3.2-1 and 6.1-1, and UFSAR Subsections 6.5.1.5 and 6.5.1.6, and drawing M-89 are accordingly revised.

Unit 2 Standby Gas System Overpressurization Protection per Design Change Package (DCP) 9700403 and UFSAR Revision
The DCP installed 20" diameter valve 2VG023 on the Unit 2 standby gas treatment system (VG) primary containment suction piping in order to provide a method of isolating the standby gas treatment system from the primary containment vent/purge system during the purging/venting process. Installation of this design change provides over-pressurization protection in the event of a LOCA during the purging or venting of the drywell or the suppression chamber. UFSAR Tables 3.2-1 and 6.1-1, and UFSAR Subsections 6.5.1.5 and 6.5.1.6, and drawing M-89 are accordingly revised.

Unit 1 Permanent Installation of Existing Transient Analysis Data System (TADS) Panel per Design Change Package (DCP) 9100236 and UFSAR Revision
The TADS panel 1PA19J had been previously located in the AEER until it was identified that the panel was not seismically mounted (LER 97-027). The DCP permanently installed the TADS Panel 1PA19J and the associated nine (9) interconnection cables inside Unit 1 Auxiliary Electrical Equipment Room (AEER). UFSAR Figure H.4-1 is revised to show the location of the TADS panel 1PA19J in the AEER.

Design Change Package (DCP) 9700180
DCP 9700180 replaced and rerouted the reactor core isolation cooling (RCIC) turbine condensation drain lines 1RI10B-3/4", 1RI10BA-3/4", 1RI10BB-3/4", 1RI14A-3/4", and 1RI96A-3/4", and installed a sight glass in the turbine condensation drain pot. The new stainless steel drain lines replace carbon steel lines. The use of stainless steel and the rerouting of the lines is intended to prevent low point condensation accumulation and subsequent rust formation. Stem packing leakoff line 1RI38B-3/4" from valve 1E51-F360 replaced and reconfigured to ensure that the pipe has continuous slope to the RCIC barometric condenser 1E51-C002 to minimize low point condensation accumulation. A new strainer and restricting orifice, 1E51-D319 and 1E51-D320, respectively, are added to drain line 1RI10B-3/4". UFSAR Drawing M-101 Sheet 1 (RCIC system) is revised.

UFSAR Revision associated with Procedure LTS-300-5, Revision 22
Changes incorporated to procedure LTS-300-5 Revision 22, LaSalle Station Primary Containment Leak Rate Testing Program, are associated with an Assessment of the Appendix J Program, Licensee Event Report (LER) 97-014-00, plant modifications associated with NRC Generic Letter 96-06, and other various issues. Corresponding revisions to UFSAR Section 6.2.6 involve editorial changes, administrative changes, acceptance criteria changes, new components added to program, physical containment penetration changes, and change in testing methodology, all of which reflect the changes to LTS-300-5.

UFSAR Drawing Revision per Design Change Package (DCP) 9600300 – Revise Reject Line High Pressure Alarm Circuit.
Spare limit switch "IO" contacts on condenser valve 1G33-F034 and radwaste collector valve 1G33-F035 were wired to the alarm circuit of existing pressure switch 1G33-N014 to disable the high pressure alarm when both valves are closed. New cables were routed from the valve limit switches to local panel 1H22-P002 and the alarm circuit in local panel 1H22-P002 was rewired to obtain the required logic.
UFSAR Drawing M-97 Sheet 1 is revised to include dashed lines to indicate an interlock between the high pressure alarm and the F034 and F035 valves.

UFSAR Update per Removal of Remote Indication Hardware from Unit 1 Division 3 Emergency Core Cooling System (ECCS) Testable Check Valve, Design Change Package (DCP) 9700489
DCP 9700489 removed remote indication hardware from Unit 1 Division 3 ECCS testable check valve 1E22-F005. This was done to eliminate a recurring problem in which the valve failed to completely close. This is attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP increases the margin by reducing the frictional forces, thereby eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 9.3.1.2.2, Table 6.2-21, and drawings M-66 Sheet 2 and M-95 are revised. An evaluation identified the hold points which needed to be resolved and documented prior to the performance of operability tests associated with DCP 9700489.

The safety evaluation documented the acceptability of using an interference fit to prevent the rotation of the disc bushing relative to the disc of testable check 1E22-F005, as opposed to employing tack welds. Tack welding the stellite bushing to the carbon steel disc was used when the valves were manufactured. This method was previously abandoned by the valve manufacturer due to cracking of the tack welds.

Removal of Remote Indication Hardware from Unit 1 Division 1 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700487

DCP 9700487 removed remote indication hardware from Unit 1 Division 1 ECCS testable check valves 1E12-F041A, 1E12-F050A, and 1E21-F006, to eliminate a recurring problem in which the valves fail to completely close. This was attributed to the small margin between the forces to close the valves and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves the performance of each valve, increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, and 9.3.1.2.2, Table 6.2-21, and drawings M-66 Sheet 2, M-94, and M-96 are revised.

Engineering Change Notice (ECN) 001450M for Design Change Package (DCP) 9700487, Removal of Remote Indication Hardware from Unit 1 Division 1 ECCS Testable Check Valves 1E12-F041A, 1E12-F050A, and 1E21- F006

Upon Disassembly and inspection of the Division 3 ECCS testable check valve 1E22-F005, the disc bushings were found to be loose and the tack welds cracked. Based upon conversations with the valve manufacturer, BW/IP - Anchor Darling, it was determined that the design configuration utilizing tack welds is obsolete. The new configuration relies upon an interference fit between the outside diameter of the bushing and the inside diameter of the bore in the disc, and has been successfully used for years without problems.

ECN 001450M was issued to revise the existing tack welded bushing configuration to the present BW/IP - Anchor Darling interference fit bushing configuration. The UFSAR changes proposed by DCP 9700487 remains valid.

Removal of Remote Indication Hardware from Unit 1 Division 2 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700488

DCP 9700488 removed remote indication hardware from Unit 1 Division 2 ECCS testable check valves 1E12-F041B, 1E12-F041C, and 1E12-F050B, to eliminate a recurring problem in which the valves fail to completely close. This was attributed to the small margin between the forces to close the valves and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves the performance of each valve, increases the margin by reducing the frictional forces and eliminating the problem, and reduces both the frequency of maintenance and radiological exposures. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 9.3.1.2.2, Table 6.2-21, and drawings M-66 Sheet 2 and M-96 are revised.

UFSAR Changes per Design Change Package (DCP) 9500483 – Install Filter in 1FW01KA/B Turbine Driven Reactor Feed Pump (TDRFP).

This DCP added in-line filters to the high pressure control and hydraulic oil piping just before the TDRFP turbine controllers. One duplex filter was added to each TDRFP 1FW01KA & B. This new filtration system will trap particles that could affect the hydraulic operation of the turbine speed controller and the turbine drive trip spool. Additionally, new differential pressure indicators were added outside the TDRFP room walls to minimize dose to personnel. UFSAR Section 9.5.1 and Drawings M-INDEX Sheet 1 and M-7 are revised to reflect this change.

Design Change Package (DCP) 9700578, Relocation of Pressure Switches 1B21-N413A and C
The design change relocated pressure switches 1B21-N413A and C from pipe stand mounts to instrument rack 1H22-P026, where better instrument needle valves are available to minimize spiking caused by instrument valve operations. This will aid in minimizing the incidence of scrams and/or engineered safety feature actuations resulting from pressure spiking associated with instrument valve operations. Drawing M-93 Sheet 5 is revised.

Design Change Package (DCP) 9700579, Relocation of Pressure Switches 1B21-N413B and D
The design change relocated pressure switches 1B21-N413B and D from pipe stand mounts to instrument rack 1H22-P027, where better instrument needle valves are available to minimize spiking caused by instrument valve operations. This will aid in minimizing the incidence of scrams and/or engineered safety feature actuations resulting from pressure spiking associated with instrument valve operations. Drawing M-93 Sheet 4 is revised.

Removal of Unit 1 Main Steam Isolation Valve (MSIV) Closure Scram Bypass Pressure Switches per Design Change Package (DCP) 9700461 and UFSAR revision.
This DCP disconnected and removed the existing MSIV closure bypass pressure switches 1B21-N020A, 1B21-N020B, 1B21-N0202C, and 1B21-N020D along with the associated tubing, valves and fittings from instrument racks 1H22-P004, 1H22-P027, 1H22-P005 and 1H22-P026 respectively. The cables between the instrument racks and the main control room (MCR) panels were de-terminated and left in place unassigned, and the associated terminal points in the MCR panels were jumpered. The DCP implements License Amendment No. 121 to Unit 1 license.
UFSAR Sections 7.2.2.4.6, 7.A.2.1.2, 7.A.2.1.14, 7.A.3.2, 15.2.4, Figure 7.2-1 Sheets 2 and 3, and Drawings M-93 Sheet 4 and Sheet 5 are revised accordingly.

Turbine Building Supply Airflow Reduction for Turbine Building Negative Pressure, Design Change Package (DCP) 9700397

The DCP reduced the supply air to the Turbine Building to ensure a negative pressure is maintained by installing new balancing dampers 1VT106Y and 1VT107Y on the common supply air header of the turbine building ventilation (VT) supply fans 1VT01CA, 1VT01CB, and 1VT01CC. Two recirculation dampers were added in the common supply fan discharge duct, to reduce the total VT system supply flow to the turbine building, to route part of the fan discharge flow back to the inlet side of the fans. Various VT system instrumentation setpoints and ranges were adjusted to accommodate the change in system air flows. UFSAR Sections 9.4, 11.3, and turbine building ventilation system drawings M-1459 sheets 1, 2, and 3 are revised.

Unit 1 Design Change Package (DCP) 9700339, Generic Letter (GL) 96-06 Overpressure Protection for Penetration Piping.
The DCP added two ¾" diameter relief valve assemblies between containment penetrations M-16 and M-17 and existing inboard containment isolation valves 1WR179 and 1WR180 to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the relief valves will prevent potential over-pressurization during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event. UFSAR Section 6.2.4.2.2, Table 6.2-21 Sheets 1A and 1B, Table 6.2-28 Sheet 7, Figure 6.2-31 Sheet 2 and Drawing M-90 Sheet 2 were revised accordingly. Administrative Technical Requirements (ATR) Table 3.6.3-1 was revised.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700335, Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-25 and M-27.
This DCP installed ¾"x1" relief valves on the Primary Containment Penetrations M-25 and M-27 piping between the primary containment penetrations and the inboard isolation valves 1VP113A and 1VP114A to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the relief valves will prevent potential over-pressurization of the piping between the PCIS valves during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event.
UFSAR Section 6.2.4.2.2, Table 3.2-1, Table 6.2-21 Sheets 1C and 1D, Table 6.2-28 Sheet 7, Figure 6.2-31 (new figure) and Drawing M-86 Sheet 1 are revised accordingly. Administrative Technical Requirements (ATR) Table 3.6.3-1 is revised.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700336, Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-26 and M-28.
This DCP installed ¾"x1" relief valves on the Primary Containment Penetrations M-26 and M-28 piping between the primary containment penetrations and the inboard isolation valves 1VP113B and 1VP114B to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the relief valves will prevent

potential over-pressurization of the piping between the PCIS valves during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event.
UFSAR Section 6.2.4.2.2, Table 3.2-1, Table 6.2-21 Sheets 1C and 1D, Table 6.2-28 Sheet 7, Figure 6.2-31 (new figure) and Drawing M-86 Sheet 1 are revised accordingly. Administrative Technical Requirements (ATR) Table 3.6.3-1 is revised.

Generic Letter 96-06 Over pressurization Protection for Primary Containment Piping, Design Change Package (DCP) 9700341
The DCP installed a relief valve on the residual heat removal (RHR) supply line between primary containment isolation system (PCIS) valves 1E12-F008 and 1E12-F009 (primary containment penetration M-7). The design change was installed to resolve overpressure concerns associated with NRC Generic Letter 96-06. UFSAR Table 5.2-6, Subsection 6.2.4.2.1, Tables 6.2-21and 6.2-28, Figure 6.2-31, and drawing M-96 Sheet 3 are revised to reflect the installation of the design change.

UFSAR Revision to reflect Design Change Packages 9700564, 9700565, 9700566, and 9700567
Two ventilation intake dampers on the 0, 1A, 1B, and 2A diesel generator (DG) ventilation equipment rooms were modified to include a warm weather manual bypass blade per DCPs 9700564, 9700565, 9700566, and 9700567, respectively. The bypass blades were installed to allow in-leakage of outside air into the DG rooms during the summer per original design. UFSAR Sections 9.4 and 9.5 and drawings M-1444, M-1445, and M-1447 are revised.

UFSAR revision to reflect Unit 1 Design Change Package (DCP) 9700130, Replace Unit 1 Loose Parts Monitoring System (LPMS)
The DCP removed the loose parts monitoring equipment from panel 1PA15J and replaced it with a new state-of-the- art data acquisition system manufactured by Siemens Power Corporation. The new equipment is designed to work with existing accelerometers and preamplifiers (charge converters), and the existing annunciator system and power supply. The previous LPMS did not conform to the configuration described in the SER and the response to FSAR Question 221.14. UFSAR Section 4.4.6 is revised by adding Section 4.4.6.1 to include a description of the installed upgraded LPMS configuration applicable to Unit 1.

Unit 1 Number 1 and 2 Feedwater Heater Drain Control Valve Replacements per Design Change Package (DCP) 9700287
The DCP replaced the Unit 1 number 1 feedwater heater drain normal control valves 1HD072A, B, C and emergency drain control valves 1HD065A, B, C with valves of larger flow capacity, and, replaced the internal trim of the number 2 feedwater heater emergency drain control valves 1HD062A, B, C in order to increase their flow capacity.

Insulation was also installed on normal drain lines which were not previously installed on the number 1 feedwater heater. UFSAR Drawings M-61 Sheets 3 and 4 of the feedwater heater drains system are to be revised.

LaSalle Operating Procedure LOP-WS-02 Revision 9, "Service Water Pump and Service Water Jockey Pump Startup and Operation", and Clarification to UFSAR Section 9.2.2.2
UFSAR 9.2.2.2 is revised to clarify that during startup or shutdown of one of the units, the service water pump combination can be adjusted such that the required number of main service water or jockey pumps is operating to meet that system's cooling requirements. The revision to procedure LOP-WS-02 incorporates the above UFSAR clarification.

Revision to UFSAR drawings per Unit 1 Design Change Package (DCP) 9700507 – Permanent Installation of the Unit 1 Heater Bay Cameras.
This DCP replaced the nine (9) existing cameras in the Unit 1 Heater Bay with permanently installed cameras and added one new camera in the Condenser Pit. The permanently installed cameras are cooled by forced air supplied by a skid mounted compressor assembly (1CQ013) and will allow visual inspection of Heater Bay components with the Unit at power without exposing personnel to high dose rates. UFSAR Drawings M-Index and M-8 are revised accordingly.

Upgrade Unit 1 Reactor Recirculation Hydraulic Power Unit (RR HPU) Containment Isolation Valve and Reactor Recirculation Sample Line PCIS Isolation Valve per Design Change Package (DCP) 9700596
This design change upgraded the Unit 1 RR HPU Containment Isolation valves light indication in the Main Control Room and RR Sample line limit switch and electrical conductor seal assembly to meet Regulatory Guide 1.97 requirements. 1B33-F338A/B, 1B33-F339A/B, 1B33-F340A/B, 1B33-F341A/B, 1B33-F342A/B, 1B33-F343A/B, 1B33-F344A/B, and 1B33-F345A/B were affected by this modification. The DCP added fuses to isolate the valves' position indicating light circuits from the valves' control circuits for the inboard and outboard RR HPU solenoid isolation valves. The existing auxiliary relays were replaced with Class 1E Agastat type EGPI relays. The configuration of the Main Control Board summary indicating light circuits was revised to develop a closed indicating light to provide 'ON' indication when all the valves in the summary group are all the way closed and 'OFF' indication for the condition of any one or more being not fully closed. The lens for the valve group status indicating lights was changed from green to red. (Reference DCP 9700166.)

Revision to UFSAR Subsection 9.3.5.2 to reflect as-built condition of the facility

UFSAR Subsection 9.3.5.2 was revised to reflect the as-built condition of the standby liquid control system (SBLC) on Unit 1 and Unit 2. The description of the ambient temperature in subsection 9.3.5.2 is expanded from '70 °F - 100 °F' to '65 °F to 104 °F'.

Main Control Room (MCR) and Auxiliary Electric Equipment Room (AEER) Penetration Seals per Design Change Package (DCP) 9700594 (Addendum #2) and Engineering Change Notice (ECN) 001416S and UFSAR revisions.
The ECN and DCP provide alternate generic penetration sealing material and methods for the purpose of reducing air leakage from the outer envelopes of the MCR and AEER to adjacent areas. The volume of air leakage from the MCR and AEER is one of the contributing factors to the inability of the VC/VE systems to maintain their respective areas at the 1/8" water column (WC) positive pressure with respect to surrounding areas as required by the UFSAR.
UFSAR Section H.1.3 and Figure H.1-1 are revised to mention the option of coating the fire seals utilized at the top of concrete block walls in seismic structures with Vimasco 3IR cable coating air seal.
Revision to UFSAR drawings per Design Change Package (DCP) 9700605 – Relocate VC Train B Outside Air Intake to Return Fan Suction.
This DCP relocated the outside air intake connection in the VC system Train B from its present connection point (suction of the supply fan) to the suction of the return fan. The work included relocation of dampers 0VC04YB, 0VC06YB and 0VC70YB, rerouting existing ductwork, removal of existing hanger (973-S), installation of new hangers, and removal of an air flow monitor (0FE-VC037). This change ensures sufficient air is drawn into the system during normal and emergency modes of operation for Main Control Room pressurization and enhances the overall VC system airflow.
UFSAR Drawings M-1443 Sheet 1 and M-3443 Sheets 1, 3, 4, 5, 6 and 17 are revised to reflect the changes.

Design Change Package (DCP) 9700598, Replacement of RHR Heat Exchanger Relief Valve 1E12-F313A
The DCP replaced the residual heat removal (RHR) B heat exchanger tube side relief valve 1E12-F313A in response to past setpoint test failures. The valve was also relocated and re-oriented to the vertical position, per ASME requirements. UFSAR drawing M-91 Sheet 3, Reactor Building Equipment Drains, is being revised to reflect the installation of DCP 9700598.

Design Change Package (DCP) 9700599, Replacement of RHR Heat Exchanger Relief Valve 1E12-F313B
The DCP replaced the residual heat removal (RHR) B heat exchanger tube side relief valve 1E12-F313B in response to past setpoint test failures. The valve was also relocated and re-oriented to the vertical position, per ASME requirements. UFSAR

drawing M-91 Sheet 3, Reactor Building Equipment Drains, is being revised to reflect the installation of DCP 9700599.

Revision to UFSAR drawings per Design Change Package (DCP) 9700604 – Relocate VC Train A Outside Air Intake to Return Fan Suction.
This DCP relocated the outside air intake connection in the VC system Train A from its present connection point (suction of the supply fan) to the suction of the return fan. The work included relocation of dampers 0VC04YA, 0VC06YA and 0VC70YA, rerouting existing ductwork, removal of existing hangers (942-S/943-S), installation of new hangers, and removal of an air flow monitor (0FE-VC032). This change ensures sufficient air is drawn into the system during normal and emergency modes of operation for Main Control Room pressurization and enhances the overall VC system airflow. UFSAR Drawings M-1443 Sheet 1 and M-3443 Sheets 1, 3, 4, 5, 6 and 17 are revised to reflect the changes.

Design Change Package (DCP) 9700532, High Energy Line Break (HELB) Leak / Break Detection Modification and UFSAR revisions.
The DCP modified the Leak Detection System for the Reactor Water Cleanup (RWCU), Reactor Core Isolation Cooling (RCIC), and the Residual Heat Removal (RHR) systems to resolve a concern identified with the original Leak Detection calculations (PIF L1997-04896 and LER 1-97-031-00). The modifications generally consisted of temperature sensor relocation, addition of temperature monitoring functions, and addition of a high flow monitor for HELB.
UFSAR Sections 1.2.2.6.6, 1.7, 3.1.2.2.4, 3.1.2.4.1, 5.2.5.1, 5.2.5.1.2, 5.2.5.2, 5.2.5.4, 5.2.5.5.4, 5.2.5.6, 5.4.7.3.1, 7.3.2.2.3.9, 7.3.2.2.3.10, 7.3.2.2.3.13, 7.4.1.2.6, 7.6.2.2.4, 7.6.2.2.5, 7.6.2.2.6, 15.9.3.4, H.3, Table 5.2-8, Table 7.3-2, Figure 7.3-7, and Drawings M-155 and M-2097 are revised accordingly.

Design Change Package (DCP) 9700532 (Addendum 3), High Energy Line Break (HELB) Leak / Break Detection Modification, Supplemental Engineering Change Notices (ECNs) 001368E-02, and 001369E-02 and UFSAR revisions.
The DCP modified the Leak Detection System for the Reactor Water Cleanup (RWCU), Reactor Core Isolation Cooling (RCIC), and the Residual Heat Removal (RHR) systems to resolve a concern identified with the original Leak Detection calculations (PIF L1997-04896 and LER 1-97-031-00). The modifications generally consisted of temperature sensor relocation, addition of temperature monitoring functions, and addition of a high flow monitor for HELB. The setpoint used in the instrument loop is 550gpm +/-2.0gpm. UFSAR Sections 1.2.2.6.6, 1.7, 3.1.2.2.4, 3.1.2.4.1, 5.2.5.1, 5.2.5.1.2, 5.2.5.2, 5.2.5.4, 5.2.5.5.4, 5.2.5.6, 5.4.7.3.1, 7.3.2.2.3.9, 7.3.2.2.3.10, 7.3.2.2.3.13, 7.4.1.2.6, 7.6.2.2.4, 7.6.2.2.5, 7.6.2.2.6, 15.9.3.4, H.3, Table 5.2-8, Table 7.3-2, Figure 7.3-7, and Drawings M-155 and M-2097 are revised accordingly. No additional UFSAR changes are required based on Addendum #3.

Update to UFSAR Table 6.2-21 Sheet 14, Item 18
Note 18 of UFSAR Table 6.2-21 describes the TIP drive guide tube ball valve and shear valve isolation capabilities, and that the time period that the valves are opened is very limited. The note has a final statement that states "However, at the insistence of the NRC, these valves will be tested in accordance with the requirements of 10CFR50, Appendix J." This final statement is being changed to indicate that the TIP ball valves are tested in accordance with 10CFR50, Appendix J and that the TIP shear valves are tested as specified in Technical Specification 4.6.3.5, which verifies continuity of the explosive charge and batch sampling testing of the explosive squib charges, with replacement of the explosive squib before expiration of the shelf-life and operating-life.

UFSAR Drawings M-96 Sheets 1 and 2, and M-142 Sheets 1 and 2 Update
UFSAR drawings M-96 sheet 1 and 2 and M-142 sheet 1 are revised to reflect installed (as-built) conditions. Carbon steel piping is installed in portions of the system that were designed as stainless steel (and vice versa), and dissimilar welds (carbon to stainless) were not previously analyzed. A note was also added to drawings M-96 sheet s 1 and 2, and M-142 sheets 1 and 2 to reflect that SA-333 Grade 6 material may have been installed in the residual heat removal shutdown cooling lines during original construction. This has been evaluated as an acceptable alternate material per as-built drawing change request (DCR) 960156.

Revision to UFSAR subsections 3.8.4.1.2 and 10.3.6.2
UFSAR subsections 3.8.4.1.2 and 10.3.6.2 are revised to achieve consistency with original design drawings M-9 (General Arrangement Ground Floor Plan) and M-806, Sheet 2 (Turbine Cycle Feedwater Heater Drain Piping).

Installation of stem clamps on valves 1G33-F034 and 1G33-F035 per Design Change Package (DCP) 9700610
The DCP installed a stem clamp on valve 1G33-F034 to gag it closed to support an out-of-service (OOS) boundary and to allow an upgrade to the valve operator. The clamp was installed as Temporary Alteration (TALT) 1-0250-97.

Installation of stem clamp on valve 1G33-F035 per Design Change Package (DCP) 9700611
The DCP installed a stem clamp on valve 1G33-F035 to gag it closed to support an out-of-service (OOS) boundary and to allow an upgrade to the valve operator. The clamp was installed as Temporary Alteration (TALT) 1-0251-97.

Emergency Diesel Generator 0 Speed Sensor Replacement per Design Change Package (DCP) 9800002

The station's diesel generators have recently experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 0 emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch.

Emergency Diesel Generator 1A Speed Sensor Replacement per Design Change Package (DCP) 9800003

The station's diesel generators have recently experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 1A emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch. UFSAR Section 1.7, Electrical, Control and Instrumentation drawings, is accordingly revised per DCP 9800003.

Emergency Diesel Generator 1B Speed Sensor Replacement per Unit 1 Design Change Package (DCP) 9800004

The station's diesel generators have experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 1B emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch. UFSAR Section 1.7, Electrical, Control and Instrumentation drawings, is accordingly revised per DCP 9800004.

Containment Penetration General Design Criteria Inconsistency

UFSAR Sections 6.2 and 9.3 are revised to eliminate an inconsistency between containment penetration General Design Criteria (GDC) and its description in the UFSAR. For the compressed gas systems in subsection 9.3.1.3, the reference to the lines penetrating primary containment is being changed to clarify the station air system and drywell pneumatic system lines that penetrate primary containment are provided with containment isolation valves which meet the requirements as applicable of GDC 56 or 57 of Appendix A of 10CFR50, as described in section UFSAR 6.2. Subsection 6.2.4.2.2, the evaluation against GDC 56, is being expanded to include a description of the containment penetration line isolation for the service air and clean condensate systems.

Revision to UFSAR drawings per Design Change Package (DCP) 9800059 – Addition of Supports to Pipe Line 1HD37AA-1½" and 1HD37AB-1½.
This DCP added one new pipe support each on lines 1HD37AA-1½" and 1HD37AB-1½", which brings the pipe stress into conformance with Code allowables. The DCP also provided for as-built routing of the pipe and existing supports.
UFSAR Drawing M-61 Sheet 3 and Sheet 4 are revised to reflect the as-built line size from ¾" to 1½".

Emergency Diesel Generator 2A Speed Sensor Replacement per Design Change Package (DCP) 9800006
The station's diesel generators have recently experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 2A emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch.

UFSAR Change per Engineering Request (ER) 9707441
UFSAR drawing M-90 Sheet 2, Reactor Building Closed Cooling Water (RBCCW) System, is changed as a result of field walkdowns associated with the plant labeling effort. The drawing revision is a non-function change which reflects the relocation of an interconnection between the A and B reactor recirculation pump motor windings RBCCW outlet drain lines and the A and B reactor recirculation pump motor windings RBCCW outlet lines.

Unit 1 Division 1 Low Pressure Coolant Injection (LPCI) Pump Discharge Pressure Automatic Depressurization System (ADS) Permissive Setpoint Change per Design Change Package (DCP) 9700616;
Unit 1 Division 2 Low Pressure Coolant Injection (LPCI) Pump Discharge Pressure Automatic Depressurization System (ADS) Permissive Setpoint Change per Design Change Package (DCP) 9700617;
Unit 1 Low Pressure Core Spray (LPCS) Pump Discharge Pressure Automatic Depressurization System (ADS) Permissive Setpoint Change per Design Change Package (DCP) 9700618
During the System Functional Performance Review, it was determined that pump discharge ADS permissive setpoints did not account for head correction. The DCPs affect instruments 1E12-N016A, B, C, 1E12-N019A, B, C, 1E21-N001, and 1E21-N009. The DCPs do not physically change any instrumentation hardware, as the nominal calibration setpoints are changed to account for elevation differences between the instruments and the process points on the discharge lines.

Change to UFSAR Subsection 9.2.1.1.1.a.4
Engineering Request (ER) 9604121 identified that UFSAR Subsection 9.2.1.1.1.a.4 incorrectly states that system sizing is based upon a minimum 20 gpm flow of cooling water to the RHR pump seal coolers. Vendor Drawing (Spec J-2500) VPF- 2993-174-1 sheet 2 identifies that the shell side of the seal coolers (the CSCS-ECWS side of the exchanger) is designed for a flow of 9 gpm with a cooler water temperature of 80^{0}F. The maximum design temperature of the Ultimate Heat Sink (UHS) is 100^{0}F. Subsequent correspondence received from the seal cooler manufacturer provided a data sheet detailing that 12.5 gpm are required for a cooling water temperature of 100^{0}F (based upon 85% cleanliness). The change required for UFSAR Subsection 9.2.1.1.1.a.4 was identified and evaluated during the preparation of Design Change Packages (DCPs) 9800053 and 9800054. This change was not dependent upon installation of these DCPs.

Revision to UFSAR drawings per Design Change Package (DCP) 9700075 – Modify 16A/B High Pressure Heater Tube Side Relief Valves.
This DCP replaced the Unit 1 High Pressure Feedwater Heater tube side relief valves (1DV002A and 1DV0002B). These relief valves were replaced with new relief valves that meet the requirements of ASME Section VIII and are UV stamped. The existing inlet and outlet piping of the relief valves was modified to fit the new relief valves. The original valves were not UV stamped as required by ASME Section VIII.
UFSAR Drawing M-62 Sheet 1 is revised to reflect the new line numbers for the relief valve inlet piping, and to show the new pipe flanges at the relief valve inlets.

Revision to UFSAR drawings per Design Change Package (DCP) 9700078 – Modify all Unit 1 Low Pressure Feedwater Heater Tube Side Relief Valves.
This DCP replaced the Unit 1 Low Pressure Feedwater Heater tube side relief valves (1DV003A/B/C, 1DV0004A/BC, 1DV007A/B/C, 1DV009A/B/C and 1DV012A/B/C). These relief valves were replaced with new relief valves that meet the requirements of ASME Section VIII and are UV stamped. The existing inlet and outlet piping of the relief valves was modified to fit the new relief valves. The original valves were not UV stamped as required by ASME Section VIII.
UFSAR Drawing M-62 Sheet 2, Sheet 3, and Sheet 4 are revised to reflect the new line numbers for the relief valve inlet piping, and to show the new pipe flanges at the relief valve inlets.

Revision to UFSAR drawings M-91 Sheet 3 and M-137 Sheet 3
UFSAR drawings M-91 Sheet 3 and M-137 Sheet 3 are revised to switch line numbers and valve equipment part numbers to provide consistency in the numbering and

labeling of the drain lines and drain valves associated with the A and B heat exchangers of the Unit 1 and 2 residual heat removal (RHR) systems.

Revision to UFSAR Drawings M-Index Sheet 4 and M-19.
M-Index Sheet 4 (General Arrangement Index) and M-19 (General Arrangement Lake Screen House) are revised to reflect the as-built condition of the plant. Pumps and equipment being removed from drawing M-19 and M-Index Sheet 4 do not exist, and pumps that do exist in the plant are being added to these drawings.

Revision to UFSAR Subsection 2.4.8.4
The description of the blowdown waterline in subsection 2.4.8.4 of the UFSAR is revised to achieve consistency with the generalized waterline description of UFSAR subsection 10.4.5.2.

Revision to UFSAR Subsection 7.3.9.2.1
UFSAR Section 7.3.9.2.1 is revised to indicate that containment spray is not required to be initiated on recombiner operation. Containment spray initiation is based on containment pressure and/or combustible levels of hydrogen /oxygen concentrations, as opposed to recombiner operation.
The containment spray mode does not have to be initiated if the recombiners are required for service. Suppression chamber spray is required to be initiated prior to suppression chamber pressure reaching 8 psig. If suppression chamber pressure exceeds 8 psig, drywell spray is also initiated.

Information from FSAR Question 312.21 is transferred to UFSAR subsection 6.1.2, Organic Materials, and UFSAR Table 6.1-2, Organic Materials Within the Primary Containment, to bring forward applicable information from the FSAR into the UFSAR. All exposed metal surfaces inside containment are not prime coated with an inorganic zinc compound that has been fully qualified in accordance with ANSI standards. Some exposed metal surfaces inside containment are coated with coatings not qualified in accordance with ANSI standards N101.2, N101.4 and N512. These unqualified coatings have been previously identified and addressed in FSAR Question 312.21 and the NRC has issued an SER, NUREG-0519, Section 6.1.2, Organic Materials, approving the use of this unqualified coating.

Revision to UFSAR Tables 9.4-1 (Sheet 1) and 9.4-3 due to revised Filter Pressure Drop
In conjunction with a change to an alternate supply air filter for use in the control room and the auxiliary electrical equipment room (AEER) HVAC systems, the filter pressure drop, clean (inches water) parameter as listed in UFSAR Tables 9.4-1 (Sheet 1) and

9.4-3 is increased from "0.35" to " < 0.8" inches water column for the control room and AEER HVAC systems (VC and VE, respectively). The increase in the rated pressure drop clean value was made in association with an upgrade to safety related rating for the supply air filter for use in the control room and AEER HVAC systems.

Update to UFSAR Table 6.2-28 (Sheet 5) reflect Unit 1 Main Steam Isolation Valve (MSIV) Leakage Control System (LCS) Abandonment
Design Change Package (DCP) 9500167 cut and capped the MSIV-LCS piping at the Unit 1 main steam lines during Unit 1 refuel outage L1R07. This work was associated with the approval of licensing amendment No. 112 to Unit 1 license NPF-11. Valves 1E32-F001A, E, J, and N are no longer connected to the primary containment/reactor coolant pressure boundary, and are accordingly deleted from the list of Unit 1 primary containment isolation valves. UFSAR Table 6.2-28 (Sheet 5) and Administrative Technical Requirements (ATR) page 3/4 6-11 are revised.

Revision to UFSAR drawing per Design Change Package (DCP) 9700368 – Install Isolation Valve between FC Demineralizers and SA System.
The DCP relocated the existing orifice 0FE-FC001 from downstream of check valve 0FC035 to downstream of check valve 0SA048. Existing check valve 0FC035 and isolation valve 0FC034 were relocated such that isolation valve 0FC034 is downstream of check valve 0FC035. Valve 0FC034 was replaced with a new ball valve and an additional isolation valve (0FC038) was installed downstream of 0FC034. A drip leg, consisting of a drip isolation valve (0FC039) and a new line 1FCC1A-3/4" was added between 0FC034 and 0FC038. A pressure indicator (0PI-FC009), a shut-off valve (0FC039) and an instrument line 1FCC2A-1/2" were added to the drip leg.
UFSAR Drawing M-98 Sheet 2 was revised to reflect the changes.

Revision to UFSAR Subsection 8.3.1.1.3 per Design Change Package 9800039
An evaluation of the Reactor Protection System (RPS) Electrical Protection Assembly (EPA) overvoltage, undervoltage, and underfrequency setpoints was performed in calculation L-001678. This calculation recommends a change to the calibration settings of the RPS EPA overvoltage, undervoltage, and underfrequency trips to account for instrument inaccuracies including drift. DCP 9800039 doesn't physically change hardware, as it adjusts the desired calibration setting to account for instrument inaccuracies including drift. The revised calibration settings insure compliance with the Technical Specifications, and change neither the Technical Specification setpoints nor how they were established. The proposed change insures that the setpoint requirement is maintained in accordance with the design and licensing basis currently specified in the UFSAR and the Technical Specifications.

Revised Reactor Water Level (RWL) Feedwater control selection circuitry per Design Change Package (DCP) 9600197 and Modification Approval Letter – Addendum No. 1 and UFSAR revisions

The DCP 9600197 replaced two-position selector switch 1C34A-S001 in Main Control Board panel 1H13-P603 with a three-position selector switch and installed required wiring connections to provide one-out-of-three channel selection capability for RWL monitoring circuits. The DCP also removed local and remote channel selected and channel out of service indication and associated pushbutton switches, indicating lights, and fuses.

The changes identified in the addendum did not affect the conclusion of the original safety evaluation; however, a new safety evaluation was performed to identify additional UFSAR changes. UFSAR subsection 7.7.4.2, Figure 7.7-5 Sheet 1 and drawing 1E-1-4603AP (revised via ECN 000941E) are accordingly revised.

Revision to UFSAR Sections 4.6.1, 7.2.2, and 7.7.6

The changes implement UFSAR improvements in response to Engineering Requests (ERs) 9701543, 9702560, 9703059, and 9704829. The revisions to UFSAR Subsections 4.6.1.1.1.1.1.c.3 (Safety Design Bases, CRD Drive Mechanical System), 7.2.2.4.10 (CRD Low Charging Pressure), and 7.7.6.2.2.b ((LPRM) Physical Arrangement) are editorial (i.e., typographical error corrections, clarifying information). The revision to UFSAR Subsection 7.7.6.4.2 for the Traversing Incore Probe (TIP) Physical Arrangement, requires a change to the description of the X-Y recorder used to record TIP data. The change also clarifies the valve system described in the last paragraph referring to the physical arrangement of the TIP system.

Revision to UFSAR Subsection 9.2.1.1.1.a.11

UFSAR Subsection 9.2.1.1.1.a.11 is revised to correct an ambiguous designation of the flow rate and the pump supplying it for the containment fill (flooding) function provided by each unit's fuel pool emergency makeup system. The flowrate is revised to being a nominal value of 300 gpm, and the supplying pump is specified as being the unit's Division 2 fuel pool emergency makeup pump, 1(2)FC03PB.

As-Built Drawing Change Request Tip Purge Valve Assembly 1C51-J009

Drawing M-66 Sheet 1, Unit 1 Drywell Pneumatic System, was revised to reflect the as-built condition of the traversing incore probe (TIP) purge valve assembly 1C51-J009. The valve assembly was previously modified to reflect changes shown in General Electric (GE) Field Disposition Instruction (FDI) dated 2/11/82. The FDI added a new purge air control panel, modified TIP purge equipment, and index mechanisms. The upgrade to the purge system protects the TIP detectors and other components from dependence upon the quality of installation.

UFSAR Change per Engineering Request (ER) 9800832
UFSAR drawing M-63 Sheet 4, Circulating Water System, is revised per Engineering Request 9800832 to delete a redundant detail from the drawing, reflecting the proper design specifications, in order to assure that future repairs are made with the correct materials.

UFSAR Change per Engineering Request (ER) 9707835
UFSAR drawing M-69 sheet 2, Service Water, is being revised per ER 9707835 to reflect the as-built condition of the plant. Correction of the valve omission will provide for better control of the valves.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability of obtaining drywell and suppression pool atmosphere iodine and particulate samples for radionuclide analysis. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was made in anticipation that the information would be used by the core damage assessment methodology later approved for use by the NRC. The approved methodology does not require that these samples be obtained and analyzed. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability of obtaining a stripped gas sample from reactor coolant for radionuclide analysis. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was made in anticipation that the information would be used by the core damage assessment methodology later approved for use by the NRC. The approved methodology does not require that this sample be obtained and analyzed. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a dissolved oxygen analysis of reactor coolant. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was intended to provide information on the corrosion potential of materials in contact with the reactor coolant under post accident conditions. The concentration level

of concern for dissolved oxygen in reactor coolant is 0.1 parts per million (PPM) or greater. Under post accident conditions, the reactor coolant dissolved oxygen concentration will be greater than 0.1 PPM since there is no capability to remove dissolved oxygen from the coolant under shutdown conditions and the sources of water injected into the reactor system for makeup contain dissolved oxygen concentrations in excess of 4 PPM. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a dissolved hydrogen analysis of reactor coolant. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was intended to provide information on the possibility of forming a gaseous bubble in the reactor system that may prevent or reduce core cooling as well as to provide some information on the degree of core damage. The design of the LaSalle reactor systems precludes the possibility of forming gaseous bubbles under post-accident conditions that could inhibit core cooling. The core damage assessment methodology approved by the NRC does not require reactor coolant dissolved hydrogen analysis for the calculation. A review of the site's emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a conductivity analysis of reactor coolant. This commitment was not required by NUREG-0737, Item II.B.3 or Regulatory Guide 1.97. The capability was intended to provide information on the corrosion potential of materials in contact with the reactor coolant under post-accident conditions. A review of the site's emergency operating procedures and generating station emergency plan shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a pH analysis of reactor coolant. This commitment was not required by NUREG-0737, Item II.B.3, but was described in Regulatory Guide 1.97. The capability was intended to provide information to facilitate the assessment of the potential inventory of activity available that could be released from the plant under post-accident conditions. Later NRC guidance does not require that a pH determination

be made (NUREG-1228 and NUGEG-1465). A review of the site's emergency operating procedures and generating station emergency plan shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability to perform a chloride analysis of reactor coolant. This commitment was made to meet NUREG-0737 and Regulatory Guide 1.97 requirements and was intended to provide information on the corrosion potential of materials in contact with reactor coolant under post-accident conditions. The primary method for performing a reactor coolant chloride analysis is an in-line analyzer. This analyzer will be retired and a laboratory method will be used instead to generate the reactor coolant chloride concentration data. UFSAR Section 11.5.5 is revised to change this commitment within the Post Accident Sampling program description.

UFSAR Revision to Section 11.5
A commitment was made as part of a licensing condition for operation to provide for the post-accident capability of obtaining drywell equipment and floor drain sump samples for radionuclide and chemical analysis. This commitment was not required by NUREG-0737, Item II.B.3 but was described in Regulatory Guide 1.97. This commitment was made to facilitate core damage assessment calculations. Sampling containment sump is a PWR plant issue and does not apply to LaSalle since coolant leakage is collected in the suppression pool under post-accident loss of coolant conditions. A review of the site's core damage assessment procedure, emergency operating procedures and generating station emergency plan also shows that this information is not required. UFSAR Section 11.5.5 is revised to remove this capability from the Post Accident Sampling program description.

UFSAR Revision reflect Cable Qualification to IEEE 383-1974
UFSAR subsections 8.3.1.4.2.2, 9.5.1.1.2, and H.1.1.1 presently imply that all cables at LaSalle, without exception, are qualified to IEEE 383-1974. These UFSAR subsections are revised to clarify the requirements for using cables that are qualified to IEEE 383-1974. Cables which do not interact with division or division associated cables, that are not routed in cable trays, that are routed in dedicated enclosed raceways and that present acceptable combustible loading (e.g., lighting and communications) do not require IEEE 383-1974 qualification.

Revision to UFSAR drawings per Design Change Request (DCR) 980523.
The UFSAR drawings for the Instrument Air (IA) and Service Air (SA) Systems are revised to reflect the as-built configuration of the system. The as-built changes are

implemented to update the drawings to resolve Operator Work Around (OWA) #224 and various PIFs
UFSAR Drawings M-82 Sheets 1, 2, 3, 4 and 6, M-92 Sheet 1 and M-56 Sheet 1 are revised to reflect the as-built configuration of the IA/SA system.

Revision to UFSAR Subsection 4.3.2.5.1.2
The current description in UFSAR 4.3.2.5.1.2 for control rod withdrawal sequences in the rod worth minimizer (RWM) power range, first paragraph, is incorrect per GE design document NEDO – 21231, Banked Position Withdrawal Sequence, (BPWS), and contradicts the second paragraph of the section. UFSAR Subsection 4.3.2.5.1.2 is revised to reflect actual BPWS rules.

Installation of Temporary Plug in Service Water line per Design Change Package (DCP) 9800047
The DCP installed a temporary pipe plug in service water backflush line 1WS05A-6" just before it enters 12" drain header 0WS06A. This was done per Temporary Alteration (TALT) 1-0017-98 to allow the piping downstream of valves 1WS013A/B to be replaced. Following piping replacement, the plug was removed and the piping welded.

UFSAR Revision to Incorporate Previously Approved Technical Specification revisions associated with the Main Steam Isolation Valve (MSIV) Limit Switch Setpoint Values
The original evaluation associated with the licensing amendment did not identify all of the required UFSAR changes. These UFSAR changes will resolve discrepancies between the current Technical Specifications and the UFSAR, as well as discrepancies within the UFSAR (e.g., sections that incorporated the change and those sections that were missed).
The applicable sections of the UFSAR are revised to reflect the previously approved MSIV limit switch setpoint values (nominal, allowable and analytical) currently identified in the Technical Specifications. At the time the Technical Specifications were revised not all applicable portions of the UFSAR affected by the change were identified and revised to incorporate the revised Technical Specification values.
The current Technical Specification scram setpoints are less than or equal to 8% closure trip and less than or equal to 12% closure allowable. The basis for these values is the 85% analytical value based on the General Electric (G. E.) reanalysis of the MSIV closure transient position scram. The affected UFSAR sections and subsections consist of 5.4.5.2, 5.4.5.4, 7.2.2.4.6, 7.A.2.1.2, 15.0.8; 15.0.9 (new), 15.1.3.2, 15.1.3.3, 15.1.5, 15.2.4.1, 15.2.4.2, 15.2.4.3 and 15.2.10; Tables 7.2-1 and 7.3-4; Figure 7.2-7; and Table of Contents page 15.0-I.

Administrative Technical Requirements (ATR) Amendment 13

The ATRs were amended to add a requirement for functionality of the main steam isolation valve (MSIV) alternate leakage treatment (ALT) paths approved by License Amendments 112 and 97 for LaSalle Units 1 and 2, respectively. It additionally involves required actions when one or both MSIV ALT paths are not functional when in Operational Conditions 1, 2, and 3. The ATR amendment assures that the MSIV ALT paths are maintained reliable as committed to by the license amendment submittals.

Update to UFSAR Table 9.4-15
UFSAR Table 9.4-15, Diesel-Generator Facilities Ventilation System Equipment Parameters, is revised to specify the filter pressure drop for a dirty filter is 0.40 inches water in lieu of 0.35 inches water for ventilation supply filters 0VD01F, 1VD01F, 1VD02F, 2VD01F, and 2VD02F.
This proposed change reflects Sargent & Lundy (S&L) Design Criteria DC-VD-01-LS, dated 12/21/78, and Design Calculation VD-1C, dated 6/6/78, which specify the dirty filter pressure drop as being 0.40 inches of water.

Placement of freeze seals on the Turbine Building Closed Cooling Water (TBCCW) lines to the Unit 2 station air compressor
Freeze seals were placed on lines 2WT20A-4 and 2WT21A-4 to the Unit 2 station air compressor per work requests 950059371-02 and 960033303-02, respectively, in support of repairs to boundary valves 2WT106 and 2WT107. The valves provide cooling water to and from the station air compressor while Unit 2 TBCCW system remains in operation.

