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**Nuclear Business Unit**

FEB 24 2000

LR-N000052

United States Nuclear Regulatory Commission  
Document Control Desk  
Washington, D.C. 20555

**RADIOACTIVE EFFLUENT RELEASE REPORT - 47  
SALEM GENERATING STATION UNIT NOS. 1 AND 2  
DOCKET NOS. 50-272 AND 50-311**

Gentlemen:

In accordance with Section 6.9.1.8 of Appendix A to the Operating Licenses for Salem Generating Station, Public Service Electric and Gas Company (PSE&G) hereby transmits one copy of the semiannual Radioactive Effluent Release Report, RERR-47. This report summarizes liquid and gaseous releases and solid waste shipments from the Salem Generating Station for the period of July 1, 1999 to December 31, 1999. Should you have any questions regarding this transmittal, please contact us.

Sincerely,

A handwritten signature in cursive script that reads "Mark B. Bezilla".

Mark B. Bezilla  
Vice President - Operations

Attachment

The power is in your hands.

IE48

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**SALEM GENERATING STATION**  
**SEMI-ANNUAL RADIOACTIVE EFFLUENT RELEASE REPORT**

**SGS RERR-47**

**SALEM UNIT NOS. 1 & 2**

**DOCKET NO. 50-272**

**DOCKET NO. 50-311**

**OPERATING LICENSE NO. DPR-070**

**OPERATING LICENSE NO. DPR-075**

**February 2000**

**SALEM GENERATING STATION**

**RADIOACTIVE EFFLUENT RELEASE REPORT**

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***JULY - DECEMBER 1999***

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## SALEM GENERATING STATION

### RADIOACTIVE EFFLUENT RELEASE REPORT

JULY -DECEMBER 1999

#### INTRODUCTION

This report, SGS-RERR-47 summarizes information pertaining to the releases of radioactive materials in liquid, gaseous and solid form from the Salem Generating Station (SGS) for the period July 1, 1999 to December 31, 1999.

Salem Unit 1 is a Westinghouse Pressurized Water Reactor which has a licensed core thermal power of 3411 MWt and an approximate net electrical output of 1115 MWe. Salem Unit 1 achieved initial criticality on December 11, 1976 and went into commercial operation on June 30, 1977.

Salem Unit 2 is a Westinghouse Pressurized Water Reactor which has a licensed core thermal power of 3411 MWt and an approximate net electrical output of 1115 MWe. Salem Unit 2 achieved initial criticality on August 2, 1980 and went into commercial operation on October 13, 1981.

This report is prepared in the format of Regulatory Guide 1.21, Appendix B, as required by Specification 6.9.1.8 of the Salem Technical Specifications. Preceding the tables summarizing the gaseous and liquid discharges and solid radwaste shipments are our responses to parts A-F of the "Supplemental Information" section of Regulatory Guide 1.21, Appendix B.

As required by Regulatory Guide 1.21, the Salem Technical Specification limits are described in detail within this report along with a summary description of how measurements and determinations of the total activity discharged were developed.

To facilitate determination of compliance with 40CFR190 requirements, the following information on electrical output is provided.

Salem Unit 1 generated **3,572,792** megawatt-hours of electrical energy (net) during the reporting period.

Salem Unit 2 generated **4,789,363** megawatt-hours of electrical energy (net) during the reporting period.

Results of liquid and gaseous composites analyzed for Sr-89, Sr-90 and Fe-55 for the fourth quarter of 1999 were not available for inclusion in this report. The results of these composites will be provided