UFSAR revisions per Design Change Package (DCP) 9800044, Modification of the Control Room Toilet Exhaust Fan Ductwork.
This DCP changed the existing configuration for the Main Control Room (MCR) toilet exhaust air system from a direct exhaust that vents to the Turbine Building to a recirculation system with a filter that returns air to the toilet area. The current arrangement of VC system MCR toilet exhaust air ductwork interfaces with the Turbine Building which could allow steam to enter the MCR and affect its habitability during a main steam line break in the Turbine Building.
The existing wall grille in the Turbine Building and fire damper 0VC39Y was removed and discarded and the duct penetration opening filled with concrete grout. Duct sections were cut, removed and end caps were installed on the duct that was abandoned in place. The ducting from the MCR toilet exhaust fan (0VC06C) was rerouted above the toilet room drop ceiling to reenter the toilet room and terminate in a charcoal filter assembly. This DCP eliminated the interface between the MCR and the Turbine Building main floor.
UFSAR Sections 6.4.2.3, 6.5.1.1.2.c, 9.4.1.1.1.1.g, and 9.4.1.1.2.b are revised to delete the reference to providing makeup air for toilet exhaust. Drawing M-1443 Sheet 2 is revised to reflect the changes to the system.

Upgrade of Core Standby Cooling System Bypass Line and Valve 0E12-F300
The safety classification of the 54" Core Standby Cooling System - Equipment Cooling Water System (CSCS - ECWS) screen bypass supply pipe line 0RH01AA and valve (0E12-F300) to the service water intake tunnel was upgraded to "Safety Related". The 54-inch bypass line assures access to a continuous supply of water to the service water intake tunnel located in the lower level of the lake screen house, to cool various safety related equipment and equipment important to safety. The CSCS-ECWS also provides a source of emergency makeup water for fuel pool cooling and also provides containment flooding water for post-accident recovery. The pipe line and valve were originally classified as Pipe Class D, Non-Safety Related, Non-Seismic, and were recently upgraded to Class D, Seismic. Upon completion of the drawing change request (DCR) 960135 upgrade process, the subject pipe line and valve are classified as Pipe Class D, Safety Related, Seismic Category I. UFSAR Table 3.2-1 and drawing M-87 Sheet 1 are revised.

Revision to UFSAR Subsection 9.5.1.5.3 and Table 13.1-1
UFSAR Subsection 9.5.1.5.3 is revised to allow a qualified individual (other than a Field Supervisor) to assume the duties of the Fire Brigade Leader.
UFSAR Table 13.1-1 is revised to allow specific Shift Manager of Unit Supervisor Administrative duties to be performed by a qualified individual with either an RO or SRO license if they meet minimum ANSI N18.1-1971 qualifications for supervisors requiring an NRC license.

Modification to Unit 1 Containment Leak Test Channels per Design Change Package (DCP) 9800041
The DCP removed eighteen leak test plugs for the leak test system around the Unit 1 safety relief valve (SRV) pipe support embedment plates at the containment wall above elevation 700' -0" in the Unit 1 suppression pool. The DCP also clarifies that all other test plugs in the suppression pool and the containment drywell may be permanently left in place. The leak-test channels were originally installed over containment liner welds so that these welds could be pressure tested to verify leak-tightness. Threaded plugs were installed in openings in these leak-test channels to facilitate this pressure testing. It was the intent of the original design that these plugs be removed after these local leakage tests were complete so that during future Containment Integrated Leak Rate Tests (CILRT), the liner welds would see the test pressures. The leak-test channels and plugs were not designed to act as the containment pressure boundary. Licensee Event Report (LER) 97-030 documents that the plugs were not removed as originally intended after the initial local leak rate tests. UFSAR Subsections 6.2.1.1.2 and 6.2.6.1 are revised.

Main Control Room (MCR), Auxiliary Electric Equipment Room (AEER), and Technical Support Center (TSC) penetration seals per Design Change Package (DCP) 9700594 (Addendum #3) and Supplemental Engineering Change Notice (ECN) 001416S-01. The ECN and DCP provide alternate generic penetration sealing material and methods for the purpose of reducing air leakage from the outer envelopes of the MCR and AEER to adjacent areas. The supplemental ECN was issued to perform the same type of penetration sealing work in the TSC, the State of Illinois Rad Processor Equipment Room, and the two access airlocks to the TSC to reduce air leakage from the rooms to adjacent areas and maintain the required room pressure.
No revisions to the UFSAR are required as a result of this supplemental ECN to DCP9700594.

Revision to UFSAR Subsection 6.4.1
The first sentence of the third paragraph of UFSAR Subsection 6.4.1.g is revised to reflect the availability of self-contained breathing air systems (air packs) dedicated for use by the fire brigade.

Revision to UFSAR Drawing M-80 Sheet 2
Drawing M-80 Sheet 2, Turbine Building Equipment Drains incorrectly showed the following: Drain lines 1ES47BA - 2" and 1ES47BB - 2" connected to drain header 1TEC4A - 8", they are actually connected to drain header 1TEC5A - 8"; Drain line 1TD01B - 2" connected to drain header 1TEC5A - 8", whereas it is connected to drain header 1TEC6A - 8"; and, the drawing did not properly reflect the sheet number on the drawing jump arrow on lines 1TD01B - 2" and 1TD02C - 2" by showing M-65 instead of M-65-1 as should have been the case. The drawing was revised to reflect actual field conditions.

Revision to UFSAR Appendix B to reflect Updating of the status of the Discussion of Compliance with Regulatory Guide (RG) 1.100, Revision 1
The Discussion of the Regulatory Guide (R.G.) in FSAR Appendix B was last changed in 1977, when LaSalle was beginning evaluations for equipment originally qualified to IEEE 344 - 1971 to show qualification to IEEE 344-1975. Although FSAR section 3.10 was updated, Appendix B concerning R.G. 1.100, Rev. 1, was not. This UFSAR change brings forward and updates LaSalle conformance to R.G. 1.100, Revision 1, per section 3.10 of the UFSAR and adds the requirement to qualify non like-for-like replacements or new components to the 1975 standard and R.B. 1.100, Revision 1. This puts the qualification requirements in the appropriate place rather than in only specific cases, such as indicated in Tables 7.1-2 through 7.1-8. This change makes the requirements more clear in Section 3.10, which is referenced by the Tables.

LTS-400-27 Revision 0, Standby Gas Treatment Suction Line Isolation Damper 1(2)VG023 Local Leak Rate Test

Design change packages 9700402 and 9700403 installed valves 1VG023 and 2VG023 in the standby gas treatment system primary containment suction piping of Unit 1 and 2, respectively. The valves provide a method of isolating the standby gas treatment system from the primary containment vent/purge system during the purging/venting process. The procedure verifies valve seat integrity and the capability to maintain system isolation between the standby gas treatment and containment ventilation systems during accident conditions.

Revision to UFSAR Subsection 9.4.5.3.e
UFSAR Subsection 9.4.5.3 and Table 9.4-20 were revised to clarify ECCS area temperature indication on the main control board. This package supersedes a previously proposed change to Subsection 9.4.5.3.e. This change deletes reference to fan shutdown.

UFSAR change per Engineering Request (ER) 9703090
UFSAR Drawings M-69 Sheet 1, Service Water, and M-125 Sheet 1, Service Water, are revised per Engineering Request (ER) 9703090 to reflect as-built conditions of the plant.

Revision to UFSAR Subsection 2.4.13.2.2.3.2
UFSAR Subsection 2.4.13.2.2.3.2 is revised to specify that after completion of the ground water monitoring program specified in Section 6.3.3 of NUREG-0486 "Final Environmental Statement" (November 1978), the number of observation wells monitored and the frequency of monitoring will be performed as described in the plant surveillance program.

Resizing RHR Service Water Restricting Flow Orifice 1E12-D304B per Design Change Package 9800054
The diameter of restricting orifice plate 1E12-D304B was enlarged to allow for increased flow test conditions, assuring that the design basis of 7400 gpm can be realized during accident situations (low lake level of 690') when taking instrument uncertainty and pump/system degradation into account. The associated change to UFSAR Subsection 9.2.1.1.1.a.4 was previously made per Engineering Request (ER) 9604121.

Resizing RHR Service Water Restricting Flow Orifice 1E12-D304B per Design Change Package 9800053
The diameter of restricting orifice plate 1E12-D304A was enlarged to allow for increased flow test conditions, assuring that the design basis of 7400 gpm can be realized during accident situations (low lake level of 690') when taking instrument uncertainty and pump/system degradation into account. The associated change to

UFSAR Subsection 9.2.1.1.1.a.4 was previously made per Engineering Request (ER) 9604121.

Change to UFSAR Subsections 1.2.3.1.3 and 10.4.2.2 to Reflect Engineering Request (ER) 9704131
UFSAR Subsections 1.2.3.1.3 and 10.4.2.2 are revised to allow operation of the mechanical vacuum pump 1(2)OG02P following reactor shutdown in accordance with LaSalle General Procedure LGP-2-1, *Normal Unit Shutdown*. This is to allow main condenser vacuum to be maintained as long as possible following reactor shutdown to minimize condensate polisher resin breakdown caused by the combination of high dissolved oxygen (when vacuum is lost) and high condensate water temperature (right after shutdown).

UFSAR Table 6.2-21 Revision to reflect As-built Conditions
UFSAR Table 6.2-21 Sheet 6A is revised to reflect As-built Conditions for containment penetration I-8D. The restricting orifice referenced by the note does not exist in the plant. The note states that the applicable instrument lines are provided with flow restricting orifices, manual isolation valves, and excess flow check valves. The table is revised to match plant configuration, as the flow restricting orifice does not exist. Additionally, the valve number is corrected from 1&2VO061 to 1&2VQ061.

Operability Evaluation 98014 for Switchgear Heat Removal System Gravity Dampers
In response to long standing generic problems with gravity damper shutter performance at LaSalle, dampers 1(2)VX04Y, 09Y, 11Y, 17Y, 51Y, 53Y, and 55Y were evaluated to determine their operability. The dampers were found to be operable to perform their switchgear heat removal function.

Procedure LLP-98-006 Revision 0, ECCS Suction Strainer Installation Sequence
The procedure was written to control critical evolutions in support of the ECCS and RCIC suction strainer replacement in the Unit 2 suppression pool, with the unit in Mode 5 and the vessel defueled. This procedure applied to strainers in the following systems: 'A' RHR, 'B' RHR, 'C' RHR, LPCS, HPCS, and RCIC. Design issues are addressed per the applicable design change packages (DCPs).

UFSAR Revision per Temporary Alteration (TALT) 1-0028-98
Reactor Water Cleanup (RWCU) may be required by Technical Specification 3/4.4.9.2 action statements to be OPERABLE as an alternate shutdown cooling system. Modifications to the leak detection isolation circuitry for the Unit 1 inboard and outboard RWCU isolation valves are to be installed per Design Change Package (DCP)

9700532. These valves must remain open to maintain the shutdown cooling function. This TALT assists in the implementation of DCP 9700532.
This temporary alteration prevents the RWCU inboard and outboard isolation valves 1G33-F001 and 1G33-F004 from automatically isolating as a result of leak detection isolation signals from high differential flow, room high differential temperature, or loss of power to the leak detection heat exchanger room temperature/differential temperature logic circuit while this TALT was in place. UFSAR Subsection 7.6.2.2.6 is accordingly revised to discuss the continuous bypassing of the Reactor Water Cleanup System Leak Detection isolation trip functions during operational conditions when a unit is in cold shutdown, refuel, or defueled.
UFSAR Vol. XI Drawings M-155 Sheet 2, Leak Detection, and M-2097 Sheet 2, Reactor Water Cleanup System are temporarily marked to indicate the temporary alteration being in place defeating the leak detection isolations. These drawings are to be restored following removal of the temporary alteration.

UFSAR Revision Associated with Station Blackout Rule
The NRC issued a Supplemental Safety Evaluation of the LaSalle County Station Response to the Station Blackout Rule (TAC Nos. M98864 and M98865) dated December 4, 1997. This was in response to a clarification submitted by LaSalle Station to the NRC, dated May 28, 1997. UFSAR Sections 8.3, 15.9, and H.4 are being revised to reflect the NRC accepted method for calculating battery capacity utilizing the minimum 5% remaining margin, and adjustment of the aging factor, if necessary, to maintain the margin.

UFSAR Revision to Reflect Operating Experience (OPEX) Program
UFSAR Appendix L Section L.12 is revised to reflect the company organization and philosophy changes resulted in revisions to site procedures previously referenced in FSAR Appendix L. Changes were also incorporated in LaSalle Administrative Procedure LAP-850-6 Revision 9, Processing of Operating Experience (OPEX) Information and Changes to Regulatory Rules. Use of this procedure serves to ensure that OPEX information is appropriately reviewed and disseminated as required by NUREG-0737.

VC/VE System Ductwork Insulation per Design Change Package (DCP) 9800087.
This design change provided generic details for use as required to insulate portions of the VC/VE ductwork systems with Scrim Wrap type as an alternate to rigid fiber board insulation. The VC/VE system ductwork insulation was removed by various DCPs to facilitate modifications, repair/replacement of damaged sections of ductwork, and to seal leaking ductwork joints.

Increase Unit 1 Flow Control Valve Upshift Position Setpoint for Reactor Recirculation Pumps, DCP 9700512
The DCP revised the valve maximum open position setpoint (or minimum position) of the reactor recirculation (RR) flow control valves (FCV) 1B33-F060A and 1B33-F060B associated with RR pump start. This change increases the valve position when the RR pumps are transferred from low to high speed to reduce the possibility of FCV binding.

Removal of springs from check valves per Engineering Request (ER) 9707782.
The springs from the Division 1 and 2 Diesel Generator Starting Air Compressor discharge check valves 0DG023A/B (Div. 2), 1DG049A/B (Div 1) and 2DG049A/B (Div. 1) were removed. The springs were removed to reduce the impacting of the check valve disk on the backstop and valve seat (valve chattering) during compressor operation. Vendor and Engineering evaluations indicated that if the valve orientation was such that it was either installed in a horizontal line with its disk axis in the vertical plane (+/-20 degrees from the vertical) or installed in a vertical line with the flow upward, the disk would reseat under its own weight without assistance from the spring. All six valves were field verified as installed in horizontal lines therefore, meeting the stated spring criteria for spring removal.
Revision to UFSAR subsections 3.8.4.1.2 and 10.3.6.2
UFSAR subsections 3.8.4.1.2 and 10.3.6.2 are revised to achieve consistency with original design drawings M-9 (General Arrangement Ground Floor Plan) and M-806, Sheet 2 (Turbine Cycle Feedwater Heater Drain Piping).

UFSAR Change Associated with Procedure LTS-200-9, Revision 5, RHR Pump Seal Cooler Service Water Flowrate Test
UFSAR Subsection 9.2.1.2 is revised since the procedure may leave the seal cooler outlet valves throttled if necessary to remain within design flows, as opposed to the seal cooler outlet valves being fully open.
UFSAR Subsection 9.2.1.5 is revised to reflect that there are no flow element installed in the discharge path of the residual heat removal (RHR) seal cooler outlet lines and Low Pressure Core Spray (LPCS) motor cooler lines.
UFSAR drawings M-87 sheets 1 and 2, and M-134 sheets 1 and 2 are to be revised since the procedure proposes to leave these valves throttled if necessary to remain within the vendor stated maximum flow limit, as opposed to the locked open position.

Coating of Unit 1 Division 2 Pressure Transmitter Instrumentation Circuit Terminations per Design Change Package (DCP) 9800093
The DCP applied Patel Engineers Conformal Coating (PECC) on the terminations associated with pressure transmitters 1B21-N026CA, 1B21-N026BA, 1B21-N051B, 1B21-N405B, 1B21-N407D, 1B21-N408B, and 1B21-N407B. Re-analysis of the reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) high energy line break (HELB) concluded that the humidity in Room 19 (environmental zone H4A) may

increase from 95% to 100%. The increase in the accident humidity parameter results in a potential increase in the leakage at the pressure transmitter terminations. The DCP applied the coating as a means to reduce the leakage to an acceptable value.

Revision to UFSAR Drawing M-83 Sheet 1 per Drawing Change Request (DCR) 980515.
The DCR documents two existing (as-built) configurations of piping and pipe fittings on the 1DG01S Standby Diesel Generator Starting Air Compressor Skid. The first change required is to show the field verified configuration of ½" diameter piping of the vendor furnished drain line from the 1DG03MA Moisture Separator in lieu of ¾" diameter. The second configuration change shows the material grade of the approximately 4-inch long pipe spool of 1-1/2" piping between valves 1DG049A(B) and 1DG050A(B) as carbon steel, ASTM A-106 Grade B in lieu of Grade C.
UFSAR Drawing M-83 Sheet 1 is revised accordingly.

Technical Support Center (TSC) Emergency Filter Unit Fan 0VS11C Shaft Seal per Design Change Package (DCP 9700594 (Addendum #4) and Engineering Change Notice (ECN) 001486H.
This DCP provided details for fabricating and installing the fan shaft seal for the TSC Emergency Filter Unit Fan 0VS11C which minimizes unfiltered in-leakage to the TSC HVAC system and maximizes radiation dose protection of the occupants inside the TSC upon loss of coolant accident (LOCA). The TSC HVAC system is designed to provide a habitable environment for emergency personnel during post-accident plant operations by providing positive pressure in the TSC with respect to surrounding areas to preclude infiltration of potentially contaminated air. Unfiltered in-leakage air calculation (L-001069, Rev. 0) determined that the total system in-leakage was approximately 155cfm, 88cfm of which were due to leakage around the shaft seal. Installation of the new fan shaft seal reduced the shaft seal leakage to approximately 27cfm and the total system in-leakage to 92cfm.

Modification to Unit 1 Reactor Building Trackway Doors 19 and 20 per Design Change Packages (DCPs) 9400368 and 9400369
Reactor Building Trackway Doors 19 and 20 serve as a passive barrier between the outside and the Reactor Building, and part of Secondary Containment. Due to a history of maintenance problems, the doors were modified by replacing the damaged embedded gasket of each door with a new gasket having a slightly revised detail, which permits simpler gasket replacement for future maintenance, and, replacing the previous gear/chain pin/knife plate drive mechanism with a hydraulic drive system. DCP 9400368 modified door 19, and DCP 9400369 modified door 20.

Revision to UFSAR drawings per Design Change Package (DCP) 9800078 – Reinstate 11 and 12 Feedwater Heater Normal Drain and Emergency Spill Valve Alarms.

This DCP reinstated the normal drain valve closed and emergency spill valve open alarms for Feedwater Heaters 11 and 12, and removed the emergency spill valve level solenoid valves, associated stop valves and level switches, which were previously abandoned in place. The spill and drain valves for the 11 and 12 heaters were modified under DCP 9700287, permitting throttling capability to maintain heater level. This design change (9800078) restored the control room annunicators that were previously removed by modification M01-1-89-014.
UFSAR Drawings M-61 Sheets 3 and 4 are revised to show the deletion of the solenoid valves.

UFSAR Update to reflect as-built Tygon Tubing Diesel Generator Drain Lines
3/4" drain lines are connected to the air box of each diesel generator. The air box is a part of each generator's skid package. The installed 1" tygon tubing is mechanically connected to the 3/4" drain pipe off of the air box of each diesel engine. The other end of the tygon tube rests in the floor drain funnel opening. The connection provides a drain path for the accumulation of liquids from the engine air box. Drawing M-83 Sheets 1, 2, and 3 are revised per as-built Drawing Change Request (DCR) 980304.

LaSalle Special Test Procedure LST-97-546 Revision 0, EHC On-Line System Calibration and Data Gathering
The procedure sets forth instructions for measuring and recording acceleration data of the Electro-Hydraulic Control (EHC) system during turbine acceleration. It also provides instructions for fine tuning the EHC power supplies, the speed signal from the frequency-to-voltage converters and the speed error signal form the low value gates when the generator is synchronized to the power grid.

Modification to the Curb Angle of roll-up doors D-503 and D-505 per Design Change Package (DCP) 9800105
The removable curbing angle for Diesel Generator Rooms (2A and 2B) roll-up doors D-503 and D-505 did not match the design drawing and it was not able to be installed to match the design drawing. The DCP relocated the curb angle further from the 2A and 2B Diesel room roll-up doors to provide clearance for the door lip. The side portion of the curb angle was extended further from the track to permit easier installation.

Main Control Room (MCR) and Auxiliary Electric Equipment Room (AEER) Penetration Seals per Design Change Package (DCP) 9700594 (Addendum #5) and Engineering Change Notice (ECN) 001487S.
The original ECN (001416S) and DCP provided alternate generic penetration sealing material and methods for the purpose of reducing air leakage from the outer envelopes of the MCR and AEER to adjacent areas. The losses were due to cracks in the floor, ceiling, walls and penetrations through walls. This ECN (001487S) enhanced the

double doors between the AEER and the Unit 1 and Unit 2 Cable Spreading Rooms (Doors 262 and 265) and the Unit 2 Division 2 Switchgear Room (Doors 259 and 266). The ECN installed a solid, stainless steel threshold and provided sealing details for around the head, side jambs, and sill and at the astragal of each door. The doorknobs were changed to lever type and heavy-duty hydraulic door closers were installed. This safety evaluation applies only to the portion of work covered in the subject ECN (001487S).
It was determined that no UFSAR revisions were required as a result of the changes.

Correction of discrepancies in UFSAR Subsection 10.4.7.2
The capacities of the Turbine Driven Reactor Feed Pumps (TDRFPs) and the Motor Driven Reactor Feed Pumps (TDRFPs) in UFSAR Subsection 10.4.7.2 have been determined to be incorrect. The discussion in the UFSAR is revised to reflect the actual operating capacities of the TDRFPs and the MDRFPs.
The revision corrects a discrepancy between the stated and actual capacities of the above pumps, which was discovered during the 1997 System Functional Performance Review (SFPR). The change identifies the design target capacity of 68% for the TDRFPs and deletes the incorrect design target capacity of 40% for the MDRFPs. Additionally, the actual operational capability of 57% to 60% for the TDRFPs and 30% to 32% for the MDRFPs is listed to eliminate the inference that the unit is operated at 100% with a TDRFP and the MDRFP.

Coating of Unit 1 Division 1 Pressure Transmitter Instrumentation Circuit Terminations per Design Change Package (DCP) 9800092
The DCP applied Patel Engineers Conformal Coating (PECC) on the terminations associated with pressure transmitters 1E31-N015, 1E31-N035, 1B21-N026AA, 1B21-N051A, 1B21-N026E, 1B21-N407A, 1B21-N407C, 1B21-N405A, and 1B21-N408A. Re-analysis of the reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) high energy line break (HELB) concluded that the humidity in Room 19 (environmental zone H4A) may increase from 95% to 100%. The increase in the accident humidity parameter results in a potential increase in the leakage at the pressure transmitter terminations. The DCP applied the coating as a means to reduce the leakage to an acceptable value.

Revision to UFSAR Subsection H.3.4.17 per Design Change Package (DCP) 8300039
The addition of Chemical Feed Stations on Unit 2 changed the number of floor drains in fire zone 4F2 (Unit 2 Division 1 Essential Switchgear Room), from two to one. To install the DCP, a core bore was required in the Unit 2 Division 1 Switchgear room. This core bore accidentally cored through an existing floor drain line. A supplemental engineering change notice (ECN) was issued to define how to cap both ends of the floor drain line. However, the number of floor drains in this room was specifically described in the

UFSAR. UFSAR Subsection H.3.4.17 is revised to state that the description of zones 4F1 and 4F2 is similar, except that the Unit 2 zone only contains 1 floor drain.

Coating of Unit 1 Division 3 and Reactor Protection System Divisions A1, 2 and B1, 2 Pressure Transmitter Instrumentation Circuit Terminations per Design Change Package (DCP) 9800094
The DCP applied Patel Engineers Conformal Coating (PECC) on the terminations associated with pressure transmitters 1B21-N403A, B, C, D, 1B21-N406A, B, C, D, and 1B21-N409A and B. Re-analysis of the reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) high energy line break (HELB) concluded that the humidity in Room 19 (environmental zone H4A) may increase from 95% to 100%. The increase in the accident humidity parameter results in a potential increase in the leakage at the pressure transmitter terminations. The DCP applied the coating as a means to reduce the leakage to an acceptable value.

UFSAR Change Associated with Electrohydraulic Control System (EHC) Pressure Regulator Failure - Closed transient analysis
General Electric (GE) Service Information Letter (SIL) 614 states that plants must have specific evaluation of the pressure regulator failure - closed transient without a backup pressure regulator available to support operation without both pressure regulators available. LaSalle does not have such an analysis. The potentially restrictive core thermal limits such an analysis would impose makes performing such an analysis undesirable. Operation must accordingly be limited to meet the initial conditions assumed in the present Pressure Regulator Failure - Closed transient. This requires that both pressure regulators be available, to ensure that a single failure of one pressure regulator will result in operation of the backup regulator. UFSAR Subsections 7.7.5.2.2 and 15.2.1.1 are correspondingly revised.

UFSAR drawings M-67 Sheets 1, 2, and 3, M-91 Sheet 3, M-124 Sheet 2 and M-137 Sheet 3 revised per Drawing Change Request (DCR) 980591.
The DCR revised the UFSAR drawings to reflect the as-built configuration and current design of the Turbine Building Closed Cooling Water (TBCCW) System (WT), the Reactor Building Closed Cooling Water (RBCCW) System (WR) and the Reactor Building Equipment Drains (RE). The current drawings did not reflect the actual field configuration of the systems and were not in agreement with the Electronic Work Control System (EWCS).

Addendum 2 to Design Change Packages (DCPs) 9600216 and 9600217 incorporated the revised safety evaluation into the DCP along with revising the ECN backup calculation list to reference additional calculations for the mounting of the backdraft dampers.

The original safety evaluation was revised to address installation of backdraft dampers (1VT104Y and 1VT105Y) in the blowout panels (57 and 60) between the turbine operating deck and the pump room. The Addendum letter did not impact the previously identified UFSAR changes or necessitate additional UFSAR changes.

LaSalle Special Test Procedure LST-98-018 Revision 0, LPCS Pump Data Acquisition Test
The procedure was written and performed to obtain low pressure core spray (LPCS) pump performance data on Unit 1, i.e. flow, temperature, pressure, and delta pressure, for evaluation by Systems Engineering. The test operated the Unit 1 LPCS pump at various flows to and from the suppression pool and injected into the reactor vessel at full flow conditions. The test results allowed determination of degradation in system flow with the minimum flow valve open, determine system flow resistance during injection, and validation of the LPCS pump curve.

A previous reference to calculation L-001363 was deleted, as it is not required for Design Change Package. The applicable portion of this calculation was included in calculation L-001367.

Reroute VE Ductwork from Computer Room to Units 1 & 2 Auxiliary Electric Equipment Room (AEER) per Design Change Package (DCP) 9700551 (Addendum #6) and Supplemental Engineering Change Notice (ECN) 001392H-01, and UFSAR revisions. The revisions to the evaluation reflect the changes to the DCP per Supplemental ECN 001392H-01. Supply air zone one (1) of the VE system, originally designed to serve the computer room, was rerouted to Units 1 & 2 AEER as part of the original DCP. The duct re-routing involved abandonment of the section of the duct serving the computer room. Supplemental ECN 001392H-01 abandoned in place the duct heaters (0VE03AA/AB) and disconnected the associated heater controls located in the section of duct that now serves the AEER.
UFSAR Section 9.4.1.2.2, Table 9.4-3, and Drawing M-1443 Sheet 4 are revised to show 0VE03AA/AB are abandoned in place.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800073 – Loss of Coolant Accident (LOCA) / Purge Analysis.
This DCP analyzed and modified the VQ piping system as a result of postulating a LOCA during containment purge. During investigation of LER 97-005, it was discovered that in the event of a LOCA coincident with containment purging, the VQ ductwork could potentially rupture and VQ piping downstream of the VQ Containment Isolation Valve could experience temperature increases beyond the originally analyzed conditions.

As a result of the VQ piping analysis, two VQ pipe supports (1VQ02-1035X and 1VQ02-1040X) were removed to control piping stresses under thermal conditions resulting from the postulated LOCA during purging evolutions. A local temperature gauge (0TI-VQ010) was added in the Auxiliary Building to provide local ambient temperature indication. In addition to analyzing the VQ piping system, an analysis to evaluate the environmental impact on equipment and radiological impact on the onsite and offsite personnel by the VQ ductwork rupture and resultant steam release that occurs as a result of the postulated LOCA was performed. This analysis determined that a new harsh environmental zone (designated H10) must be created, requiring a change to Section 3 of the UFSAR. UFSAR Section 3.11.1 is revised, and Figure 3.11-6 sheets 1 and 2 are added.

Correction of Discrepancies in UFSAR Subsections 9.2.8.2 and 9.2.8.5
Discrepancies in UFSAR Subsections 9.2.8.2 and 9.2.8.5 for the Turbine Building Closed Cooling Water (TBCCW) are corrected.
The proposed changes apply to the description of system flow and heat exchange capability, a change in TBCCW system leakage, correction to the UFSAR list of equipment to which TBCCW provides cooling water, and a change in TBCCW abnormal pressure and temperature indications.

Replacement of Drain Lines for Unit 1 Drywell Flow Element 1FE-RF021 per Design Change Package (DCP) 9700003
The DCP replaced the carbon steel drain lines of Unit 1 drywell coolers 1VP03AA and 1VP03AB with stainless steel drain lines. Carbon steel globe valve 1RE051A was replaced with a stainless ball valve, and carbon steel p-traps were replaced with stainless steel crud traps. Flow element 1FE-RF021 was relocated away from the Unit 1 reactor pressure vessel for ALARA purposes. The DCP was installed to preclude clogging of the flow element 1FE-RF021 from rust and soot accumulation, which produced erroneous readings in the control room.

LaSalle Special Test Procedure LST-98-044 Revision 0, Unit 1 Heater Drain Tuning and Performance Test
LaSalle Special Test Procedure LTS-98-044 provided for performance of Unit 1 feedwater heater drain level controllers (normal and emergency) during various power level plateaus during power ascension using temporary test equipment. Evaluation of gathered data allows for future tuning and system optimization.

Unit 1 & 2 Design Change Package (DCP) 9700314 for VC/VE A Train Condenser Bypass Damper – Snow Mitigation (Design Change Approval Letter Addendum #4), and UFSAR revisions.

The original modification provided a VC and VE (Train A) refrigeration condenser unit fan recirculation flow path to allow continued condenser operation without opening the plenum door and preventing fan operation in an unstable region of the fan curve. Addendum #4 identifies performance of an additional calculation (L-001925) to verify the acceptability of the negative static pressure within the condensing unit due to potential snow/ice blockage across the coils. The calculation determined that the coil and support members for the condensing units are adequate for the differential pressure load of approximately 9 inches of water, maximum ice load of 1 inch thickness over 80% of the coil area and seismic effects. There was no physical work associated with this addendum.
No UFSAR revisions are required as a result of addendum #4. UFSAR Sections 9.4.1.1.2c and 9.4.1.2.2c are revised.

Unit 1 & 2 Design Change Package (DCP) 9700504 for VC/VE B Train Condenser Bypass Damper – Snow Mitigation (Design Change Approval Letter Addendum #4), and UFSAR revisions.
The original modification provided a VC and VE (Train B) refrigeration condenser unit fan recirculation flow path to allow continued condenser operation without opening the plenum door and preventing fan operation in an unstable region of the fan curve. Addendum #4 identifies performance of an additional calculation (L-001925) to verify the acceptability of the negative static pressure within the condensing unit due to potential snow/ice blockage across the coils. The calculation determined that the coil and support members for the condensing units are adequate for the differential pressure load of approximately 9 inches of water, maximum ice load of 1 inch thickness over 80% of the coil area and seismic effects. There was no physical work associated with this addendum.
No UFSAR revisions are required as a result of addendum #4. UFSAR Sections 9.4.1.1.2c and 9.4.1.2.2c are revised.

Several Technical Specifications specify the condition: "operations with a potential for draining the reactor vessel," and "operations that have a potential for draining the reactor vessel," but provide no definition. This condition is referred to as an Operation with the Potential for Draining the Reactor Vessel (OPDRV). Technical Specification Clarification 01-98 was initiated to define the statement "operations with a potential for draining the reactor vessel," and "operations that have a potential for draining the reactor vessel". This definition was required to ensure that the Technical Specification requirements are applied when the appropriate conditions exist.

Out of Service (OOS) 960002031
The OOS which has been in effect for a prolonged period of time. Unit 1 leak detection system equipment valves 1E31N007AB-HI/LO/EQ, 1E31N007BB-HI/LO/EQ ,

1E31N013AB-HI/LO/EQ, and 1E31N013BB-HI/LO/EQ were abandoned in place (AIP) or controlled by the OOS program.
The valves are administratively prevented from being operated on a permanent basis and are left in the open/closed position as follows:
Instrument LO side stop valves closed; Equalizing stop valves open; and Instrument HI side stop valves closed.
Equipment associated with these valves, DP switches 1E31-N007AB/BB and 1E31-N013AB/BB, and their respective instrument lines, were removed per modification M01-1-88-052. The abandoned instrumentation ports of the manifold valves were plugged. The DP switches were previously removed to prevent spurious RCIC isolation, eliminating these switches reduced maintenance and surveillance efforts.
The deletion of switches improved the availability of the reactor core isolation cooling system to mitigate events for which it is relied upon. Placing the stop valves permanently in the designated positions accommodated the removal of the DP switches.

Revision to UFSAR drawings per Design Change Package (DCP) 9800074 – Replacement of Outlet Throttle Valve 1DG020 for NW Area Cubicle Cooler (1VY01A).
The DCP replaced the existing 4-inch 1DG020 globe valve, downstream of VY cooler 1VY01A, with a 3-inch globe valve. A portion of the existing 4-inch piping was replaced with reducing fittings to fit-up the new valve with the existing piping. The existing valve had deteriorated and was replaced with a smaller valve to increase the pressure drop to facilitate flow balancing.
UFSAR Drawing M-87 Sheets 2 and 3 are revised to show the smaller valve and associated reducers.

Reroute VE Ductwork from Computer Room to Units 1 & 2 Auxiliary Electric Equipment Room (AEER) per Design Change Package (DCP) 9700551 (Addendum #8) and Supplemental Engineering Change Notice (ECN) 001392H-02, and UFSAR revisions.
During L1F35, extensive changes were made to the VC/VE system to establish airflows that provide the required positive pressure in the Main Control Room (MCR) and the AEERs per DCP 9700551 and its previous addenda. With the extensive changes, the system will balance and operate with flowrates that are different from the design flowrates given on the Piping & Instrument Diagrams (P&IDs). Therefore, calculated minimum and maximum flowrates supporting system requirements were established. Supplemental ECN 001392H-02 was issued to document the changes to the fan blade pitch settings for fans 0VE01CA/CB and 0VE02CA/CB to establish the design flowrates and the revised acceptance criteria for the modification testing.
UFSAR Drawings M-1443 Sheets 1 through 4 are revised to include clarifying information on airflow rates for the VC/VE system duct segments to support system testing and balancing.

Unit 1 Primary Containment Chilled Water Expansion Tank Water Level Control Changes per DCP 9500283
The DCP revised the High/Low level alarm setpoints, and the automatic makeup Start/Stop setpoints for the Unit 1 VP system expansion tanks 1VP01TA and 1VP01TB. This design change eliminates unnecessary drawing of clean condensate water through the makeup lines to the VP expansion tanks.

LaSalle Special Test Procedure LST-98-019 Revision 0, HPCS Pump Data Acquisition Test
The procedure was written and performed to obtain high pressure core spray (HPCS) pump performance data on Unit 1, i.e. flow, temperature, pressure, and delta pressure, for evaluation by Systems Engineering. The test operated the Unit 1 HPCS pump at various flows to and from the suppression pool and injected into the reactor vessel at full flow conditions. The test results allowed determination of degradation in system flow with the minimum flow valve open, determine system flow resistance during injection, and validation of the HPCS pump curve.

UFSAR Revision for VC/VE Temperature, Pressure and Humidity Limits
Design Change Packages (DCPs) 9600214 and 9600215 removed the humidification equipment from the Control Room and Auxiliary Electric Equipment Room ventilation systems (VC and VE, respectively). Not all resultant changes to the UFSAR were revised per the DCPs. The UFSAR changes encompassed by this change consist of revising the minimum, normal and maximum temperature, pressure and relative humidity parameters for the Main Control Room (MCR) and the Auxiliary Electric Equipment Room (AEER); clarification of the normal operating pressure for the VC and VE systems when not in Emergency Makeup Mode; references to pressure ranges are made to be consistent with other UFSAR sections; added a discussion of the humidity restrictions for the recirculation filters on both VC and VE to clarify their revised design basis; reference to steam humidifiers are deleted; and consistent wording is being maintained for the discussion of pressurization modes.
UFSAR Tables 3.11-24 and 3.11-25, and UFSAR Sections 6.4, 6.5, 7.3, 9.4.1.1, 9.4.1.2, and H.3.4 are accordingly revised.

Out of Service (OOS) 960005699
The OOS has been in effect for a prolonged period of time. The OOS performed the following: Isolated electrical power to the humidifier steam generators for the control room and auxiliary electrical equipment room systems; Isolated domestic water supply to the humidifier steam generators; Lifted the OOS tags on the domestic makeup water valves; and Removed electrical power to control room ventilation humidity and heater control relays.
The humidification systems have been inoperable for several years. The operation of these systems was abandoned after unsuccessful attempts to maintain the associated

steam generators and distribution components, and due to flooding of the ductwork associated with them.

Out of Services (OOS) 960001057 and 950004295
The OOSs were in effect for a prolonged period of time. OOSs 960001057 and 950004295 respectively set the time delay setting associated with the local power range monitor high alarm to 0 (zero). The out of service on the time delay relays will continue until design change packages 9700295 and 9700296 permanently remove the time delay relays.

Revision to UFSAR for Containment Monitoring Penetration Isolation
In order for the Post-LOCA H2/O2 system to be an extension of the primary containment, i.e., closed loop outside the containment, the High Radiation Sampling System (HRSS) Containment Air Sampling Isolation Valves 1(2)CM085, 1(2)CM086, 1(2)CM089, and 1(2)CM090 should have been considered containment isolation valves. These valves are designed to be ASME Class 2 and seismic Category I; however, these valves were not identified as containment isolation valves, were not specifically tested as containment isolation valves, and were not controlled as containment isolation valves. Administrative Technical Requirements Tables 3.6.3-1 and 3.6.3-2, UFSAR Table 6.2-21, Summary of Lines Penetrating the Primary Containment, and UFSAR Table 6.2-28, Primary Containment Isolation Valves, for penetrations I-35, I-47, & I-50, are revised to include High Radiation Sampling System (HRSS) Containment Air Sampling Isolation Valves 1(2)CM085, 1(2)CM086, 1(2)CM089, and 1(2)CM090.

Main Control Room (MCR) and Auxiliary Electric Equipment Room (AEER) Penetration Seals per Design Change Package (DCP) 9700594 (Addendum #8) and Engineering Change Notice (ECN) 001416S and UFSAR revisions.
The original ECN and DCP provided alternate generic penetration sealing material and methods for the purpose of reducing air leakage from the outer envelopes of the MCR and AEER to adjacent areas. The volume of air leakage from the MCR and AEER is one of the contributing factors to the inability of the VC/VE systems to maintain their respective areas at the 1/8" water column (WC) positive pressure with respect to surrounding areas as required by the UFSAR. Addendum #8 to the Design Change Approval Letter was issued to provide clarification regarding alternate materials used for coating exiting gypsum cement floor penetration fire seals in response to Offsite Review Report No. 01-98-070. UFSAR Section H.1.3 and Figure H.1-1 are revised to mention the option of coating the fire seals utilized at the top of concrete block walls in seismic structures with Vimasco 3IR cable coating air seal.

UFSAR changes per Unit 1 Design Change Package (DCP) 9800135, Install New Support on the Cooling Water Lines to the LPCS Motor, Remove Thermowell and Associated Temperature Indicator on Line 1DG23A.
This DCP added two gang hang supports to the cooling water supply and return lines for the Low Pressure Core Spray (LPCS) motor and eliminated the thermowell 1TEW-DG032 and associated temperature indicator 1TI-DG032 on line 1DG23A. One gang hang support was added to prevent an overstress condition on the pipes coming out of the LPCS motor (reference PIF L1998-03710). The other gang hang support was added to prevent an overstress condition on 1" carbon steel supply and return lines (reference PIF L1998-03806). The thermowell was removed to eliminate the flow obstruction it presented.
UFSAR sections 9.2.1.5, 7.3.3.3.1, and drawing M-87 Sheet 2 are revised to reflect the changes.

UFSAR Update for the inclusion of a holdup volume in the pathway for unidentified leakage to reach the Drywell Floor Drain Sump (DWFDS)
The UFSAR didn't previously provide definitive information as to the potential of a holdup volume of water due to irregularities in the drywell floor and the effect on the design basis for the leakage detection system in the drywell. UFSAR Subsections 3.8.3.1.1 and 5.2.5.5.4 are revised for the reactor coolant pressure boundary leakage detection system to include the addition of holdup volume caused by the irregularities in the drywell floor.

Seismic monitor software upgrade and setpoint change per Design Change Package (DCP) 9800107.
This DCP upgraded the existing Seismic Monitoring System based on review of various PIFs and test discrepancies under LST 97-987 to improve the system reliability, meet regulatory requirements, and prevent an extended period of system non-availability. Specifically, the seismic monitoring instrumentation setpoint was revised, the free field triaxial accelerometer was modified from a voltage loop to a current loop, the recorder's Random Access Memory (RAM) storage capacity was increased, along with other hardware and software changes.

Out of Service (OOS) 950005523
The OOS has been in effect for a prolonged period of time. The OOS incorporated the following: Wired closed Auxiliary Building Office HVAC System minimum outside air damper 0VA01Y; Closed instrument air valve 0FSV-VA001 to remove the motive force for damper operator OTZ-VA001; and Isolated differential pressure controller 0PDC-VA007.
Pressure fluctuations in the Auxiliary Building offices have caused the control room differential pressure with respect to surrounding areas to drop below its design value of +1/8" water gauge (w.g.). The cause of this pressure cycling in the offices has been the

modulating of the maximum outside air, return air and exhaust air dampers 0VA02Y, 0VA03Y and 0VA04Y of the auxiliary building office ventilation. The isolation of 0PDC-VA007, along with the forced closure of damper 0VA01Y, ensures that the operation of the auxiliary building ventilation system does not degrade the ability of the control room ventilation system to maintain the control room pressure at its design value.

Out of Service (OOS) 950006354
Out of Service (OOS) 950006367
Temporary Alteration (TALT) TSC 1-84-95
The OOSs have been in effect for a prolonged period of time. TALT TSC-1-84-95 provided a temporary hose to by-pass a section of pipe in line 0WW04B that requires repair. The line has severe wall thinning, and has burst on several occasions. The OOSs isolate make-up demineralizer (MUD) feed pumps 0WW12A and 0WW12B from the bad section of piping. Temporary hoses connected to well water piping downstream of valve 0WW020 provide a supply from the well water tank to the MUDS, domestic water, and gland water for the acid sump pump seals. This measure ensured that the water makeup capabilities and the various other functions were available for the units.

Out of Service (OOS) 960003815
The OOS has been in effect for a prolonged time.
The OOS was placed on the oil supply stop valve to the 1A turbine driven reactor feed pump (TDRFP) turning gear, with instructions to open the oil stop bypass valve located on the turning gear, prior to taking the hand switch from the pull to lock position. The oil stop bypass valve should be closed (OOS) after startup of TDRFP. The OOS was placed to eliminate the oil leak at the low pressure end of the turbine, and to reduce frequent maintenance required to ensure the oil leaks are contained.

Revision to UFSAR Sections 1, 3, 4, 5, 6, 7, 9, and Appendix G
UFSAR sections 1, 3, 4, 5, 6, 7, 9, and Appendix G were updated to resolve discrepancies identified by Commonwealth Edison's Nuclear Fuel Management BWR Support Services.

Clarification to UFSAR Subsection 15.6.1.2
The operator response for a stuck open safety relief valve (SRV) in UFSAR Subsection 15.6.1.2 is indeterminate and confusing. UFSAR Subsection 15.6.1.2 is revised to clarify the actions to be taken in the event that a SRV can't be closed.

UFSAR revision per Design Change Package (DCP) 9800133 – Install New Isolation Valves on the Cooling Water Lines to the LPCS Motors.

This DCP added inlet and outlet isolation valves to the Unit 1 and 2 Low Pressure Core Spray Motor Cooler Inlet and Outlet lines 1DG22A –1 ½", 1DG23A – 1 ½", 2DG22A – 1 ½" and 2DG23A – 1 ½". Installation of these additional piping isolation valves allow future pipe maintenance or replacement without having to take the entire Division 1 Diesel Generator Cooling Water System out-of-service.
UFSAR drawings M-87 Sheet 2 and M-134 Sheet 2 are revised accordingly.

UFSAR Revision to reflect use of Microtherm Type Insulation
Pre-moulded non-hydrophobic Microtherm insulation enclosed in a 24-gauge stainless steel jacket was installed on lines 1NB09A-2", 1NB09B-1", 1NB88A-1", 1NB24A-2", 1NB24B-1", and 1MSC6AK-3/4". The insulation was used on the above reactor vessel water level and main stem flow sensing lines in the Unit 1 drywell to improve reactor vessel water level instrumentation reliability through increased thermal efficiency. The microtherm insulation was used instead of metallic reflective insulation (MRI). UFSAR subsections 6.2.3.1.3, 6.1.1.1, and Table 6.1-2 are revised.

UFSAR revisions per Document Change Request (DCR) 980529, As-built Hose Racks per Engineering Request (ER) 9707865.
Nineteen (19) hose racks were installed on various concrete and masonry walls in the plant using expansion anchors (reference CHRON letters 123650 and 115241) as a method to promote good housekeeping and safety by providing a place to store miscellaneous hoses when not in use. Many of the affected walls serve as fire barriers and the new hose storage increased the combustible loading in zones identified in the UFSAR. The DCR was issued to revise the affected sections of the UFSAR.
UFSAR Appendix H.3 and Table H.3-2 are revised to reflect the additional combustible loads for each affected zone.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9700419 – Heater Drain Pump Minimum Flow Changes to Facilitate Idle Pump Warm-up
The performance of battery surveillance discharge tests per LTS-700-6 and LTS-700-7 was deleted as a modification test. The battery capacity calculations were revised to include the load increases caused by addition of relays per the DCP.

Revision to UFSAR Tables 6.2-21 and 6.3-5
The UFSAR description of the control circuits for the low pressure core spray (LPCS) pump suction valves 1(2)E21-F001 and the residual heat removal (RHR) pump suction valves 1(2)E12-F004A, B, and C do not agree with actual plant configuration. UFSAR Tables 6.2-21 and 6.3-5 indicate that these valves receive an auto-open signal following a LOCA. However, they do not receive any auto-actuation signal. Rather than having an auto-open circuit, these valves are operated by keylock switches in the control room and maintained in the open position. These valves are checked monthly

per the Technical Specifications to ensure that they are maintained in the proper position.
This UFSAR change brings the tabular description of the control circuits for these valves into agreement with actual plant configuration, descriptions in the UFSAR, ComEd responses to NRC questions, and GE design documents.

Revision to UFSAR Table 9.3-1 and drawing M-99
Grab samples of the standby liquid control (SBLC) storage tank are gathered by dip sample in accordance with approved station procedure LCP-310-09. Sample pump 1C41-D303 was not installed as original equipment on either LaSalle unit, yet it is depicted on drawing M-99 (Unit 1 SBLC system). UFSAR Table 9.3-1 Sheet 5 indicates that one pump is required for the purpose of obtaining grab samples. If installed, the pump would serve no function that differs from the currently approved method of sampling. UFSAR Table 9.3-1 and drawing M-99 are revised to delete mention of the pump.

Out of Services (OOS) 940012585, 940012586, 940012594, 950004863, 950004907, 960010581
The OOS were in effect for a prolonged period of time. The OOSs ensure that these damaged systems cannot be operated, and do not pose personnel or equipment hazards during and after the implementation of design change package 9500091.
OOS 940012585 provided administrative controls to the 0AC008 valve for the concentrated acid day tank pending demolition or abandonment in place.
OOS 940012586 provided administrative controls for the inlet vale to acid day tank pending demolition or abandonment of the panel.
OOS 940012594 de-energized the air supply to valve 0AC032 pending demolition or abandonment.
OOS 950004863 provided administrative controls to isolate the transfer pumps for the caustic day tanks pending their demolition or abandonment.
OOS 950004907 provided administrative controls to isolate and de-energize acid and caustic feed pumps for the condensate polishing system their demolition or abandonment in place.
OOS 960010581 provided administrative controls to isolate and de-energize pumps and tanks pending their inspection and possible demolition or abandonment in place.

Revision to UFSAR Drawings M-94 and 1E-1-4601AB per Design Change Request (DCR) 980504.
These drawings are revised to incorporate the nameplate nomenclature on panel 1H13-P601 for the Overload Bypass Hand Switch associated with valve 1E21-F001, and to correct the EPN for the LPCS Minimum Flow Bypass Valve Hand Switch on the P&ID. The changes are editorial and are as-built configuration changes based on the LPCS system walkdown.

Revision to UFSAR drawing M-55 Sheet 10 per Design Change Request (DCR) 980501.
As a result of the EHC Functional Walkdown (ER #9801496), UFSAR drawing M-55 Sheet 10 was revised document the as-found field configuration of the Unit 1 Turbine EHC system (as-built). The previous drawing was functionally incorrect and required revision to reflect the installed configuration.

Installation of High Point Vents on the Cooling Water Lines to the Unit 1 LPCS Motor Cooler per Design Change Package (DCP) 9800134
The DCP added vent valves in low pressure core spray (LPCS) motor cooler supply and return lines. The vent valves will permit proper venting to drain the lines for maintenance activities. This activity requires a revision to drawing M-87 Sheet 2.

Revision to UFSAR for 125 VDC Bus Ties
UFSAR Subsection 8.3.2.1.1 is revised to extend the use of the 125 VDC ESF Division 1, 2, and 3 bus ties to include battery charger failure, battery charger surveillance, and ground detection, and to reflect the battery testing is performed in accordance with IEEE 450-1980.

Replacement of Unit 1 Capacitance Probes with Displacement Probes per Design Change Package (DCP) 9700477
The DCP replaced the sensors in the Reactor Floor Drain Sump (RF) weir and the Reactor Equipment Drain Sump (RE) with more reliable instrumentation. Specifically, the drywell floor drain sump capacitance fill up rate type probe 1LE-RF002, its coaxial cables, and its remote transmitter 1LT-RE002 were replaced with a new displacement type probe, shielded cables and a remote transmitter. Likewise, the drywell equipment drain sump capacitance fill up rate type probe 1LE-RE001, its coaxial cables, and its remote transmitter 1LT-RE001 were replaced with a new displacement type probe, shielded cables and a remote transmitter. The reliability and inherited problems with the capacitance probes necessitated their replacement with more reliable instruments.

Out of Service (OOS) 950005202
This safety evaluation written for the OOS which has been in effect for a prolonged period of time. The OOS is administratively preventing the 2" domestic water valve to the service building laundry room from being operated on a permanent basis and is left in the closed position. Placing the valve permanently in the designated closed position stops leakage of water from unused equipment in the laundry room and prevents contamination of the domestic water system from stagnant water in unused laundry room equipment.

Out of Service (OOS) 950005507
The OOS has been in effect for a prolonged period of time. The 'old' service building domestic water heater, 0WD04T, is no longer in use. Repairs to the damaged water heater are cost prohibitive. Its certificate of inspection from the State of Illinois previously expired. Two smaller hot water heaters, at two different levels, are installed to provide the necessary supply of hot water for occupants of the building. To prevent water leakage, accumulation of stagnant water and gasses, and inadvertent supply of electricity to the water heater, the OOS maintains associated vent and drain valves in the open position, other associated valves are kept in the closed position, while associated power supply breakers are racked out or put in the off position.

UFSAR changes per Design Change Package (DCP) 9700208 – Reactor Water Cleanup (RT) System Recirculation Pumps and Return to Hot Suction.
This DCP restored the "hot suction" configuration of the RT system, as originally designed by General Electric, by replacing / reworking piping and associated valving. The design change installed the Reactor Water Cleanup pumps upstream of the system heat exchangers and routed the piping from outside the primary containment to the pump suction bypassing the heat exchangers. The pump discharge was routed to the system heat exchangers. The DCP replaced the three existing non-safety related 50% capacity RT System recirculation pumps with two new 100% capacity pumps.
UFSAR Sections 1.7, 7.3.2.2.3.8,and 7.7.1.2.2, Tables 5.4-1, 8.1-2, 8.1-9, 8.3-1, 12.3-16 Sheet 1, Figures 4.6-5, 4.6-6, 5.4-6 Sheet 1 and Sheet 2, 5.4-8, 12.3-1 Sheet 4, 12.3-2 Sheet 4, and 12.3-4 Sheet 2, and H.2-1 Sheet 3 and Drawings M-Index Sheet 1, M-7, M-74, M-90 Sheet 3, M-91 Sheets 2 and 6, M-97 Sheet 1, M-100 Sheet 1, M-104 Sheet 1, and M-2097 are revised accordingly.

Unit 1 & 2 Design Change Package (DCP) 9700504 for VC/VE B Train Condenser Bypass Damper – Snow Mitigation (Design Change Approval Letter Addendum #5), and UFSAR revisions.
The original modification provided a VC and VE (Train B) refrigeration condenser unit fan recirculation flow path to allow continued condenser operation without opening the plenum door and preventing fan operation in an unstable region of the fan curve. Addendum #3 identified modification testing requirements for DCP 9700504. During testing activities, not all of the acceptance criteria were met. Calculation L-001992, Minimum Airflow for the VC/VE Air Cooled Condensers, was performed to evaluate the minimum requirements for airflow through the condenser during the different tested conditions. The results were issued as Addendum #5 and the safety evaluation was revised to include the calculation as a reference and to reflect the minimum airflow rates to be used as acceptance criteria in the airflow testing.
No UFSAR revisions are required as a result of addendum #5. UFSAR Sections 9.4.1.1.2c and 9.4.1.2.2c are revised.

UFSAR Revision for the Standby Gas Treatment (VG) System Charcoal Adsorber High Temperature Alarm Setpoint
Design Basis documents for the standby gas treatment system either do not specify the charcoal adsorber high temperature permissive alarm setpoint or else indicate a value of 310 °F. The alarm setpoint value of 250 °F in UFSAR Subsection 6.5.1.2.1.c.7 is revised to an alarm setpoint of 310 °F.

UFSAR Revision for Motor Operated Valve Thermal Overload Protection
UFSAR Section 6.3.2.2.13 is revised to reference UFSAR Table 6.3-9 for the HG valves and to add reference to Regulatory Guide 1.106, Revision 1.
UFSAR Table 6.3-9 was revised as follows:
Valves 1(2)G33-F001, 1(2)E12-F006A, and 1(2)E12-F011A are added to the table;
A clarification that Motor Operated Valves (MOVs) 1VQ037, 1VQ038, 2VQ037, and 2VQ038 have thermal overload bypass logic from both Unit 1 and Unit 2 was added to the table;
Unit 1 and Unit 2 hydrogen recombiner (HG) MOVs were added to the table.
Deleted the Main Steam Isolation Valve-Leakage Control System (MSIV-LCS) valves and 2E51-F091 were deleted from the table.
Table 6.3-9 was also reformatted to include the type of thermal overload bypass like Tech Spec Table 3.8.3.3-1, and to add allowance for no bypass for HG MOVs, as discussed in UFSAR section 6.3.2.2.13.
UFSAR Appendix B was revised by adding an update discussion on the applicability of Regulatory Guide 1.106, Revision 1.

UFSAR Revision per Design Change Package (DCP) 9800150
Unit 1 initial start-up included a Mark II containment test to analyze hydrodynamic forces in the suppression pool during safety relief valve (SRV) actuation. Some instruments remain in the suppression pool, which are attached to the suppression pool liner, SRV discharge pipes and quenchers, drywell floor support columns, and drywell downcomers. The suppression pool test installations were to be removed at the earliest convenient opportunity. The instruments were installed prior to 1981, while the test was completed in 1983. The boxes on the drywell floor, the instruments in the suppression pool, and the cables between them are still installed. For maximum visibility for removal, the suppression pool should be drained, which has not occurred since that time. Per DCP 9800150 (Temporary Alteration 1-0069-98), the cables and instruments are to remain installed during plant operation through the remainder of the current Unit 1 fuel cycle until refuel outage L1R08, when they are scheduled to be removed. An engineering evaluation concluded that the original technical and licensing basis for continued operation with the instrumentation remaining installed in Unit 1 containment continues to be valid. UFSAR Sections 1.2, 6.1, and 6.2 are revised. These proposed

changes were subsequently superseded by implementation of DCP 9900187. DCP 9900187 removed old SRV test equipment, valves, and cables from the Unit 1 drywell.

Revisions to UFSAR Subsections 6.5.1.2.1.C.7, 9.5.1.2.3, H.3.2.2, H.3.4.2, and H.3.5.33
The above Subsections state that the charcoal deluge valves are operated locally from the main control room board. The normally manual closed isolation valves upstream of the deluge valves, in all cases, require local actions to initiate water flow. The proposed change to these UFSAR subsections clarifies the operation of the deluge valves to reflect manual operation of the charcoal deluge systems.

The use and acceptance of cast iron bodied valves was evaluated and documented per Engineering Request (ER) 9802882. Reference Drawing Change Request (DCR) 980539. An as-built DCR was issued to reflect that the existing 2" condensate demineralizer recycle line butterfly valves 1(2)CP-013A-G and 1(2)CP-017 A-G are cast iron bodied valves in lieu of carbon steel bodies specified in PDT 100LS.

Design Change Package (DCP) 9600532 – 1WS043 Control Valve Replacement
The DCP replaced and relocated the carbon steel Service Water Control Valve 1WS043 (Masoneilan control valve) with a stainless steel Fisher-Rosemount Vee-Ball control valve with a noise attenuator ball. Upstream isolation valve 1WS042 was also relocated and downstream isolation valve 1WS044 was replaced with a flanged end butterfly valve. The carbon steel piping between 1WS043 and 1WS044 was replaced with stainless steel pipe. The changes were made to minimize the cavitation erosion damage problem previously experienced.
UFSAR Drawing M-69 Sheet 2 is revised to reflect the new control valve and the downstream piping as stainless steel.

Unit 1 Number 1 and 2 Feedwater Heater Drain Control Valve Replacements per Design Change Package (DCP) 9700287
A revision to the evaluation consists of a change to the insulation thickness to be installed on the normal drain lines, removal of holds to reflect completion of calculations, added clarifications to discussions concerning testing, and further revises drawings M-61 Sheets 3 and 4.

Revision to UFSAR Table 9.3-1 and Drawing M-143 Sheet 1 to reflect as-built condition of the plant
UFSAR Table 9.3-1 Sheet 1, Process Sampling System (Reactor Building Samples), and drawing M-143 Sheet 1, Reactor Water Cleanup System, are revised reflect the as-built configuration of the subject sample line piping. These process sampling lines

include the reactor recirculation water sample line, the RWCU sample lines from each of the filter demineralizers, and the sample line off the discharge of the RWCU recirculation pumps.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800112, VR System Exhaust Plenum Overpressure Protection Damper Due to High Energy Line Break (HELB) in Main Steam Tunnel (MST).
This DCP installed a new relief damper (1VR90Y) in the VR system between 1VR05YB and the VR plenum wall to prevent a failure of the plenum following a postulated Main Steam Line Break in the Main Steam Tunnel. Stiffeners were added to the existing transition piece to allow for the addition of the relief damper. Additional supports were added to support all the added loads due to the modified duct, associated stiffeners and the relief damper.
UFSAR Section 9.4 is revised to include descriptions of the safety and design bases and operation of the new pressure relief damper 1VR90Y. Drawing M-1455 Sheet 1 is revised to reflect the addition of the new pressure relief damper.

Revision to UFSAR Subsection 7.5.3.c.4
UFSAR Subsection 7.5.3.c.4 is revised to reflect that safety relief valve position indication is actually powered by 125 VDC from Division I distribution panels 111Y (Unit 1) and 211Y (Unit 2). This was identified by the Design Basis Initiative project.

Revision to UFSAR Subsection 11.3.3 per Unit 1 Design Change Package (DCP) 9700530 – Modify VR Flow to the RT Pump / Valve Rooms.
The design change replaced the existing Reactor Water Cleanup (RWCU) pump room pneumatic controlled balancing dampers (1VR16Y, 1VR17Y, & 1VR18Y) with smaller manual controlled balancing dampers (1VR84Y, 1VR85Y, 1VR86Y, 1VR87Y, 1VR88Y, & 1VR89Y). The air regulators, temperature controllers, and actuators on the existing dampers were removed from the affected areas. The instrument air line to the regulators was cut and capped. The design change also installed and balanced new manual controlled balancing dampers (1VR80Y and 1VR81Y) in the associated ductwork outside of the RWCU pump rooms, along with balancing (adjusting) flow through existing manual controlled balancing dampers in several areas. Additionally, the duct to wall penetrations between the existing RWCU pump rooms were sealed. The design change was made to revise the variable exhaust flow in the RWCU pump rooms to the revised new fixed flows. The installation of the additional new manual controlled balancing dampers and the balancing of the dampers in the associated valve and heat exchanger rooms assures proper flows throughout the area.
UFSAR Subsection 11.3.3 is revised to indicate the new ventilation system capacity of 110,800 scfm.

Rerouting of Electrohydraulic Control (EHC) Tubing per Design Change Package (DCP) 9800156
The DCP relocated the 2-inch EHC tubing header and re-routed the 1-1/4 inch individual branch lines for the Unit 1 Main Steam Bypass valves, 1B21-MSBPV-1, 1B21-MSBPV-2, 1B21-MSBPV-3, 1B21-MSBPV-4, and 1B21-MSBPV-5. The lowering of the header and the re-routing of the individual branch lines is designed to allow individual removal during maintenance. This will provide flexibility in the system, allow improved fit-up at the valve ports, improve valve maintainability, and improve the system reliability by reducing the potential for leaks.
Administrative Technical Requirements (ATR) Amendment 17, Secondary Containment Automatic Isolation dampers
ATR Amendment 17 was created to administratively control the opposite unit secondary containment ventilation system isolation dampers to the Technical Specification requirements for the same unit secondary containment ventilation system isolation dampers. The Secondary Containment for LaSalle Units 1 and 2 is common to both units. Technical Specifications 3/4.6.5.2 for each unit only lists same unit Secondary Containment Ventilation System Automatic Isolation Dampers in Technical Specifications Table 3.6.5.2-1. The ATR maintains positive control of the Secondary Containment Automatic Isolation Dampers not listed in the respective Technical Specifications in the interim until a license amendment is submitted and approved to provide final resolution.

Replace NAMCO Limit Switches on Turbine Stop Valves (TSV) 1(2)C71-N006A/C/E/G per Engineering Request (ER) 9707722. Reference Drawing Change Request (DCR) 980549.
This change replaced the original NAMCO Model No. EA 750-70000 valve position limit switches with Model No. EA 740-80001 on the Main Turbine Stop Valves 1(2)C71-N006A/C/E/G. New specially fabricated junction boxes, called "blister boxes", were attached on the original existing junction boxes to house the new limit switches because the new limit switches were longer. The original model limit switches were failing and were no longer manufactured by NAMCO; therefore, the newer model limit switches were approved for use.

Air supply to inlet valves for the A and B concentrator waste tanks disconnected and capped to allow the valves to be maintained normally closed per Design Change Package (DCP) 9200145 and Design Change Approval Letter Addendum #2 for ECN 001508M and UFSAR revisions.
The original administrative controls on the inlet valves were eliminated, the air supply to the valves disconnected and the air cylinders associated with each valve vented to ensure that the inlet valves remain closed as detailed in ECN 001508M. UFSAR Subsection 11.2.2.5.5 and drawing M-103 Sheet 14 are revised.

Out of Service (OOS) 960002250 for valves 1B21-F538 and 1B21-F539 and associated breakers 1AP71E-G5 and 1AP71E-G6
OOS 960002250 is administratively preventing valves 1B21-F538 and 1B21-F539 and associated breakers 1AP71E-G5 and 1AP71E-G6 from being operated. The breakers are in the OFF position, valve 1B21-F538 in the OPEN position, and 1B21-F539 is CLOSED. This administrative method of controlling the valves and associated breakers has occurred over a prolonged period of time. The OOS was evaluated as a permanent plant change. Drawings M-93 Sheet 4 and M-55 Sheet 1 are revised to reflect the prolonged OOS with the valves 1B21-F538 and 1B21-F539 being abandoned in place in the above stated positions.

UFSAR revision per Design Change Package (DCP) 9800148, Abandoning Main Steam (MS) Supply to Radwaste Reboiler 1AS01B.
The DCP modified main steam line 1MS41A-3" by removing a section of pipe by cutting and capping it in two locations. This isolated the main steam supply to Unit 1 Radwaste Reboiler 1AS01B. This reboiler is no longer used and is slated for abandonment. UFSAR pending change section 3.1.2.6.1 is revised to delete reference to evaporators (Unit 1 only) and UFSAR pending change 11.2.2.3 is revised to delete reference to evaporators/bypass and indicate the use of a vendor system to process liquid radwaste (applicable to Unit 1 only).

Revision to UFSAR discussion of the Reactor Mode Switch Bypass of the Charging Header Low Pressure Scram
UFSAR Section 7.2.2 is revised to add grammatical corrections and additional level of detail relevant to the operation of the control rod drive (CRD) charging header low-pressure trip bypass test switches (1/2C11-S600A to D). These switches were part of the original design and installation of the low-pressure trip circuit, but were not described well in the UFSAR. The existence of these test switches was implicit in the existing text, but it was not clearly stated.
UFSAR Figure 7.2-4 is revised to correct the normal position of the CRD low charging pressure scram bypass contacts from OPEN to CLOSED. This is an editorial correction of a typographical error. The text in the body of NUREG-0519 Supplement 7, the LaSalle UFSAR, and the LaSalle Technical Specification Bases make clear that the scram contacts are bypassed (i.e., bypass contacts CLOSED) during "normal" operation.

Revise drawings to reflect as-built conditions per Drawing Change Request (DCR) 980717 (Engineering Request (ER) 9707834).
This change removed the triangular plenum doors from the interior of the Unit 1 and Unit 2 Moisture Separator Reheaters [1(2)TG03AA/AB] per General Electric (GE) recommendation. The moisture separator reheaters (MSR) have plenum doors in each of 15 partitioned sections inside the MSR that are used solely for personnel access

during internal inspections. GE determined that the doors were causing undesirable localized heating due to unequal flow throughout the MSR and could cause water to be brought up the drain trough due to differential pressure across the sections. GE recommended that the doors be removed.

Revision to UFSAR drawing per Design Change Package (DCP) 9800146 – Replace Turbine Building Closed Cooling Water (TBCCW) Heat Exchanger Flow Control Valve 1WS029
This DCP replaced the TBCCW Heat Exchanger Flow Control Valve 1WS029, which was a Masoneilan model 37-20521 AOV, with a Masoneilan model 37-41612 AOV with anti-cavitation trim. The replacement was necessary because the valve had cavitation damage and was obsolete. In addition the DCP replaced the existing filter/regulator, revised the bench set values, revised the pressure regulator setpoint and permitted field re-routing of the air tubing and supports to accommodate the new valve assembly. This activity requires a revision to drawing M-69 Sheet 2.

Procedure CWPI-NSP-TQ-1-1, Nuclear Generation Group Conduct of Training Manual, Instruction One, New Employee Training Program
The procedure incorporates the Conduct of Training Manual authorized and controlled by NSP-TQ-3005, Conduct of Training, which implements the New Employee Orientation Program (NEOP). This program is standardized across all Commonwealth Edison Nuclear Generation Group facilities.

Out of Service OOS 950004895
The OOS has been in effect for a prolonged period of time. The OOS left well house power panel breaker number 10 in the off position, and potable water pressurizer tank (0WD01T) outlet valve in the closed position, administratively preventing them from being operated on a permanent basis. The potable water pressurized tank was used to provide potable water at the time of initial construction of the plant, required for the construction activity and human consumption. It was later used for the fish hatchery. The potable water pressurized tank is no longer in use.

Install Temperature Monitoring Equipment for Feedwater Heater Drains, Design Change Package (DCP) 9800155, Temporary Alteration 1-0066-98
The temporary alteration installed temporary pressure transducers on the input and output signals of various heater drain controllers in support of Unit 1 heater drain system control valve tuning.

UFSAR Revision to Reflect Failure Modes of Turbine Building Ventilation Isolation Dampers

During a system functional performance review, of the turbine building ventilation (VT) system, it was discovered that the above dampers would not close quickly enough to prevent over-pressurization of the VT exhaust tunnel in the event of a main steam line break in the turbine building main streamline tunnel. UFSAR Section 9.4 is revised to reflect the failure modes of turbine building ventilation isolation dampers 1(2)VT079YA, 1(2)VT079YB, and 1(2)VT079YC.

UFSAR Revision for Control Room Ventilation System (VC) and Auxiliary Electric Equipment Room (AEER) Ventilation System (VE)
UFSAR Sections 6.4, 7.3, 9.4, and 9.5 are revised to reflect the proper operation of the VC/VE systems, correct grammatical errors, and clarify for consistency the discussion of VC and VE systems.

Revision to UFSAR Sections 9.4 and 9.5
DCPs 9700350 and 9700351 modified the Control Room and Auxiliary Electric Equipment Room ventilation (VC and VE systems, respectively) manual purge control circuit for Trains A and B to initiate automatic purge damper isolation upon detection of smoke in the outside air when the VC/VE system is aligned to purge the Control Room or Auxiliary Electric Equipment Room air (purge mode). UFSAR Subsections 9.4.1.1.1.1.d and 9.5.1.2.4 are revised, as the DCPs revised M-3443 sheets 5, 18, and 24. The changes to the above subsection are revised to be consistent with the DCPs and drawing changes.
The original safety evaluation supported the design changes described above and changed the UFSAR, but only to the extent of revising these circuits as shown on drawings M-3443 Shts. 5, 18, 24.

Revision to UFSAR to Reflect Unit 1 Cycle 8 Core Operating Limits (L1C8 COLR) and Reload Transient Accident Analysis (RTAT)
1. Reanalysis of the pressurization transients (including transients analyzed with currently allowed Equipment Out Of Service (EOOS) modes) was required to support a change to the analytical value for the APRM flux scram from 122.4% to 124.2%. This analytical value change was necessary to ensure the APRM flux scram setpoint did not need to be lowered from its current value of 118% to meet the required difference between the setpoint and analytical value calculated under the changed ComEd setpoint methodology. These transient reanalyzes have resulted in revised thermal limits, which have been included in the revised COLR.

2. Reanalysis of the pressurization transients (including EOOS modes) was also required to resolve an issue related to operation at less than rated pressure. The original GE transient analyses assumed the plant was at 1005 psig at 100% power, and at lower pressures at reduced power based on GE analytical modeling. ComEd discovered (PIF L1997-07035), and GE concurred, that operation at lower pressures

than those modeled by GE are frequently seen at LaSalle during startup and other modes of operation (up to approximately 15# lower), and that this can be non-conservative for some transient analyses. In their words, the GE analytical assumptions for the plant's pressure vs. power operational characteristics were inaccurate. GE re-performed those transients such that they reflect actual plant operation.

3. An error in the generic TCV(s) slow closure EOOS analysis was discovered. The transient applicable to this EOOS condition was reanalyzed to ensure the core thermal limits are bounding. Revised thermal limits are included in the COLR.

The Single Loop Operation flow dependent thermal limits have been modified based on reanalysis of the idle recirculation loop startup event for a revised minimum reactor recirculation flow control valve minimum position.

UFSAR Sections 7.7 and 15.A are revised.

Resolution of Issues Involving Errors in UFSAR Containment Analysis
UFSAR Sections 5.4 and 6.2 describe the analytical results of a loss of coolant (LOCA) accident, e.g., recirculation line break or main steam line break within containment, and the specific assumptions used in both the original and 1988 GE containment analyses. The assumption that feedwater flow instantaneously stops upon accident initiation, while being conservative with respect to peak cladding temperature (PCT) and accident blowdown, is not conservative for analysis of the suppression pool long term temperature. This analysis will be supplemented by including the injection of feedwater, this will account for the additional mass and energy to the suppression pool and contribute to higher long-term suppression pool temperatures. The suppression pool temperature limit in Technical Specification 3/4.6.2.1 was increased from 100°F to 105°F via Amendments 67 and 49, for Units 1 & 2 respectively, in 1988. General Electric provided the supporting calculations that concluded that the allowable temperature increase would have a negligible affect on the accident analyses. However, it was recently identified that two of the assumptions used in both the original and 1988 containment analyses were non-conservative when evaluating post-accident suppression pool temperature response. UFSAR Sections 5.4 and 6.2 are revised to resolve the Containment Analysis.

Unit 1 Control Room HVAC Train 'A' radiation monitor power supply filters per Design Change Package (DCP) 9800167
The design change installed a Transient Voltage Surge Suppresser (TVSS) on the 120 vac line input to the power supply located inside control room panel 0PM14J. It separated instrument ground wires and power supply ground wires to their respective grounds for 1D18-K751A/B/C/D, Train 'A' Control Room HVAC Air Intake Radiation

Monitors. This was done mitigate power supply "lock-up" experienced during the performance of diesel generator (DG) response time testing.

Unit 2 Control Room HVAC Train 'B' radiation monitor power supply filters per Design Change Package (DCP) 9800168
The design change installed a Transient Voltage Surge Suppresser (TVSS) on the 120 vac line input to the power supply located inside control room panel 0PM15J. It separated instrument ground wires and power supply ground wires to their respective grounds for 2D18-K751A/B/C/D, Train 'B' Control Room HVAC Air Intake Radiation Monitors. This was done mitigate power supply "lock-up" experienced during the performance of diesel generator (DG) response time testing.

Unit 1 Post LOCA Gross Gamma Analyzer Power Supply Filters modification per Design Change Package (DCP) 9800169
The DCP installed a transient voltage surge suppresser on the 120 VAC line input to the power supply, and separated instrument ground wires and power ground wires to their respective grounds of the power supply for radiation monitors 1RIT-CM011 "Post LOCA A Gross Gamma Analyzer", and 1RIT-CM017 "P/C Post LOCA B Gross Gamma Analyzer". This was done mitigate power supply "lock-up" experienced during the performance of diesel generator (DG) response time testing.

UFSAR Revision for Cable Tray and Cable Tray Support System
UFSAR Subsection 3.7.3.16 is revised to reflect that the design includes consideration of LOCA and hydrodynamic loads as described in section 8.1.6.2 of Sargent and Lundy (S&L) calculation DC-SE-01-LS and sections 4.3.2 and 5.3.2 of the LaSalle Mark II Design Assessment Report (DAR).

UFSAR Revision for Operation with Control Rod Drives with Higher Than Normal Withdrawal Speeds
There are occasions when the withdrawal rate of a control rod drive cannot be adjusted to be within the nominal band of 3.0 ± 20% inches per second via the speed controller on the appropriate directional control valve. The UFSAR presents control rod withdrawal rate (time) limits that reflect the Original Equipment Manufacturer's (OEMs) operational recommendations, 3.0 ± 20% inches per second. Recent evaluations have determined that the maximum control rod drive withdrawal rate may be safely increased to 5.14 inches per second when the Operating Limit Minimum Critical Power Ratio (MCPR) is based upon or exceeds the results of the Rod Withdrawal Error – at Power event analysis.

The maximum control rod withdrawal rate (or travel time) is increased from the 3.6 inches per second to a new maximum of 5.14 inches per second (28 seconds full-travel time) with an administrative constraint. UFSAR Sections 3.1, 4.6, and 15.4 are revised.

Revise UFSAR drawings per Drawing Change Request (DCR) 980706.
This DCR revised design documents that incorrectly described the current plant configuration and were in disagreement with other design documents that correctly described the plant configuration. Drawing M-1461 Sheet 1 is revised to add the correct panel reference to control switches 0HS-VW038A, 0HS-VW039B and 0HS-VW038C. Drawing M-1461 Sheet 2 is revised to correct the nomenclature used to describe four cubicles served by Radwaste Ventilation, to add a missing EPN for a damper and to correctly depict a damper as a fire damper versus a standard damper. UFSAR Drawings M-1461 Sheets 1 and 2 are revised accordingly.

Revision to UFSAR Subsection 9.2.1.1.1.a.5
Test data obtained during performance of LaSalle Special Test (LST) procedure LST-97-183 in June 1998 to determine low pressure core spray (LPCS) Motor Cooler heat exchanger thermal heat transfer efficiency was utilized by General Electric (GE) to perform an updated baseline flow requirement using empirical data. The results of the GE heat transfer model indicated that the 4 gpm flowrate stated in UFSAR Section 9.2.1.1.1a.5 was overly conservative for LaSalle Station LPCS Motor Coolers, and that a value of 2 gpm is acceptable with the recommendation that the flow be periodically directly monitored to verify continued adequacy and absence of plugging. The new 2.0-gpm value will be the vendor recommended nominal value. Administratively, penalty factors consisting of Lake level affects and instrument tolerances will comprise the new value specified in procedures LTS-200-27 and LTS-200-10 for the LPCS Motor Cooler flowrate and will be variable based on test methodology utilized.
UFSAR Subsection 9.2.1.1.1.a.5 is revised from to reflect 2-gpm flow for the LPCS Motor Cooler.
Revising the flow balancing bands for Unit 1(2) loads listed in LTS-200-27/29 & LTS-200-10 to encompass the recommendations of Nuclear Design Information Transmittals (NDITs) #LS-0850 & 0854 resulted in the following flowrate changes:
0DG01A, 0 DG Cooling Water Cooler from 970 - 1030 to 1010 (± 20).
1(2)VY04A, NE Cubicle Area Cooler, from 240 - 280 to 240 (± 10)
1VY01A, NW Cubicle Area Cooler, from 190 - 260 to 200 (± 10)
2VY01A, NW Cubicle Area Cooler, from 190 - 230 to 200 (± 10)
1VY02A, SW Cubicle Area Cooler, from 200 - 220 to 185 (± 10)
1E22-S001, 1B DG Cooling Water Cooler from 840 - 860 to 880 (± 20)
1(2)E21-C001, LPCS Pump Motor Cooler from ≥ 4.7 to ≥ 2.8 by timed accumulation flow and Ultrasonics as information only.
Specified upper limit on 0 and 1B DG Cooling Water Cooler Pump Strainer of 300 gpm.

Procedure LTS-200-10 was revised to incorporate:
New LPCS motor cooler CSCS service water flowrate values.
Delete valve throttling repeatability Attachment since cooler is incapable of passing upper flow limit specified.

Of the changes to flowrate values, only the LPCS Motor Cooler Flowrate represents a change to the UFSAR, the others are considered Generic Letter (GL) 89-13 programmatic changes based on recent test data results and system performance trending.
Other administrative (non-intent) changes to LTS-200-27/29 and LTS-200-10, to aid in user performance.

LaSalle Special Test Procedure LST-97-547 Revision 0, Unit 1 Pressure Regulation System Startup Test Procedure
The procedure provided instructions for testing the pressure regulator system of the Unit 1 Electro-Hydraulic Control (EHC) system during power ascension operations. It established that recommended pressure control system tuning parameters provided acceptable performance, demonstrated the backup capability of the pressure regulators by simulating a failure of the controlling pressure regulator, demonstrated that plant parameters remained within acceptable limits during pressure regulator induced transients, and verified variation in incremental regulation was within acceptable limits.

Revision to UFSAR Drawings per Drawing Change Request (DCR) 980634.
The DCR revised UFSAR Drawings M-101 Sheet 1 and M-147 Sheet 1 by assigning EPNs to existing components and corrected the nomenclature on instrument 1E51-R904 (Barometric Condenser Water Temperature) from pressure indicator (PI) to temperature indicator (TI). These changes were determined to be editorial and correction of a typographical error. UFSAR drawings M-101 Sheet 1 and M-147 Sheet 1 are revised accordingly.

UFSAR Revision to reflect GE ARTS Analysis and Idle Loop Startup Analysis
UFSAR Subsection 6.B.3.1 is revised to reflect General Electric's APRM – Rod Block Technical Specification improvement program, and for abnormal startup of an idle reactor recirculation loop. The GE ARTS analysis was previously implemented for LaSalle. UFSAR Subsection 6.B.3.1 was not revised during the implementation. Much of the discussion that describes all two loop transients as bounding single loop operation (SLO) transients is changed due to the recently discovered limiting nature of the idle loop startup event.

Isolate Unit 1 TSI Instrument Ground from EHC Instrument Ground per Design Change Package (DCP) 9800172.

The DCP installed optical isolators 1ISO-TS003-A/B in the Auxiliary Electric Equipment Room (AEER) panel 1PA07J between the total control valve and total bypass valve summer in AEER panel 1PA01J and turbine supervisory position indicator 1ZIY-TS003 in AEER panel 1PA07J. The current ground configuration for the Turbine Electro-Hydraulic Control (EHC) system and the Turbine Supervisory (TS) system instrumentation poses the potential for causing indication errors. The EHC and TS system instrumentation are both connected to ground but via different paths such that ground differentials have been observed between the instrument panels. The installation of the optical isolators will eliminate these observed ground differentials and potential indication errors.

Out-Of-Service (OOS) 960008947 and 980005198
OOS 960008947 and 980005198 provided administrative controls for the Unit 2 primary containment vent and purge system isolation valves to prevent their inadvertent operation while inboard isolation valves 2VQ031 and 2VQ034 were removed for maintenance. OOS 960008947 maintained drywell isolation valve 2VQ036 and bypass valve 2VQ068 in the normally closed position. OOS 980005198 maintained suppression chamber isolation valve 2VQ040 in the normally closed position.

Relocation of temperature sensors for 0VC01AB per Design Change Package (DCP) 9800138.
This design change rotated the temperature sensors for temperature controllers 0TC-VC050A and 0TC-VC050B. These sensors are attached to the outboard side of the Control Room HVAC Emergency Makeup Air Filter Electric Heating Coil (0VC01AB). The sensors, which are mounted flush with the heating coil, were rotated down approximately 45 degrees and into the flow of air through the heating coil. The 'B' train sensor alignment now matches the 'A' train.

Revise UFSAR drawing per Drawing Change Request (DCR) 980640.
This DCR revised UFSAR Drawing M-134 Sheet 1 to reflect that the 2B Fuel Pool Emergency Makeup Pump Discharge Pressure Gauge Sensing Line is connected between the discharge check valve (2FC044B) and the discharge isolation valve (2FC045B), and not upstream of the discharge check valve (2FC044B) as originally shown.
UFSAR drawing M-134 Sheet 1 is revised to correct the drawing to reflect how the line is connected in the plant.

UFSAR revisions per Unit 1 Design Change Package (DCP) 9800139, Replace 1B21-F569, Add Tee and Test Connection Assembly.
This DCP replaced existing isolation valve 1B21-F569 with a similar valve and added a test connection to provide an alternate method for testing the excess flow check valve

1B21-F571. A tee with two isolation valves and a cap were added between 1B21-F569 and 1B21-F571 to permit testing of 1B21-F571.
UFSAR Table 6.2-21 Sheet 1C was revised to reference new detail, Figure 6.2-31 (new sheet 10D) was added to show a new detail reflecting the addition of the tee valves and cap, and Drawing M-93 Sheet 5 was revised to add the tee and branch line with valves and cap.

UFSAR revisions per Document Change Request (DCR) 980716, Update Drawing M-1455 Sheet 1 to Reflect OOS for Pumps 1VR01PA/B.
The reactor building evaporative coolers have never worked effectively, are high cost maintenance items, and have not been used for some time. The evaporative cooler spray pumps are controlled by OOS #960001935.
UFSAR Sections 6.2.3.2, 9.4.2.1.2, 9.4.2.2, Table 9.4-5, and Drawing M-1455 Sheet 1 are revised accordingly.

Design Change Package (DCP) 9800182 left a portion of insulation off of valve 1E12-F050A. This is the shut down cooling mode train A testable check valve. An engineering evaluation found that a lack of full insulation was acceptable as a temporary condition, which is being tracked by temporary alteration (TALT) 1-0092-98.

UFSAR Revision Associated with Automatic Depressurization System (ADS) Logic Change
UFSAR Subsection 7.3.1.2.2.4 is revised to clarify that the manual ADS initiation circuits do not contain interlocks. Additionally, the last sentence of the first paragraph under "Manual Initiation (IEEE 279-1971 Paragraph 4.17)" in UFSAR Subsection 7.A.3.1.1.3 is deleted. The sentence to be deleted reads "The two switches have the a-c interlocks as a permissive." The changes correct wording associated with the manual ADS initiation circuits, and provides consistency with other UFSAR Sections and schematic drawings 1E-1(2)-4201AB and AH. Most of the UFSAR Sections affected by modifications 1-1-84-036 and 1-2-84-069 were revised at the time the modifications were implemented, but wording in Sections 7.3.1.2.2.4 and 7.A.3.1.1.3 was inadvertently missed. The current configuration of the ADS manual initiation circuits is consistent with the design intent and licensing basis approved by the NRC in License Amendments 29 and 27 for Units 1 and 2, respectively.

Revise UFSAR drawing per Drawing Change Request (DCR) 980691.
This DCR revised UFSAR drawing M-69 Sheet 2 to correct the specified line size for 0WS89A. The line was field verified to be 1 ½" rather than ½" as shown on the drawing.
UFSAR Drawing M-69 Sheet 2 is revised to show the as-built condition in the plant.

Revision to UFSAR Drawings M-90 Sheet 2 and M-115 Sheets 1 and 2 per Design Change Request (DCR) 980693.
The UFSAR drawings are revised to reflect as-built changes for components in the Reactor Building Closed Cooling Water (RBCCW) System associated with the Reactor Building process sample sink and sample coolers.

Revision to UFSAR Section 9.4.10 for the Containment Purge and Vent (VQ) System
UFSAR Section 9.4.10 is revised to more accurately describe the Containment Purge and Vent (VQ) System. When the function and operating modes of the system was changed prior to initial plant startup, the SAR was not revised to reflect the changes. This change reflects the use of the system for containment purge during power operation, and identifies the potential failure of the VQ ductwork should a LOCA occur during containment purging operations at power.

Revision to UFSAR Subsection 12.3.4.2 and Table 12.3-17 on Continuous Airborne Radioactivity Monitoring Instrumentation.
The specified flowrate for the Continuous Air Monitors (CAM) in UFSAR Section 12.3.4.2 is revised from "3 to 10 cfm" to "2 to 10 cfm", and Table 12.3-17 is revised to state that the CAM setpoints for the high radiation alarm are based on two times 100% power background. These changes provide consistency between continuous airborne radioactivity monitoring instrumentation and plant conditions.

1FW01PA Turbine Driven Reactor Feed Pump (TDRFP) Upgrade per Design Change Package (DCP) 9800140.
This DCP modified the 1FW01PA TDRFP radial end casing flange and seals. The work included repair of the pump casing flange surface (radial end), installation of a different spiral wound gasket between the pump casing and the breakdown bushing housing on both the radial and thrust ends of the pumps, installation of an additional full face fiber gasket between the pump casing and the radial breakdown bushing housing, and installation of hardened washers on both the radial and thrust end pump casing studs. This work was required to fix observed leakage and damage to the pump.

Revision to UFSAR Table 6.2-21
UFSAR Table 6.2-21 Sheets 2B and 10 are revised to reflect the correct location of remote manual switches 1(2)B33A-S800, S801, 802S, and S803 for the reactor recirculating flow control valve hydraulic power unit isolation valves 1(2)B33-F338A&B, F339A&B, F340A&B, F341A&B, F342A&B, F343A&B, F344A&B, and F345A&B are located in the auxiliary electric equipment room (AEER), rather than the main control room, and are capable of remote manual operation from there. Previously omitted data for valves 1(2)B33-F345A&B is added to Sheet 2B.

Addition of Oil Deflector to Instrument Nitrogen Compressor 1IN01CB per Design Change Package (DCP) 9800187
The DCP installed and oil splash guard (oil deflector) mounted around the piston rod of the instrument nitrogen (IN) drywell pneumatic air compressor. The splash guard deflects oil dripping off of the bottom half of the piston rod prior to the oil scraper rings. This enhances the ability of the oil scrapers to prevent oil from being carried over into the non-lubricated distance piece.

Revision to Technical Specification Bases 3/4.7.7
The last sentence in Technical Specification Bases 3/4.7.7, which states that the area temperature limits include an allowance for instrument error of ±7 °F, is deleted. The area temperature limitations specified in Technical Specification Table 3.7.7-1 ensure that safety-related equipment is not subjected to temperatures in excess of environmental qualification (EQ) temperatures. As stated in the bases discussion, exposure to excessive temperatures may degrade equipment and can cause loss of its operability. A review of associated EQ documentation indicates that the current EQ calculations do not include any allowance for instrument error. A review of selected vendor documentation also failed to show any consideration for instrument error. These values are considered analytical limits based on either EQ calculations for harsh environments or vendor environmental specifications. Therefore, the bases discussion relative to instrument error for these area temperature limits is considered not technically justified, and is deleted.

As-Built Drawing Change Request (DCR) for Drawings M-87 Sheets 1 and 2 and M-134 Sheets 1 and 2
A drawing change was initiated for the subject drawings to assign new equipment part numbers (EPNs) for RHR service water and diesel generator cooling water pump vent valves 0DG056, 1&2DG112, and 1&2E12-F462A, B, C, D. The valves were not previously designated with assigned numbers. UFSAR drawings M-87 Sheets 1 and 2 and M-134 Sheets 1 and 2 are to be revised.

Prolonged Out-of-Services (OOS) 970011578, 970003154, and 980008414.
The OOS were in effect for a prolonged period of time. The clean gland water tank 0WG01T was placed OOS, with the tank mechanically isolated and the associated tank level alarm annunciators deactivated. OOS 970011578 for the mechanical isolation and OOS 980008414 for the annunciators, remains in effect until the installation of design change packages 9600491 and 9600492, Unit 1 and 2 gland water cooling pump demolition phase activities. The tags on valves 2WG001A/B/C were to remain in place per OOS 970003154 at least until the downstream line is cut and capped.

Revision to UFSAR Section 13.1.1.3
UFSAR Subsection 13.1.1.3, Qualifications of Management and Technical Support Organization, defines the qualifications of support personnel (off-site ComEd personnel). Although historically accurate, this summary didn't reflect the present qualifications of support personnel. UFSAR Subsection 13.1.1.3 is revised to provide both a historical and a current perspective.

Revision to UFSAR Subsection 7.8.2 for the Safety Parameter Display System (SPDS)
UFSAR subsection 7.8.2 is revised to reflect standardized Nuclear Utility Management Resources Council (NUMARC) emergency action levels (EAL) information previously approved in accordance with Regulatory Guide 1.101.

Revision to UFSAR Table H.4-78
Design Change Package (DCP) 9600115 installed instrumentation cable 1HP297 between Diesel Generator (DG)-1B panels 1H22-P028 and 1E22-P301B in the Division 3 DG room. The DCP did not identify this cable as a safe shutdown cable. UFSAR Table H.4-78, "Safe Shutdown Equipment Located in Fire Zone 7B1", is appropriately revised.

Revision to UFSAR Appendix H Tables
UFSAR Tables H.4-67 (Safe shutdown equipment located in fire zone 4FI - Division 1 ESF Switchgear Room) and H.4-68 (Safe shutdown equipment located in fire zone 4F2 - Division 1 ESF Switchgear Room) are revised to achieve consistency with design bases drawings. In Table H.4-67, cable 1DC012 is replaced with cables 1DC128, 1DC129, 1DC130, 1DC131, 1DC132, 1DC133, 1DC134, and 1DC135. In Table H.4-68 cable 2DC050 is deleted, and cable 2DC012 is replaced with cables 2DC128, 2DC129, 2DC130, 2DC131, 2DC132, 2DC133, 2DC134, 2DC135.

The following cables are deleted from the associated UFSAR Tables.
Cable 1NBE44 from Table H.4-14 (Safe shutdown cables located in the fire subzone 2E-2).
Cables 1NBE45 and 46 from Table H.4-13 (Safe shutdown cables located in the fire subzone 2E-1).
Cable 2NBE44 from Table H.4-16 (Safe shutdown cables located in the fire subzone 3E-2).
Cables 2NBE45 and 46 from Table H.4-15 (Safe shutdown cables located in the fire subzone 3E-1).

The safe shutdown cables listed in UFSAR Tables H.4-67 and H.4-68 did not agree with the previous design bases drawings.

Cable 1DC012 was replaced with cables 1DC128, 1DC129, 1DC130, 1DC131, 1DC132, 1DC133, 1DC134, 1DC135 per modification M01-1-88-001, which replaced the Unit 1 250VDC Division 1 battery (1DC01E).

The Unit 2 250VDC Division 1 battery (2DC01E) was replaced under modification M01-2-88-001, replacing cable 2DC012 with cables 2DC128, 2DC129, 2DC130, 2DC131, 2DC132, 2DC133, 2DC134, 2DC135.

Modification M01-2-88-004 replaced the Unit 2 125VDC Division 1 battery (2DC07E), deleting cable 2DC050.
The above modifications were installed in the early 90's and all are operable. The associated omitted the revision to the Safe Shutdown sections of the UFSAR.

Cables 1NBE44, 45, 46, and 2NBE44, 45, 46 were added to UFSAR Appendix H in the UFSAR Revision 7 1991 update. These cables are deleted as they were never installed as part of modifications M01-1-87-097 and M01-2-87-085, or any other plant modifications, as the cable numbers were reserved for these modifications. The removal of these cables corrects the UFSAR tables to agree with design bases.

Reconfiguration of Unit 1 Reactor Core Isolation Cooling (RCIC) Condensate Pot Level Control, Steam Trap, and Rupture Disks to Prevent Disk Blowout, Design Change Package (DCP) 9800227
The Unit 1 RCIC exhaust rupture disk assembly was removed from the top of the RCIC downstream drain pot and relocated further downstream of the RCIC turbine to reduce the potential for disk ruptures due to pressure oscillations and wet steam impingement during system startup. The RCIC upstream drain pot level control switch 1E51-N010 was relocated to avoid interference and to improve level control. The condensate pot steam trap orifice was replaced with a smaller diameter orifice. The instrument line, valves, and components for the pressure switch 1E51-N012A/B/C/D for the between rupture disk pressure sensor were relocated.
Repeated rupture disk blow outs have occurred during RCIC fast start tests due to unanticipated water hammers or wet steam impingement on the rupture disks. These blow outs create a steam leak to the reactor building and breach the RCIC exhaust pressure boundary. The steam is radiolytic and creates a potential release and personnel hazard/exposure problem, as well as challenging the operability and safety functions of the RCIC system. Further, the leak detection system responds to these leaks by isolating RCIC and is unavailable if needed. These changes are intended to prevent recurrence of the blowout problem. UFSAR Drawing M-101 Sheet 1 (RCIC system) is revised.

UFSAR drawing 1E-1-4602AJ was updated per Unit 1 Design Change Package 9700596.

Revision to UFSAR Sections 7.6.3 and 7.7.6
UFSAR subsections 7.6.3.2.2, 7.6.3.3.2, 7.7.6.1.2, 7.7.6.2.2, 7.7.6.3.2 and 7.7.6.4.2 are revised to provide needed flexibility in the application of new calibration techniques and station specific commitments to test and calibration procedures for the associated neutron monitoring systems, and to correct a spelling error in UFSAR subsection 7.7.6.1.3. The UFSAR previously stated that tests and calibrations are performed in accordance with procedures contained in system instruction manuals. Conversely, station procedures are used for test and calibration. These procedures are based on the recommended methods from the system instruction manual, industry standard techniques, and requirements specific to LaSalle. This revision corrects the overly restrictive UFSAR wording and brings it into compliance with Tech Spec requirements for specific stations procedures for these test and calibration activities.

As-Built Drawing M-83 Change Request for Unit 1 B Diesel Generator (DG) A Starting Air Compressor Continuos Air Pressure Switch 1E22-N506 Root Valve 1E22-F372A
A Drawing Change Request (DCR) was required to assign a new equipment part number (EPN) for root valve 1E22-F372A and to incorporate the valve in to the drawing. The root valve is on a ¼" air pressure sensing line between the common discharge header of air receivers 1E22-T302A and 1E22-T302C and 1B DG (Train A) Starting Air Compressor Continuous Air Pressure Switch 1E22-N506. Drawing M-83 sheet 1 for the diesel generator auxiliary system is to be revised.

Installation of pulsation dampener on 2PI-DG101 Sensing Line per Design Change Package (DCP 9200204 Revision 1)
A pulsation dampener (snubber) was installed on the sensing line to pressure gauge 2PI-DG101 at the base of the gauge to minimize oscillations. This was done to permit obtaining accurate gauge readings to ensure the performance and reliability of diesel generator cooling water pump 2A (2DG01PA). Inaccurate gauge indication, rapid degradation of the gauge internals, and gauge calibration can result from oscillations during normal system operation. The snubber prevents these oscillations.

Replacement of Reactor Recirculation (RR) system snubbers per Design Change Package (DCP) 9800255
The DCP replaced mechanical snubbers M09-RR00-1001S and M09-RR00-1003S of the reactor recirculation system with hydraulic snubbers. The hydraulic snubbers are better suited to an environment of high frequency low amplitude vibrations, which are typically flow induced.

Revision to UFSAR Chapter 13, Section 13.2, Training
The UFSAR is returned to the level of detail required by the Generic Letter 80-110 and Regulatory Guide 1.70. This revision modifies the description in the UFSAR of the following programs within the Training Department: 1) New Employee Orientation, 2) Nuclear General Employee Training, and 3) Replacement Training of Certain Specialties (Mechanical Maintenance, Electrical Maintenance, Instrument Maintenance, Radiation Protection Technicians, and Maintenance Supervisors).

"INPO" is replaced with "the National Academy for Nuclear Training" where applicable.

The revision also implements changes to the New Employee Orientation program to standardize this program across all ComEd sites, and removes the requirement for Staff (Non-Licensed) System Description training.

Installation of 250 Volt Division 1 Battery 1DC01E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800237
The DCP installed a time delay relay for the 250 volt division 2 battery 1DC01E to the output of the high discharge battery alarm 1IY-DC043 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

Installation of 125 Volt Division 1 Battery 1DC07E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800238
The DCP installed a time delay relay for the 125 volt division 1 battery 1DC07E to the output of the high discharge battery alarm 1IY-DC045 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

Installation of 125 Volt Division 2 Battery 1DC14E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800239
The DCP installed a time delay relay for the 125 volt division 2 battery 1DC14E to the output of the high discharge battery alarm 1IY-DC047 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

Installation of 125 Volt Division 3 Battery 1DC18E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800240
The DCP installed a time delay relay for the 125 volt division 3 battery 1DC18E to the output of the high discharge battery alarm 1E22-K503 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

As-Built Drawing Change Request Tip Purge Valve Assembly 2C51-J009

Drawing M-66 Sheet 3, Unit 2 Drywell Pneumatic System, was revised to reflect the as-built condition of the traversing incore probe (TIP) purge valve assembly 2C51-J009. The valve assembly was previously modified to reflect changes shown in General Electric (GE) Field Disposition Instruction (FDI) dated 2/11/82. The FDI added a new purge air control panel, modified TIP purge equipment, and index mechanisms. The upgrade to the purge system protects the TIP detectors and other components from dependence upon the quality of installation.

UFSAR change associated with Chem-Nuclear Systems Procedure DM-OP-043-41314 Revision 1, Operating Procedure For CNS High Flow Dual Train System At LaSalle Station
The procedure provides instructions for the setup, operation, and removal of the CNS High Flow Dual Train System (HFDTS) at LaSalle Station. A portion of the vendor processing system is moved from the radwaste building truck bay to the south low level storage area. A redundant train was added to the vendor processing system. UFSAR Section 11.4 is revised to reflect system operation in the south low level storage area.

Installation of B Train VC/VE Backdraft Dampers per Design Change Package (DCP) 9800195
The DCP added manual backdraft dampers 0VC73YB and 0VE80YB in the normal outside makeup air lines for the 'B' train Control Room (VC) and Auxiliary Electric Equipment Room (VE) HVAC systems at elevation 802' in the Auxiliary Building. The dampers were added to prevent back flow of air during emergency makeup filter unit operation. New ductwork support S-3077 was installed to accommodate the additional loading on the VE ductwork due to the addition of damper 0VE80YB. Drawings M-1443 sheets 1 and 3 are to be revised.

UFSAR Update for the inclusion of a holdup volume in the pathway for unidentified leakage to reach the Drywell Floor Drain Sump (DWFDS)
UFSAR Subsections 3.8.3.1.1 and 5.2.5.5.4 were revised for the reactor coolant pressure boundary leakage detection system to include the addition of holdup volume caused by the irregularities in the drywell floor. The UFSAR didn't previously provide definitive information as to the potential of a holdup volume of water due to irregularities in the drywell floor and the effect on the design basis for the leakage detection system in the drywell.

Installation of High Point Vent on Stator Cooler Service Water Outlet Line 1WS12A-12" per Design Change Package (DCP) 9800197
The DCP installed a 3/4" vent valve to line 1WS12A-12" to allow for proper venting of the high point of the line. Proper venting of the line mitigates pipe rumbling, and will

prevent damage to the line and supports resulting from water hammer. Drawing M-69 Sheet 2 is revised.

As-Built drawing change to M-88 sheet 3 and M-135 sheet 3
Unit 1 and 2 Off Gas system drawings do not reflect plant configuration, as valve 2N62-F422 does not exist. The valve will be eliminated from the UFSAR drawing M-135 sheet 3. The piping flow path will be altered on M-88 sheet 3 and M-135 sheet 3. Revising the drawings to reflect as-built plant configuration will resolve the conflict. UFSAR Drawings M-88 sheet 3 and M-135 sheet 3 will be revised to reflect as-built plant configuration.

UFSAR revisions per Unit 2 Design Change Package (DCP) 9800276 – "Loss of Coolant Accident (LOCA) / Purge Analysis."
This DCP analyzed and modified the VQ piping system as a result of postulating a LOCA during containment purge. During investigation of LER 97-005, it was discovered that in the event of a LOCA coincident with containment purging, the VQ ductwork could potentially rupture and VQ piping downstream of the VQ Containment Isolation Valve could experience temperature increases beyond the originally analyzed conditions. The required support modifications for Unit 2 were performed per this DCP following the completion of the thermal modes analysis for the Unit 2 VQ and VG piping, supports, and penetrations. UFSAR sections 3.0, 3.11.1.1, and Tables 3.11-28 and Table 3.11-29 are revised as a result of this design change.

Design Change Packages (DCPs) DCP 9600216 and 9600217 for the Unit 1 "A" and "B" Turbine Driven Reactor Feed Pump Rooms (TDRFP) for the following: Clarify that the equipment supports are not safety-related (all supports are classified as non-safety related and seismically qualified, and safety-related work associated with the supports is limited to installation of the expansion anchors drilled into the safety-related walls and floors); Correct inadvertent checking of multiple blocks in a question on the previous safety evaluation form; Remove operability holds; and, Correct minor grammatical and administrative errors.

LaSalle Operating Procedure LOP-HW-03 Revision 0, Hydrogen Water Chemistry Shutdown
The procedure was issued to provide guidance for placing the hydrogen water chemistry system in a shutdown condition.
LaSalle Operating Procedure LOP-HW-01M Revision 0, Unit 1 Hydrogen Water Chemistry System Mechanical Checklist
The procedure was issued to establish an initial system line-up for the Unit 1 hydrogen subsystem of the hydrogen water chemistry system.
LaSalle Operating Procedure LOP-HW-01E Revision 0, Unit 1 Hydrogen Water Chemistry System Electrical Checklist
The procedure was issued to establish an initial system line-up for the Unit 1 hydrogen water chemistry system.
LaSalle Operating Procedure LOP-HW-03M Revision 0, Unit 1 Hydrogen Water Chemistry Oxygen System Mechanical Checklist
The procedure was issued to establish an initial system line-up for the Unit 1 oxygen subsystem of the hydrogen water chemistry system.

Revision to UFSAR Table 13.1-1
The UFSAR Table 13.1-1 title of Radiation Protection Manager is replaced with Health Physics Supervisor. The statement allowing that a technical person reporting to the Health Physics Supervisor may qualify for the position of Radiation Protection Manager is deleted. This change reflects the more restrictive requirements of Technical Specifications.

Addition of Test Tap to Relief Valve 2E12-F088C per Design Change Package (DCP) 9500425
The DCP added a test tap to the outlet flange of Emergency Core Cooling System (ECCS) relief valve 2E12-F088C. The test tap provides a means of performing a local leak rate test (LLRT) of the outlet flanged connection in lieu of an integrated leak rate test (ILRT). Leak rate testing is required because the valve and the flanged connection are part of the primary containment pressure boundary. Additionally, the flanged joint must be tested to verify its pressure integrity whenever the valve is removed for calibration or maintenance. The pressure tap results in substantial time savings as the effort to perform a LLRT is substantially less than the effort to perform a ILRT.

Addition of Test Tap to Relief Valve 2E21-F031 per Design Change Package (DCP) 9500428
The DCP added a test tap to the outlet flange of Emergency Core Cooling System (ECCS) relief valve 2E21-F031. The test tap provides a means of performing a local leak rate test (LLRT) of the outlet flanged connection in lieu of an integrated leak rate test (ILRT). Leak rate testing is required because the valve and the flanged connection are part of the primary containment pressure boundary. Additionally, the flanged joint must be tested to verify its pressure integrity whenever the valve is removed for calibration or maintenance. The pressure tap results in substantial time savings as the effort to perform a LLRT is substantially less than the effort to perform a ILRT.

Unit 2 Reactor Building Ventilation System Isolation Logic Power Supply Modification per Design Change Package (DCP) 9500477
The DCP changed the power supply for the Unit 2 Group IV isolation logic from the reactor protection system (RPS) AC to 125 VDC to prevent isolation of the reactor building ventilation system upon loss of a single RPS bus. UFSAR subsection 7.3.2.2.1, Figure 7.3-10, and Table 8.3-13 are revised.

Unit 2 Design Change Packages (DCP) 9500487, Relocate Main Steam Tunnel Thermocouples, and 9500488, Main Steam Tunnel Leak Detection Logic Change
DCP 9500481 relocated ten thermocouples in the main steam tunnel (MST) leak detection system, and changed their high differential temperature setpoints. DCP 9500482 made two significant changes to the MST leak detection system. Permanent jumpers were installed to eliminate the Group 1 Main Steam Line isolation function associated with high ambient temperature in the MST. Key-lock bypass switches were installed in the control room to allow bypassing the Group 1 isolation logic associated with high differential temperature in the MST. The switches replace the temporary jumpers previously used. The design changes significantly reduce the risk of inadvertent reactor scrams related to the MST leak detection system response to Reactor Building Ventilation System (VR) operating transients. The DCPs were installed to implement licensing amendment No. 96 to Unit 2 license NPF-18. The associated UFSAR changes were incorporated in UFSAR Revision 12 due to Unit 1 DCPs 9500481 and 9500482.

Upgrade of Unit 2 Reactor Recirculation Flow Control Valves per Design Change Package (DCP) 9600156
The DCP upgraded reactor recirculation flow control valve 2B33-F060A and B position monitoring by providing redundant rotary variable differential transformer (RVDT) based valve position indication in addition to the linear variable differential transformer (LVDT) based valve position indication to be selectable by a selector switch, upgraded the (LVDT) based valve position indication

instrumentation, and upgraded cable connections for linear velocity transducer (LVT) based flow control valve velocity fedback monitoring instrument loops. UFSAR Section G.5.2.3.4.11 is accordingly revised.

Design Change Package (DCP) 9600198, Unit 2 Division 2 Residual Heat Removal - Service Water Keep Fill Cross-Tie
The DCP added two cross-ties to Division 2 of the Unit 2 residual heat removal (RHR) - service water (WS) system to ensure that it is kept filled and pressurized. One cross-tie is from the service water system, the other is from the diesel generator cooling water (DGCW) system.
The cross-tie from WS will keep the RHR-WS system filled during normal operation, while the cross-tie from the DGCW will keep it filled in the event of an accident, Loss of Offsite Power (LOOP), or seismic event.
UFSAR Sections 7.3.3.3.1, 9.2.1.2, 9.2.1.5, 9.2.2, and 9.2.2.2 are revised to include a discussion of the keep fill for Unit 2 Division 2 RHR-WS, addressing an overview of the keep fill system, interfaces with DGCW, and alarm annunciation.

Design Change Package (DCP) 9600284, Elimination of Unit 2 Main Steam Isolation Valves Closure and Scram Functions of the Main Steam Line Radiation Monitors
The DCP improves unit availability by reducing spurious scrams and isolations caused by the Main Steam Line Radiation Monitors (MSLRMs). The original design function of the MSLRM was for detection/mitigation of consequences associated with fuel failure and the rod-drop design basis accident. The DCP consisted of the following: removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Protection System (RPS) Reactor Auto-Scram Trip logic circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Main Steam Line (MSL) MSL Isolation and Drain Valve circuits, removing the High-High Radiation and Inoperative Trip interlocks from MSLRMs to Reactor Water Sample Valve circuits and associated Normal/Test Selector Switches in Main Control Room (MCR) Panels, revising MSLRM's High and High-High alarm setpoints, rewiring MSLRM alarms per recommendation of ComEd Human Factors Group and Operations, rewiring computer digital inputs and outputs associated with the MSLRMs, revising off gas pre-treatment radiation monitor High and High-High alarm setpoints, and add appropriate safety-related banana plugs per ComEd recommendation to one terminal at relays located in the Main Control Room panels. UFSAR Sections 1.2, 7.1, 7.2, 7.3, 7.6, 7.7, 7.A, 11.5, 15.2, and 15.4 are revised.

Reactor Recirculation System Primary Containment Isolation Valves Upgrade per Design Change Package (DCP) 9600412
The DCP upgraded the actuators of reactor recirculation system process sampling primary containment isolation valves 2B33-F019 and 2B33-F020to ensure appropriate

valve seat closing forces to prevent internal valve and system degradation. This improves reliability and proper performance of the valves without impacting the function of the valve actuator and system performance. A revision to drawing M-139 sheet 2, Unit 2 nuclear boiler and reactor recirculating, is required.

Drywell Pneumatic Primary Containment Isolation Valves Upgrade per Design Change Package (DCP) 9600414
The DCP upgraded the actuators of drywell pneumatic primary containment isolation valves 2IN001A, 2IN001B, 2IN017, 2IN074, and 2IN075 to ensure appropriate valve seat closing forces to prevent internal valve and system degradation. This improves reliability and proper performance of the valves without impacting the function of the valve actuator and system performance. A revision to drawing M-66 sheet 3, Unit 2 drywell pneumatic system, is required.

Unit 1 EHC Scram Reduction: Stator Cooling Runback Logic Scheme per Design Change Package (DCP) 9800351
The DCP installed a redundant trip system for temperature, pressure, and flow parameters to reduce the number of false trips produced by the Unit 1 turbine runback system. This upgrade included the removal and replacement of temperature indicator 1TI-GC003, temperature element 1TE-GC003, new flow switch 1FS-GC045, and activation of existing pressure switch 1PS-GC021A.

Addition of Drain Connection to Pipeline 2RH83AA-20" per Design Change Package (DCP) 9700149
The DCP installed a 4" drain connection to pipeline 2RH83AA-20", which was used to dewater the piping to permit repairs to Residual Heat Removal (RHR) valve 2E12-F068A.

Repairs to Valve 2E12-F068A per Design Change Package (DCP) 9700145
The DCP repaired the internals of Residual Heat Removal (RHR) valve 2E12-F068A which included: replacing the carbon steel valve disc with a stainless steel disc to minimize corrosion; replacing the carbon steel disc guides with carbon steel disc guides which are stellite faced, in order to minimize wear; replacing the stainless steel valve stem with a stem of differing grade of stainless steel; replacing the spiral wound stainless steel asbestos bonnet gasket with a spiral wound stainless steel graphite filled gasket, due to the discontinued availability and use of asbestos due to its health hazards; replacing the stem nut, bonnet studs, and bonnet nuts like-for-like.

Repairs to Valve 2E12-F068B per Design Change Package (DCP) 9700146
The DCP repaired the internals of Residual Heat Removal (RHR) valve 2E12-F068B which included: replacing the carbon steel valve disc with a stainless steel disc to

minimize corrosion; replacing the carbon steel disc guides with carbon steel disc guides which are stellite faced, in order to minimize wear; replacing the stainless steel valve stem with a stem of differing grade of stainless steel; replacing the spiral wound stainless steel asbestos bonnet gasket with a spiral wound stainless steel graphite filled gasket, due to the discontinued availability and use of asbestos due to its health hazards; replacing the stem nut, bonnet studs, and bonnet nuts like-for-like.

Addition of Drain Connection to Pipeline 2RH083AA-20" per Design Change Package (DCP) 9700149
The DCP installed a 4" drain connection to pipeline 2RH083AA-20", which was used to dewater the piping to permit repairs to Residual Heat Removal (RHR) valve 2E12-F068A.

Addition of Drain Connection to Pipeline 2RH083BB for Dewatering 2E12-F068B, Design Change Package (DCP) 9700150
The DCP installed a 4-inch drain connection to pipeline 2RH083BB used for dewatering the piping to support repairs to the internals of residual heat removal (RHR) valve 2E12-F068B.

Design Change Package (DCP) 9600567, Modification to Diesel Generator 2B Voltage Regulatory Circuit Wiring
The DCP revised the 2B diesel generator voltage regulating circuit so that it functions as designed following the replacement of the generator voltage raise and lower assembly, voltage regulator device, and the removal of the volts per cycle device. The replacement of the voltage regulator and the removal of the volts per cycle device was required due to aging and near term non-functionality of the of previous voltage regulator.

Replacement of the Residual Heat Removal Service Water Liquid Process Radiation Monitor Probe, Design Change Package (DCP) 9700527
The DCP replaced liquid process radiation monitor probe 2E12-N511, which monitors the Division 2 residual heat removal (RHR) heat exchanger 2B service water discharge. The previous probe failed due to flow induced vibration. The new probe is a design which is shorter in length, and utilizes an open end with a forty-five degree elbow. The new probe is assigned specialty part number 1E12-D329. Drawing M-134 is revised.

Unit 2 Electro-Hydraulic Control Oil Trip Test Logic Setpoint Change per Design Change Package (DCP) 9600373
The DCP changed the time delay settings of two relays and installed a jumper in another relay of the main turbine trip reset circuits to provide more time to ensure that reset proceeds to completion when actuated.

Design Change Package 9600456, Unit 2 Circulating Water Pump Gland Water Modification
The DCP changed the source of the Circulating Water (CW) pumps gland water supply (for cooling the lower bearing and lubricating the stuffing box). The new source is from the discharges of the existing Service Water strainers located in the Lake Screen House. The previous source was the Clean Gland Water Head Tank (located at Aux. Building, 786 feet). The service water is further strained through a new automatic backwash strainer to ensure cleanliness of gland water to the packing and lower bearing of the CW pumps. The original piping had become plugged with corrosion products over the years and is resolved by the installation of the new system. The proposed changes to UFSAR subsections 1.2.3.6.3 and 9.2.2.2 were previously incorporated due to installation of DCP 9600455, Unit 1 Circulating Water Pump Gland Water Modification.

Design Change Package (DCP) 9600462, Deletion of Timer Interlock for Valve 2E12-F04A
DCP 9600462 changed the interlock that prevents closure of RHR heat exchanger bypass valve 2E12-F048A during a LOCA from a 10 minute interlock to a permissive interlock. This allows cooling of the RHR LPCI injection by the RHR heat exchanger immediately rather than wait 10 minutes. The control circuit was also modified such that thermal overloads are always bypassed whenever an accident signal is present. UFSAR subsection 7.3.1.2.4.6 is revised.

Design Change Package (DCP) 9600463, Deletion of Timer Interlock for Valve 2E12-F048B
DCP 9600463 changed the interlock that prevents closure of RHR heat exchanger bypass valve 2E12-F048B during a LOCA from a 10 minute interlock to a permissive interlock. This allows cooling of the RHR LPCI injection by the RHR heat exchanger immediately rather than wait 10 minutes. The control circuit was also modified such that thermal overloads are always bypassed whenever an accident signal is present. UFSAR subsection 7.3.1.2.4.6 is revised.

Design Change Package 9600546
Unit 2 Main Turbine and Reactor Feedwater Pumps Level 8 Trip Logic Control Modification
The DCP added an interlock from the Unit 2 Reactor Core Isolation Cooling (RCIC) Division 1 level 8 trip relay 2B21A-K705AX to Channel C trip logic of the Main turbine / Feedwater pumps trip. This change allows the RCIC Division 1 level 8 trip to actuate the 'C' channel main turbine / feedwater pumps level 8 trip.

UFSAR Figure 7.7-5 Sheet 1 and Subsection 7.7.4.2.1 are revised to reflect the DCP.

Administrative Technical Requirements (ATR) Amendment 19.
ATR Amendment 19 incorporated changes to ATR Tables 3.6.3-1 and 3.6.3-2 to achieve compliance with previously evaluated UFSAR changes.
The maximum isolation time for the reactor water cleanup isolation valves 1G33-F001 and 1G33-F004 is revised in ATR Table 3.6.3-1.
ATR Tables 3.6.3-1 and 3.6.3-2 were revised for the respective Unit 1 and 2 valves.
Primary containment ventilation relief valves 1VP197A, 1VP197B, 1VP198A, and 1VP198B, residual heat removal system relief valve 1E12-F460, reactor building closed cooling water relief valves 1WR225 and 1WR226, reactor recirculation system relief valve 1B33-F395, and high radiation sampling system containment air sampling isolation valves 1CM085, 1CM086, 1CM089, 1CM090 were added to ATR Table 3.6.3-1.
High radiation sampling system containment air sampling isolation valves 2CM085, 2CM086, 2CM089, and 2CM090 were added to ATR Table 3.6.3-2.

Revision of the Thermal Overload Bypass of Residual Heat Removal (RHR) Motor Operated Valves per Design Change Package (DCP) 9700028
The DCP implemented the corrective actions identified in Licensee Event Report (LER) 96-022, Revision 0, for the thermal overload bypass logic of the Engineered Safety Features (ESF) Division 2 motor operated valves (MOVs).
The control circuits of MOVs 2E12-F024B, 2E12-F027B, 2E12-F042B, and 2E12-F042C were modified to ensure that the thermal overloads are bypassed whenever a LOCA signal is present. The modified logic removed the interlock between the thermal overload bypass circuit and the manual override circuit, such that the thermal overload bypass logic is only interlocked with the high drywell pressure and low reactor level (i.e., LOCA) logic.

Suppression pool strainer replacement per Design Change Package (DCP) 9700547
The DCP replaced the high pressure core spray (HPCS) suppression pool suction strainer to increase the surface area with a larger capacity strainer to reduce pump net positive suction head. UFSAR subsections 15.9.3.7 and 15.9.5, and Figures 6.3-3, 6.3-6, and 6.3-9 are revised.

Suppression pool strainer replacement per Design Change Package (DCP) 9600291
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 "A" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce

pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). UFSAR subsections 15.9.3.7 and 15.9.5, and Figures 6.3-3, 6.3-6, and 6.3-9 are revised.

Suppression pool strainer replacement per Design Change Package (DCP) 9700543
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 "B" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Figure 6.3-9 and Subsections 15.9.3.7 and 15.9.5 are revised.

Suppression pool strainer replacement per Design Change Package (DCP) 9700544
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 "C" residual heat removal (RHR) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Figure 6.3-9 and Subsections 15.9.3.7 and 15.9.5 are revised.

Suppression pool strainer replacement per Design Change Package (DCP) 9700545
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 Reactor Core Isolation Cooling (RCIC) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Subsection 15.9.3.7 and 15.9.5 are revised.

Suppression pool strainer replacement per Design Change Package (DCP) 9700546
The DCP replaced the emergency core cooling system (ECCS) suction strainer on the Unit 2 low pressure core spray (LPCS) system suction line in the suppression pool. The replacement strainer has increased capacity to reduce

pump net positive suction head (NPSH) loss due to accumulated strainer debris resulting from a design basis leak or loss of coolant accident (LOCA). The strainer surface area is increased, as is the available flow area of the strainer. The strainer installation partially addresses the actions required by NRC Bulletin 96-03. UFSAR Figure 6.3-6 and Subsection 15.9.5 are revised.

Modify mounting for Primary Containment Cooler Fans 2VP02CA/B per Unit 2 Design Change Package (DCP) 9600569
Vibration isolators installed for the primary containment cooler fans 2VP02CA/B were not capable of carrying seismic loads. During an investigation it was noted that the housing itself was not qualified for the seismic loads resulting from the fan on its roof. This DCP installed new vibration isolators capable of transferring seismic loads from fans 2VP02CA/B and reinforced the VP housing so that it is acceptable for seismic loads resulting from the fan and its self-weight.

Design Change Package (DCP) 9700398, Turbine Building Supply Airflow Reduction for Turbine Building Negative Pressure
The DCP reduced the supply air to the Turbine Building to ensure a negative pressure is maintained by installing two recirculation dampers on the common supply header of the turbine building ventilation (VT) system supply fans 2VT01CA, 2VT01CB, and 2VT01CC. The dampers are installed in the supply air header before it penetrates the VT system supply air housing. UFSAR Sections 9.4 and 11.3 are revised.

Design Change Package 9700568, 2B Diesel Generator Ventilation Intake Dampers Modification
DCP 9700568 installed a warm weather manual bypass blade in the two ventilation intake dampers of the 2B diesel generator (DG) ventilation equipment room. The bypass blade was installed to allow in-leakage of outside air into the DG room during the summer per original design. UFSAR Sections 9.4 and 9.5 are revised.
Unit 2 Division 1 Low Pressure Coolant Injection (LPCI) Pump Discharge Pressure Automatic Depressurization System (ADS) Permissive Setpoint Change per Design Change Package (DCP) 9700619;
Unit 2 Division 2 Low Pressure Coolant Injection (LPCI) Pump Discharge Pressure Automatic Depressurization System (ADS) Permissive Setpoint Change per Design Change Package (DCP) 9700620;
Unit 2 Low Pressure Core Spray (LPCS) Pump Discharge Pressure Automatic Depressurization System (ADS) Permissive Setpoint Change per Design Change Package (DCP) 9700621;
Procedure LIS-RH-401A, Unit 2 RHR A (LPCI Mode) Pump Discharge Pressure ADS Permissive Functional Test;

Procedure LIS-RH-401B, Unit 2 RHR B & C (LPCI Mode) Pump Discharge Pressure ADS Permissive Functional Test
During the System Functional Performance Review, it was determined that pump discharge ADS permissive setpoints did not account for head correction. The DCPs affect instruments 2E12-N016A, B, C, 2E12-N019A, B, C, 2E21-N001, and 2E21-N009. The DCPs do not physically change any instrumentation hardware, as the nominal calibration setpoints are changed to account for elevation differences between the instruments and the process points on the discharge lines.
The LIS-RH-401A and LIS-RH-401B procedures are revised to incorporate adjustments for head corrections.

Modification to Unit 2 Containment Leak Test Channels per Design Change Package (DCP) 9800042
The DCP removed eighteen leak test plugs for the leak test system around the Unit 2 safety relief valve (SRV) pipe support embedment plates at the containment wall above elevation 700' -0" in the Unit 2 suppression pool. The DCP also clarifies that all other test plugs in the suppression pool and the containment drywell may be permanently left in place. The leak-test channels were originally installed over containment liner welds so that these welds could be pressure tested to verify leak-tightness. Threaded plugs were installed in openings in these leak-test channels to facilitate this pressure testing. It was the intent of the original design that these plugs be removed after these local leakage tests were complete so that during future Containment Integrated Leak Rate Tests (CILRT), the liner welds would see the test pressures. The leak-test channels and plugs were not designed to act as the containment pressure boundary. Licensee Event Report (LER) 97-030 documents that the plugs were not removed as originally intended after the initial local leak rate tests. UFSAR Subsections 6.2.1.1.2 and 6.2.6.1 are revised.

UFSAR Revision to Section 9.5
Section 9.5 revisions consist of: providing general clarifications; reflect Nuclear Mutual Limited (NML) now being known as Nuclear Electric Insurance Limited (NEIL); deleting the north service building; identifying that <u>manual</u> deluge systems are operated only locally (not from the control room); identifying that fire protection is relocated from the Technical Specification to Administrative Technical Requirements; clarified overall fire protection responsibilities, and rewriting the communication systems description.
Appendix H revisions consist of: updated transient fire loadings; documenting installed safety-related and radioactive equipment which was not previously identified; deleted fire zone designations 9A – 9E as fire zone 9 is no longer addressed by the fire hazards analysis; updated design fire loads, combustible materials loading, fire detection equipment, and fire protection equipment for the majority of fire areas and zones; updated valve positions; corrected cable numbers; and revised safe shutdown components as required for each fire

area/zone. These changes will be incorporated in the UFSAR Revision 14 update.

Revision to Unit 1 and 2 Tech Spec Bases Section 2.1.4 and Figure B 3/4 3-1
UFSAR Figures 5.2-2 and 5.3-5
An amendment to Bases Section 2.1.4 was evaluated to more thoroughly describe the top of active fuel and the manner in which it is used.
An amendment to Figure B 3/4 3-1 evaluated revising the instrumentation values on the figure to reflect the correct configuration. This activity corrects the fuel zone span, the top of active fuel (TAF) instrumentation value, the bottom of active fuel (BAF) instrumentation value, and the instrumentation value that corresponds to the setpoint level number zero. In addition, a footnote is added to specify the differences between the fuel zone instrumentation setpoints and the physical fuel elevations.

UFSAR Figure 5.2-5 provides values for the top of active fuel water level indication. The value that is presented with respect to vessel zero is incorrect. For that value, the elevation of the physical top of active fuel was provided instead. The change corrects the top of active fuel elevation to correctly reflect the physical location of the instrumentation setpoint and corrects the instrumentation value to reflect actual plant description. A footnote is added that clarifies the difference between the top of active fuel instrumentation setpoint and the physical top of active fuel.

UFSAR Figure 5.3-2 provides nominal reactor vessel water level elevations. The elevations for the recirculation outlet nozzle, the feedwater nozzle, top of active fuel (TAF), and bottom of active fuel (BAF) are incorrect. The change corrects the values and adds a footnote that specifies the differences between fuel zone instrumentation setpoints and physical fuel elevations.

UFSAR Revision to Correct Section 15.2
The description of turbine feedwater pump low condenser vacuum trip sepoint and time to trip in the loss of condenser vacuum accident scenario in UFSAR Subsections 15.2.5 and 15.2.3 are revised to correct discrepancies.

Design Change Packages (DCP) 9600317 and 9600318, Installation of Radio Frequency Remote Controller on Unit 1 and Unit 2 Turbine Building Cranes
DCP 9600317 and 9600318 added portable radio controls for operating the Unit 1 and Unit 2 main turbine room overhead cranes 1HC01G 2HC01G from the turbine building elevation 786' floor. The remote radio controls provide similar features and control functions at the portable control unit as the existing cab and pendant controls have for operating the cranes.

The radio controls were installed for the ALARA (As Low As Reasonably Achievable), personnel safety, and performance reasons. The advent of hydrogen water chemistry addition results in elevated dose rates in the main turbine and the main condenser to increase significantly. Locating the crane operator on the turbine deck, behind the concrete shield wall, minimizes the potential exposure as opposed to that in the crane cab. The cab is located diagonally above the main turbine and main condenser shield walls such that the cab would receive a radiation dose much greater than the dose outside the shield walls in the general area at elevation 786'.
Personal safety of the operator is enhanced because the operator is not isolated in the crane cab, but rather is on the turbine deck with other personnel. This work location minimizes the need for elaborate rescue techniques and equipment needed to remove and lower an operator who becomes ill or incapacitated while in the crane cab.
Radio controls increase the accuracy in heavy lifts and movements of turbine components as the operator can be in the immediate area of the lift, not remotely located in the crane cab.

Installation of Interposing Relays in Turbine Master Trip Solenoid Valves Test Circuits per Design Change Package 9600302
General Electric Company (GE) Technical Information Letter (TIL) 1212 concerns the failure of the turbine master trip solenoid valves (MTSV) to reset at turbine reset or during MTSV testing. This has been attributed to inadequate voltage across the solenoid coil. The DCP installed a 24 VDC interposing relay in the test circuit of each MTSV. The functions of the MTSV turbine-generator electrical trips are maintained, as a valid electrical trip will de-energize both MTSV solenoids to trip the turbine-generator regardless of test status.

Unit 2 Post LOCA Gross Gamma Analyzer Power Supply Filters modification per Design Change Package (DCP) 9800170
The DCP installed a transient voltage surge suppresser on the 120 VAC line input to the power supply, and separated instrument ground wires and power ground wires to their respective grounds of the power supply for radiation monitors 2RIT-CM011 "Post LOCA A Gross Gamma Analyzer", and 2RIT-CM017 "P/C Post LOCA B Gross Gamma Analyzer". This was done mitigate power supply "lock-up" experienced during the performance of diesel generator (DG) response time testing.

LaSalle Special Test Procedure LST-98-213 Revision 0, Unit 2 Pressure Regulation System Startup Test Procedure
The procedure provided instructions for testing the pressure regulator system of the Unit 2 Electro-Hydraulic Control (EHC) system during power ascension operations. It established that recommended pressure control system tuning parameters provided acceptable performance, demonstrated the backup capability of the pressure regulators, demonstrated that plant parameters

remained within acceptable limits during pressure regulator induced transients, and verified variation in incremental regulation was within acceptable limits.

Reactor Core Isolation Cooling (RCIC) Sight Flow Indicator Replacement per Design Change Package (DCP) 9500105
The DCP replaced Unit 2 RCIC high point vent flapper type sight flow indicator 2E51-D306 with a rotary wheel type sight flow indicator. Flow verification was difficult to perform with the previous flapper type sight flow indicator, and its horizontal configuration caused the hinged flapper to stick open.

Addition of drain between RHR Loop B Spray Header Containment Isolation Valves, DCP 9400418
The DCP added a new drain assembly consisting of lines 2RHL1B-3/4" and 2RHL2B-3/4", and isolation valves 2E12-F438B and 2E12-F439B onto the residual heat removal (RHR) loop "B" drywell spray header line 2RH59AB-16" between containment isolation valves 2E12-F016B and 2E12-F017B. The drain line assembly provide a means to drain the entrained volume between valves 2E12-F016B and 2E12-F017B, to valve 2E12-F017B from pressure locking. . The DCP provides a means to prevent valve 2E12-F017B from pressure locking as described in NRC Information Notices 92-26 and 95-14.

Replacement of 6" Masoneilan Control Valve 2WS077B per Design Change Package (DCP) 9500361
The DCP replaced the Unit 2 6-inch primary containment ventilation chiller service water condenser Masoneilan control valve 2WS077B with a 10-inch Control Component Inc. (CCI) DRAG control valve. Noise, vibration, and downstream cavitation associated with the operation of the Masoneilan valve has caused erosion of the control valve body and the outlet piping. The CCI DRAG valve is designed to eliminate noise, vibration, and downstream cavitation such that erosion is minimized.

Replacement of 6" Masoneilan Control Valve 2WS077A per Design Change Package (DCP) 9500362
The DCP replaced the Unit 2 6-inch primary containment ventilation chiller service water condenser Masoneilan control valve 2WS077A with a 10-inch Control Component Inc. (CCI) DRAG control valve. Noise, vibration, and downstream cavitation associated with the operation of the Masoneilan valve has caused erosion of the control valve body and the outlet piping. The CCI DRAG valve is designed to eliminate noise, vibration, and downstream cavitation such that erosion is minimized.

Unit 2 Design Change Package 9700064, Splice Local Power Range Monitor Cable

A section of local power range monitor (LPRM) cable 2NR362 was found to be damaged. The DCP cut the cable at the detector connector and junction box, and spliced a replacement section to 2NR362 in the junciton box.

Design Change Package (DCP) 9600301 – Revise Reject Line High Pressure Alarm Circuit.
Spare limit switch "IO" contacts on condenser valve 2G33-F034 and radwaste collector valve 2G33-F035 were wired to the alarm circuit of existing pressure switch 2G33-N014 to disable the high pressure alarm when both valves are closed. New cables were routed from the valve limit switches to local panel 2H22-P002 and the alarm circuit in local panel 2H22-P002 was rewired to obtain the required logic.

Permanent Supports for Unit 2 Reactor Water Cleanup (RWCU) Instrument Lines in Reactor Building, Design Change Package (DCP) 9700066
The DCP re-routed non-safety related instrument lines associated with reactor water cleanup system (RWCU) filter demineralizer vessels A and C resin trap differential pressure transmitters, and vessel C differential pressure transmitters, between the valve manifold and the instruments located on instrument rack 2G33-Z001-25.The instrument sensing lines were originally designed and built as capillary tubing. The capillaries were subsequently replaced with rigid piping/tubing. The instrument lines were previously bundled together using plastic bands and hung on plastic straps from piping or conduit supports. The lines were extremely flexible in this configuration, allowing excessive deflection. The DCP provided for permanent and more rigid supports for the lines. Additionally, "for record" changes were made to P&IDs M-143 Sheets 2 and 4 to show the as-built configuration of piping/instrument lines.

Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-26 and M-28, Design Change Package (DCP) 9700337
The DCP installed a ¾" diameter relief valve assembly on containment penetration M-26 and M-28 (VP Train B) piping between the respective inboard containment isolation valves 2VP113B and 2VP114B. The DCP was implemented to resolve overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. The addition of the relief valve prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the primary containment becomes isolated and experiences a pressure and temperature rise as a result of the accident. The water volume between the inboard isolation valves 2VP113B and 2VP114B and the respective outboard isolation valves, 2VP063B and 2VP053B, becomes trapped. The valve provides a relief path to prevent overpressurization of the piping and valves. UFSAR Table 6.2-21, 6.2-28, and Figure 6.2-31 are revised accordingly.

Generic Letter (GL) 96-06 Overpressure Protection for VP Primary Containment Penetrations M-25 and M-27, Design Change Package (DCP) 9700338
The DCP installed a ¾" diameter relief valve assembly on containment penetration M-25 and M-27 (VP Train A) piping between the respective inboard containment isolation valves 2VP113A and 2VP114A. The DCP was implemented to resolve overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. The addition of the relief valve prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the primary containment becomes isolated and experiences a pressure and temperature rise as a result of the accident. The water volume between the inboard isolation valves 2VP113A and 2VP114A and the respective outboard isolation valves, 2VP063A and 2VP053A, becomes trapped. The valve provides a relief path to prevent overpressurization of the piping and valves. UFSAR Table 6.2-21, 6.2-28, and Figure 6.2-31 are accordingly revised.

Generic Letter (GL) 96-06 Overpressure Protection for Reactor Recirculation Containment Penetration M-36 Piping per Unit 2 Design Change Package (DCP) 9700344
The DCP installed a ¾" diameter bypass line, including a check valve and a manual isolation globe valve, around Inboard Containment Isolation Valve 2B33-F019 to resolve overpressure protection concerns as part of LaSalle's response to GL 96-06. The addition of the bypass check valve will prevent potential over-pressurization during a Loss of Coolant Accident (LOCA) or a Main Steam Line Break (MSLB) event. UFSAR Table 6.2-21, Table 6.2-28, and Figure 6.2-31 are revised. Administrative Technical Requirements (ATR) Table 3.6.3-2 was revised.

Generic Letter 96-06 Overpressure Protection for Reactor Building Closed Cooling Water (WR) Containment Penetrations M-16 and M-17 Piping, Unit 2 Design Change Package (DCP) 9700340
The DCP installed ¾" diameter relief valve assemblies between containment penetrations M-16 and M-17 and the associated inboard containment isolation valves 2WR179 and 2WR180, respectively. The DCP resolves overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. Adding the relief valves prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the Primary Containment becomes isolated and experience a pressure and temperature rise as a result of the accident. The volume of water between the inboard (2WR179 and 2WR180) and outboard (2WR029 and 2WR040) containment isolation valves becomes trapped. The relief valve provides a path to prevent overpressurization. UFSAR Table 6.2-21, 6.2-28 Sheet 7, and Figure

6.2-31 are revised accordingly. Administrative Technical Requirements (ATR) Table 3.6.3-2 was also revised.

Generic Letter 96-06 Overpressurization Protection for Primary Containment Piping, Design Change Package (DCP) 9700342
The DCP installed a ¾" diameter relief valve assembly between containment penetration M-7 and Inboard Containment Isolation valves 2E12-F009. This was done to resolve overpressure protection concerns as part of LaSalle's response to NRC Generic Letter 96-06. The addition of the relief valve prevents potential overpressurization during a Loss of Coolant Accident (LOCA) or Main Steam Line Break (MSLB) event. During these events, the Primary Containment becomes isolated and experiences a pressure and temperature rise as a result of the accident. The volume of water between the inboard containment isolation valve 2E12-F009 and outboard containment isolation valve 2E12-F008 containment isolation valve becomes trapped. As the temperature of the trapped water rises, without a relief path, the pipe and valves could become overpressurized. UFSAR Tables 5.2-6, 6.2-21, and 6.2-28, and Figure 6.2-31 are accordingly revised. Administrative Technical Requirements (ATR) Table 3.6.3-2 was revised. Drawing M-142 sheet 3 is revised.

Re-routing of Unit 2 Reactor Water Cleanup Water Instrument Lines, Design Change Package (DCP) 9700066
The DCP re-routed Unit 2 reactor water cleanup water (RWCU) instrument lines between the valve manifold and the instruments located on instrument rack 2G33-Z00125. The sensing lines to instruments 2G33-Z00187C, 2G33-Z00188A, and 2G33-Z00188C were originally designed and built as capillary tubing. The capillaries were subsequently replaced with rigid piping/tubing. Re-routing of the lines provides for permanent and rigid supports, and helps to avoid future interferences for the replacement of RWCU valves.

Replacement of Love Controllers 2TCS-FW911 and 2TCS-FW912 per Design Change Package (DCP) 9700361
The DCP replaced Love Controllers 2TCS-FW911 and 2TCS-FW912 with a Yokogawa digital indicating controller Model UT350-00 as a functional equivalent. The controllers modulated seal injection flow to Unit 2 feedwater pump A. The Love Controllers are no longer manufactured, and spare parts aren't available.

Replacement of Love Controllers 2TCS-FW913 and 2TCS-FW914 per Design Change Package (DCP) 9700362
The DCP replaced Love Controllers 2TCS-FW913 and 2TCS-FW914 with a Yokogawa digital indicating controller Model UT350-00 as a functional

equivalent. The controllers modulated seal injection flow to Unit 2 feedwater pump B. The Love Controllers are no longer manufactured, and spare parts aren't available.

Removal of Internals for Unit 2 High Pressure Core Spray (HPCS) Check Valve, Design Change Package (DCP) 9500325
The DCP removed internal parts from Unit 2 High Pressure Core Spray (HPCS) check valve 2E22-F016. The removal of the internal parts resulted in the check valve body becoming a flanged spool piece in the HPCS pipeline. The valve is now a passive component that is only required to maintain system pressure and structural integrity. The valve functioned to prevent back flow of cycled condensate water from the cycled condensate storage tank into the suppression pool and to allow normal flow when the HPCS pump is taking suction from the suppression pool. Removal of the check valve internals and the subsequent loss of the flow checking function is acceptable since the alternate HPCS pump suction path (cycled condensate storage tank) is no longer used due to micro-biologically induced corrosion in the underground piping. The valve was not part of the containment isolation function. UFSAR Figure 6.3-1, HPCS System Diagram, and drawing M-141 are revised.

Addition of Cooling Water Flow Gauges for Unit 2 Core Standby Cooling System (VY) Area Coolers, Design Change Package (DCP) 9700020
The DCP installed individual cooling water flow indicating gauges for coolers 2VY02A and 2VY03A, and combined flow indicating gauges for coolers 2VY01A, 2VY04A, and 2E21-C001. The addition of the flow indicating gauges allows for measurement of flow through the VY area coolers, which was not previously monitored.

Reactivation of the North Access Facility per Design Change Package (DCP) 9800220
The DCP reactivated the North Access Facility (NAF) by making all previously abandoned equipment functional and accessible. The primary objective of this design was to streamline personnel ingress and egress for Unit 2 restart and other LaSalle site activities.

Removal of Unit 2 Main Steam Isolation Valve Closure Bypass Switches, Design Change Package (DCP) 9700462
The DCP removed Unit 2 main steam isolation valve (MSIV) trip bypass scram closure bypass pressure switches 2B21-N020A, 2B21-N020B, 2B21-N020C, and 2B21-N020D, along with the associated tubing, valves and fittings from instrument racks 2H22-P004, 2H22-P027, 2H22-P005 and 2H22-P026 respectively. The cables between the instrument racks and the main control room

(MCR) panels were de-terminated and left in place unassigned, and the associated terminal points in the MCR panels were jumpered. The switches were previously used in the reactor protection system (RPS) and the primary containment isolation system (PCIS) circuitry to automatically bypass the MSIV closure scram signals and provided an interlock input to bypass the main condenser low vacuum trip. The DCP implements License Amendment No. 106 to Unit 2 license. Drawings M-139 sheet 4 and 5 are revised.

Upgrade Unit 2 Reactor Recirculation Sample Line Valve per Design Change Package (DCP) 9700597
The DCP replaced the electrical conductor seal assemblies at the open and close position limit switches on reactor recirculation sample line valve 2B33-F019. Installation of the electrical conductor seal assemblies permits the limit switches of valve 2B33-F019 to be considered environmentally qualified, and satisfies Regulatory Guide 1.97 requirements.

Replacement of Unit 2 Reactor Building Closed Cooling Water system Outlet Header per Design Change Package (DCP) 9700391
The DCP replaced a portion of the Unit 1 Reactor Building Closed Cooling Water (RBCCW) heat exchange outlet Service Water (WS) system outlet header 2WS26B-20" from carbon steel to stainless steel. The replaced portion of piping was eroded due to severe cavitation and impingement. The replacement stainless steel piping is more resistant to cavitation and impingement. Drawing M-125 Sheet 1 (Unit 2 Service Water system) is revised.

Unit 2 Reactor Water Cleanup Voiding Issue Resolution, Design Change Package 9700209

Replacement of Air Actuator on Reactor Building Drain Sump Valve 2RE056, Design Change Package (DCP) 9700427
Valve 2RE056 is a 2" remotely controlled air operated isolation valve on the suction of the drywell equipment drain sump pump. It is located in the reactor building just downstream of the system primary containment isolation system (PCIS) valves. The air supply for the actuator is provided by the instrument air system through a local pressure regulator and solenoid valve. Valve 2RE056 was determined to have an insufficient supply air setpoint to meet minimum seat load requirements. The DCP resized the valve's air regulator to ensure adequate design margin to meet the required valve travel and seat load criteria. The model 67FR regulator was replaced with a model 67AFR regulator, allowing a higher pressure to be supplied to the actuator. Drawing M-81 sheet 19 is revised.

Replacement of Air Actuator on Reactor Building Drain Sump Valve 2RF021, Design Change Package (DCP) 9700428
Valve 2RF021 is a 2" remotely controlled air operated isolation valve on the suction of the drywell equipment drain sump pump. It is located in the reactor building just downstream of the system primary containment isolation system (PCIS) valves. The air supply for the actuator is provided by the instrument air system through a local pressure regulator and solenoid valve. Valve 2RF021 was determined to have an insufficient supply air setpoint to meet minimum seat load requirements. The DCP resized the valve's air regulator to ensure adequate design margin to meet the required valve travel and seat load criteria. The model 67FR regulator was replaced with a model 67AFR regulator, allowing a higher pressure to be supplied to the actuator. Drawing M-81 sheet 19 is revised.

Revision of the Thermal Overload Bypass Scheme of Unit 2 Residual Heat Removal/Low Pressure Core Spray Motor Operated Valves per Design Change Package (DCP) 9700027
The DCP implemented the corrective actions identified in Licensee Event Report (LER) 96-022, Revision 0, for the thermal overload bypass logic of the Unit 2 Engineered Safety Features Division 1 motor operated valves (MOVs). The control circuits of MOVs 2E12-F024A, 2E12-F027A, 2E12-F042A, and 2E21-F005 were revised to ensure that the thermal overloads are bypassed whenever a loss of coolant accident (LOCA) signal is present. The thermal overload bypass signal was previously removed when the manual override feature for these valves was enabled by the operator.

Drywell Equipment Drain System Valve 2RE035 Actuator Upgrade per Unit 2 Design Change Package (DCP) 9700047
The DCP upgraded the actuator of valve 2RE035 to ensure appropriate valve seat closing force to prevent internal valve and stem degradation. The actuator spring and actuator spring adjusting screw were replaced. The bench sets were revised to obtain the correct force from the diaphragm to the spring and the supply air regulator was adjusted to compensate for the additional spring force, and two test taps in the air supply tubing to the actuator were installed.

Design Change Package (DCP) 9100215, Permanently Installation of Transient Analysis Data System (TADS) Panel 2PA19J
DCP 9100215 permanently installed Transient Analysis Data System (TADS) Panel 2PA19J and associated cables in a permanent location inside the Unit 2 Auxiliary Electrical Equipment Room (AEER). Previously, the TADS panel was rolled from a storage area and plugged into the Startrec panel as needed. UFSAR Figure H.4-2 is revised to reflect the resulting Unit 2 Auxiliary Electric Equipment Room layout.

Replacement of Unit 2 High Pressure Heaters Tube Side Relief Valves, Design Change Package (DCP) 9700076
The DCP replaced the Unit 2 High Pressure Feedwater Heater tube side relief valves (2DV002A and 2DV0002B). These relief valves were replaced with new relief valves that meet the requirements of ASME Section VIII and are UV stamped. The existing inlet and outlet piping of the relief valves was modified to fit the new relief valves. The original valves were not UV stamped as required by ASME Section VIII. Drawings M-123 sheets 1, 2, 3, and 4 are revised.

Replacement of Unit 2 Low Pressure Feedwater Heater Tube Side Relief Valves, Design Change Package (DCP) 9700079
The DCP replaced the Unit 2 Low Pressure Feedwater Heater tube side relief valves (2DV003A/B/C, 2DV0004A/BC, 2DV007A/B/C, 2DV009A/B/C and 2DV012A/B/C). These relief valves were replaced with new relief valves that meet the requirements of ASME Section VIII and are UV stamped. The existing inlet and outlet piping of the relief valves was modified to fit the new relief valves. The original valves were not UV stamped as required by ASME Section VIII. Drawings M-123 sheets 1, 2, 3, and 4 are revised.

Replacement of Reactor Building Closed Cooling Water Heat Exchanger Service Water Outlet Valves and Piping, Design Change Package (DCP) 9500364
The scope of the DCP consisted of the following:
The reactor building closed cooling water (RBCCW) heat exchanger (HX) service water (WS) outlet flangeless carbon steel-Masoneilon control valve (2WS087B) body, actuator, and positioner was replaced with a flanged stainless steel Fisher V-Ball valve body with a noise attenuator ball, positioner, and actuator;
Replaced the flangeless downstream isolation butterfly valve 2WS088B with a new flanged butterfly valve of the same design; and,
Replaced the carbon steel piping downstream of the control valve up to the isolation valve with stainless steel.
Additionally, a new ¾" instrument air (IA) system valve, stop valve 2IA816 was added in the common air supply line upstream of the individual ½" air isolation valves for the pneumatic controllers to 2WS087A and 2WS087B.
These changes enhance the cavitation performance of control valve 2WS087B, and reduce cavitation erosion in the valve and downstream piping. The new Fisher valve has a noise attenuator ball to reduce cavitation. The body of the new valve is made of stainless steel, which resists cavitation induced erosion over carbon steel by 20:1. Replacement of the flangeless downstream isolation valve 2WS088B with a flanged valve allows in-place repair of the piping spool upstream between 2WS087B and 2WS088B, and on the downstream valve itself. The installation of isolation valve 2IA816 on the common air line to 2WS087A & 2WS087B allows maintenance on the downstream air valves without losing air to other equipment and instrument panels.

Replacement and Revision of Settings of Molded Case Circuit Breakers per Design Change Package (DCP) 9600347
The DCP replaced the molded case circuit breakers (MCCBs) and revised the magnetic trip setpoints for the motor operators of Unit 2 valves 2E12-F023, 2HG002B, 2E12-F064A, and 2E21-F001. The DCP implements corrective actions identified in a root cause report addressing the tripping of several MCCBs during a response time test of the "0" Diesel Generator. The DCP provides a greater margin to ensure nuisance tripping does not occur during motor starting conditions.

Replacement and Revision of Settings of Molded Case Circuit Breakers per Design Change Package (DCP) 9600348
The DCP replaced the molded case circuit breakers (MCCBs) and revised the magnetic trip setpoints for the motor operators of Unit 2 valves 2VQ035, 2VQ037, 2E51-F086, 2E12-064B, and 2E12-F064C. The DCP implements corrective actions identified in a root cause report addressing the tripping of several MCCBs during a response time test of the "0" Diesel Generator. The DCP provides a greater margin to ensure nuisance tripping does not occur during motor starting conditions.

Replacement and Revision of Settings of Molded Case Circuit Breakers per Design Change Package (DCP) 9600350
The DCP replaced the molded case circuit breakers (MCCBs) and revised the magnetic trip setpoints for the motor operators of Unit 2 valves 2B21-F065A and 2B21-F065B. The DCP implements corrective actions identified in a root cause report addressing the tripping of several MCCBs during a response time test of the "0" Diesel Generator. The DCP provides a greater margin to ensure nuisance tripping does not occur during motor starting conditions.

Relocation of Unit 2 Electro-hydraulic Control (EHC) Pump Vent Lines, Design Change Package (DCP) 9700349
The DCP relocated the pump discharge vent lines associated with air bleed valves 2EH011 and 2EH012 from an area of high vibration to an area of low vibration. The relocation to area of low vibration is needed to resolve past tubing failures induced by vibration. Drawing M-116 sheet 10 is revised.

Demolition Phase of the Unit 2 RWCU Voiding Issue Resolution, Design Change Package (DCP) 9700209
The DCP was initiated to modify the reactor water cleanup (RT) system configuration to provide the RT pumps with "hot suctions" as was originally designed by General Electric.

The demolition phase supported the demolition of equipment, piping and structures associated with the reactor water cleanup system, reactor building structures, reactor building floor drains system, reactor building equipment drain system, reactor building ventilation system, cycled condensate storage system, auxiliary power system, fuel pool cooling system, the leak detection system, instrument air, and reinstallation and relocation of portions of the reactor building closed cooling water system system. This temporary condition applied to Unit 2 only while it was defueled. This phase also supported the demolition of equipment and piping associated with the reactor building closed cooling water system as well as the reinstallation and relocation of portions of this system.

Circulating Water Pump Shaft Packing and Bearing Enhancements, Design Change Package (DCP) 9800247
Circulating water pumps 1(2)CW01PA, PB, and PC have a history of packing, stuffing box, and shroud related corrosion problems. These are due to packing leakage and mounting fits in the casing behind the shroud. The DCP addressed these material condition concerns, and provides engineering basis for future work on the pumps.

Source Range Monitor (SRM) Retract Permissive and Downscale Trip Setpoint per Design Change Package 9700573
The SRM retract permissives didn't satisfy Technical Specifications Table 3.3.6-1, Trip Function 3.a. Note b, which states that the trip function of the SRM will be automatically bypassed if the detector count rate is greater than or equal to 100 counts per second (cps). This was documented in Licensee Event Report (LER) 97-011. Based upon General Electric (GE) calculations, the DCP revised the Unit 2 SRM retract permissive setpoints to 306 cps from 100 cps. The SRM downscale trip setpoints were also revised to 1.51 cps from 1.18 cps. UFSAR Tables 7.3-5 and 7.7-4 are revised.

Change to VL Ductwork Insulation Retainers per Design Change Package (DCP) 9800248
Design Change Package (DCP) 9800248 repaired, reconfigured, and re-installed board type insulation attached to laboratory HVAC (VL system) ducts. The installation was restored to the original design configuration, except that the attachment dome headed pins were replaced by straight pins with a restraining washer and separable dome cap. Revisions to Drawing Specifications IT-7000-M-HV-07, 08, and 09 are incorporated per the DCP.

Resizing of Residual Heat Removal Service Water Restricting Flow Orifice 2E12-D304A, Design Change Package (DCP) 9800055

The DCP resized restricting orifice 2E12-D304A from 8.75" to 10.25" in diameter, to allow for increased service water flow through residual heat removal service water heat exchanger 2E12-B001A. The increased flow is required to assure that the specified design flow of 7400 gpm through the heat exchanger can be met during accident conditions (low lake level of 690') while accounting for instrument uncertainty and pump/system degradation.

Resizing of Residual Heat Removal Service Water Restricting Flow Orifice 2E12-D304B, Design Change Package (DCP) 9800056
The DCP resized restricting orifice 2E12-D304B from 8.75" to 10.25" in diameter, to allow for increased service water flow through residual heat removal service water heat exchanger 2E12-B001B. The increased flow is required to assure that the specified design flow of 7400 gpm through the heat exchanger can be met during accident conditions (low lake level of 690') while accounting for instrument uncertainty and pump/system degradation.

2WS043 Control Valve Replacement, Design Change Package (DCP) 9600531
The DCP replaced and relocated the carbon steel Service Water Control Valve 2WS043 (Masoneilan control valve) with a stainless steel Fisher-Rosemount Vee-Ball control valve with a noise attenuator ball. Downstream isolation valve 2WS044 was replaced with a flanged end butterfly valve. The carbon steel piping between 2WS043 and 2WS044 was replaced with stainless steel pipe. The changes were made to minimize the cavitation erosion damage problem previously experienced. Drawings M-78 sheet 1 and M-125 sheet 2 are revised.

Addition of Low Point Drains in Service Water Pipingper Design Change Package (DCP) 9700423
The DCP added low point drain lines with a manual valve and pipe cap to Unit 2 Turbine Building Service Water supply lines 2WS09A-14" (Turbine Oil Cooler Supply Header) and 2WS11A-20" (Stator Cooling and Generator Hydrogen Cooler Units Supply Header). These low point drain lines were added to allow draining of the piping during extended system lay-up to prevent corrosion damage to the piping due to stagnant water conditions. Drawing M-125 sheet 2 is revised.

Resizing of the RCIC Water Leg Minimum Flow Orifice 2E51-D011, Design Change Package (DCP) 9600486
The DCP resized the Unit 2 reactor core isolation cooling (RCIC) water leg minimum flow orifice 2E51-F011 from the previous 0.300" to 0.625". This change results in a RCIC standby line pressure below the high pressure setpoint while remaining adequate margin above the minimum required system "keep filled" pressure.

Installation of 250 Volt Division 1 Battery 2DC01E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800243
The DCP installed a time delay relay for the 250 volt division 1 battery 2DC01E to the output of the high discharge battery alarm 2IY-DC043 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

Installation of 250 Volt Division 1 Battery 2DC07E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800244
The DCP installed a time delay relay for the 250 volt division 1 battery 2DC07E to the output of the high discharge battery alarm 2IY-DC045 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

Installation of 125 Volt Division 2 Battery 2DC14E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800245
The DCP installed a time delay relay for the 125 volt division 2 battery 2DC14E to the output of the high discharge battery alarm 2IY-DC047 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

Installation of 125 Volt Division 3 Battery 2DC18E High Discharge Alarm Time Delay per Design Change Package (DCP) 9800246
The DCP installed a time delay relay for the 125 volt division 3 battery 2DC18E to the output of the high discharge battery alarm 2E22-K503 to prevent inadvertent alarms during rapid/transient demand changes on the DC system.

UFSAR Table 6.2-21 is revised to explicitly delete reference to LaSalle Administrative Procedure LAP-300-30, Check Valve Preventative Maintenance Program, and to reflect the addition of monitoring to the scope of the check valve preventative maintenance program. The LAP is superseded by standardized procedure NSP-ER-3017, Check Valve Monitoring and Preventative Maintenance Program.

Replacement of Diesel Generator 2A VAR Meter per Design Change package (DCP) 9600116
The DCP replaced the Diesel Generator (DG) 2A VAR meter and transducer. Due to failures of the DG VAR metering equipment and their obsolescence, the metering equipment was replaced to provice more reliable VAR indication with consistent ranges.

Replacement of Diesel Generator 2B VAR Meter per Design Change package (DCP) 9600117

The DCP replaced the Diesel Generator (DG) 2B VAR meter and transducer. Due to failures of the DG VAR metering equipment and their obsolescence, the metering equipment was replaced to provide more reliable VAR indication with consistent ranges. UFSAR Table H.4-92 is accordingly revised.

Replacement of Internals and Removal of Stem Leakoff Line of Reactor Recirculation Isolation Valve 2B33-F023 per Design Change Package (DCP) 9600121
The DCP installed a new valve bonnet, disc, and stem to reactor recirculation (RR) pump suction valve 2B33-F023B in accordance with vendor recommended upgrades. The revised stem provides a packing design with a single stack and no gland area. The stem leakoff line to the gland seal leakoff reservoir was accordingly removed. UFSAR Figure 7.3-7 and Table G.B.1-1, drawings M-139 Sheet 2, M-157 Sheet 1, and M-2139 Sheet 9, are revised.

Procedure LMP-MS-06 Revision 12, Removal/Installation of Main Steam Safety Relief Valves
The procedure provides direction for removal, installation, and "like for like" replacement of main steam safety relief valves (SRVs). Revision 12 incorporates guidance for the removal and installation of horseshoe ductwork and fire detection instrumentation to facilitate removal and installation of SRVs.

DCP9300163, Replacement of Conductivity and Flow Recorders
The DCP replaced two 8-point Honeywell condensate polisher/demineralizer (CP) system conductivity and flow recorders 2CR-CP015 and 2FJR-CP001 on Turbine Building Panel 2PL05J with four 4-point Yokogawa recorders 2CR-CP015A and B, and 2FJR-CP001A and B. The Honeywell recorders are obsolete, are no longer manufactured, and spare parts are not available. All CP functions remain the same.

Heater Drain Pump Minimum Flow Changes to Facilitate Idle Pump Warm-up per Design Change Package (DCP) 9700420
Solenoid valves were added to the minimum flow bypass valves of the Unit 2 heater drain system (HD) pumps recirculation lines. This enables the valves to remain open for a period of time sufficient to allow recirculation of cold water in idle heater drain pumps upon startup of the idle pumps. Timer relays were added in the switchgears for the HD pumps to provide an adjustable timer permissive for energizing and deenergizing the solenoid valve. The pump discharge flow (differential pressure type) transmitters were replaced with flow transmitters that provide linear outputs, eliminating the need for square root extractors to modulate the DP type signal into a linear signal. Pressure breakdown devices in the minimum flow bypass line were replaced with straight

pipe to allow for a greater flow of cold stagnant water back to the heater drain tank. UFSAR Section 10.4.7.2 and drawing M-122 sheet 2 is revised.

UFSAR Revision to Chapter 9.1, Fuel Handling and Storage
UFSAR Chapter 9.1 was to revised to make the UFSAR consistent with the plant's operating license; Clarify that either pool may store new or spent fuel from either unit; Reflect that LaSalle has chosen to comply with 10CFR50.68(b), "Criticality Accident Requirements"; and corrected typographical errors.

Design Change Package (DCP) 9700600, Replacement of RHR Heat Exchanger Relief Valve 2E12-F313A
The DCP replaced the residual heat removal (RHR) B heat exchanger tube side relief valve 2E12-F313A, in response to past inservice testing failures. The valve was also relocated and re-oriented to the vertical position, per ASME requirements. This activity requires a revision to drawing M-137 sheet 3.

Unit 2 Cycle 8 Reload Licensing Analysis
The operation of Unit 2 with fuel manufactured by Siemens Power Corporation (SPC) Atrium 9B fuel and General Electric (GE) fuel, utilizing SPC analytical methodologies were evaluated and found to be acceptable. UFSAR Sections 1.2, 1.6, 3.1, 3.9, 4.0, 5.0, 4.1, 4.2, 4.3, 4.4, 5.2, 6.0, 6.3, 6.B, 6.3, 7.7, 10.4, 15.0, 15.1, 15.2, 15.3, 15.4, 15.5, 15.6, 15.7, 15.8, 15.A, G.3, and G.7 are revised for Unit 2 Cycle 8 operation. The associated Core Operating Limits Report was approved Administrative Technical Requirements (ATR) Amendment 26.

Design Change Package (DCP) 9700601, Replacement of RHR Heat Exchanger Relief Valve 2E12-F313B
The DCP replaced the residual heat removal (RHR) B heat exchanger tube side relief valve 2E12-F313B, in response to past setpoint test failures. The valve was also relocated and re-oriented to the vertical position, per ASME requirements. This activity requires a revision to drawing M-137 sheet 3.

DCP 9600219, New Exhaust Fan and Vent Duct For the Unit 2 TDRFP Room B, installed vane axial fan 2VT13CB and ductwork over the existing floor opening in TDRFP room 2B to create a forced transfer of air from the pump room to the heater bay below. UFSAR Table 9.4-13, and subsections H.3.5.1 and H.3.5.3 are revised. Drawings M-Index sheet 1, M-7, and M-1460 sheet 2 are revised.

DCP 9600218, New Exhaust Fan and Vent Duct For the Unit 2 TDRFP Room A, installed vane axial fan 2VT13CA and ductwork over the existing floor opening in

TDRFP room 2A to create a forced transfer of air from the pump room to the heater bay below. UFSAR Table 9.4-13, and subsections H.3.5.1 and H.3.5.3 are revised.

Changes to the Turbine Building Ventilation System to Provide Cooling to the Area of the Turbine Valves' Electro-Hydraulic Controls (EHC) in the Unit 1 Turbine Building Low Pressure Heater Bay per Design Change Package (DCP) 9600528.
The DCP installed two new 10,000 cfm vane axial fans (1VT14C and 1VT15C) in the low pressure heater bay. Discharge ductwork from the fans was routed to the vicinity of the EHC controls for the turbine control valves, the turbine stop valves, and the main steam bypass valves to provide additional cooling air to reduce the temperature and thermal stratification in this area. UFSAR Table 9.4-13 is revised.

Changes to the Turbine Building Ventilation System to Provide Cooling to the Area of the Turbine Valves' Electro-Hydraulic Controls (EHC) in the Unit 2 Turbine Building Low Pressure Heater Bay per Design Change Package (DCP) 9600529
The DCP installed two new 10,000 cfm vane axial fans (2VT14C and 2VT15C) in the low pressure heater bay. Discharge ductwork from the fans was routed to the vicinity of the EHC controls for the turbine control valves, the turbine stop valves, and the main steam bypass valves to provide additional cooling air to reduce the temperature and thermal stratification in this area. UFSAR Table 9.4-13 is revised. Drawings M-9, M-1459 sheet 2, and M-1460 sheet 2 are revised.

Changes to the Turbine Building Ventilation System to Provide Cooling to the Area of the Turbine Valves' Electro-Hydraulic Controls (EHC) in the Turbine Building Low Pressure Heater Bay per Design Change Package (DCP) 9600529
The DCP installed two new 10,000 cfm vane axial fans, 2VT14C and 2VT15C, in the low pressure heater bay. Discharge ductwork from the fans was routed to the vicinity of the EHC controls for the turbine control valves, the turbine stop valves, and the main steam bypass valves to provide additional cooling air to reduce the temperature and thermal stratification in this area. UFSAR Table 9.4-13 is revised.

Unit 2 Design Change Package (DCP) 9700131, Replacement of Unit 2 Loose Parts Monitoring System (LPMS)
The DCP removed the loose parts monitoring equipment from panel 2PA15J and replaced it with a new state-of-the-art data acquisition system manufactured by Siemens Power Corporation. The new equipment is designed to work with existing accelerometers and preamplifiers (charge converters), and the existing

annunciator system and power supply. The previous LPMS did not conform to the configuration described in the SER and the response to FSAR Question 221.14. UFSAR Section 4.4.6.1 is revised to include a description of the installed upgraded LPMS configuration applicable to Unit 2.

Replacement of Relief Valves 2CD141A/B and 2CD142A on the Steam Jet Air Ejectors (SJAEs) and the Steam Packing Exhauster (SPE) per DCP 9700269
The DCP replaced the Unit 2 socket welded condensate system (CD) relief valves 2CD141A/B and 2CD142A on the "A" and "B" SJAEs and on the "A" SPE, respectively, with UV-stamped ASME Section VIII, flanged relief valves and associated fit-up flanges. The DCP also routed 1" discharge drain lines from the outlets of the three new relief valves and existing flanged relief valve 2CD142B to the turbine building system area floor drains. The welded in relief valves weren't UV-stamped as required by ASME Section VIII. The new UV-stamped relief valves are flanged in, allowing the valves to be temporarily removed and bench tested per ASME Section VIII to comply with the requirements of the Illinois Department of Nuclear Safety (IDNS). Drawings M-119 sheet 1 and M-151 sheet 1 are revised.

Replacement of Limitorque Actuator and Motor on Motor Operated Valve 2G33-F004 per Design Change Package (DCP) 9700526
The DCP replaced the 15 ft-lb. SMB-0 actuator on Valve 2G33-F004 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed to provide power to the motor operated valve and the molded case circuit breaker and thermal overload relay were replaced. UFSAR Table 6.2-28, Table H.4-16, Table H.4-19, Table H.4-23 and Table H.4-49 in addition to Unit 2 Administrative Technical Requirements (ATR) Table 3.6.3-2 are accordingly revised.

Replacement of Limitorque Actuator and Motor on Motor Operated Valve 2G33-F001 per Design Change Package (DCP) 9700525
The DCP replaced the 15 ft-lb. SMB-0 actuator on Valve 2G33-F001 with a larger actuator (type SB-1) rated at 40 ft-lb. to decrease the valve's stroke time to be less than 10 seconds. A new three (3) conductor 6 AWG cable was installed to provide power to the motor operated valve and the molded case circuit breaker and thermal overload relay were replaced. The DCP asle drilled a vent hole in the upstream (reactor side) disc of valve 2G33-F001 to address NRC Generic Letter (GL) 96-06 concerns dealing with primary containment isolation valve arrangements that are susceptible to thermal overpressurization following a LOCA in the drywell. UFSAR Table 6.2-28, Table H.4-16, Table H.4-19, Table H.4-23 and Table H.4-49 in addition to Unit 2 Administrative Technical Requirements (ATR) Table 3.6.3-2 are accordingly revised.

Installation of Emergency Battery Packs for Valves 2E12-F003B, 2E12-F018B, and 2E12-F047B per Design Change Package (DCP) 9700002
The DCP installed emergency battery packs for valves 2E12-F003B, 2E12-F018B, and 2E12-F047B in order to illuminate the valve operators in accordance with 10CFR50 Appendix R requirements. The power for the battery pack is fed from 480-V motor control center (MCC) 234X-2, Compartment D2, through regular lighting cabinet (RLC) #216. UFSAR Tables H.4-3, H.4-30, and H.4-31 are revised.

Installation of Above Ground Diesel and Gasoline Fuel Tanks per Design Change Package (DCP) 9600324
The DCP placed the original in ground Diesel Fuel Oil and Gasoline tanks out of service. Two new 2000-gallon capacity tanks were installed abov7e ground about 370 feet East-Northeast (ENE) of the main access facility, inside the protected area. UFSAR subsections 2.2.3.1, 2.2.3.2, and 3.5.1.5 are revised.

Increase Unit 2 Flow Control Valve Upshift Position Setpoint for Reactor Recirculation Pumps, DCP 9700513
The DCP revised the valve maximum open position setpoint (or minimum position) of the reactor recirculation (RR) flow control valves (FCV) 2B33-F060A and 2B33-F060B associated with RR pump start. This change increases the valve position when the RR pumps are transferred from low to high speed to reduce the possibility of FCV binding.

Unit 2 Reactor Recirculation Hydraulic Power Unit (RR HPU) Containment Isolation Valve Switch and Cover Replacement per Design Change Package (DCP) 9700168
This DCP affected sixteen (16) RR HPU Containment Isolation valves: 2B33-F338A/B, 2B33-F339A/B, 2B33-F340A/B, 2B33-F341A/B, 2B33-F342A/B, 2B33-F343A/B, 2B33-F344A/B, and 2B33-F345A/B.
The modification replaced the steel housing on the solenoid and limit switches (top) of each valve with a two-piece design stainless steel housing. The previously existing assemblies of limit switch brackets, limit switches, and terminal blocks were replaced with new assemblies of limit switch brackets, limit switches, terminal blocks, and vernier adjustment devices for setting limit switch actuation positions. Additionally, cables from each of the valves to the first junction box was replaced with high-temperature cable. This modification was installed to resolve repeated position indication problems experienced by these valves.

Replacement of Unit 2 Capacitance Probes with Displacement Probes per Design Change Package (DCP) 9700478

The DCP replaced the sensors in the Reactor Floor Drain Sump (RF) weir and the Reactor Equipment Drain Sump (RE) with more reliable instrumentation. Specifically, the drywell floor drain sump capacitance fill up rate type probe 2LE-RF002, its coaxial cables, and its remote transmitter 2LT-RE002 were replaced with a new displacement type probe, shielded cables and a remote transmitter. Likewise, the drywell equipment drain sump capacitance fill up rate type probe 2LE-RE001, its coaxial cables, and its remote transmitter 2LT-RE001 were replaced with a new displacement type probe, shielded cables and a remote transmitter. The reliability and inherited problems with the capacitance probes necessitated their replacement with more reliable instruments.

Addition of Flex Hoses and Isolation Valves to Unit 2 Main Steam Bypass Valves, Design Change Package (DCP 9800157)
The DCP provided the details to add flex hoses and isolation valves to each of the electro hydraulic control (EHC) fluid actuator supply lines for the five main steam bypass valves, and (2) add isolation valves to the supply lines to each of the two supply manifolds on the EHC skid of Unit 2.
The flex hoses and isolation valves were added to each of the EHC supply lines to the main steam bypass valve actuators to eliminate the hard pipe connections. The hard pipe connections transmit vibrations from the main steam bypass valves, which has resulted in leakage of the flared fittings near the actuator at their threads. The manifold isolation valves were added to allow isolation of the rest of the EHC skid from the main steam bypass valves to enhance the performance of maintenance activities. Drawing M-116 Sheet 10 is revised.

DCP 9700556, Replacement of 24/48 VDC lead-antimony batteries 2DC31E and 2DC32E with lead-calcium batteries
DCP 9700557 Replacement of 24/48 VDC lead-antimony batteries 2DC33E and 2DC34E with lead-calcium batteries
Inspections of the model DKR-13 24/48 VDC battery cells revealed damage due to swelling of the post seals, which cracked cells and deteriorated the plastic hold down nuts. These batteries provide power to the process radiation monitors and the SRM and IRM startup range neutron monitors. The DKR-13 batteries are no longer manufactured. Based upon the recommendation of the manufacturer, GNB Technologies, the DKR-13 batteries were replaced with GNB's lead-calcium model 2-MCX-5 batteries. UFSAR Section 8.3.2.1.1 is revised.

Insulation of LaSalle Unit 2 Main Steam Bypass Valve Tailpipes per Design Change Package (DCP) 9700380
Main steam bypass valve tailpipes 2MS33AA-12", 2MS33AB-12", 2MS33AC-12", 2MS33AD-12", 2MS33AE-12", 2MS33BA-18", 2MS33BB-18", 2MS33BC-18", 2MS33BD-18", and 2MS33BE-18" were not previously insulated. As part of the turbine bypass system, these lines are used to control reactor pressure during the reactor heat-up to rated pressure while the turbine-generator is being brought

to speed and synchronized, during power operation when the reactor steam generation exceeds the transient turbine steam requirements, and during reactor cool down.
A portion of the lines is routed under cable trays causing the trays to be aged at an unacceptable accelerated rate. The DCP added calcium silicate insulation with aluminum lagging on the lines to prolong the life of the cables, in addition to reduce the heat load on the turbine building ventilation system.

Replacement of Reactor Recirculation (RR) Loop Double Block Drain Valves 2B33-F051A and 2B33-F052A with Single Block Drain Valves per DCP9700377
The DCP replaced each of the two 1-1/2" double block Anderson Greenwood drain valves, 2B33-F051A and 2B33-F052A, with a single ¾" Anchor Darling valve on each valve's respective loop. The previous valves experience leakage past their seats. The common-body double-valve construction previously used in this application is non-standard. The valves are obsolete and not readily repairable. The use of two single valves is intended to eliminate leakage problems, improve ease of maintenance, and still provide double isolation of the reactor coolant pressure boundary. Drawing M-139 sheet 1 is revised.

Replacement of Reactor Recirculation (RR) Loop Double Block Drain Valves 2B33-F051B and 2B33-F052B with Single Block Drain Valves per DCP 9700378
The DCP replaced each of the two 1-1/2" double block Anderson Greenwood drain valves, 2B33-F051B and 2B33-F052B, with a single ¾" Anchor Darling valve on each valve's respective loop. The previous valves experience leakage past their seats. The common-body double-valve construction previously used in this application is non-standard. The valves are obsolete and not readily repairable. The use of two single valves is intended to eliminate leakage problems, improve ease of maintenance, and still provide double isolation of the reactor coolant pressure boundary. Drawing M-139 sheet 2 is revised.

Replacement of Drain Lines for Unit 2 Drywell Flow Element 2FE-RF021 per Design Change Package (DCP) 9600564
The DCP replaced the carbon steel drain lines of Unit 2 drywell coolers 2VP03AA and 2VP03AB with stainless steel drain lines. Carbon steel globe valve 2RE051A was replaced with a stainless steel ball valve, and carbon steel p-traps were replaced with stainless steel crud traps. Flow element 2FE-RF021 was relocated away from the Unit 2 reactor pressure vessel for ALARA purposes. The DCP was installed to preclude clogging of the flow element 2FE-RF021 from rust and soot accumulation, which produced erroneous readings in the control room. Drawings M-129 sheet 1 and M-137 sheet 4 are revised.

Unit 2 Number 1 and 2 Feedwater Heater Drain Control Valve Replacements per Design Change Package (DCP) 9700288
The DCP replaced the Unit 2 number 1 feedwater heater drain normal control valves 2HD072A, B, C and emergency drain control valves 2HD062A, B, C with valves of larger flow capacity, and, replaced the internal trim of the number 2 feedwater heater emergency drain control valves 2HD065A, B, C in order to increase their flow capacity. Drawings M-122 sheet 3 and 4 are revised.

Replacement of Emergency Diesel Generator 2B Speed Sensor per Unit 2 Design Change Package (DCP) 9800005
The station's diesel generators have experienced failures or erratic operation of their associated speed sensor assemblies. Replacement assemblies were not readily available, while maintenance and repair activities have proven to be very difficult for both station and vendor personnel. The DCP replaced and upgraded the speed sensor assembly of the 2B emergency diesel generator. The new speed sensing assembly is a Synchrostart DG Electronic Speed Switch model ESSB-4AT, which provides the same control functions as the previous Stewart & Stevenson DG speed switch. UFSAR Section 1.7, Electrical, Control and Instrumentation drawings, is accordingly revised per DCP 9800005.

DCP 9700556, Replacement of 24/48 VDC lead-antimony batteries 2DC31E and 2DC32E with lead-calcium batteries
DCP 9700557 Replacement of 24/48 VDC lead-antimony batteries 2DC33E and 2DC34E with lead-calcium batteries
The specific gravity drop in UFSAR Section 8.3.2.1.1 is revised to be consistent with the new 24 volt batteries installed per DCPs 9700556 and 9700557. UFSAR Section 8.3.2.1.1 is revised.

Relocation of pressure switches 2B21-N413A and C, Design Change Package (DCP) 9800292
The design change relocated pressure switches 2B21-N413A and C from pipe stand mounts to instrument rack 2H22-P026, where better instrument needle valves are available to minimize spiking caused by instrument valve operations. This will aid in minimizing the incidence of scrams and/or engineered safety feature actuations resulting from pressure spiking associated with instrument valve operations. Drawing M-139 Sheet 5 is revised.

Relocation of pressure switches 2B21-N413B and D, Design Change Package (DCP) 9800293
The design change relocated pressure switches 2B21-N413B and D from pipe stand mounts to instrument rack 2H22-P027, where better instrument needle valves are available to minimize spiking caused by instrument valve operations.

This will aid in minimizing the incidence of scrams and/or engineered safety feature actuations resulting from pressure spiking associated with instrument valve operations. Drawing M-139 Sheet 4 is revised.

Revision to Drawings M-1456 Sheet 2 and 3
The restriction on indicated airflow in Note 3 of drawing M-1456 sheet 2 and Note 4 of M-1456 Sheet 3 were deleted in lieu of the new airflow tolerances in calculations L-001281 Revision 5 and L-001324 Revision 5. This allows greater flexibility when balancing airflows.

Replacement of Continuous Air Monitors 2PL15J and 2PL75J (Phase I), Design Change Package (DCP) 9700070
This DCP completed the preliminary work to support replacement of continuous air monitor (CAM) panels 2PL15J and 2PL75J. New manual isolation valves were installed in the inlet sample line, return sample line for panel 1PL75J, and return sample line for panel 2PL15J. Portions of stainless steel piping from the new isolation valves to the panels were replaced with stainless steel tubing. Two new grab sample stations for each panel were installed and previously existing manual equipment isolating valves were relocated to a higher elevation. Drawing M-158 Sheet 4 is revised.

Offgas Air Operated Valves Actuator Upgrades and Stem Bellows Replacement, Design Change Package (DCP) 9700060
Based upon effective diaphragm area (EDA) test results, new bench sets, supply air setpoint values, and stem travel adjustments were required for the following offgas system air operated valves (AOVs) to assure appropriate seat pressures and leak tightness: 2N62-F019A/B/C/D, 2N62-F025A/B, 2N62-F042, 2N62-F043, 2N62-F047, 2N62-F048, 2N62-F049, 2N62-F394, and 2N62-F019D. These changes included upgrading and adjusting valve stem stroke, relocating solenoid valves, and re-tubing air lines as needed. Other minor changes and adjustments were made to improve valve operation. Drawing M-135, Sheet 2 was revised as a "for record" change to correct the air supply solenoid valve (SV) symbol for valve 2N62-F019D to deenergized and vented instead of energized when F019D is closed, as it is shown on the drawing.

UFSAR changes per Installation Phase of Design Change Package (DCP) 9700209 – Unit 2 Reactor Water Cleanup System Pumps and Return to Hot Suction
The DCP restored the "hot suction" configuration of the Unit 2 ractor water cleanup system (RT) system, as originally designed by General Electric, by replacing / reworking piping and associated valving. The design change installed the Reactor Water Cleanup pumps upstream of the system heat exchangers and

routed the piping from outside the primary containment to the pump suction bypassing the heat exchangers. The pump discharge was routed to the system heat exchangers. The DCP replaced the three existing non-safety related 50% capacity RT System recirculation pumps with two new 100% capacity pumps. UFSAR Sections 1.7, 4.6.1.1.2.4.2, 5.4.8.2, 7.3.2.2.3.8, 7.7.1.2.1, and 9.2.3.2, Tables 5.4-1, 8.1-2, 8.1-10, 8.3-1 Sheet 2, 12.3-16 Sheet 1, Figures 4.6-5, 4.6-6, 5.4-6 Sheets 1, 2, and 3, 5.4-8, 8.3-4, 12.3-1 Sheet 4, 12.3-2 Sheet 4, 12.3-4 Sheet 2, and H.2-1 Sheet 3 are revised accordingly.

Replacement of Reactor Building Closed Cooling Water Heat Exchanger Service Water Outlet Valves and Piping, Design Change Package (DCP) 9500366
The scope of the DCP consisted of the following:
The reactor building closed cooling water (RBCCW) heat exchanger (HX) service water (WS) outlet flangeless carbon steel-Masoneilon control valve (2WS087A) body, actuator, and positioner was replaced with a flanged stainless steel Fisher V-Ball valve body with a noise attenuator ball, positioner, and actuator;
Replaced the flangeless downstream isolation butterfly valve 2WS088A with a new flanged butterfly valve of the same design; and,
Replaced the carbon steel piping downstream of the control valve up to the isolation valve with stainless steel.
These changes enhance the cavitation performance of control valve 2WS087A, and reduce cavitation erosion in the valve and downstream piping. The new Fisher valve has a noise attenuator ball to reduce cavitation. The body of the new valve is made of stainless steel, which resists cavitation induced erosion over carbon steel by 20:1. Replacement of the flangeless downstream isolation valve 2WS088A with a flanged valve allows in-place repair of the piping spool upstream between 2WS087A and 2WS088A, and on the downstream valve itself.

Unit 2 Design Change Package (DCP) 9700531 – Modify VR Flow to the RT Pump / Valve Rooms
The design change replaced ductwork in the Reactor Water Cleanup (RWCU) pump rooms with new ductwork. Pneumatically operated dampers 2VR16Y, 2VR17Y, and 2VR18Y were replaced with manual dampers 2VR84Y, 2VR85Y, 2VR86Y, 2VR87Y, 2VR88Y, and 2VR89Y. Manual balancing damper 2VR80Y was added in the common exhaust ductwork serving RWCU pump rooms and associated rooms. Manual balancing damper 2VR81Y was added in the common exhaust ductwork serving the drywell pump room and associated rooms. Drawings M-1456 sheets 1, 2, and 3 are revised.

Repair Modifications to RHR Service Water Pump 2E12-C300A
Unit 2 Residual heat removal (RHR) service water pump 2E12-C300A has shown degradation due to corrosion of various pump parts resulting from stagnant

water. Repairs consisted of grinding, welding, and machining of affected parts to return the pump to an acceptable mechanical condition.

Repair Modifications to RHR Service Water Pump 2E12-C300D
Unit 2 Residual heat removal (RHR) service water pump 2E12-C300D has shown degradation due to corrosion of various pump parts resulting from stagnant water. Repairs consisted of grinding, welding, and machining of affected parts to return the pump to an acceptable mechanical condition.

Unit 2 Primary Containment Chilled Water Expansion Tank Water Level Control Changes per DCP 9500283
The DCP revised the High/Low level alarm setpoints, and the automatic makeup Start/Stop setpoints for the Unit 2 VP system expansion tanks 2VP01TA and 2VP01TB. This design change eliminates unnecessary drawing of clean condensate water through the makeup lines to the VP expansion tanks.

Selector Switch replacement per Design Change Package (DCP) 9700453
The DCP replaced a two-position selector switch with a three-position selector switch to provide one-out-of-three channel selection capability among narrow range reactor water level channels 2C34-N004A, B, or C.

Revised Reactor Water Level (RWL) Feedwater control selection circuitry per DCP 9600453
The DCP replaced two-position selector switch 2C34A-S001 in Main Control Board panel 2H13-P603 with a three-position selector switch and installed required wiring connections to provide one-out-of-three channel selection capability for RWL monitoring circuits. The DCP also removed local and remote channel selected and channel out of service indication and associated pushbutton switches, indicating lights, and fuses.

Installation of High Point Vent on Stator Cooler Service Water Outlet Line 2WS12A-12" per Design Change Package (DCP) 9800310
The DCP installed a 3/4" vent valve to line 2WS12A-12" to allow for proper venting of the high point of the line. Proper venting of the line mitigates pipe rumbling, and will prevent damage to the line and supports resulting from water hammer. Drawing M-125 Sheet 2 is revised.

Unit 2 Reactor Water Cleanup Septa Tube Replacement, Design Change Package (DCP) 9500261

The LaSalle Unit 2 Reactor Water Cleanup (RWCU) system (RT) provides a recirculation loop for reactor coolant through filter demineralizers. The RWCU filter demineralizer system continuously filters and demineralizes reactor coolant to maintain reactor chemistry within specified limits. The RWCU system includes three filter demineralizer vessels along with supporting precoating and backwashing equipment. The system is normally operated with two of the three filter demineralizer vessels in service. Fouled septa elements in the RWCU System filter demineralizers resulted in poor filter pre-coats, short filter run lengths, and degraded reactor water chemistry. The DCP replaced the original septa in the 2C RWCU filter demineralizer vessel with new elements. The attachment fittings and top lattice structure were replaced, as the replacement elements are of a slightly different design, due to original replacements no longer being available. The septa replacement should improve Unit 2 reactor water chemistry, and reduce the volume of radwaste generated due to the improved precoating and longer filter run times.

Replacement of Air Actuator on Valves 2VP070A and 2VP070B per Design Change Packages (DCP) 9500356 and 9500357
DCPs 9500356 and 9500357 replaced the Masoneilan size 9 reverse air actuator with a Masoneilan size 11 reverse air actuator on each of primary containment chilled water (PCCW) expansion tank condensate makeup flow control valves 2VP070A and 2VP070B, respectively. This also included replacement of the valve stems and refurbishment of the valves. The larger effective diaphragm area and stiffer spring of the size 11 actuators produces sufficient thrust to eliminate seat leakage. Previous seat leakage resulted in overfilling of the PCCW expansion tanks, which sent clean condensate to the auxiliary building floor drains.

Unit 2 Division 1 Core Standby Cooling System Local Flow Indicators and Motor Operated Valve Removal, Design Change Package (DCP) 9800320
The DCP installed two locally indicating flow elements (calibrated flow orifices) in Core Standby Cooling System (CSCS) supply and return lines. One was installed upstream of the low pressure core spray (LPCS) pump motor cooler, and the other was installed downstream of the northwest (NW) cubicle area cooler. Motor operated valve (MOV) 2DG035 was removed from the LPCS Pump Motor Cooler supply line and a flanged orifice installed. UFSAR Sections 9.2.1.2 and 9.2.1.5 are revised to reflect the new flow element on the inlet to the LPCS pump motor cooler. Drawings M-134 sheets 2 and 3 are revised.

Modification of the Unit 2 Condensate Polishing Demineralizer Panel per Design Change Package (DCP) 9600572 (Modification M01-2-9600572)
The DCP removed the condensate polisher automatic regeneration mode of operation from Unit 2, in addition to removing the valve interlocks and

permissives which control transfer between the condensate polishers (CP) and the tanks related to regeneration, to instead be controlled by manual operator action from the control panel. The DCP modified the transfer of resin from the cation/separation tank to the mix/storage tank. The Unit 2 regenerate cycle no longer includes the full chemical cleaning process.
UFSAR Subsections 10.4.6.2, 10.4.6.3, 10.4.6.5, 11.2.1.7, 11.2.1.7.1, and 11.2.2.3 are revised to reflect that regeneration is no longer possible in Unit 2.

Removal of Remote Indication Hardware from Unit 2 Division 1 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700490
DCP 9700490 removed remote indication hardware from Unit 2 Division 1 ECCS testable check valves 2E12-F041A, 2E12-F050A, and 2E21-F006, to eliminate a recurring problem in which the valves fail to completely close. This was attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves the performance of each valve, increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.2.2.3, 6.3.2.2.4, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.3.1, 7.3.1.2.4.1, 7.3.1.2.5, 7.A.3.1.1.1, 7.A.3.1.1.2, 9.3.1.2.2, and Table 6.2-21 Sheet 11 are revised.

Removal of Remote Indication Hardware from Unit 2 Division 2 Emergency Core Cooling System (ECCS) Testable Check Valves, Design Change Package (DCP) 9700491
DCP 9700491 removed remote indication hardware from Unit 2 Division 2 ECCS testable check valves 2E12-F041B, 2E12-F041C, and 2E12-F050B, to eliminate a recurring problem in which the valves fail to completely close. This was attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves the performance of each valve, increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.2.2.4, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.4.1, 7.3.1.2.5, 7.A.3.1.1.1, 9.3.1.2.2, and Table 6.2-21 Sheet 11 are revised.

Removal of Remote Indication Hardware from Unit 2 Division 3 Emergency Core Cooling System (ECCS) Testable Check Valve, Design Change Package (DCP) 9700492
DCP 9700492 removed remote indication hardware from Unit 2 Division 3 ECCS testable check valve 2E22-F005, to eliminate a recurring problem in which the valve fails to completely close. This was attributed to the small margin between the forces to close the valve and the frictional forces associated with the packing, operator linkage, and indicator linkage. The DCP improves valve performance,

increases the margin by reducing the frictional forces and eliminating the problem. UFSAR Subsections 3.1.2.4.7, 6.2.4.2.1, 6.3.4, 7.1.3.4.2.2, 7.3.1.2.1.10, 7.A.3.1.1.4, 9.3.1.2.2, and Table 6.2-21 Sheet 11 are revised.

Addition of Manual Vent Valve to Instrument Air Supply per Design Change Package (DCP) 9700417
The DCP added manual vent valve 2IA809 to the non-safety-related Instrument Air (IA) supply to the safety-related Turbine Building Ventilation Check Dampers 2VT79YA/B/C. The valve was installed between the existing isolation valve (2IA255) and the check dampers. These normally open check dampers are designed to automatically close on high differential pressure following a high energy line break (HELB) within the main steam tunnel. The addition of the manual vent valve assures that the actuators of the check dampers can be manually deactivated and eliminates the potential for such failures adversely impacting their safety function.

Revision to UFSAR drawing per Design Change Package (DCP) 9800300 – Replace Valve Trim in Turbine Building Closed Cooling Water (TBCCW) Heat Exchanger Flow Control Valve 2WS029
The DCP replaced valve 2WS029 trim with a new trim that has larger holes in the cage and a higher Cv. The larger holes prevent plugging of the valve by material that has passed through the service water strainers. The higher Cv ensures that the valve will pass the TBCCW design service water flow rate under all conditions. D M-125 Sheet 2 is revised.

Design Change Package (DCP) 9800113, Addition of HELB Excess Flow Check Damper 2VR91Y
The DCP installed High Energy Line Break (HELB) excess flow check damper 2VR91Y between secondary containment isolation damper 2VR05YB and pressure relief damper 2VR90Y in the VR system ductwork located on elevation 786'-6" in the Auxiliary Building.
The new check damper, in conjunction with the downstream pressure relief damper, maintains the pressurization of the masonry exhaust plenum within acceptable limits following a postulated HELB in the Unit 2 main steam tunnel. UFSAR Table 3.2-1, and sections 9.4.2.1.1, 9.4.2.3, 9.4.2.4, and Table 9.4-6 are revised.

Modification to Control Room Ventilation Exhaust Plenum and Install HELB Check Damper in Control Room Ventilation Exhaust Ductwork per Design Change Package (DCP) 9800224
This DCP installed a fast acting excess flow check damper, 1VR91Y, in the VR system between 1VR05YB in the control room ventilation system (VR) exhaust plenum. This

damper further reduces the High Energy Line Break (HELB) pressure in the VR exhaust plenum. The DCP also modified hangers, blockwall, and relocated an isokinetic probe. UFSAR Table 3.2-1 is revised to reflect the addition of the damper.

Design Change Notice (DCN) to DCP 9700131
DCP 9700131 replaced the Unit 2 Loose Parts Monitoring System (LPMS). DCN 0016101-01 replaced the Rockwell LPMS preamplifiers located inside the drywell near inboard containment penetration E-19 with Technology for Energy (TEC) preamplifiers. Coaxial adapters to connect the Microdot cable plugs to the BNC input signal receptacles on the new TEC preamplifiers were also installed.

Resloping Unit 2 RCIC Drain Line with Stainless Steel Pipe, Design Change Package (DCP) 9700181
The DCP replaced the carbon steel reactor core isolation cooling (RCIC) drain lines with stainless steel material and components to reduce rust formation and plugging of the lines or orifice plate. Plugging of the lines would result in water accumulation in the RCIC turbine exhaust drain pot, which in turn could lead to failure of the exhaust rupture discs. The new lines were installed with a minimum of 1/8 inch/foot slope to ensure positive drainage to the barometric condenser. Orifice plates 2E51-D010A&B were moved from a vertical orientation to a horizontal orientation. New stainless steel restricting orifices and strainer were installed to replace the carbon steel components. A sight glass 2E51-D318 and associated isolation valves 2E51-F379A/B were installed to the exhaust drain pot 2RI02B-18". The sight glass was installed to verify the absence of condensate in the exhaust drain pot.
The internals of steam trap 2E51-D003 were removed, and replaced the seat with a seat that has a smaller "Size A" orifice. Removal of the internal parts and replacement of the seat effectively turns the steam trap into a flow restricting orifice. This minimizes the possibility of corrosion products causing failure of the steam trap due to plugging or binding. Rupture discs 2E51-D001 and 2E51-D002 were relocated from line 2RI12A-6" to 2RIA1A-6" which is connected to line 2RI02A-10". Line 2RI13A-1" was rerouted and reconnected to the subject rupture disc at its new location. The DCP implements corrective actions resulting from the root cause investigation into the blowing of the RCIC exhaust rupture discs during Unit 1 operation. Results of the investigation determined that water was ingested into the turbine, then expelled. Some of this water impinged upon the rupture discs causing them to blow. Relocation of the rupture discs to a location further away from the process line minimizes the possibility of water particles entrained in the flow from impacting the rupture disc. Magnetrol level switch 2E51-N010 was relocated such that the actuation set-point of the level switch corresponds to the mid level point of the steam supply drain pot. This corrective action results from the same root cause investigation into the blowing of the RCIC exhaust rupture discs.

Unit 2 Heater Drain Level Switch Control Support Additions, Design Change Package (DCP) 9800301
The piping systems for instruments 2LSH-HD136 and 137 were identified as not being properly supported. An "as-built" walkdown of the piping systems determined that additional supports are required to meet ANSI B31.1 code requirements. The DCP added a spring can support to each moisture separator reheater (MSR) instrument train to correct this deficiency. In addition, line 2HD38AB-1 ½", was rerouted due to thermal movement requirements. The piping meets all of the ANSI B31.1 code allowables due to the rerouting of the line and the addition of new supports. Drawings M-122 sheets 3 and 4 are revised.

Unit 2 RETS and FAS Isolation Valves, RETS, FAS, and FCD Flex Hose Connections per Design Change Package (DCP) 9800312
The DCP installed isolation valves in the relayed emergency trip supply (RETS) and fluid actuator supply (FAS) lines to the actuators of the four (4) main turbine control valves of Unit 2. It also replaced the RETS, FAS, and fluid cooling drains (FCD) tubing to these actuators with flexible hoses. Additional tubing supports were installed, as necessary. The design change reduces the potential for EHC tubing failures at the connection interface to the main turbine control valves and provides the capability to isolate individual control valve actuators in order to perform minor "on-line" maintenance. The reduction in the potential for electrohydraulic control (EHC) system tubing failures also reduces the potential for plant trips attributable to EHC failures. The proposed as-built changes correct drawing errors on the P&ID that were identified during the design review. Drawing M-116 sheet 10 is revised to reflect that the main turbine stop valves are supplied by the emergency trip supply (ETS) rather than RETS, and corrects typographical errors in labeling of several FCD lines.

Loss of Coolant Accident (LOCA) / Purge Analysis per Unit 2 Design Change Package (DCP) 9800276
This DCP analyzed and modified the VQ piping system as a result of postulating a LOCA during containment purge. During investigation of LER 97-005, it was discovered that in the event of a LOCA coincident with containment purging, the VQ ductwork could potentially rupture and VQ piping downstream of the VQ Containment Isolation Valve could experience temperature increases beyond the originally analyzed conditions. The required support modifications for Unit 2 were performed per this DCP following the completion of the thermal modes analysis for the Unit 2 VQ and VG piping, supports, and penetrations. UFSAR sections 3.0, 3.11.1.1, and Tables 3.11-28 and Table 3.11-29 are revised as a result of this design change.

Implementation of Hydrogen Addition to Unit 2 per Design Change Package (DCP) 9500083

The DCP upgraded process sample panels 2PL13J, 2PL14J, and 2PL40J in support of hydrogen water chemistry (HWC) addition to Unit 2. UFSAR Table 9.3-1 Sheets 1 and 2 are revised.

Rerouting of Pressure Sensing Line 2MS80AA-1", Design Change Package (DCP) 9800319
The DCP rerouted pressure sensing line 2MS80AA-1" to obtain the appropriate slope. Supports were added to the pressure sensing line to comply with ANSI B31.1. A condensing chamber was also added, to assure a solid leg of water to the pressure transmitter to decrease pressure fluctuations in the sensing line.

Procedure LEP-DC-113 Revision 0, Installation and Removal of Temporary Battery Charger
The procedure provides instructions to install and remove a temporary battery charger/eliminator to support permanent battery charger inspection, testing, and out-of-service. The affected DC bus is maintained available while its associated permanent charger is out of service.

Procedure LOP-DC-01 Revision 12, Battery Charger Startup and Shutdown
The procedure provides the steps necessary to startup and shut down both permanent and temporary battery chargers. It reflects temporary charger components and locations, and provides direction for opearation with the temporary charger.

DCP 98000343 and Temporary Modification 2-0073-98, Temporary Installation of Equipment to Support RHR Chemical Cleaning
The shell side of the Unit 2 residual heat removal (RHR) heat exchanger was chemically cleaned to remove scale buildup, and increase the overall heat transfer capability. This was part of an effort to re-baseline the service water system to comply with the guidelines of Generic Letter 89-13(Service Water System Problems Affecting Safety-Related Equipment).

Replacement of Offgas Preheater Steam Flow Control Isolation Valves 2N62-F313B and 2N62-F315B, Design Change Package (DCP) 9700357
The DCP replaced the upstream and downstream offgas preheater steam flow control isolation valves 2N62-F313B and 2N62-F315B. The valves were replaced due to leakage past their seats and obsolescence.

Drilling of Vent hole in Disc of HPCS High Pressure Pump Minimum Flow Valve 2E22-F012 per DCP 9800346

The DCP drilled a 1/4" vent hole in the upstream disc of valve 2E22-F012. The valve is the high pressure core sprary (HPCS) high pressure pump minimum flow valve. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. Addition of the vent hole satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

Drilling of Vent hole in Disc of RHR Supression Chamber Spray Valve 2E12-F027B per DCP 9400404
The DCP drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 2E12-F027B. The hole was drilled on the side closest to the RHR heat exchanger. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent hole also resolves the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installation satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

Drilling of Vent hole in Disc of RHR Supression Chamber Spray Valve 2E12-F027A per DCP 9400405
The DCP drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 2E12-F027A. The hole was drilled on the side closest to the RHR heat exchanger. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent hole also resolves the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installation satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

LaSalle Operating Annunciator Response Procedure (LOR) 2N62-P600-A102 Revision 1, Off Gas 2A Hydrogen/Oxygen Analyzer Trouble
LaSalle Operating Annunciator Response Procedure (LOR) 2N62-P600-B102 Revision 1, Off Gas 2B Hydrogen/Oxygen Analyzer Trouble
Design change package 9500083 upgraded process sample panels 2PL13J, 2PL14J, and 2PL40J, and associated instrumentation in support of hydrogen water chemistry (HWC) addition to Unit 2. The procedures were revised to reflect changes to the monitors, monitor setpoints, and alarm functions.

Replacement of Love Controllers 1TCS-FW911 and 1TCS-FW912 per Design Change Package (DCP) 9700360
The DCP replaced Love Controllers 1TCS-FW911 and 1TCS-FW912 with a Yokogawa digital indicating controller Model UT350-00 as a functional equivalent. The controllers

modulated seal injection flow to Unit 1 feedwater pump A. The Love Controllers are no longer manufactured, and spare parts aren't available.

Unit 2 Refueling Platform Pneumatic System Upgrades, Design Change Package (DCP) 9800287
The DCP upgraded the pneumatic system of the Unit 2 refuel platform, 2F21-E003. The entire compressed air system was replaced with a new oil-free compressor, refrigerant dryer, receiver tank, particulate filter, and new stainless steel tubing and piping. Maintaining proper air quality will reduce future personnel (machine operators) exposures, minimize maintenance costs and critical path time due to bridge breakdowns, and prevent fuel handling accidents.

Replacement of Unit 2 Refueling Platform Main Hoist Brake Assembly, Design Change Package (DCP) 9800294
The DCP replaced the main hoist safety (backup) brake assembly of the Unit 2 refuel platform, 2F21-E003, with an electric motor brake. The new brake is similar to the motor brakes used on the main hoist, the frame hoist, and the trolley hoist. This brake is an improved design that reduces impact forces from the solenoid plunger upon actuation of the brake solenoid. This failure mechanism was discussed in General Electric Service Information Letter (SIL) 530.

Installation of Test Tees for Excess Flow Check Valves per Design Change Package (DCP) 9800311
The DCP provides for an alternate method for testing Unit 2 excess flow check valves (EFCV) in the Nuclear Boiler (NB) system instrument lines.
Local leak rate testing (LLRT) is performed for the EFCVs during the Unit 2 nuclear boiler hydrostatic test, which consists of filling and pressuring the reactor pressure vessel. This often delays completion of the hydrostatic test, as valves which fail LLRT can't be certified as operable. The test tees are located between the manual isolation valve outside the primary containment penetration and the excess flow check valve (EFCV). The test tees, valves, and capped test connections provide a method of leak testing excess flow check valves with the upstream isolation valve closed, independent of the pressure vessel hydrostatic test. This will be the preferred method of testing, although leak testing during the hydrostatic test will remain an acceptable option. UFSAR Table 3.2-1 sheet 2, Table 6.2-21 Sheet 1C, and Figures 6.2-31 Sheets 9 and 10 are revised. A previously proposed change for Figure 6.2-31 sheet 10D, detail (AE), issued per DCP 9800139, is retracted.

Replacement of Fuel Pool Cooling and Cleanup Heat Exchanger Service Water Flow Control Valve 2WS128A, Design Change Package (DCP) 9500372

The DCP replaced the flangeless carbon steel Masoneilan control valve body, actuator and positioner of service water valve 2WS128A with a stainless steel Fisher-Rosemount Vee-Ball flanged control valve body with a noise attenuator ball, positioner and actuator. The carbon steel pipe spool downstream of the control valve up to isolation valve 2WS129A was replaced with stainless steel. These changes enhance the cavitation performance of control valve 2WS128A and reduce cavitation erosion in the valve and downstream piping. The new Fisher valve has a noise attenuator ball to reduce cavitation. The body of the new valve and the pipe spool are made of stainless steel, which resists cavitation induced erosion over carbon steel by 20:1.

Revision to Unit 2 P-Bypass Setpoint, Design Change Package (DCP) 9800068
DCP 9800068 revised the Unit 2 P-Bypass setpoint from less than or equal to 30% rated thermal power (RTP) to less than or equal to 25% RTP. Implementation of the revised setpoint is permitted per issuance of License Amendment number 114 to Facility Operating License NPF-18 (Unit 2). The P-Bypass setpoint is the core thermal power below which the reactor protection system scram signals initiated by turbine stop valve (TSV) closure, turbine control valve (TCV) fast closure, and end-of-cycle reactor recirculation pump (EOC-RPT) trips are bypassed. LaSalle Unit 2 has approximately a 30% steam bypass capability. A scram on turbine control valve or turbine stop valve closure is not needed until 30% RTP is reached, as adequate bypass capacity is available. Reduction of this setpoint to 25% aids the plant transient response between 25% and 30% RTP. TCV / TSV fast closure and EOC-RPT pressure switches 2C71-N003A, 2C71-N003B, 2C71-N003C, and 2C71-N003D were replaced with Ashcroft B4 series pressure switches. UFSAR Sections 7.2, 7.A.2, 15.2, 15.3, G.3, and G.5 are revised.

Installation of Bonnet Vent on Valve 2E51-F031, Design Change Package (DCP) 9600295
The DCP added a bonnet assembly to allow for a point of release of bonnet pressure in the event of a pressure locking condition of reactor core isolation cooling (RCIC) pump suppression pool suction isolation stop gate valve 2E51-F031 on pipeline 2RI17A-8". Gate valve 2E51-F031 was susceptible to pressure locking resulting from water accumulation in the bonnet area in conjunction with temperature and/or system pressure changes. Accumulated water in the bonnet may have prevented the valve from opening due to an increase in pressure in the bonnet resulting from temperature changes (increase) at the valve location or a drop in the process pipeline pressure while the trapped bonnet pressure remains high. The bonnet vent line provides a vent path to release the pressure in the bonnet to prevent pressure locking of the valve. The bonnet vent line satisfies a LaSalle commitment to Generic Letter 95-07 by providing a means to vent the bonnet. UFSAR Table 6.2-21 is revised.

Improvement of Grouding at the Unit 2 Feedwater Control System Card Racks and Replacement of Relays, Design Change Package (DCP) 9800340
The DCP upgraded the grounding system of circuit cards in panel 2H13-P612 by removing the daisy-chain style jumper wires, and replacing them with a copper bar (shorting strip) to join the common grounding terminals of each of six card racks. Each copper car was connected directly to the common ground bus. The daisy-chain wiring was suspected of creating differences in ground potentials which resulted in the creation of electrical noise, which led to offsets in calibration of Bailey 7000 series instrumentation for the feedwater system. The DCP also replaced twenty-four Aromat/Agastat relays with Potter Brumfield relays, model number KGS-17A13-120. The Aromat/Agastat relays, which were not hermetically sealed, experienced corrosion and oxidation, resulting in increased contact resistance. The increased contact resistance in low-voltage signal applications. Malfunctions in the feedwater control system have been attributed to the increased contact resistance. The replacement Potter and Brumfield relays are hermetically sealed, and have proven themselves to be consistently reliable in other applications at LaSalle Station.

Revision to UFSAR Table 6.2-21 per UFSAR change package LU1999-002
UFSAR Table 6.2-21 is revised to explicitly delete reference to LaSalle administrative procedure LAP-300-30, and to reflect the addition of monitoring to the scope of the check valve preventative maintenance program.

Deletion of Gland Seal Leakoff Line to Valve 2G33-F102 per Unit 2 Design Change Package 9500288
The DCP removed the gland seal leakoff line to the reactor water cleanup (RWCU) suction header stop valve 2G33-F102. This included removal of valves 2E31-F004F4 (manual leakoff line isolation valve), 2E31-F005F4 (solenoid operated leakoff line isolation valve), and sightglass 2E31-D001F4. Upgraded packing was installed in the upper and lower packing glands to significantly reduce leakage.

Flood Seals for Penetrations 2TB-1201 and 2TB-1202, Design Change Package (DCP) 9900002
The DCP provides the modified design detail of flood seals for penetrations 2TB-1201 and 2TB-1202 which correspond to lines 2RI07B-2" and 2RT09B-4", respectively. The 4" penetration was grouted without a sleeve, and angle iron was welded to the penetration sleeve on both ends of the opening to act as reinforcement to prevent the grout plug from coming out during a postulated flood. The 2" hot pipe penetration was insulated and fitted with an extension sleeve made of a minimum gauge 20 galvanized sheet prior to grouting and the installation of a water seal.

The seals for penetrations 2TB-80, 248, 249, 250, 251, 1200, 1203, 1204, 1205, and 1206 were replaced with a fiberglass reinforced rubber boot around the opening sleeve and the pipe. The boot was then sealed along its longitudinal seam and clamped in place around the sleeve of the opening and the pipe.

Installation of Backdraft Dampers per Design Change Package (DCP) 9800194
The DCP installed two manual backdraft dampers, 0VC73YA and 0VE80YA in the normal outside makeup air ducts for the Train A control room (VC) and auxiliary electric equipment room (VE) ventilation systems. The dampers were added to prevent backflow of air during emergency makeup filter unit operation, ensuring that the entire flow goes to the control room and auxiliary electric equipment room as intended. Drawings M-1443 sheets 1 and 3 are revised.

Unit 2 Division 1 Core Standby Cooling System Local Flow Indicators and Motor Operated Valve Removal, Design Change Package (DCP) 9800320, Addendum 2
The addition of the 2FE-DG124 orifice flanges, to house a flow measurement device, was previously evaluated based upon flanges specified as carbon steel. DCP 9800320 installed stainless steel flanges. The stainless steel is considered a more noble metal than surrounding carbon steel piping, and is not susceptible to galvanic corrosion. Drawing M-134 sheet 3 is revised.

Turbine Building Supply Airflow Reduction for Turbine Building Negative Pressure, Design Change Package (DCP) 9700398
The DCP reduced the supply air to the Turbine Building to ensure a negative pressure is maintained by installing new balancing dampers 2VT106Y and 2VT107Y on the common supply air header of the turbine building ventilation (VT) supply fans 2VT01CA, 2VT01CB, and 2VT01CC. Two recirculation dampers were added in the common supply fan discharge duct, to reduce the total VT system supply flow to the turbine building, to route part of the fan discharge flow back to the inlet side of the fans. Various VT system instrumentation setpoints and ranges were adjusted to accommodate the change in system air flows.

Out-Of-Service (OOS) 980009391
OOS 980009391 provided administrative controls for the Unit 2 primary containment vent and purge system isolation valves to prevent their inadvertent operation while outboard isolation valves 2VQ036 and 2VQ040 were removed for maintenance. OOS 980009391 maintained inboard isolation valves 2VQ031 and 2VQ034, and isolation bypass valves 2VQ031 and 2VQ034 closed.

Installation of Manual Vacuum Breaker Downstream of Valve 2E12-F021 per Design Change Package (DCP) 9800344
The DCP installed a one-inch pipe with manual globe valves and a pipe cap downstream of the Unit 2 residual heat removal (RHR) C full flow test return line stop valve, 2E12-F021. This modification provides a convenient means of breaking vacuum and draining down the line following a full flow test to protect against water hammer. Drawing M-142 sheet 3 is revised.

Material Upgrade for Erosion Corrosion Control On Blowdown Piping to Condenser of Unit 2
The material upgrade for piping 2TEF2A-3" consisted of replacing the section of carbon steel pipe from control valve 2GS-AOV-EDV-C to the condenser with chrome-moly pipe. The material upgrade for piping 2GS09A-1" consisted of replacing the section of carbon steel piping from the steam steal evaporator to the floor penetration at elevation 768'-0" with chrome-moly pipe. Drawing M-116 sheet is revised to reflect the material control upgrades of the piping.

Administrative Technical Requirements 3.3.7.9
Administrative Technical Requirements (ATR) 3.3.7.9 is revised to change the surveillance requirements so that fire detection instruments which are accessible during unit operation, with the exception of ultraviolet fire detectors on the refuel floor, be demonstrated operable at least once per 12 months by the performance of a channel functional test. The ATR surveillance requirements for the refuel floor ultraviolet fire detectors remain once per six months.

Line Freeze for 2DG14A-6"
A freeze seal/plug was installed on line 2DG14A-6" at elevation 684'-0" in the Offgas Filter Building. The freeze was required to support an out of service boundary for work on valve 2DG023 and possible line plugging on northeast area cooler 2VY04A. 2DG023 is the cooling water supply side valve to 2VY04A.

Contingency Replacement of Obsolete Static-O-Ring Pressure Switches for LPCS/LPCI Injection Valve, Injection Line, and Reactor Vessel Low Pressure Permissive, Design Change Package (DCP) 9900013
The DCP provided for a contingency replacement of Static-O-Ring (SOR) pressure switches for low pressure core spray/low pressure coolant injection (LPCS/LPCI) injection valve, injection line, and reactor vessel low pressure permissive. The change applies to pressure switches 1(2)B21-NB413A, 413B, 413C, 413D, 1(2)E12-N413A, 1(2)E12-N413B, 1(2)E12-N413C, and 1(2)E12-N413D. SOR model 5N6-B45-NX-C1A-JJTTX6/X7 and 5N6-E45-NX-C1A-JJTTX6/X7 pressure switches are obsolete, and are no longer manufactured. SOR model 5N6-B45-U8-C1A-JJTTNQ switches are the vendor

recommended replacement that are of the same form, fit, and function. The DCP issued a drawing change only and required no fieldwork. Drawing M-1340 Sheet 179 contains notes that define requirements which must be implemented with replacing one of the switches.

Replacement Breaker for RHR Valve 2E12-F042A, Design Change Package (DCP) 9900043
The DCP changed the magnetic trip setting for residual heat removal (RHR) low pressure coolant injection (LPCI) valve 2E12-F042A. The setpoint was changed from 112 amps to 150 amps. To accomplish the higher magnetic trip setting, the molded case circuit breaker at motor control center 235Y-2 compartment C5 was replaced with a Klockner-Moeller model NZMH-6-63/ZM 6-33-200-OBI-CAN circuit breaker. The new breaker and the 150 ampere setting provides a greater margin for preventing nuisance trips of valve 2E12-F042A during motor starting conditions.

High Temperature Lead Wire Replacement on Valcor Solenoid Valves – Containment Monitoring, Design Change Package 9000250 (DCP) Revision 1
The DCP installed equipment qualification (EQ) high temperature wire to replace deteriorated lead wires on the following Valcor solenoid valves which provide containment monitoring isolation functions: 2CM17A, 2CM17B, 2CM18A, 2CM21B, 2CM23B, 2CM27, 2CM28, 2CM29, 2CM30, 2CM31, and 2CM32.

Snubber Replacements per Design Change Package (DCP) 9500095 and 9500096
DCP 9500095 replaced mechanical snubber M09-RR00-1053S of the reactor recirculation system with a hydraulic snubber.
DCP 9500096 replaced mechanical snubbers M09-RR00-1032S and M09-RR00-1025S of the reactor recirculation system with hydraulic snubbers. Hydraulic snubbers are better suited an environment with high frequency low amplitude vibrations. Reactor recirculation system piping has been identified with this type of vibration.

LOP-SC-07 Revision 3, Standby Liquid Control Tank System Flushing Procedure
The procedure revision permits installation of floor drain plugs per the procedure. Previous floor drain plugs would be installed as a temporary modification per a separate procedure.

As-Built Change to Drawings M-104 Sheets 2 and 3
Drawings M-104 Sheets 2 and 3 are revised to reflect that the drain line from instrument panel 1H22-P025 drains into a floor drain on 694'6" in the residual

heat removal heat exchanger room as opposed to being hard piped into a floor drain header; drain lines from instrument panels 1H22-P006 and 1H22-P010 drain to a floor drain on elevation 694'6" in the reactor building as opposed to being hard piped into a floor drain header; the drain lines from coolers 1VY03A and 1VY04A drain to a floor drain at elevation 694'6" in the reactor building; proper row and column numbers of four floor drains.

Addendum to Design Change Package (DCP) 9700621
The addendum to the DCP replaced a defective SOR model 6N6-B45-NX-C1A-JJTTX7 pressure switch with a SOR model 6N6-B45-U8-C1A-JJTTNQ pressure switch. The defective pressure had failed during implementation of the setpoint change specified in the original DCP.
Replacement of Valve 2B21-F070 per Design Change Package (DCP) 9900036
The DCP replaced the 3" Anderson Greenwood main steam drain line valve 2B21-F070 with a 2.5" Edwards valve. The Anderson Greenwood valve was obsolete. The new valve has slightly different flow characteristics, however it provides the same design functions of the original valve. P&ID M-116 Sheet 7 is revised.

As-Built Change to Drawing M-66 Sheets 1 and 2
Drawings M-66 sheets 1 and 2 are revised to reflect the as-built condition to reflect the properly orientation of check valves 1C51-J009-6 and 1C51-J009-6. The check valves contribute to the containment isolation function in the event of a failure of the traversing incore probe (TIP) system.

As-Built Drawing Change Request Tip Purge Valve Assembly 2C51-J009
Drawing M-66 Sheet 3, Unit 2 Drywell Pneumatic System, was revised to reflect the as-built condition of the traversing incore probe (TIP) purge valve assembly 2C51-J009. The valve assembly was previously modified to reflect changes shown in General Electric (GE) Field Disposition Instruction (FDI) dated 2/11/82. The FDI added a new purge air control panel, modified TIP purge equipment, and index mechanisms. The upgrade to the purge system protects the TIP detectors and other components from dependence upon the quality of installation.

Revision to UFSAR Subsection 7.3.2.2.3.8
UFSAR subsection 7.3.2.2.3.8 was revised per the validation to resolve conflicting changes proposed by DCP 9700532 (High Energy Line Break (HELB) Leak / Break Detection Modification) and DCP 9700208 (Reactor Water Cleanup System Recirculation Pumps and Return to Hot Suction). Index page 7.0-iii is also revised.

DCP 9500485 – Install Filter in 2FW01KA/B Turbine Driven Reactor Feed Pump
The DCP added in-line filters to the high pressure control and hydraulic oil piping just before the turbine driven reactor feed pump (TDRFP) turbine controllers. One duplex filter was added to each TDRFP, 2FW01KA and 2FW01KB. The new filtration system was added to trap fine particles that could affect the lockout and other valves in the control system.

Revision to UFSAR Sections 6.5, 7.3, 9.5, and H.3
UFSAR Sections 6.5, 7.3, 9.5, and H.3 are revised to correct previously identified discrepancies relating to the description of the operation of the charcoal filter deluge system. These changes correct the UFSAR description to correspond with LaSalle operating procedure LOP-FP-05, Charcoal Filter Beds Manual Deluge Valve Reset Operation and Initiation.

Design Change Package (DCP) 9500288
DCP 9500288 deleted the leak-off line for reactor water cleanup (RWCU) suction stop valve 2G33-F102 from the valve to the pipe header 2REH9A-2", along with associated supports and in-line components. UFSAR Figure 7.3-7 Sheet 2 is revised to reflect the deletion of the leak-off line.

Unit 2 High Energy Line Break (HELB) Leak / Break Detection Modification, DCP 9700533
The DCP modified the Leak Detection System for the Reactor Water Cleanup (RWCU), Reactor Core Isolation Cooling (RCIC), and the Residual Heat Removal (RHR) systems of Unit 2 to resolve a concern identified with the original Leak Detection calculations. The modifications generally consisted of temperature sensor relocation, addition of temperature monitoring functions, and addition of a high flow monitor for HELB.
UFSAR Subsections 5.2.5.1, 5.2.5.1.2, 5.2.5.5.4, 5.4.7.3.1, 7.4.1.2.6, 7.6.2.2.4, 7.6.2.2.5, 7.6.2.2.6, 15.9.3.4, Table 5.2-8, Table 7.3-2, and Figure 7.3-7 are revised accordingly.

Out of Service (OOS) 950004941
This safety evaluation was written for the OOS which was in effect for a prolonged period of time. OOS 950004941 provided administrative controls to isolate and de-energize acid and caustic feed pumps for the condensate polishing system, and prevent acid or caustic instrusion into the cycled condensate system, pending their demolition or abandonment in place.

Installation of Permanent Shielding on 2FC04BA-8" For Radiation Monitors, per Design Change Package (DCP) 9800171
The DCP installed permanent shielding on Unit 2 fuel pool cooling line 2FC04BA-8". The line was permanently shielded to reduce the general background dose in the area and to reduce the radiation exposure of nearby radiation detectors, 2D18-N015A, B, C, and D. These detectors monitor the presence of radiation in a HVAC duct that is released to the pipe. The permanent shielding replaces previously installed temporary shielding.

Replacement of Sections of Pipe 2RI07B-2" through Penetrations MK-2RB-40 and MK-2RB-48, per Design Change Package (DCP) 9900022
The design change decreased the size of the reactor core isolation cooling (RCIC) supply steam drain pot drain line to condenser (2RI07B-2") from 2" down to 1.5" pipe where it passes through penetrations MK-2RB-40 and MK-2RB-48. Due to flow accelerated corrosion concerns (FAC), some carbon steel sections of line 2RI07B-2" were replaced with chrome moly A335 piping. Utilizing sections of the 2" carbon steel pipe as sleeves for the new 1.5" chrome moly pipe provided a means to reduce radiation dose to personnel. Drawing M-147 Sheet 1 is accordingly revised.

Unit 1 P-Bypass Setpoint Change, Design Change Package (DCP) 9800067
The DCP changed the Unit 1 P-bypass setpoint from $\leq$ 30% of reactor thermal power (RTP) to $\leq$25% of RTP. The P-bypass setpoint is the RTP level below which the reactor protection system scram signals initiate stop valve closure, turbine control valve fast closure, or end of cycle recirculation pump trip are bypassed. This change resolves difficulties associated with low power transient response analysis required at each fuel reload. The DCP incorporates Amendment 130 to facility license NPF-11, approved February 12, 1999. UFSAR Sections 6.B, 7.2, 7.A.2, 15.2, 15.3, G.3, and G.5 are revised.

Service Air Receivers Drain Trap Upgrades, Design Change Packages (DCPs) 9700311, 9700312, and 9700313
DCPs 9700311, 9700312, and 9700313 upgraded the service air receiver traps for Units 0, 1, and 2, respectively. The applicable equipment part numbers are 0SA01DA, 0SA03M, 1SA01DA, 1SA03M, 2SA01DA, and 2SA03M. The upgrades consisted of adding redundant isolation valves on the cross-tie on the receiver supply lines, swapping of the inlet and outlet ports on the air receiver to reflect the original vendor design, replacing the drap with a newer style trap, and modifying pipe supports to accommodate new piping loads. The DCPs enhance the reliability of the isolation valves, the train traps, and allows the receivers the operate as designed. UFSAR Section 9.3, Table H.3-2, and drawing M-82 sheet 1 are revised accordingly.

Contingency Replacement of Obsolete Static-O-Ring Pressure Switches for HPCS Discharge Pressure Minimum Flow Bypass, and LPCS/LPCI Discharge Pressure ADS Permissive Pressure, Design Change Package (DCP) 9900080
The DCP provided for a contingency replacement of Static-O-Ring (SOR) pressure switches for high pressure core spray (HPCS) discharge pressure minimum flow bypass, and low pressure core spray/low pressure coolant injection (LPCS/LPCI) discharge pressure automatic depressurization system (ADS) permissive pressure.
The change applies to pressure switches 1(2)E12-N016A, B, C; 1(2)E12-N019A, B, D; 1(2)E21-N001, 1(2)E21-N009, and 1E22-N012A and B.
SOR model 5N6-B5(45)-NX-C1A-JJTTX6/X7 pressure switches are obsolete and are no longer manufactured. SOR model 5N6-B5(45)-U8-C1A-JJTTNQ switches are the vendor recommended replacement that are of the same form, fit, and function. The DCP issued a drawing change only and required no fieldwork. Drawing M-1340 Sheet 180 contains notes that define requirements which must be implemented when replacing one of the switches.

Addendum to Design Change Package (DCP) 9700491, Removal of Remote Indication Hardware from Unit 2 Division 2 Emergency Core Cooling System (ECCS) Testable Check Valves
DCP 9700491 removed remote indication hardware from Unit 2 Division 2 ECCS testable check valves 2E12-F041B, 2E12-F041C, and 2E12-F050B, to eliminate a recurring problem in which the valves fail to completely close. An addendum to the modification removed the requirement to perform an injection test to verify valve function in the open direction. This test was not required and not performed in Unit 2.

Addendum to Design Change Package (DCP) 9700490, Removal of Remote Indication Hardware from Unit 2 Division 1 Emergency Core Cooling System (ECCS) Testable Check Valves
DCP 9700490 removed remote indication hardware from Unit 2 Division 2 ECCS testable check valves 2E12-F041A, 2E12-F050A, and 2E22-F006, to eliminate a recurring problem in which the valves fail to completely close. An addendum to the modification removed the requirement to perform an injection test to verify valve function in the open direction. This test was not required and not performed in Unit 2.

UFSAR Revision for Drilling of Vent Hole in Valve 1E22-F012 per Design Change Package (DCP) 9800347
The DCP drilled a 1/4" vent hole in the upstream disc of valve 1E22-F012. The valve is the high pressure core spray (HPCS) high pressure pump minimum flow valve. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. Addition of the vent hole satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

Installation of Continuous Oxygen Monitor per Unit 2 Design Change Package (DCP) 9400072
This DCP removed the drywell humidity monitoring system (trains A & B) and installed a new continuous oxygen monitoring system for sampling suppression chamber air and drywell air. The drywell sample line was reused. The return line to the suppression chamber was rerouted to a new containment penetration and is to be used as a sample line to obtain the suppression chamber sample. This design change installed a dedicated system to continuously monitor suppression chamber and drywell oxygen concentration and eliminated the use of the Post-LOCA containment monitoring system for drywell oxygen concentration monitoring during normal plant operation.

Implementation of Hydrogen Addition to Unit 2 per Design Change Package (DCP) 9500083
The DCP upgraded process sample panels 2PL13J, 2PL14J, and 2PL40J, and associated instrumentation in support of hydrogen water chemistry (HWC) addition to Unit 2. A remote test gas applicator for Unit 2 hydrogen area monitors 2P71-N151 and 2P73-N403 was installed to perform routine calibration of the ceiling mounted monitors. Moisture separators were replaced with drain traps to improve system performance. Heat tracing for the drain traps was deleted since it is not required for operation of the drain traps. UFSAR Table 9.3-1 Sheets 1 and 2 are revised.

Replacement of Unit 2 Hotwell Level Recorder per Design Change Package (DCP) 9400108
The DCP replaced the Unit 2 hotwell lever recorder 2LR-CD031 with a model manufactured by Yokogawa. The previous Bailey model recorder is obsolete, is no longer manufactured, and spare parts became unavailable.

Consolidation of Emergency Operations Facilities
Commonwealth Edison (ComEd) has consolidated its four near-site emergency operations facilities (EOFs) and corporate EOF into a single EOF. NRC approval of ComEd's proposed change is documented in NRC letter dated February 9, 1999 from Mr. Stuart Richards (NRC) to Mr. Oliver Kinsley (ComEd). "Corporate Emergency Operations Facility (CEOF)," and "Backup Emergency Operations Facility (BEOF) (Zion only)," are correspondingly deleted in UFSAR Section 13.3. Additionally, and editorial change revises "Site Area Emergency" to "Site Emergency" in UFSAR Section 13.3

Revision to UFSAR Section 9.2 for the Core Standby Cooling System Equipment Cooling
Core Standby Cooling System (CSCS) equipment cooling flow rates, specifically those of the northwest, southwest, southeast, and northeast cubicle area cooling coils are revised to reflect station efforts to re-balance the CSCS equipment cooling water system per the implementation of NRC Generic Letter 89-13.

Activities required for compliance to NRC Bulletin 96-03
Implementation of NRC Bulletin 96-03 "Potential Plugging of Emergency Core Cooling Suction Strainers by Debris in Boiling Water Reactors" was evaluated for LaSalle Units 1 and 2. Safety Evaluations governing upgrading of the suction strainers are included with each of the implementing design change packages. The Bulletin requires BWR licensees to implement appropriate measures to ensure the capability of the ECCS to perform its safety functions following a LOCA.
The following implement the proposed change:
LaSalle Administrative Procedure LAP-400-20 "Primary Containment Debris Material Control Program", Revision 0;
LaSalle Surveillance Procedure LTS-600-41 "Primary Containment Inspections for ECCS Suction Strainer Debris Sources", Revision 0;
LaSalle Maintenance Procedure LMP-GM-80 "Suppression Chamber Desludging", Revision 0;
Unit 1 design change packages 9600290, 9700300, 9700301, 9700302, 9700303, and 9700304;
Unit 2 design change packages 9600291, 9700543, 9700544, 9700545, 9700546, and 9700547;
Safety Evaluation Report (SER) for NEDO-326896, Revision 0 "Utility Resolution Guidance Document for ECCS Suction Strainer Blockage", NRC Office of Nuclear Reactor Regulation, August 20, 1998;
Calculation L-002051, ECCS Strainer Head Loss Performance Analysis, Revision 1;
Calculation L-001222, Estimation of Worst-Case Unit 1 RMI Debris Inventory Available for Transport to the Suppression Pool", Revision 1;
Calculation L-001261, Estimation of Worst-Case Unit 2 RMI Debris Inventory Available for Transport to the Suppression Pool", Revision 1;
Previous installation of larger capacity passive strainer designs performed by Design Change Packages (DCPs) 9600290, 9700300, 9700301, 9700302, 9700303, and 9700304 for Unit 1, and DCPs 9600291, 9700543, 9700544, 9700545, 9700546, 9700547 for Unit 2 accomplish the necessary physical changes for implementing Option 1 of NRC Bulletin 96-03. The replacement strainers significantly increase the surface and flow area so as to improve the ECCS pumps' ability to maintain adequate Net Positive Suction Head (NPSH) during potential plugging from fibrous material and other debris transported into the Suppression Pool under LOCA conditions.

LaSalle Administrative Procedure LAP-400-20 "Primary Containment Debris Material Control Program", Revision 0 establishes a new LaSalle Administrative Procedure which defines the program, necessary requirements and assigns responsibilities to ensure compliance with Bulletin 96-03.
LaSalle Surveillance Procedure LTS-600-41 "Primary Containment Inspections for ECCS Suction Strainer Debris Sources", Revision 0 is required to demonstrate through periodic inspections that the required ECCS pump NPSH is available in regard to strainer plugging. This is accomplished by assuring that debris quantities remain below design limits. LaSalle Maintenance Procedure LMP-GM-80 "Suppression Chamber Desludging", Revision 0 is required to define the actions necessary to maintain potential wetwell strainer plugging debris quantities below those used in the design basis.
Calculation L-002051 Revision 1, "ECCS Strainer Head Loss Performance Analysis", was required to determine the performance of the new LaSalle ECCS suction strainers in terms of expected head loss under DBA (LOCA) conditions in accordance with NRC SER for NEDO-326896, Revision 0, "Utility Resolution Guidance Document for ECCS Suction Strainer Blockage", dated August 20, 1998.
Calculation L-001222 Revision 1, "Estimation of Worst-Case Unit 1 RMI Debris Inventory Available for Transport to the Suppression Pool", was required to determine the quantity of RMI debris generated for possible transport to the Unit 1 Suppression Pool during a LOCA in accordance with NRC SER for NEDO-326896, Revision 0 "Utility Resolution Guidance Document for ECCS Suction Strainer Blockage", dated August 20, 1998.
Calculation L-001261 Revision 1, "Estimation of Worst-Case Unit 2 RMI Debris Inventory Available for Transport to the Suppression Pool", was required to determine the quantity of RMI debris generated for potential transport to the Unit 2 Suppression Pool during a LOCA in accordance with NRC SER for NEDO-326896, Revision 0 "Utility Resolution Guidance Document for ECCS Suction Strainer Blockage", dated August 20, 1998.
UFSAR Section 6.3.2.2.6, and ECCS pumps characteristic curves Figures 6.3-3, 6.3-6, and 6.3-9, are accordingly revised.

Procedure LLP-99-002, Revision 0, Unit 2 Main Condenser Circulating Water Side Chemical Cleaning
The procedure controlled the chemical cleaning of the circulating water side of the Unit 2 main condenser. Cleaning of the condenser removed tube scale, to increase cycle efficiency. Sulfuric acid was injected into the circulating water pump discharge piping with the circulating water system in operation. The resultant low pH acidic water dissolved the calcium carbonate scale to improve heat transfer.

Drilling of Vent Hole in RHR Valves 1E12-F027A

Design Change Package (DCP) 9400401 drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 1E12-F027A. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent hole also resolves the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installation satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

Drilling of Vent Hole in RHR Valve 1E12-F027B
Design Change Package (DCP) 9400402 drilled a 1/4" vent hole in the upstream side of the 'A' residual heat removal (RHR) suppression chamber spray isolation valve 1E12-F027B. The hole provides a vent path to prevent pressure locking which may result from water being trapped in the bonnet area. The vent hole also resolves the potential for bonnet over-pressurization which can occur as the ambient temperature increases. The vent hole installation satisfies a LaSalle commitment to Generic Letter 95-07. UFSAR Table 6.2-21 is revised.

UFSAR Update to Table 8.3-1
UFSAR Table 8.3-1, Load on 4160-Volt ESF Buses, identifies the coincidental loading on the 4160 volt ESF buses following a Loss Of Coolant Accident (LOCA) on Unit 1 and a simultaneous Loss Of Offsite Power (LOOP) for both units. The table is revised to correct calculational errors, and to correct sum totals of the loads to reflect revised loads.

Revision to UFSAR Sections 3.4 and 3.11
UFSAR Subsections 3.4.1.1, 3.4.1.4, 3.11.1.4.2, and Figures 3.4-1 and 3.4-2 are revised to more accurately describe the actual design and flood protection measures at LaSalle. The changes concern results from an operability assessment and walkdowns. Various design basis deficiencies associated with the location of certain lake-connected piping relative to the condenser pit flood zone, and deficiencies discovered with the elevation of certain ventilation ducts associated with the core standby cooling system (CSCS) and equipment water cooling system (ECWS) pump room flood zone, are addressed by the UFSAR changes.

Replacement of Relay House System 1 125 Volt DC Batteries, Design Change Package (DCP) 9900041
DCP 9900041 replaced the System 1 125 volt DC batteries in the Relay House. The previous batteries were 60 cell, 200 Ampere-hour batteries. The new batteries are 58 cell 270 Ampere-hour batteries. The original batteries were 25 years old and near the end of life. The new batteries improve the reliability of the control power supplied to the 345 kV switchyard breakers and the protective

relay systems associated with the transmission lines. UFSAR Section 8.2.1.5 is revised.

Replacement of Relay House System 2 125 Volt DC Batteries, Design Change Package (DCP) 9900042
DCP 9900042 replaced the System 2 125 volt DC batteries in the Relay House. The previous batteries were 60 cell, 200 Ampere-hour batteries. The new batteries are 58 cell 270 Ampere-hour batteries. The original batteries were 25 years old and near the end of life. The new batteries improve the reliability of the control power supplied to the 345 kV switchyard breakers and the protective relay systems associated with the transmission lines. UFSAR Section 8.2.1.5 is revised.

Administrative Technical Requirements (ATR) Amendment 25
ATR Amendment 25 changed the maximum isolation time for the reactor water cleanup isolation valves and added valves to ATR Table 3.6.3-2 as follows. Reactor water cleanup isolation valves 2G33-F001 and 2G33-F004 (isolation time revised), primary containment ventilation relief valves 2VP197A, 2VP197B, 2VP198A, and 2VP198B, residual heat removal system relief valve 2E12-F460, reactor building closed cooling water relief valves 2WR225 and 2WR226, and reactor recirculation system relief valve 2B33-F395.

A safety evaluation documented the station's acceptance of the Unit 2 cycle 8 reload licensing package and supporting evaluations, analyses, and documentation to support startup and operation of Unit 2 with Siemens ATRIUM-9B fuel.

Revision to UFSAR Appendix H
UFSAR Appendix H Subsection H.4.2.47.2 is not related to the suppression pool cooling path, as the valves described are not associated with a suppression pool cooling path. The only RHR loop A cables or equipment in fire subzone 4E2-1 necessary for safe shutdown is a flow indicator circuit. The revised discussion describes the indication available in lieu of a flow indicator.
Tables H.4-51 (Sheet 6 of 6), H.4-58 (sheet 5 of 5), H.4-65 (Sheet 4 of 5), H 4-68 (Sheet 6 of 6), H.4-70 (Sheet 7 of 7) and H.4-104 (Sheet 2 of 2) are revised to correct an erroneous cable number. Plant walkdowns and drawing reviews determined that an incorrect safe shutdown cable number is stated in the above Tables.

Administrative Technical Requirements (ATR) Amendment 24

The Unit 2 main steam isolation valve (MSIV) leakage control system (LCS) was deleted by design change packages (DCPs) 9500168, 9500169, 9600092, 9600263, and 9600264. Unit 2 Facility Operating License Amendment 97 approved the deletion of the Unit 2 MSIV Leakage Control System and the establishment of the MSIV alternate leakage paths to allow 100 scfh per line for a total maximum MSIV leakage limit of 400 scfh. This makes Units 1and 2 the same in this respect. MSIV alternate leakage paths are the analyzed paths for MSIV leakage to leak to the environment as a ground level release from the main condenser.
The change to ATR 3/4.6.1.4 makes it applicable to the Unit 2 MSIV Alternate Leakage Paths, and includes a table of the associated Unit 2 motor operated valves (MOVs). Drawing M-116 sheet 8 was voided.

Out of Services (OOS) 970011070 and 970009753
This safety evaluation was written for the OOSs which have been in effect for a prolonged period of time. The reactor building tendon tunnel floor drain sump pump 2RF04P was taken out of service by OOS 970011070. The reactor building tendon tunnel floor drain sump pump 2RF04P trouble alarm 2PM13J-B403-07A was taken out of service by OOS 970009753. Following failure of the motor of sump pump 2RF04P, the pump was taken out of service to prevent the motor from operated and causing further damage. The circuit for sump pump trouble alarm 2PM13J-B403-07A was taken out of service due to a ground fault. The out of services were to remain in effect until repairs were made to correct the deficient conditions.

Procedure LLP-99-012 Revision 0, MSR Test Equipment Installation
The procedure governs the installation of test equipment for monitoring the Unit 2 moisture separator reheater (MSR) system during startup and periodically during operation.

Out of Service (OOS) 970000269
This safety evaluation was written for the OOS which were in effect for a prolonged period of time. Radwaste floor drain system relief valve 2WF289 was damaged and required replacement. Valves, breakers, and pumps in the radwaste floor drain, cycled condensate water, and auxiliary power systems were administratively taken out of service to stop water and steam in the pipe segments on both sides of 2WF289.

Procedure LLP-99-007 Revision 0, Test Equipment Installation To Support Heater Drain Tuning
The procedure installed temporary pressure transducers on the input and output signals of various heater drain controllers in support of Unit 1 heater drain system control valve tuning.

DCP 9900018, Rendering Unit 2 Blanketing Steam Non-functional
The station does not presently utilize blanketing steam from the auxiliary boiler for the first and second stages of the moisture separator reheaters 2TG03AA and 2TG03AB. For this reason, the following was performed per DCP 9900018: Removed valve 2B21-2BSFV2; Abandoned in place valves 2B21-2BSFV1, 2B21-1BSFV1, and 2B21-1BSFV2, and associated hand switches; Added pipe caps to lines 2MS53CA-1" and 2MS53BA-3" to isolate auxiliary steam from main steam header 2MS38FA-12".

LaSalle Operating Procedure LOP-AS-04 Revision 8, Startup of the Inerting Steam Electrode Boilers, Startup of the Steam Inerting of the Reheater Tube Bundles, and Shutdown of the Steam Inerting of the Reheater Tube Bundles
The procedure was revised to reflect design change package 9900118, which rendered the Unit 2 blanketing steam non-functional.

Revision to UFSAR Table 6.2-21 and Figure 6.2-31
UFSAR Table 6.2-21 and Figure 6.2-31 are revised to reflect the correct valve arrangement and figure detail for containment penetration M-37. The revised UFSAR Figure 6.2-31 contains a new detail showing the configuration of the clean condensate (MC) system piping and valve drops inside the primary containment.

Installation of Accumulators in Unit 1 EHC at Main Turbine Control, Design Change Package (DCP) 9500450
The DCP installed an accumulator / manifold assembly to each of the four (4) Unit 1 turbine control valves (TCVs). This serves to reduce pressure pulsations seen in electrohydraulic control systems (EHC). Pressure pulsations have been found to cause line breaks in EHC systems resulting in unit shutdown. General Electric (GE) recommended this in Technical Information Letter (TIL) 1123-3. Drawing M-55 sheet 10 is revised.

Removal of Packing Leak Off Line from 2B33-F023A per Design Change Package (DCP) 9600120
DCP 9600120 removed the packing leakoff line from reactor recirculation (RR) suction valve 2B33-F023A. UFSAR Figure 7.3-7 Sheet 2 is revised.

Evaluation of the Radiological Consequences of Core Reload with Siemens ATRIUM-9B Fuel

The change to Siemens ATRIUM-9B fuel required an evaluation of the radiological consequences for the rod drop, fuel handling, and cask drop accidents. This was due to the higher exposure and fuel rod fission product inventory of Siemens fuel. UFSAR Sections 7.7, 15.4, and 15.7 are revised. The associated Core Operating Limits Report was approved Administrative Technical Requirements (ATR) Amendment 26.

UFSAR Revision to Reflect the Unit 2 Cycle 8 Reload Licensing Package
UFSAR Sections 1.2, 1.6, 3.1, 3.9, 4.0, 5.0, 4.1, 4.2, 4.3, 4.4, 5.2, 6.0, 6.3, 6.B, 6.3, 7.7, 10.4, 15.0, 15.1, 15.2, 15.3, 15.4, 15.5, 15.6, 15.7, 15.8, 15.A, G.3, and G.7 are revised for Unit 2 Cycle 8 operation. The changes reflect Unit 2 operation with fuel manufactured by Siemens Power Corporation (SPC) and General Electric (GE). SPC Atrium 9B fuel and analytical methodologies are reflected in the changes. The associated Core Operating Limits Report was approved Administrative Technical Requirements (ATR) Amendment 26.

UFSAR Update for Lost Parts Analyses
UFSAR Subsection 4.2.3.13 and 4.2.5 are revised to reflect the new lost parts analysis from Siemens Power Corporation (SPC) and the latest revision to General Electric's lost parts document (NEDO-10174, Revision 1). The SPC analysis was performed in support of introducing the use of ATRIUM-9B fuel at LaSalle Station.

UFSAR revision per High Energy Line Break (HELB) Re-analysis
The UFSAR is revised to reflect new environmental parameters following a HELB. The reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) HELB calculation initially was being revised as a result of design change packages (DCPs) 9700208 and 9700209, which return the RWCU system to hot suction. Review of the calculation led to the identification of non-conservatisms (Licensee Event Report 97-033). Corrective action modifications were subsequently implemented. The following UFSAR changes revise the reactor building parameters and equipment qualification (EQ) zones. UFSAR Sections 3.0, 3.6, 3.11, Table 3.11-6, and Figure 3.11-1 Sheets 1, 2, 3, and 4 are revised.

Installation of Manual Vacuum Breaker Downstream of Valve 1E12-F021 per Design Change Package (DCP) 9800345
The DCP installed a one-inch pipe with manual globe valves and a pipe cap downstream of the Unit 1 residual heat removal (RHR) C full flow test return line stop valve, 1E12-F021. This modification provides a convenient means of breaking vacuum and draining down the line following a full flow test to protect against water hammer. UFSAR Figure 6.2-31 sheet 7, Table 6.2-21, and Drawing M-96 sheet 3 are revised. A new sheet is added to Figure 6.2-31.

Degraded Voltage Relay Setpoint Changes for Unit 1, Design Change Packages (DCP) 9500018, 9500019, and 9500030

Design Change Packages (DCPs) 9500018 and 9500019 revised the trip setpoint of Unit 1 Buses 141Y and 142Y degraded voltage relays from 3885 volts to 3870 +/- 7 volts. These DCPs also reduce the trip setpoint of the system auxiliary transformer (SAT) winding undervoltage (UV) relays from 4040 volts to 3500 volts. DCP 9500030 revised the Unit 1 Bus 143 degraded voltage relay trip setpoint from 3814 volts to 3870 +/- 7 volts. These DCPs were required to bring the degraded voltage protection circuit in compliance with the safety analysis report design bases requirements and GDC-17. LaSalle committed to implement the Unit 1 degraded voltage setpoint changes prior to startup from L1R08.

UFSAR Section 8.2.3.3 is revised to change the setpoint for the Unit 1 second level undervoltage (degraded voltage) protection and to provide the lower and upper analytical limits for this parameter. The new values for the trip setpoint (3870 V), lower analytical limit (3814 V), and upper analytical limit (3900 V) are in conformance with Unit 1 Facility Operating License NPF-11 Amendment 135. UFSAR Table 8.3-2 is revised to add the protective functions of the degraded voltage relay. The purpose of this table is to summarize the relay protection for ESF 4160-volt equipment, but it currently does not identify the protective functions provided by the degraded voltage relays. This change applies to both units.

Valve 2E51-F091 was physically removed from the RCIC System by DCP 9500158, which was completed on 8/16/96. The removal of the valve from the system was evaluated. The 2E51-F091 valve (RCIC Steam to RHR warmup valve), previously used in the Steam Condensing Mode of RHR, has been deleted since the steam condensing mode of RHR has been deleted from use at LaSalle.

DCP 9500158 revised UFSAR Tables 6.2-21 (Summary of Lines Penetrating the Primary Containment) and 6.2-28 (Primary Containment Isolation Valves) to reflect that the 2E51-F091 valve had been deleted. Valve 2E51-F091 was not deleted from the list of Steam Condensing Valves in UFSAR Subsection 5.4.7.2.2.3 of the UFSAR. UFSAR Subsection 5.4.7.2.2.3 is correspondingly revised to delete valve 2E51-F091.

DCP 9700554, Replacement of 24/48 VDC lead-antimony batteries 1DC31E and 1DC32E with lead-calcium batteries

DCP 9700555 Replacement of 24/48 VDC lead-antimony batteries 1DC33E and 1DC34E with lead-calcium batteries

Inspections of the model DKR-13 24/48 VDC battery cells revealed damage due to swelling of the post seals, which cracked cells and deteriorated the plastic hold down nuts. These batteries provide power to the process radiation monitors and the SRM and IRM startup range neutron monitors. The DKR-13 batteries are no longer manufactured. Based upon the recommendation of the manufacturer, GNB

Technologies, the DKR-13 batteries were replaced with GNB's lead-calcium model 2-MCX-5 batteries. UFSAR Section 8.3.2.1.1 is revised.

Revision to UFSAR Subsection 12.5.3.2
UFSAR Subsection 12.5.3.2 is revised to reflect the station practice of reading the thermoluminescent dosimeters (TLDs) on a quarterly frequency. The TLDs measure the amount of radiation received by individuals working at the station. TLDs were previously changed out on a monthly frequency. The UFSAR revision achieves consistency with ComEd's and industry practices. TLD collection permits recording each individual's permanent dose history. The annual exposure report is based on the information collected by the TLDs. Testing has demonstrated that TLDs will not indicate erroneous data due to the longer exposure time.

Revision to UFSAR for Installation of Unit 1 OPRM per Design Change Package (DCP) 9700500
DCP 9700501 installed a microprocessor based oscillating power range monitor (OPRM) system on Unit 1. The OPRM is intended to detect and suppress core oscillations that BWRs are susceptible to during high power – low coolant flow conditions. Once it is armed, the OPRM will function to automatically suppress oscillations. UFSAR Chapters 1, 3, 4, 7, and 15 are revised.

Installation of Hot Tap on Heater Drain Pump 2HD01P per Design Change Package (DCP) 9900129
DCP 9900129 provided for isolation of the 2HD01P heater drain pump discharge header 2HD15AC-14" to allow for maintenance activities of upstream components during power operation with the heater drain system in service.

Inhibit Unit 1 Exhaust Hood High Temperature Trip Above 30% Power per Design Change Package (DCP) 9800354
High exhaust hood temperatures are not normally experienced above 30% power. There is no compelling need for a high hood temperature turbine trip, as higher steam flow through the low pressure turbines actually cools the hoods. Turbine trips have been experienced at high power due to problems with the high exhaust hood temperature circuitry. The DCP inhibited the Unit 1 high exhaust hood temperature turbine trip when intermediate steam flow exceeds 30%. The associated control room high exhaust hood trip annunciator is not inhibited and remains operable at all power levels. This DCP will reduce unnecessary turbine trips and reactor scrams. UFSAR Section 10.2 is revised to reflect that the Unit 1 high exhaust hood temperature trip is inhibited above 30% power.

Unit 1 Moisture Separator Reheater High Level Trip Logic Change per Design Change Package (DCP) 9800350
The DCP added new level switches at the same locations of existing level switches on the piping between the moisture separator reheaters 1A and 1B bottom shells the moisure separator reheater drain tanks 1A and 1B. Following a review of General Electric Technical Information Letter 1212-2, this change was implemented to reduce single-point false sensor trips associated with moisture separator high level. UFSAR drawings M-61 sheet 3 and M-61 sheet 4 will require revision to reflect the new switches on Unit 1.

Replacement of Unit 1 Backup Overspeed Trip per Design Change Package (DCP) 9800352
The DCP replaced a backup overspeed relay megacycler card in Unit 1 electrohydraulic control (EHC) system with a frequency/voltage circuit card. The original megacycler card is obsolete and is no longer available. An industry forced outage has been attributed to a failed megacycler card. The design change is an EHC system scram reduction effort. UFSAR Section 10.2 is revised.

Modification of Electro-Hydraulic Control Lines for Unit 1 Main Turbine Valves and Main Steam Bypass Valves, Design Change Package (DCP) 9800313
The DCP changed the electro-hydraulic control (EHC) tubing connected to the Unit 1 main turbine control (CV), main stop valves (MSV), intermediate stop valves (ISV), intercept valves (IV), and main steam bypass valves (MSBPV).
The modifications were implemented in response to the "SCRAM Frequency Reduction" initiatives documented in the General Electric (GE) Technical Information Letter (TIL) 1212-2. TIL 1212-2 provides numerous GE recommendations for improving the main turbine generator EHC system to reduce the potential for unit trips. Drawing M-55 Sheet 10 is revised.

Replacement of Heater Drain Control Valve 1HD032A per Design Change Package (DCP) 9900076
The DCP replaced heater drain control valve 1HD032A of the Unit 1 14A low pressure feedwater heater. The replacement valve is larger and has a higher flow capacity. This is in support of the planned power uprate on Unit 1, and to alleviate a heater level transient which occurs when the 1A heater drain pump is brought on line during a swap of operating heater drain pumps.

Revision of Primary Containment Isolation System (PCIS) Group I Surveillance Procedures to Incorporate Scram Reduction Test Methodology and change to UFSAR Section 7.A.3.2

The change to selected procedures incorporates scram reduction test methodology. The scram reduction test methodology consists of using a trip indication test box during the surveillance testing of the instrument channels. The text box consists of a lamp and resistor, and it is connected across the instrument channel output contact (i.e., instrument channel relay contact or differential pressure (dP) switch contact) that is in the main steamline (MSL) isolation trip logic. The test box is installed before the instrument channel is removed from service for testing, and is disconnected following completion of the instrument channel testing. The test box functions to bypass and monitor the trip function of the instrument channel output contact without causing the activation of the associated MSL trip logic channel.

Whenever the test box is installed, the instrument channel is prevented from actuating the associated MSIV isolation logic trip system when the instrument is tested. Thus, the inadvertent actuation of an instrument in the trip system during the testing will not result in automatic closure of the MSIVs.

UFSAR section 7.A.3.2 formerly stated in the subsection on channel bypass or removal from operation that the "calibration of each sensor introduces a single instrument channel trip" and that "this does not cause a protective function without the coincident trip of at least one other instrument channel."

The UFSAR is revised to indicate that the MSL isolation sensors or channel relays may also be bypassed during their calibration to prevent a system trip. Special test equipment may be installed across the instrument channel contacts in the trip logic. This test equipment allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration of the sensor.

Incorporation of Scram Reduction Methodology in Selected Procedures

The following procedures incorporate scram reduction test methodology which utilizes a trip indication test box during the surveillance testing of the associated instrumentation channels.

LIS-MS-101A Revision 1, Unit 1 Main Steam Line Low Pressure Main Steam Isolation Valve Isolation Calibration In Run Mode;

LIS-MS-105A Revision 6, Unit 1 Main Steam Tunnel Area Vent High Differential Temperature Isolation Instrument Channels A & C Calibration;

LIS-MS-105B Revision 6, Unit 1 Main Steam Tunnel Area Vent High Differential Temperature Isolation Instrument Channels B & D Calibration;

LIS-MS-106A Revision 1, Unit 1 Condenser Low Vacuum Main Steam Isolation Valve Isolation Calibration With Vacuum In Condenser;

LIS-MS-201A Revision 1, Unit 2 Main Steam Line Low Pressure Main Steam Isolation Valve Isolation Calibration In Run Mode;

LIS-MS-202 Revision 10, Unit 2 Main Steam Line High Flow MSIV Isolation Calibration;

LIS-MS-304A Revision 4, Unit 1 Main Steam Tunnel Area Vent High Differential Temperature Isolation Instrument Channels A & C Functional Test;

LIS-MS-304B Revision 4, Unit 1 Main Steam Tunnel Area Vent High Differential Temperature Isolation Instrument Channels B & D Functional Test;

LIS-MS-107A Revision 7, Unit 1 Reactor Vessel Low Water Level 1 and Level 2 Isolation Instrument Channels A & C Calibration;
LIS-MS-107B Revision 6, Unit 1 Reactor Vessel Low Water Level 1 and Level 2 Isolation Instrument Channels B & D Calibration;
LIS-MS-307A Revision 5, Unit 1 Reactor Vessel Low Water Level 1 and Level 2 Isolation Instrument Channels A & C Functional Test;
LIS-MS-307B Revision 6, Unit 1 Reactor Vessel Low Water Level 1 and Level 2 Isolation Instrument Channels B & D Functional Test;
LIS-NB-205A Revision 4, Unit 2 Reactor High Pressure Scram Channels A & C Calibration
LIS-NB-205B Revision 4, Unit 2 Reactor High Pressure Scram Channels B & D Calibration

Procedure LIS-MS-102 Revision 10, Unit 1 Main Steam Line High Flow Main Steam Isolation Valve Isolation Calibration
The procedure incorporates scram reduction test methodology which utilizes a trip indication test box during the surveillance testing of the associated instrumentation channels.

Change to UFSAR Section 9.4.3.4.2.c
UFSAR Section 9.4.3.4.2.c implies that two of the three Radwaste Building Exhaust Fans (0VW02CA, 0VW02CB, and 0VW02CC) are operated at all times. The section is revised to state the function of these fans without committing to the operation of a specified number.

Compensatory Actions from Root Cause Report 373-180-99-SCAQ00001
The root cause report identified that a single failure of the electro-hydraulic control damper 1(2)VX22Y could block one of the exhaust air paths from all of the switchgear rooms in each unit. The dampers are normally open, and fail in the open position. Failure of the dampers in the closed position would result in the Division 1 and 2 switchgear and reactor protection system motor generator set rooms being overpressurized, due to the increased pressure drop across the remaining backdraft dampers in the auxiliary building. The overpressurization could cause possible air in-leakage into the control room envelope.
The root cause report identified the following compensatory actions: Electrical disconnection of the actuators on dampers 1&2VX22Y to ensure that the dampers remain open, and securing the switchgear heat removal fans in the off position to maintain contamination control. The safety evaluation was performed to ensure that these compensatory items do not impact other aspects of the facility as described in the UFSAR.
Installation of Bypass Switches for Power Load Unbalance and Backup Overspeed Test Circuits in Unit 1, Design Change Package (DCP) 9500452

The DCP added a normally open contact of a new bypass selector switch was added to the Unit 1 simulated power load unbalance and backup overspeed test signal circuits. The normally open contact was added in series with and downstream of the test push-button contact. The revised logic configuration causes the simulated simulated power load unbalance and backup overspeed test signal circuits to remain disabled until the bypass switch is set to the TEST position.
The previous testing configuration for the power load unbalance and backup overspeed circuits allowed for inadvertent trips due to a single failure/misoperation of time-delay Agastat relays upon release of the test pushbuttons.

Installation of Two 4" Sub-in Connections On 1CW01CA-108", Design Change Package (DCP) 9900136
The DCP was implemented to attach two stub-in assemblies to the circulating water pump 1A discharge piping, 1CW01CA-108", on the upstream side of the pump's discharge valve, 1CW006A. This allows the the valve disk to be gagged closed for maintenance purposes. During normal operation the stub-ins are blind flanged.

Revision to Administrative Technical Requirements and Procedure LAP-900-14 Revision 20, Fire Protection Program
Administrative Technical Requirements (ATR) Section 4.3.7.9.1 and 4.3.7.9.2 were revised to change the channel functional test frequency for inaccessible fire instrumentation; Station fire brigade shift manning requirements were added to Section 6.0 of the ATRs; The test frequency of the battery pilot cell and overall voltage checks in ATR Section 4.7.5.3a was revised; LAP-900-14 was revised to reflect station organizational changes and to comply with fire brigade manning requirements of the ATR.

Restore Original Function of Reactor Recirculation Drain Line 1RR17BB-3/4" per Design Change Package (DCP) 9900150
The function of reactor recirculation drain line 1RR17BB-3/4" was restored to its original design. Specifically, the welded cap was changed to a threaded cap, and the piping downstream of the 1B33-F051B and 1B33-F052B double isolation valves was restored to the original Class D piping classification and material. The isolation valves were restored to the original normally closed, unlocked position. Drawing M-93 Sheet 2 is revised to reflect this change.

Replacement of Unit Feedwater Heaters Normal Drain Valves per Design Change Package (DCP) 9900077
The DCP replaced the internal valve trims of the Unit 1 low pressure feedwater heaters 11A/B/C normal drain valves 1HD072A, B, C. This was done to increase

the flow capacity of the valves and to minimize the cycling of emergency drain valves.

Improvement of Grouding at the Unit 1 Feedwater Control System Card Racks and Replacement of Relays, Design Change Package (DCP) 9900141
The DCP upgraded the grounding system of circuit cards in panel 1H13-P612 by removing the daisy-chain style jumper wires, and replacing them with a copper bar (shorting strip) to join the common grounding terminals of each of six card racks. Each copper car was connected directly to the common ground bus. The daisy-chain wiring was suspected of creating differences in ground potentials which resulted in the creation of electrical noise, which led to offsets in calibration of Bailey 7000 series instrumentation for the feedwater system. The DCP also replaced twenty-four Aromat/Agastat relays with Potter Brumfield relays, model number KGS-17A13-120. The Aromat/Agastat relays, which were not hermetically sealed, experienced corrosion and oxidation, resulting in increased contact resistance. The increased contact resistance in low-voltage signal applications. Malfunctions in the feedwater control system have been attributed to the increased contact resistance. The replacement Potter and Brumfield relays are hermetically sealed, and have proven themselves to be consistently reliable in other applications at LaSalle Station.

UFSAR Subsection 7.2.2.10 indicated that the system response times of all trip channel sensors were verified during pre-operational testing. UFSAR Subsection 7.2.2.10 is revised to state that the response time testing was of those functions with times assumed in the accident analysis. This provides for agreement with Technical Specifications and aligns with actual pre-operational testing.

Drawing Change Request (DCR) 990641, Revision to Drawings M-91 Sheet 5 and M-137 Sheet 5
The DCR corrected an drawing error on drawings M-91 Sheet 5, "Unit 1 Reactor Building Equipment Building Drains," and M-137 Sheet 5, "Unit 2 Reactor Building Equipment Building Drains." The drawings reflect the as-built configuration with the north-east corner room equipments drains routed to the 1(2)RE07 sump rather than the 1(2)RE08 sump.

Revision to UFSAR Chapter 11
UFSAR Section 11.2.2.2 is revised to reflect the use of ion exchange resins for floor drain processing. UFSAR Section 11.4 is revised to reflect the present strategy of using offsite vendors for compaction/incineration, and/or sorting of dry active waste (DAW). UFSAR Table 11.4-2 is revised to reflect present disposal volumes. These changes result from a corporate radiation protection self assessment.

Revision to UFSAR Drawings M-74 and M-127, and Subsection 9.2.7.3
Drawings M-74 Sheet 1 (Unit 1 Cycled Condensate Storage System) and M-127 Sheet 1 (Unit 2 Cycled Condensate Storage System) incorrectly show the ASME Code breaks and piping design tables for the high pressure core spray (HPCS) and reactor core isolation cooling (RCIC) cycled condensate storage tank suction lines. UFSAR subsection 9.2.7.3 is revised to clarify the correct extent of the seismic qualification for the RCIC suction lines to the cycled condensate storage tanks and the method used for switchover to the suppression pool.

Unit 1 Design Change Package (DCP) 9900171, Replacement of Unit 1 Loose Parts Monitoring System (LPMS)
The DCP replaced twelve Rockwell loose parts monitoring system (LPMS) preamplifiers in Unit 1 with Technology for Energy (TEC) preamplifiers, located near containment penetration E-19. The DCP also installed coaxial adapters to connect Microdot cable plugs to BNC style input signal receptacles on the TEC amplifier.

Removal of Packing Leak Off Line from 2B33-F023B per Design Change Package (DCP) 9600121
DCP 9600121 removed the packing leakoff line from reactor recirculation (RR) suction valve 2B33-F023B. UFSAR Figure 7.3-7 Sheet 2 and Table G.B.1-1 Sheet 1 are revised.

Replacement of Internals and Removal of Stem Leakoff Line of Reactor Recirculation Isolation Valve 1B33-F023 per Design Change Package (DCP) 9600119
The DCP installed a new valve bonnet, disc, and stem to reactor recirculation (RR) pump suction valve 1B33-F023B in accordance with vendor recommended upgrades. The revised stem provides a packing design with a single stack and no gland area. The stem leakoff line to the gland seal leakoff reservoir was accordingly removed. UFSAR Figure 7.3-7 and Table G.B.1-1 are revised. UFSAR Figure 7.3-7 Sheet 2, Table G.B.1-1 Sheet 1, drawings M-93 sheet 2, M-155 Sheet 1, and M-2093 sheet 9 are revised.

Change to UFSAR Section 7.7.4.2.2
The change deletes parenthetical information in a sentence in the "Interlock" subsection of UFSAR Section 7.7.4.2.2. The parenthetical information is misleading and it conflicts with information contained in UFSAR Section G.2.3.3.2.2. UFSAR Section 7.7.4.2.2 Equipment Design, Interlock subsection, first paragraph, second sentence is revised from "... recirculation flow is reduced

(after a time delay) to within the power..." is changed to "... recirculation flow is reduced to within the power...".

Change to UFSAR Sections 9.4.3.4.2.b and 9.4.3.4.2.c
UFSAR Sections 9.4.3.4.2.b and 9.4.3.4.2.c provide specific information that implies the operational configuration of the radwaste building supply and exhaust fans. This change deletes the nominal fan capacities and number of fans operated from these paragraphs. This change provides the flexibility operate the radwaste building supply and exhaust fans in the configuration required by plant conditions.

Revision to UFSAR Appendix L
UFSAR Appendix L item L.75 is revised to reflect that the description of the Technical Support Center (TSC), Operational Support Center, and Emergency Operations Facility are contained within the ComEd Offsite Dose Calculation Manual (ODCM).

Revision to UFSAR Chapter 9 and Volume X
The title for drawing M-82 is corrected in Chapter 9.0 Table of Contents for Drawings, changed to "Service Air System".
UFSAR Section 9.3.1.3 discusses the verification of design to a loss-of-pneumatic supply accident as a part of the preoperational test of the Drywell Pneumatic System. This section states that the Station Air System demonstration verifies that valves fail as designed on loss of air. This section refers the user to Table 14.2-72 of the FSAR for a listing of the valves. Table 14.2-72 of the FSAR does not include a listing of the valves which fail due to loss of air. The statement "as listed in Table 14.2-72 of the FSAR" is deleted from paragraph 6.
Drawing M-81-FD is added to Volume 10 of the UFSAR. The Drawing Index is revised as well. Drawing M-81 is referenced in the text section 9.3.1.2.1, but Drawing M-81-FD will be added in Volume 10 to provide a simple diagram of the Instrument Air System.

Revision to UFSAR Section 7.6
UFSAR Subsection 7.6.2.2.4 is revised to state that there is one (as opposed to two) set of two differential pressure switches connected to measure the differential pressure created as steam flows past an elbow in the line so that the steam flow rate through it can be monitored.

Revision to UFSAR Section 5.2.2.1.3
The change revises a sentence that conflicts with UFSAR Table 5.2-9 and Technical Specification 3.4.2.e. by eliminating incorrect text in Section 5.2.2.1.3. The sentence

states, "Two of the valves are set at 1146 psig for other considerations." This sentence refers to the setpoint of the two safety relief valves that lift at the lowest pressure. The actual setpoint of the two safety relief valves that lift at the lowest pressure is 1150 psig. The 1150 psig setpoint is correctly listed in UFSAR Table 5.2-9 and Technical Specification 3.4.2.e. The contradiction occurred when the setpoint of the two Safety Relief Valves with the lowest opening pressure setpoint was changed from 1146 psig to 1150 psig. The setpoint change was implemented per license amendment numbers 28 and 15 for Unit 1 and 2, respectively. UFSAR Section 5.2.2.1.3 was not revised to reflect the setpoint change.

Revision to UFSAR Section 3.11
UFSAR Tables 3.11-21, 3.11-22, 3.11-26, and 3.11-27 are revised to correct radiation dose values in the associated environmental zones. These changes make the UFSAR and design documents consistent with each another.

Design Change Package (DCP) 9900137, Addition of Hot Tap Isolation Valve and Standpipe on 1CW15AC-36" Outlet of Circulating Water Pump1CW01PC
The DCP added valve 1CW111C with a blind flange to the manway cover downstream of valve 1CW006C and the 1CW01PC circulating water pump. The addition of the valve permits venting of the manway piping. The pipe downstream of valve 1CW006C may be inspected using this attachment point by using a standpipe. Drawing M-63 Sheet 1 is revised.

LaSalle Operating Procedure LOP-CW-01M Revision 9, Unit 0 Circulating Water System Mechanical Checklist
Valve 1CW111C was added to the procedure to reflect installation of the valve per Design Change Package 9900137.

LaSalle Operating Procedure LOP-CW-02 Revision 7, Filling of Circulating Water System
The procedure was revised to verify that the inspection point (installed on the circulating water system per Design Change Package 9900137) is closed prior to filling and venting the circulating water system per the procedure.

Drawing Change Request (DCR) 990647, Revision to Drawings M-1455 Sheet 1 and M-1456 Sheet 1
The failure positions of the Unit 1 and 2 reactor building ventilation system supply volume dampers 1&2VR06Y as represented on drawings M-1455 Sheet 1, Unit 1 Reactor Building Ventilation System, and M-1456 Sheet 1, Unit 2 Reactor Building Ventilation System, was changed from "Fail Close" to "Fail Open". This was done to reflect the as-built condition of the facility.

Revision to Reactor Protection System Surveillance Testing
UFSAR Subsection 7.2.2.10 is revised to provide an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. UFSAR 7.2.2.10 previously indicated that a logic trip occurs when a test signal is applied to a RPS channel. For the revised testing methodology, special test equipment is installed across the trip contacts in the RPS trip logic. This test equipment allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel. UFSAR Section 7.A.2 is revised to indicate that manual bypasses of the associated RPS instrument channels are indicated in the control room on the engineered safety features (ESF) status indication panel.
The following procedures incorporate scram reduction test methodology which utilizes a trip indication test box during the surveillance testing of the associated instrumentation channels.
LIS-NB-105A Revision 5, Unit 1 Reactor High Pressure Scram Channels A & C Calibration;
LIS-NB-105B Revision 5, Unit 1 Reactor High Pressure Scram Channels B & D Calibration;
LIS-NB-301A Revision 6, Unit 1 Reactor Vessel Low Water Level 3 Scram Trip Logic A1 & A2 and RHR (Shutdown Cooling Mode) Isolation Functional Test;
LIS-NB-301B Revision 5, Unit 1 Reactor Vessel Low Water Level 3 Scram Trip Logic B1 & B2 and RHR (Shutdown Cooling Mode) Isolation Functional Test;
LIS-NR-303A Revision 7, Unit 1 Average Power Range Monitor Channels A, C and E Rod Block and Scram Functional Test;
LIS-NR-303B Revision 7, Unit 1 Average Power Range Monitor Channels B, D and F Rod Block and Scram Functional Test;
LIS-NR-403A Revision 7, Unit 2 Average Power Range Monitor Channels A, C and E Rod Block and Scram Functional Test;
LIS-NR-403B Revision 7, Unit 2 Average Power Range Monitor Channels B, D and F Rod Block and Scram Functional Test;
LIS-PC-101 Revision 6, Unit 1 High Drywell Pressure Scram, Primary Containment Isolation and Secondary Containment Isolation Calibration;
LIS-RD-101 Revision 8, Unit 1 Scram Discharge Volume Level Alarm, Rod Block and Scram Calibration;
LIS-RD-103 Revision 7, Unit 1 Control Rod Drive Scram Discharge Volume Level Transmitters Calibration;
LIS-RD-104 Revision 9, Unit 1 Control Rod Drive Water Header Low Pressure Scram Calibration;
LIS-RD-301 Revision 9, Unit 1 Scram Discharge Volume Level Alarm, Rod Block and Scram Functional Test;
LIS-RD-303 Revision 10, Unit 1 Control Rod Drive Scram Discharge Level Functional Test;
LIS-RD-304 Revision 11, Unit 1 Control Rod Drive Water Header Low Pressure Scram Functional Test;

LIS-RD-403 Revision 13, Unit 2 Control Rod Drive Scram Discharge Level Functional Test;
LIS-RD-404 Revision 12, Unit 2 Control Rod Drive Water Header Low Pressure Scram Functional Test

Revision to Reactor Protection System Surveillance Testing
Incorporation of Scram Reduction Methodology in Selected Procedures
The following procedures incorporate scram reduction test methodology, utilizing a trip indication test box during the surveillance testing of the associated instrumentation channels.
LIS-NB-101A Revision 6, Unit 1 Reactor Vessel Low Water Level 3 Scram Trip Logic A1 & A2 and RHR (Shutdown Cooling Mode) Isolation Calibration
LIS-NB-101B Revision 6, Unit 1 Reactor Vessel Low Water Level 3 Scram Trip Logic B1 & B2 and RHR (Shutdown Cooling Mode) Isolation Calibration

Revision to UFSAR Table 6.2-21
UFSAR Table 6.2-21 Sheet 4B is revised by adding reference to "Note (20)" in the remarks column for containment penetrations M-77 valve 1(2)E12-F088A, M-79 & M-84 valve 1(2)E12-F302, and M-79 & M-84 valve 1(2)E12-F088B. These valves are all leak tested in the reverse direction as are many other ECCS System Relief valves/Isolation valves which serve as primary containment isolation valves in water sealed ECCS Systems. Note (20), which discusses reverse direction testing, was inadvertently omitted from the remarks section of Table 6.2-21 for these components.

UFSAR Change for Turbine Stop Valve and Turbine Control Valve Closure Scram and EOC-RPT Bypass
This change clarifies the bypass interlock wording in the UFSAR consistent with the design and Technical Specifications. These changes to UFSAR Sections 6.B, 7.2, 7.A.2, 15.2, 15.3, G.3, and G.5 supplement those previously prepared for design change packages (DCPs) 9800068 and 9800067. These DCPs implemented license amendment Nos. 130 and 114, for Units 1 and 2, respectively.

Revision to Drawing M-63 Sheet 4, Circulating Water System
The following changes were made to drawing M-63 Sheet 4 to depict the as-built condition. Pressure gauge 0PIC-W001 was deleted, whereas pressure gauge 0PI-CW005, isolation valve 0CW029, level gauge 0LI-CW001, and isolation valve 0CW030 were added to the drawing.

Revision to UFSAR Section 9.4.2
UFSAR Section 9.4.2.2.c is revised to reflect that the reactor building ventilation system filters are medium efficiency filters. This conforms with UFSAR Table 9.4-5.

Change to UFSAR Chapter 9.4
Revised the "dirty" pressure drop of 0.35 inches water column for the diesel generator ventilation supply filters listed in Table 9.4-15 to 0.40 inches water column. The pressure drop was changed to agree with the Sargent & Lundy design criteria as specified in DC-VD-01-LS.
The description for the HPCS switchgear and pump room ventilation system in Section 9.4.5.1.2 is revised to state that the supply air fan induces filtered outside air. The previous description was incorrect.
The description of the truck bay exhaust fan and the statement pertaining to the designed Interim Radwaste Storage Facility (IRSF) operating pressure is deleted from Section 9.4.13.2. The IRSF truck bay exhaust fan is permanently disabled, and the IRSF design basis is described in section 9.4.13.1.

Revision to UFSAR Section 9.1, and Procedure LOP-FC-03 Revision 15, Fuel Pool Cooling System Startup, Operation, Shutdown, and Level Changes
UFSAR Section 9.1 is revised to reflect calculations which support the capability of the fuel pool cooling system to maintain the fuel pool temperature at or below a 140 degree F limit under a maximum normal heat load (MNHL) based upon a service water temperature of 97 degree F. The use of the fuel pool cooling system for alternate decay heat removal during refueling outages is included in the revision to UFSAR section 9.1, which is also incorporated in the revision to LOP-FC-03.

Revision to UFSAR Section 9.1.3
The spent fuel pool normal maximum temperature limit of 120 °F in UFSAR Section 9.1.3 is revised to 140 °F. This limit is consistent with the allowable limit in NRC NUREG-0800, Standard Review Plan, Section 9.1.3. This proposed change supersedes a previously proposed change which restricted core offloads upon lake temperatures exceeding 95 °F. The alternate decay heat removal (ADHR) of Subsection 9.1.3.1.1 is revised to clarify the various potential lineups that may be used for the fuel pool cooling system during ADHR.

Procedure CC-AA-401 Revision 0, Installation and Control of Temporary Shielding
The procedure provides a method for the installation and control of temporary lead shielding on structures, systems, or components (SSC) to achieve a reduction in personnel radiation exposure. Guidelines are provided for the use of water shields, frisker booths, and shielding structures. The procedure applies to both operational and non-operational piping. CC-AA-401 supersedes LaSalle administrative procedures LAP-300-47, Installation and Control of Shielding Components, and LAP-300-23, Issue, Control and Installation of Temporary Shielding.

LaSalle Operating Procedure LOP-RR-07 Revision 18, Operation of the Reactor Recirculation Flow Control System
The procedure reflects the inclusion of rotary variable differential transformers (RVDTs) on Unit 2. The former linerar variable differential transformers (LVDTs) are backups. The procedure guides many operations including the swapping from LVDTs to RVDTs and back.

Revision to UFSAR Sections 6.2 and 6.5
UFSAR Sections 6.2 and 6.5 are revised to clarify text as follows.
Clarifying information is added to Subsection 6.2.3.2 to indicate that the reactor building is designed to contain a negative interior pressure of 0.25 inch H_20 gauge. Subsection 6.2.4.2.4 is revised to clarify the containment vent and purge valve description.
Section 6.5.1.4.1.b.3 is revised by removing the statement that HEPA filter elements are tested by the USNRC QA station.
Section 6.5.1.6.f.4 is revised by removing the charcoal filter tray flanges and adds the statement that o-rings are used on the charcoal filter sample canister.

Procedure CC-AA-402 Revision 0, Installation of Temporary Rigging;
Deletion of LAP-900-43, Approval and Control of Transient Loads, Temporary Rigging and Temporary Support Application;
Revision to LAP-300-29, Rigging and Lifting Program
Procedure CC-AA-402 provides the requirements for the application of temporary rigging loads to structural steel beams, auxiliary steel beams, piping and pipe support auxiliary steel. It also sets the requirements and details for the use of rigging frames. CC-AA-402 supersedes LaSalle administrative procedure LAP-900-43, Approval and Control of Transient Loads, Temporary Rigging and Temporary Support Application. Procedure LAP-300-29, Rigging and Lifting Program, was revised to reference CC-AA-402.

LaSalle Operating Procedure LOP-CW-07M Revision 3, Unit 0 Circulating Water CO2 Injection System Mechanical Checklist
Valves 0CW029 and 0CW030 were added to the prestart checklist of the procedure to ensure that they are OPEN during the prestart lineup to comply with the design of the system as describd in drawing M-63 Sheet 4, Circulating Water System.

Procedure LLP-98-028 Revision 0, Damaged Fuel Rod Recovery
The procedure provides instructions to recover a broken fuel rod and prepare it for permanent storage. The broken fuel rod segment will be obtained from Specialty Rack 3 (SR3) and placed into a General Electric (GE) 8 Rod Container. The GE 8 Rod Container, containing two fuel rods, will be placed in a GE Defective Fuel Storage Container for permanent storage.

Revision to UFSAR Section 12.3
UFSAR subsection 12.3.1.5.4 is revised by replacing "computer grade regulated voltage" in the last sentence of the first paragraph with "a reliable power source". This change to the UFSAR corrects the power source to the counting room from computer grade regulated voltage to reflect that the power supplied to the counting room is from a reliable source.

Revision to UFSAR Sections 6.2 and 7.3
UFSAR Subsections 6.2.5.1.k, 6.2.5.2, 7.3.5.1.g, 7.3.5.2.2, 7.3.5.2.3, 7.3.5.2.5, 7.3.5.2.7, and 7.3.5.2.9 are revised to specify the correct control and monitoring locations for the operation of the hydrogen recombiner system. These revisions result in UFSAR descriptions that correctly reflect current hydrogen recombiner design.

Revision to UFSAR Section 5.2.2.1.3
The change revises a sentence that conflicts with UFSAR Table 5.2-9 and Technical Specification 3.4.2.e. by eliminating incorrect text in Section 5.2.2.1.3. The sentence states, "Two of the valves are set at 1146 psig for other considerations." This sentence refers to the setpoint of the two safety relief valves that lift at the lowest pressure. The actual setpoint of the two safety relief valves that lift at the lowest pressure is 1150 psig. The 1150 psig setpoint is correctly listed in UFSAR Table 5.2-9 and Technical Specification 3.4.2.e. The contradiction occurred when the setpoint of the two Safety Relief Valves with the lowest opening pressure setpoint was changed from 1146 psig to 1150 psig. The setpoint change was implemented per license amendment numbers 28 and 15 for Unit 1 and 2, respectively. UFSAR Section 5.2.2.1.3 was not revised to reflect the setpoint change.

Revision to UFSAR Table 9.4-27
Table 9.4-27, Primary Containment HVAC System Failure Analysis, discusses the malfunction and resulting actions during two train operation. The table incorrectly lists an action which can not be accomplished.
During two train operation, both Supply Fan Coil Units are operating. Therefore, if there is a failure in one supply air fan, there is not another supply air fan which may be started.
In the description of Two Train Operation, Supply Air Fan in Fan-Coil Unit, the Comments column is revised by deleting the text "Operator starts the standby fan-coil unit if required."

Revision to UFSAR Chapters 9.1 and 9.2
UFSAR Chapters 9.1 and 9.2 are revised to reflect the raising of the maximum circulating water and service water inlet temperatures from 95 ^{0}F to 97 ^{0}F, and

provide an update of the ultimate heat sink for worst case weather conditions. This is based upon calculation L-002456 Revision 0, LaSalle County Station Cooling Lake Performance.

Revision to UFSAR Figure 7.7-5
UFSAR Figure 7.7-5, Feedwater Control System diagram, was updated to reflect the as-built condition of the feedwater control system.

Change to the Bases Section of Unit 1 and 2 Technical Specifications
Unit Bases Section 2.1 was changed to reflect the minimum critical power ratio safety limit increase from 1.07 to 1.08 for two recirculation loop operation, and from 1.08 to 1.09 for single recirculation loop operation. Unit 1 and 2 Bases Section 3/4.3.2 was changed to reflect the turbine stop valve closure scram bypass power level change from 30% to 25%.

Revision to UFSAR Section 8.3
UFSAR Subsection 8.3.2.1.1 is revised as follows. In subparagraph a., "2% of total volume" supersedes "the explosion limit." In subparagraph b., "65°F minimum" is replaced with "maintain a minimum electrolyte temperature of 60°F for the 125VDC batteries and 65°F for the 250VDC batteries". The revision provides explicit values for the percentage of hydrogen concentration per volume allowed to accumulate in the battery rooms as recommended in ANSI/IEEE Standard 484-1987. This UFSAR change also defines the specific requirements for the minimum electrolyte temperature for 125 VDC and 250 VDC battery per calculation 4266/19D30.

Snubber Replacements per Design Change Package (DCP) 9500095 Addendum 1
DCP 9500095 Addendum 1 replaced mechanical snubbers M09-RR00-1002S, M09-RR00-1010S, M09-RR00-1011S, M09-RR00-1041S, M09-RH04-1503S, and M09-RH04-1508S with hydraulic snubbers.

Installation of a Cycle Condensate Tap per Design Change Package (DCP) 9900189; LaSalle Operating Procedure LOP-CY-02M Revision 6, Unit 2 Cycled Condensate Storage and Transfer Mechanical Checklist
A supply tap was installed on cycled condensate (CY) line 2CY67A in the turbine building. The tap consists of a piping tee, a 3 inch gate valve, and piping nipple with a threaded cap. The purpose of this installation is to provide a supply of water that may be used for maintenance activities requiring reactor grade water which is no radioactively clean. UFSAR sections 9.2.7 and 9.2.7.1.2 are revised to expand the CY system description.

LaSalle Maintenance Procedure LMP-MS-06 Revision 14, Removal/Installation of Main Steam Safety Relief Valves With Reactor Defueled
The procedure provides direction for the installation, removal, and "like-for-like" replacement of the main steam safety relief valves (SRVs) with the reactor defueled. The procedure revision addresses the removal/installation of ductwork and smoke detectors in the Unit 1 drywell, and smoke detectors in the Unit 2 drywell, to allow removal and installation of SRVs.

Procedures LIS-MS-407A Revision 7, Unit 2 Reactor Vessel Low Water Level 1 and Level 2 Isolation Instrument Channels A&C Functional Test, and LIS-MS-407B Revision 8, Unit 2 Reactor Vessel Low Water Level 1 and Level 2 Isolation Instrument Channels B&D Functional Test
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Replacement of Unit 1 Pilot Solenoid Valves, Design Change Package (DCP) 9500270
The DCP replaced the IMF-2 pilot solenoid valves for automatic depressurization system valves 1B21-F013D, 1B21-F013R, and 1B21-F013S, pilot solenoid valves (B and C) for safety relief valves 1B21-F013K and 1B21-F013P, and pilot solenoid valves (C) for safety relief valves 1B21-F013A, 1B21-F013B, 1B21-F013F, 1B21-F013G, 1B21-F013J, 1B21-F013L, 1B21-F013M, and 1B21-F013N, and with new Crosby Type UMF-1 pilot solenoids. The solenoid valves were near the end of qualified life.

Special Procedure LLP-99-021 Revision 0, Badger Testing of the Unit 2 Spent Fuel Pool
The procedure provides the instructions to perform blackness testing on approximately 80 empty fuel cells within the Unit 2 spent fuel pool. The data collection will allow for characterization of the Boraflex material within the cell panels. Data collection and processing will be used as a tool to monitor and predict the amount of Boraflex degradation.

Revision to UFSAR Figures 10.1-1 and 10.1-2
UFSAR Figure 10.1-1 is revised by adding a note that states the high pressure turbine modification for power uprate will change the heat balance and that a new heat balance will be provided following approval of the power uprate license amendment. UFSAR

Figure 10.1-2 is revised by adding a note that states the heat balance is not current and will be changed when power uprate is approved.

LaSalle Maintenance Procedure LMP-MS-07 Revision 00, Removal/Installation of Unit 1 Main Steam Safety Relief Valves With Fuel In The Reactor Vessel
The procedure provides direction for the installation, removal, and "like-for-like" replacement of Unit 1 main steam safety relief valves (SRVs) with fuel in the reactor vessel. This evaluation addressed the removal/installation of main steam safety relief valves (SRVs) in Mode 5, Refuel, with fuel in the reactor vessel. Removal of SRVs in Mode 5 requires the installation of main steam line plugs and blind flanges to prevent water from draining out main steam lines when reactor vessel water level is raised above main steam line outlets during refueling activities.

LaSalle Maintenance Procedure LMP-MS-07 Revision 00, Removal/Installation of Unit 1 Main Steam Safety Relief Valves With Fuel In The Reactor Vessel
The procedure provides direction for the installation, removal, and "like-for-like" replacement of Unit 1 main steam safety relief valves (SRVs) with fuel in the reactor vessel. This evaluation addressed the removal/installation of ductwork and smoke detectors in the drywell to allow removal and installation of SRVs.

LaSalle Maintenance Procedure LMP-MS-07 Revision 00, Removal/Installation of Unit 1 Main Steam Safety Relief Valves With Fuel In The Reactor Vessel
The procedure provides direction for the installation, removal, and "like-for-like" replacement of Unit 1 main steam safety relief valves (SRVs) with fuel in the reactor vessel. This evaluation addressed the removal/installation of SRVs with the unit in Mode 4, Cold Shutdown.

Revision to UFSAR for Installation of Unit 2 OPRM per Design Change Package (DCP) 9700502
DCP 9700502 installed a microprocessor based oscillating power range monitor (OPRM) system on Unit 2. The OPRM is intended to detect and suppress core oscillations that BWRs are susceptible to during high power – low coolant flow conditions. Once it is armed, the OPRM will function to automatically suppress oscillations. UFSAR Chapters 1, 3, 4, 7, and 15 are revised.

Revision to UFSAR per Restoration of Unit 1 Jet Pump Number 9
During the LaSalle Unit 1 refuel outages numbers six and seven, L1R06 and L1R07, respectively, damage was observed on the inlet mixer wedge of jet pump number 9, the restrainer bracket pad, and associated set screws. Restoration of the jet pump per design change package (DCP) 9600289 consisted of two improved restrainer bracket wedge assemblies ("auxiliary wedges"), a replacement wedge for the inlet-mixer, and

restoration of a smooth functional surface to the wedge interface pad on the restrainer bracket. Addendums to the design change package authorized qualification and installation of mock-up auxiliary wedges, as well as the re-installation of temporary wedges, one on the vessel of jet pump number 5, and one on the shroud side of jet pump number 6. UFSAR Sections 3.9, 4.1, 4.5, and G.4 are revised.

Installation of High Point Vents on the Cooling Water Lines to the Unit 2 LPCS Motor Cooler per Design Change Package (DCP) 9800136
The DCP added vent valves in low pressure core spray (LPCS) motor cooler supply and return lines. The vent valves will permit proper venting to drain the lines for maintenance activities. Drawing M-134 Sheet 2 is revised.

Latch and Seal Auxiliary Electric Equipment Room Doors 262 and 265 per Design Change Package (DCP) 9900176
The DCP installed latched padlockable spring bolts on double door sets 262 and 265. Doors 262 and 265 allow access to the Unit 1 and 2 auxiliary electric equipment rooms (AEERs), respectively. This was intended to reduce maintenance costs associated with repeated door repairs. The DCP also allows the installation of a sealant around the outside of the doors. The doors were sealed to help reduce air inleakage from the AEERs and increase the positive pressure margin with respect to adjacent areas.

Revision to UFSAR to Clarify Table 6.2-23
The change deletes reference to the test pressure (P_t) of 39.6 psig for Type A, B, and C leak rate testing from Table 6.2-23, Containment Leakage Testing, and inserts reference to Note 6. Note 6 correctly refers the reader to ANSI/ANS 56.8-1994 to determine the test pressure for Type A, B, and C tests. This change clarifies UFSAR Table 6.2-23.

Coating of Unit 2 Division 1 Pressure Transmitter Instrumentation Circuit Terminations per Design Change Package (DCP) 9800316
The DCP applied Patel Engineers Conformal Coating (PECC) on the terminations associated with pressure transmitters 2E31-N015, 2E31-N035, 2B21-N026AA, 2B21-N051A, 2B21-N026E, 2B21-N407A, 2B21-N407C, 2B21-N405A, and 2B21-N408A. Re-analysis of the reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) high energy line break (HELB) concluded that the humidity in Room 19 (environmental zone H4A) may increase from 95% to 100%. The increase in the accident humidity parameter results in a potential increase in the leakage at the pressure transmitter terminations. The DCP applied the coating as a means to reduce the leakage to an acceptable value.

Coating of Unit 2 Division 3 and Reactor Protection System Divisions A1, 2 and B1, 2 Pressure Transmitter Instrumentation Circuit Terminations per Design Change Package (DCP) 9800318
The DCP applied Patel Engineers Conformal Coating (PECC) on the terminations associated with pressure transmitters 2B21-N403A, B, C, D, 2B21-N406A, B, C, D, and 2B21-N409A and B. Re-analysis of the reactor water cleanup (RWCU) and reactor core isolation cooling (RCIC) high energy line break (HELB) concluded that the humidity in Room 19 (envivcronmental zone H4A) may increase from 95% to 100%. The increase in the accident humidity parameter results in a potential increase in the leakage at the pressure transmitter terminations. The DCP applied the coating as a means to reduce the leakage to an acceptable value.

Procedure LLP-98-028 Revision 2, Damaged Fuel Rod Recovery
The procedure provides instructions to recover a broken fuel rod and prepare it for permanent storage. Revision 2 of the procedure removeds the requirement to use the defective fuel storage container as the permanent storage contrainer for two fuel rods.

Design Change Package (DCP) 9900193 removed surge protection from the ground circuits of wind direction at 33', 200', and 375', and replaced resistor R23 with 1000 ohms at the new meteorological tower. This was done to eliminate erratic indication of wind direction in the main control room.

Unit 1 Refuel Platform Upgrade and UFSAR Revision
The Unit 1 refuel platform was upgraded per Design Change Package (DCP) 9600258. This was done to facilitate shorter refueling outages, increase the efficiency and reliability of the refuel platform, and to standardize the fuel handling hardware associate with Commonwealth Edison's boiling water reactor stations. UFSAR Sections 1.7 and 7.7.13 are revised.

Drawing Change Request (DCR) 9900686, Revision to Drawings M-Index, M-6, M-115, and M-159
During a walkdown of the reactor water cleanup (RWCU) system, it was discovered that process sample crud panels 1&2PLH3J are not installed. The DCR was issued to remove the panels from the drawings to make them consistent with the station configuration. Drawings M-Index, M-6, M-115, and M-159 are revised.

Procedure LLP-99-020 Revision 0, Test Equipment Installation To Support Heater Drain Tuning
The procedure installed temporary pressure transducers on the input and output signals of various heater drain controllers in support of Unit 2 heater drain system control valve tuning.

Replacement of Valve 1E51-F064 with Blind Spectacle Flange, Design Change Package (DCP) 9900138
DCP 9900138 was implemented as a contingency plan for valve 1E51-F064 failing its leak rate test. The DCP removed valve 1E51-F064, reactor core isolation cooling system steam condensing supply isolation valve, and replaced it with a spectacle flange, 1E51-D324. One side of this is a blind flange and the other side is a full-port flange. Valve 1E51-F064 has experienced excessive leakage during local leak rate tests. The valve has been reworked to the point that the inbody seats can't be machined any further. In order to preclude future leakage it was replaced by a spectacle flange. This valve was used as a steam condensing isolation valve; but no longer serves that purpose because the steam condensing mode of operation is not used. Valve 1E51-F064 was closed and de-energized during modes 1, 2 and 3. The implementation of this design change reduces radiation exposure by eliminating the need to perform extended local leak rate tests on the valve, and eliminates the need to perform periodic maintenance on the valve and actuator.
UFSAR Sections 5.4, Figure 5.4-3, Figure 6.3-8, Table 6.3-9, Table 6.2-21, Table 6.2-28, Section 7.4, Table 15.9-4, Section H.4, and drawing M-101, Sheet 1, Revision AT are required to be revised.

Replacement of TBCCW Heat Exchanger Flow Control Valve 2WS029
The replacement of turbine building closed cooling water (TBCCW) heat exchanger flow control valve 2WS029 was evaluated. It was previously replaced per work request L93902.

Design Change Package (DCP) 9900187, Removal of Old SRV Test Equipment, Valves, and Cables from Unit 1
Unit 1 initial startup included a Mark II containment test to analyze hydrodynamic forces in the suppression pool during safety relief valve (SRV) actuation. This DCP removes some of the test equipment and cables (including those in two downcomers), and abandon in place other equipment installed to support the initial SRV testing. This also closes temporary alteration (TALT) 1-0069-98.
Changes to UFSAR Sections 1.2, 6.1, and 6.2 previously proposed by DCP 9800150 are superseded in their entirety.

Revision to UFSAR Section 7.4
UFSAR Subsection 7.4.2.2.9 is revised to eliminate the time required to retrieve and insert the keys into the standby liquid control system keylock switches before system initiation. The change reflects that the keys are maintained in the proper keylock switches, which expedites the initiation and subsequent injection when required.

Design Change Package (DCP) 9500415, Installation of Testable Seals on ECCS Relief Valve 1E21-F031 Flanges
The DCP installed testable seals on the flanges of emergency core cooling system relief valve 1E21-F031. This was done to permit testing the integrity of the flanged connection by a local leak rate test (LLRT) as opposed to an integrated leak rate test (ILRT). Performing a LLRT results in substantial time savings.

Replacement of Sections of Pipe 1RI07B-2" through Penetrations MK-1RB-30 and MK-1RB-21, per Design Change Package (DCP) 9900139
The design change decreased the size of the reactor core isolation cooling (RCIC) supply steam drain pot drain line to condenser (1RI07B-2") from 2" down to 1.5" pipe where it passes through penetrations MK-1RB-30 and MK-1RB-21. Due to flow accelerated corrosion concerns (FAC), some carbon steel sections of line 1RI07B-2" were replaced with chrome moly A335 piping. Utilizing sections of the 2" carbon steel pipe as sleeves for the new 1.5" chrome moly pipe provided a means to reduce radiation dose to personnel.

Installation of Bonnet Vent on Valve 1E51-F031, Design Change Package (DCP) 9600294
The DCP added a bonnet assembly to allow for a point of release of bonnet pressure in the event of a pressure locking condition of reactor core isolation cooling (RCIC) pump suppression pool suction isolation stop gate valve 1E51-F031 on pipeline 1RI17A-8". Gate valve 1E51-F031 was susceptible to pressure locking resulting from water accumulation in the bonnet area in conjunction with temperature and/or system pressure changes. Accumulated water in the bonnet may have prevented the valve from opening due to an increase in pressure in the bonnet resulting from temperature changes (increase) at the valve location or a drop in the process pipeline pressure while the trapped bonnet pressure remains high. The bonnet vent line provides a vent path to release the pressure in the bonnet to prevent pressure locking of the valve. The bonnet vent line satisfies a LaSalle commitment to Generic Letter 95-07 by providing a means to vent the bonnet. UFSAR Table 6.2-21 is revised by the replicate Unit 2 modification, DCP 9600295.

LaSalle Special Test Procedure LST-99-023 Revision 0, EHC On-Line System Calibrations and Data Collection
The procedure sets forth instructions for measuring and recording data of the Electro-Hydraulic Control (EHC) system during various turbine operating conditions from acceleration to 100% power. It also provides instructions for verifying operation of the EHC permanent magnet generator (PMG) power supplies, speed error signals, and power load unbalance (PLU), with adjustment made as necessary.

Procedure LIS-MS-206A Revision 1, Unit 2 Condenser Low Vacuum MSIV Isolation Calibration With Vacuum In Condenser
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Removal of Original Meteorological Tower
Design change package 9600526 disassembled and removed the original meteorological tower and support buildings. The meteorological and communication equipment was moved to a new tower location outside the security fence. There is no further need for the original tower. UFSAR figures 2.1-3, 2.1-4, 2.4-6, 8.2-2, and 9.5-1 and subsection 8.3.3.2 and 9.5.1.2.3 are revised to reflect removal of the tower.

LaSalle Operating Surveillance LOS-FP-A1 Revision 11, Fire Protection Flowpath Valve Cycling Test
The procedure was revised to reflect changes in valve locations due to design change package 9600526, which disassembled and removed the original meteorological tower and support buildings. The meteorological and communication equipment was moved to a new tower location outside the security fence.

LaSalle Operating Surveillance LOS-ZZ-A2 Revision 20, Preparation for Winter/Summer Operations
The procedure was revised to reflect instrumentation changes due to design change package 9600526, which disassembled and removed the original meteorological tower and support buildings. Heat trace supplies to instruments 0FT-WL001 and 0FIT-WL070 are both abandoned in place. The meteorological and communication equipment was moved to a new tower location outside the security fence.

LaSalle Operating Procedure LOP-AP-58 Revision 1, Preparation Procedure Deenergizing 252
The procedure revision deleted the meteorological tower alternate feed from the procedure to reflect design change package 9600526. The DCP disassembled and removed the original meteorological tower and support buildings. The meteorological and communication equipment was moved to a new tower location outside the security fence.

LaSalle Special Test Procedure LST-99-022 Revision 0, Unit 1 Pressure Regulator System Startup Test
The procedure performs verification that the Electro-Hydraulic Control (EHC) system calibration and tuning performed during shutdown conditions was correct by inducing transients and monitoring system response during different power levels, demonstrates the backup capability of the pressure regulators, and demonstrates that affected plant parameters remain within acceptable limits during induced transients.

Addition of Test Tap to Relief Valve 1E12-F088A per Design Change Package (DCP) 9500400
The DCP added a test tap to the outlet flange of Emergency Core Cooling System (ECCS) relief valve 1E12-F088A. The test tap provides a means of performing a local leak rate test (LLRT) of the outlet flanged connection in lieu of an integrated leak rate test (ILRT). Leak rate testing is required because the valve and the flanged connection are part of the primary containment pressure boundary. Additionally, the flanged joint must be tested to verify its pressure integrity whenever the valve is removed for calibration or maintenance. The pressure tap results in substantial time savings as the effort to perform a LLRT is substantially less than the effort to perform a ILRT. Drawings M-94, M-95, M-96 sheets 1, 2, 3, and M-101 sheet 2 are required to be revised.

Modification for Change of Drywell Head Bolt Torque Requirements for Unit 1 and 2, Design Change Package (DCP) 9900140
The design change revised the bolt pretension requirements for the drywell head of both Unit 1 and 2. Procedures LMP-PC-01, Drywell Head Removal, and LMP-PC-02, Drywell Head Installation, are revised to include the new torque values.

Out of Service to Administratively Prevent Use of Solid Radwaste Decanting Tank
Out of Service (OOS) 980014150 was initiated on solid radwaste decanting tank 0WX05TB, to administratively control the use of the associated tank mixer. The decant tank mixer was making an abnormal noise. The mixer is not required for tank operation, and has been taken out of service by lifting the leads to the decant tank mixer drive motor. This has also been incorporated in to LaSalle operating procedure LOP-WX-02, Revision 10, Decanting Station Operation.

Procedure LST-99-026 Revision 0, Unit 1 Heater Drain Tuning and Performance Test
LaSalle special test procedure LST-99-026 tunes the Unit 1 11A, B, C, and 14A low pressure heater drain valve controllers for optimum performance. It also provides for demonstration of proper operation of these heater drains during various power level plateaus during power ascension.

Revision to UFSAR to Reflect NobleChem Metal Compound Injection on Unit 1
The temporary Noblechem metal compound injection process on Unit 1 allows for lower hydrogen water chemistry (HWC) hydrogen addition rates, while still achieving the electrochemical corrosion potential required of HWC. Benefits of lower hydrogen addition rates are lower operational dose rates from main steam line radiation, reduction of administrative controls used to handle increased operating dose, decrease in personnel exposure during operation, and a reduction of localized shielding requirements. UFSAR Sections 5.2, 6.1, and 10.4 are revised.

Administrative Technical Requirements (ATR) Amendment 32
ATR Amendment 32 Revises ATR Section 3/4.4.4, Reactor Coolant System Chemistry, and its Basis section to include the NobleChem specific conductivity and pH limits, the NobleChem specific timing limits, and the deduction in conductivity allowed for conductivity limits less than 10 uS/cm due to increases in soluble irons.

Procedure LLP-99-022 Revisions 0 and 1, Noble Metal Injection
The procedure outlines the steps necessary to inject noble metal solution in to the reactor vessel and reactor recirculation piping for the purpose of reducing post startup hydrogen injection rates needed to reduce stress corrosion cracking.

Procedure LLP-99-025 Revision 0, Filling and Draining '1B' RR for L1R08
The procedure outlines the method for fill and drain of the 1B Reactor Recirculation Loop with a recirculation line suction plug installed, to support the performance of maintenance activities on the 1B reactor recirculation loop.

Procedure LOP-NB-02 Revision 1, Operations with the Potential to Drain the Reactor Vessel
The procedure revision consisted of editorial changes; added instructions for resolving contradictions between this and other plant procedures, provided a limitation that an Operation with the Potential to Drain the Reactor Vessel (OPDRV) does not exist if the vessel is defueled, the gate between the reactor cavity and fuel pool is installed, and all fuel in the fuel pool is seated; removed the requirement to declare an OPDRV for control rod drive removal or a local power range monitor (LPRM) and source range monitor/intermediate range monitor (SRM/IRM) dry tube removal from under the vessel provided a water makeup system is available to ensure that reactor pressure vessel water level is maintained; and deleted the requirement to declare supports removed from lines with vessel penetrations below normal water level as an OPDRV.

Revision to UFSAR Subsection 7.6.2.2.7
Two paragraphs in UFSAR Subsection 7.6.2.2.7 are revised to correct the description of testing methodology for temperature switches and leak detection alarm units.

Fail Open Dampers 0VE10YA/YB and Activate Heaters 0VE03AA/AB per Design Change Package (DCP) 99-981
The DCP activated Auxiliary Electric Equipment Room (AEER) heaters 0VE03AA and 0VE03AB that were previously disconnected and abandoned in place per DCP 9700551. These heaters were used to heat the computer room in the auxiliary. Dampers 0VE10YA and 0VE10YB were failed to the "full cooling" position. This modification helped to offset the cooling effects of outside air during the winter months. Failing the dampers to their fail safe mode directed a sufficient quantity of air through the cooling coils to prevent unnecessary compressor cycling.

Procedures LIS-MS-405A Revision 4, Unit 2 Main Steam Tunnel Area Vent High Differential Temperature Isolation Instrument Channels A&C Functional Test, and LIS-MS-405B Revision 4, Unit 2 Main Steam Tunnel Area Vent High Differential Temperature Isolation Instrument Channels B&D Functional Test
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Procedure LLP-99-023 Revision 0, Unit 1 Main Condenser Circulating Water Side Chemical Cleaning With Unit Shutdown
The procedure controlled the chemical cleaning of the circulating water side of the Unit 1 main condenser. Cleaning of the condenser removed tube scale, to increase cycle efficiency. Sulfuric acid was injected into the circulating water pump discharge piping with the circulating water system in operation. The resultant low pH acidic water dissolved the calcium carbonate scale to improve heat transfer.
Procedure LLP-99-023 Revision 1, Unit 1 Main Condenser Circulating Water Side Chemical Cleaning With Unit Shutdown
The procedure controlled the chemical cleaning of the circulating water side of the Unit 1 main condenser. Cleaning of the condenser removed tube scale, to increase cycle efficiency. Sulfuric acid was injected into the circulating water pump discharge piping with the circulating water system in operation. The resultant low pH acidic water dissolved the calcium carbonate scale to improve heat transfer. The procedure revision removed a requirement to sample condensate in the event of a tube rupture, and to remove leakage rate criteria for cycled condensate.

Procedure LLP-99-027, RR Pump Delta T Monitoring and Bypass
The temporary procedure provides a method for monitoring reactor recirculation pump suction to steam dome differential temperature, and bypassing the jet pump cavitation interlock to prevent spurious downshifts of the reactor recirculation pumps. The effect of this activity is to replace an automatic trip of the reactor recirculation pumps with an administrative control.

Out of Services 990012078 and 990012337
The out-of-service (OOS) activities removed average power range monitor (APRM), local power range monitor (LPRM), and intermediate range monitor (IRM) equipment from service on Unit 1 during the eighth refuel outage, L1R08. The out-of-services allowed installation of oscillation power range monitor (OPRM) equipment in the power range neutron monitoring system cabinets per design change package (DCP) 9700500. Upon completion of the OPRM installation activity, all of the monitoring equipment affected by the out-of-services were returned to their normal design configuration.

LFP-600-1 Revision 4, Control Blade Uncoupling and Coupling from the Refuel Platform, and LFP-600-2 Revision 8, Replacement of LPRM and SRM/IRM Dry Tube Assemblies
These procedures install rod position indication system (RPIS) Full-In "00" indication connectors to the withdrawn control rod(s) to defeat the one rod out interlock. These connectors are installed in the cables/lines from the control rod drive so that RPIS continuously receives a false reed switch position showing a "Full-In" or "00" position indication from the affected control rod drive(s). This activity results in bypassing the refueling interlock signals from the affected control rods.

Revision to UFSAR for Discontinued Use of Rod Sequence Control System
UFSAR Section 3.1, Table 7.1-1, and Section 7.7 are revised to reflect the discontinued use of the Rod Sequence Control System (RSCS). The RSCS was designed to restrict rod movement to minimize the individual worth of control rods to mitigate the consequences of a Rod Drop Accident (RDA). The required use of RSCS was eliminated by license amendment 88 and 73 for Units 1 and 2, respectively (facility licenses NPF-11 and NPF-18). The need for these UFSAR changes was not previously identified when the license amendments were implemented.

LOP-AP-44 Revision 4, Preparation Procedure for De-Energizing Unit 1 Division 1 Busses
Attachments K and L of the procedure were revised to support the installation of temporary power for 24 VDC battery chargers 1DC35E and 1DC36E from RLC #109. The normal power sources for the battery chargers are motor control centers 135X-3 and MCC 135X-2, respectively.

Revision to UFSAR Table 5.4-1
UFSAR Table 5.4-1 is revised to match the nameplate design pressures of the reactor water cleanup (RWCU) system heat exchangers. The RWCU regenerative heat exchanger shell and tube design pressure is changed to 1425 psig, and the RWCU nonregenerative heat exchanger tube design pressure is changed to 1425 psig.

Design Change Package (DCP) 9900221 permanently installed suppressin pool cleanup system spool pieces #4, suppression pool cleanup return from condensate, and #5, suppression pool cleanup discharge to condensate. Drawing M-96 sheet 5 is required to be revised.

Operating Procedure LOP-ZZ-07 Revision 3, Miscellaneous Temporary Installations
The procedure incorporated the addition of six former temporary modifications because they are performed regularly. These activities consist of temporary power feeds for hydrolazers in the Unit 1 and 2 reactor buildings, temporary power feed to the Unit 2 condenser tube pull area, temporary power feed for the suppression chamber/drywell, and the installation of temporary blank flanges for Unit 1 and 2 reactor building elevator rooms 1VR77Y and 2VR77Y, respectively, to control the direction of air flow.

Procedure LIS-RD-401 Revision 9, Unit 2 SCRAM Discharge Volume Level Alarm, Rod Block and SCRAM Calibration
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Installation of Spool Piece #6 (1SF10A-6) to Cold Side of 1SF10A-14" per Design Change Package (DCP) 9900243
During a shutdown, the suppression pool cleanup system utilizes the condensate polishers and a portion of the residual heat removal (RHR) system piping to route and clean suppression pool water. Blind flanges are temporarily replaced with a removable spool piece to effect the interaction of the suppression pool cleanup system with the condensate polishing system, RHR system, and feedwater system. The DCP removed the blind flanges and temporarily installed spool piece #6 in the line where the suppression pool cleanup system connects feedwater flushing piping and the suppression pool cleanup system discharge piping while Unit 1 was in operation. This was done to reduce outage time.

Operating Procedure LOP-AP-01 Revision 13, Unit Auxiliary Transformer UAT 141(241) Backfeeding Operation
The revision to LOP-AP-01 consists of implementing temporary protective relay changes prior to providing backfeed power to the unit buses from the Unit Auxiliary Transformer (UAT) and Main Power Transformer (MPT). The temporary protective relay setting changes are only to be implemented when the unit buses are to be powered from MPT/UAT with the unit shutdown. The protective relay settings are to be restored to their original configuration prior to unit startup. Changes in the settings are to be verified.
These temporary protective relay setting changes allow the MPT/UAT backfeed on the shutdown unit to be credited as an operable second off-site source of power for the operating unit. These temporary settings ensure that coordination exists between the breakers when the MPT/UAT is used to provide power to the opposite unit via the unit cross-tie breakers. The temporary breaker settings also maintain coordination if the System Auxiliary Transformer (SAT) of either unit is carrying the total load of its unit plus the ESF buses of the opposite unit.

Operating Procedure LOP-AP-01 Revision 15, Unit Auxiliary Transformer UAT 141(241) Backfeeding Operation
The revision to LOP-AP-01 consists of implementing temporary protective relay changes prior to providing backfeed power to the unit buses from the Unit Auxiliary Transformer (UAT) and Main Power Transformer (MPT). The temporary protective relay setting changes are only to be implemented when the unit buses are to be powered from MPT/UAT with the unit shutdown. The protective relay settings are to be restored to their original configuration prior to unit startup. Changes in the settings are to be verified.
The temporary settings for the Breakers 2414 and 2424 neutral overcurrent relays (2451-AP261 and 2451-AP262) were revised to agree with System Protection Department (SPD) Calculation L-002509, Revision 2, dated 10/30/99. SPD revised this calculation to ensure that the temporary settings for these two overcurrent relays are within their setting range.
These temporary protective relay setting changes allow the MPT/UAT backfeed on the shutdown unit to be credited as an operable second off-site source of power for the operating unit. These temporary settings ensure that coordination exists between the breakers when the MPT/UAT is used to provide power to the opposite unit via the unit cross-tie breakers. The temporary breaker settings also maintain coordination if the SAT of either unit is carrying the total load of its unit plus the ESF buses of the opposite unit.

Temporary Modification 1-0044-99 (Design Change Package 9900249)
The radwaste building ventilation (VW) exhaust air filtration system has three trains A, B, and C. The solenoids valves for Train A and C of the radwaste building exhaust filter damper actuators require replacement, while Train B is fully operable. It is desirable to maintain one train in service during the replacement. The individual solenoids do not

have individual isolation valves but rather one valve that isolate all three at the same time. In order to keep one train in service, a temporary air supply line was installed to the 'C' train damper actuators. This provides a means for the operator to manually manipulate the 0VW05YE and 0VW05YF dampers to support operation of the 'C' ventilation train while the failed solenoids are repaired.

Installation of Jumpers to Support Out-of-Service 990009802 per Design Change Package (DCP) 9900251
The DCP installed jumpers to defeat the auto start capability of both units standby gas treatment system from Unit 1 initiation logic (Group IV primary containment isolation system) for the purposed of replacing relays and installing banana jacks.

LOP-VR-02 Revision 20, Reactor Building Ventilation System Shutdown;
LAP-300-18 Revision 4, Transportation of Loads Over Irradiated Fuel; and
LAP-300-44 Revision 1, Floor Plug Removal and Installation.
Revision to UFSAR 9.4.2.3
LOP-VR-02 is revised to delete statements that require the fuel pool and reactor building process radiation monitors be declared inoperable, added informational reference to LOP-ZZ-07, Miscellaneous Temporary Installations, and added statements to assure that the refuel floor is at a negative pressure with respect to adjacent areas when during irradiated fuel movement, core alterations, or operations with the potential to drain the reactor vessel.
LAP-300-18 is revised to expand its scope to include all irradiated fuel, including within the cavity as opposed to solely the fuel pool, removed new fuel from its scope, and clarified secondary containment requirements.
LAP-300-44 is revised to provide guidance for plugs on the refuel floor to assure that the refuel floor is at a negative pressure with respect to adjacent areas.
UFSAR Section 9.4.2.3 is revised to reflect the following. Potentially contaminated effluents rising from the surface of the fuel pools are drawn into the exhaust openings located above the water level. The radiation monitor trip in either the Unit 1 or Unit 2 pool exhaust ducts causes isolation of the reactor buildings and activates the standby gas treatment system. The size and length of the exhaust ducts from each pool are designed to ensure that the travel time of effluents from the radiation monitor to the isolation valve is a minimum of approximately 12.5 seconds, which is more than the closure time of the isolation valves (10 seconds).

Procedure LIS-RD-101 Revision 8, Unit 1 SCRAM Discharge Volume Level Alarm, Rod Block and SCRAM Calibration
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified

without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

LaSalle Maintenance Procedure LMP-VQ-19 Revision 3, 1VQ040 Valve/Actuator Removal and Installation, incorporated guidance to address installation and removal of a blind flange on piping downstream of the procedure's respective valve, to maintain the primary containment pressure boundary while the valves are removed for maintenance.

LaSalle Maintenance Procedure LMP-VQ-18 Revision 5, 1VQ036 Valve/Actuator Removal and Installation, incorporated guidance to address installation and removal of a blind flange on piping downstream of the procedure's respective valve, to maintain the primary containment pressure boundary while the valves are removed for maintenance.

Disabling of Evaporative Cooler Spray Pumps
The Unit 1 and 2 reactor building evaporative cooler spray pumps 1VR01PA, 1VR01PB, 2VR01PA, and 2VR01PB are disabled. They have never worked effectively, are high cost maintenance items, and are not used. Revisions to UFSAR Section 6.2, 9.4, and Table 9.4-5 were previously proposed to reflect that the Unit 1 evaporative spray cooler pumps were out of service (OOS). This safety evaluation reflects that the evaporative cooler spray pumps on both units are out of service. UFSAR Section 6.2, 9.4, and Table 9.4-5 are revised per this safety evaluation to reflect that the evaporative spray cooler pumps of both units are out of service (OOS).
A previous part of UFSAR subsection 9.4.2.1.2.a was revised, its remaining portion deleted, and subsection 9.4.2.1.2.b was deleted. UFSAR subsection 9.4.2.1.2 is returned to its original text as it existed in UFSAR Revision 0.

Reclassification of Valve Disc 1B33-F023B
The disc associated with the reactor recirculation pump suction stop valve 1B33-F023B is reclassified from Code to non-Code. It is no longer subject to the American Society of Mechanical Engineers (ASME) Boiler and Pressure Vessel (B&PV) Code, Section III. The reclassification permits accepting surface indications found in the outer edge of the stellite hardfacing seat on one side of the valve disc. The linear indications do not present a functional or technical concern, as they are outside of the actual seating area and there is good fusion with the base material.

Valve 1E12-F050A Insulation Requirements, Design Change Package (DCP) 9900246
DCP 9800182 left a portion of insulation off of Unit 1 shut down cooling mode train A testable check valve 1E12-F050A. This was due to interference from a pipe support mounting beam. Temporary modification (TALT) 1-0092-98 evaluated the temporary removal of the insulation sections for one fuel cycle. DCP 9900246 permanently removed the insulation.

Procedure LLP-99-012 Revision 1, MSR Test Equipment Installation
The procedure governs the installation of test equipment for monitoring the Unit 2 moisture separator reheater (MSR) system during startup and periodically during operation. Revision 1 adds a section to allow removal of selected test equipment while in any operational condition.

Procedure LLP-99-021 Revision 0, MSR Test Equipment Installation
The procedure governs the installation of test equipment for monitoring the Unit 1 moisture separator reheater (MSR) system during startup and periodically during operation. Revision 1 adds a section to allow removal of selected test equipment while in any operational condition.

Procedure LLP-99-024 Revision 0, Radwaste Tank Cleaning
The procedure provides overall direction and sequencing for sludge removal and cleaning of various radwaste tanks using vendor supplied equipment. The following LaSalle Operating Procedures (LOP) were revised to bypass the respective tank low cutout interlock to allow the tank contents to be pump out as much as possible, as desired by radwaste supervision:
LOP-WE-03 Revision 7, Waste Collector Tank Blowdown To Waste Flocculation Tank;
LOP-WE-07 Revision 9, Waste Collector Surge Tank Blowdown To The Waste Flocculation Tank;
LOP-WE-011 Revision 8, Waste Flocculation Tank Blowdown To URC Sludge Tank;
LOP-WZ-16 Revision 6, Chemical Waste Collector Tank Sludge Transfer (Bottom Blowdown) To Waste Sludge Tank;
LOP-WZ-17 Revision 6, Chemical Waste Head Tank Transfer To Floor Drain Concentrator Sample Tank;
LOP-WF-03 Revision 8, Floor Drain Collector Tank Transfer To Floor Drain Concentrator Feed Tank;
LOP-WF-11 Revision 8, Floor Drain Head Tank Processing To The Floor Drain Concentrator Sample Tank;
LOP-WF-22 Revision 20, Floor Drain Collector Tank Transfer To Waste Sludge Tank;
LOP-WF-33 Revision 2, Process of Waste Water Using The Radwaste Liquid Processing Vendor Skid;
LOP-WX-06 Revision 12, Floor Drain Concentrator Feed Tank Sludge Transfer To The Waste Sludge Tank;
LOP-WX-08 Revision 12, Establishing A URC Sludge Tank Transfer Loop; and
LOP-WX-10 Revision 12, Establishing A Spent Resin Tank Transfer Loop.

Change to Procedure Described in UFSAR, and UFSAR Revision
Procedure LOP-WX-08, Establishing A URC Sludge Tank Transfer Loop, is revised to allow the capability of using the cycled condensate system (CY) pumps as an

alternative to using the ultrasonic resin cleaner (URC) sludge recycle pumps to provide backflushing and recirculation. UFSAR Section 11.2.2.5.3 is revised.

Revision to UFSAR for Procedure Preparation Process
Processes that are common to each of Commonwealth Edison's five operating stations are being controlled by generic corporate procedures. The corporate organization, with the assistance of each station, is preparing these generic documents. UFSAR Section 13.5.1.2 is revised to reflect the corporate involvement in the preparation of procedures.

Replacement of Primary Containment Ventilation Cooling Condenser Drain Flow Transmitter 1FE-RF021, Design Change Package (DCP) 9900078 and Addendum
The DCP replaced the flow element/transmitter with a modified model supplied by the original manufacturer, Fluid Components International. This was done to reduce the potential for crud buildup at the internal probes. The associated linearizer circuit board was replaced with a board calibrated for the modified element/transmitter.
This evaluation supersedes that of Safety Evaluation Validations L99-391 in its entirety.

Change to UFSAR Table 5.2-3, and Figure 6.3-4, for the Low Pressure Core Spray System (LPCS)
UFSAR Table 5.2-3 and Figure 6.3-4 are revised to identify the design pressure for LPCS to be 550 psig as opposed to 475 psig.

Out of Service to Administratively Prevent Use of Solid Radwaste Decanting Tank Mixer
Out of Service (OOS) 990002892 was initiated on solid radwaste decanting tank 0WX05TB, to administratively control the use of the associated tank mixer. The leads to the decant tank mixer were lifted.

Procedure LIS-NB-103A Revision 1, Unit 1 Average Power Range Monitor Channels A, C and E Rod Block and SCRAM Calibration
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Change to UFSAR Figure 6.3-4, Low Pressure Core Spray System (LPCS)
UFSAR Figure 6.3-4 is revised for the following: The design temperature for the Low Pressure Core Spray System (LPCS) is revised to 480 degrees Fahrenheit as opposed

to the current value of 212 degrees Fahrenhet for locations 3 to 8 and 7 to 7.5; Deleted the "AO" from check valve 1(2)E21-F006 operator; Added Note 13 which states "Free swinging disc. The actuator is used for local leak rate testing only." Revised the LPCS design pressure to be 550 psig as opposed to the current value of 475 psig for figure locations 3 to 8.5, 4 to 4.5 , and 7 to 7.5.

Use of Marathon and Duralife Control Blade Designs
The use Marathon and Duralife control blade designs supplied by General Electric, which utilize the Fabricast velocity limiter, are authorized for use in LaSalle cores. The velocity limiter is a General Electric revised design. The blades utilizing the Fabricast velocity limiter were inserted for Unit 1 cycle 9 operation (L1C9). UFSAR Sections 4.1 and 4.2 are revised to reflect the use Marathon and Duralife control blade designs, and to more accurately reflect the current control blade designs approved for use at LaSalle Station.

UFSAR Revision to Reflect the Unit 1 Cycle 9 Reload Licensing Package
UFSAR Sections 1.2, 2.2, 3.9, 4.2, 4.3, 5.2, 6.2, 6.3, 6.B, 7.7, 9.1, 13.1, 15.0, 15.2, 15.4, 15.A are revised for Unit 1 Cycle 9 operation. The changes reflect Unit 1 operation with fuel manufactured by Siemens Power Corporation (SPC) and General Electric (GE). SPC Atrium 9B fuel and analytical methodologies are reflected in the changes. The associated Core Operating Limits Report was approved Administrative Technical Requirements (ATR) Amendment 33.

Revision to UFSAR to reflect Compliance with Generic Letter 96-06
NRC Generic Letter (GL) 96-06, "Assurance of Equipment Operability and Containment Integrity During Design Basis Accident Conditions," includes a discussion of thermally induced overpressurization of isolated fluid filled piping sections inside primary containment. The overpressurization condition described in the GL applies to primary containment penetrations M-49 and M-50. UFSAR Subsection 3.9.3.1.2.3 is revised to address overpressurization analysis of primary containment penetrations M-49 and M-50.

Procedure LOP-GS-03 Revision 6, Gland Seal Steam System Startup In The Backup Steam Supply Mode;
Procedure LGP-1-1 Revision 61, Normal Unit Startup;
Revision to UFSAR Sections 10.4 and 15.7
An evaluation to use main steam as an alternate to steam supply from the steam seal evaporator was found to be acceptable. The main steam and steam seal evaporator steam discharge into a common header and deliver steam to the same components. Procedures LOP-GS-03 and LGP-1-1 were revised to reflect the allowance to seal the main turbine using main steam, and provide direction in sealing the main turbine using main steam.

This also effects a revision to UFSAR Sections 10.4 and 15.7.

As-Built Drawing Change Request (DCR) 990859
Drawing M-1450 sheet was previously revised to change various specific devices including future equipment/service that are serviced by machine shop ventilation units 0VJ02S and 0VJ04S to "various equipment." Per the DCR, drawing M-1450 sheet 1 will be revised to change future service to various equipment that is serviced by another machine shop ventilation unit 0VJ06S.

Installation of a Temporary Freeze Seal on Line 2CY23AB-4"
A temporary freeze seal was installed on line 2CY23AB-4" in accordance with procedure LMP-GM-79. The freeze seal allows repairing valve 2CP100B, which is leaking through its seat. Valve 2CP100B is the Condensate Demineralizer Regeneration System Feedpump 2CP05PB Suction Isolation Valve. This valve cannot be isolated from the common cycled condensate (CY) supply header 2CY23AA-4", which serves both condensate demineralizer regeneration system feedpumps 2CP05PA and B. The freeze seal serves as the upstream isolation barrier to isolate valve 2CP100B from the suction header 2CY23AA-4". This allowed feed pump 2CP05A to remain functional and operable.

Change to UFSAR Section 6.1 and 9.2 to reflect Use of Corrosion Inhibitors
UFSAR Subsections 6.1.1.2, Composition, Compatibility and Stability of Containment and Core Spray Coolants, 6.1.3, Post-Accident Chemistry, 9.2.3.2, Reactor Building Closed Cooling Water System description, 9.2.8.2, Turbine Building Closed Cooling Water, and 9.2.9.2, Primary Containment Chilled Water System description, are revised to state that limited quantities of corrosion inhibitors are present in these systems. The proposed change accurately reflects the condition of the plant in regard to the use of corrosion inhibitors, while not restricting the use of new, improved or alternate corrosion inhibitors that are evaluated to be acceptable for use at LaSalle.

Revision to Turbine Control Valve Monthly Surveillance, LaSalle Operating Surveillance procedure LOS-RP-M5
LOS-RP-M5 Revision 1 incorporates scram reduction test methodology which allows the operator performing the test to see that a scram signal is generated, but prevents the actual scram signal from the turbine control valve (TCV) fast closure from generating a "half scram." UFSAR Sections 7.2 and 7.A.2 are revised to reflect this scram reduction test methodology.

Restart of Plant Process Computer P4 Program
It was recently discovered that the feedwater flow computer points used for core thermal power calculations were not being temperature (density) corrected by the process

computer. The P4 program currently residing on the process computer normally performs this function. During the transition from the P1 program to CMC (GE's Core Monitoring Code) in 1988, the P4 program was incorrectly turned off. The P4 program residing in the plant process computer was restarted so that it performs its intended function. Following P4 program turn on, core thermal power may be calculated correctly. This is compatible with the Powerplex code, as it uses the same computer points in its core thermal power calculation. Powerplex calculations are more accurate while the P4 program is on and correctly accounting for temperature differences in the feedwater flow. Other process computer programs will continue to function normally with P4 turned on, as they did before the program was turned off.

LaSalle Technical Procedure LTP-DC-04 Revision 3, 250VDC Battery Elevated Equalize Charge;
LaSalle Technical Surveillance LTS-700-1 Revision 11, Unit 1(2) 250VDC Battery Performance Test Discharge;
LaSalle Technical Surveillance LTS-700-5 Revision 14, Unit 1(2) 250VDC Battery Service Test Discharge
The procedures are used to perform 250 vold direct current (VDC) battery testing with the plant in any operational condition. A new load bank is used as the master load bank. The configuration of the new master load bank differs from that of the previous master load bank. These procedures satisfy the guidelines of IEEE Standard 450-1980 for the performance of a service discharge test or a performance discharge test.

Procedure LIS-RD-201 Revision 7, Unit 2 SCRAM Discharge Volume Level Alarm, Rod Block, and SCRAM Calibration
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Procedure LIS-RD-203 Revision 8, Unit 2 Control Rod Drive SCRAM Discharge Volume Level Transmitters Calibration
The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.

Procedure LIS-RD-204 Revision 14, Unit 2 Control Rod Drive Water Header Low Pressure SCRAM Calibration

The procedure incorporates SCRAM reduction test methodology through the use of a trip indication test box, which is an alternative method of testing reactor protection system (RPS) instrument channels. The alternative test consists of applying a test signal to the RPS channel and observing that an instrument channel trip occurs without a logic trip. This allows the trip function of the instrument channel contacts to be verified without tripping the associated logic circuit during the calibration or functional testing of the instrument channel.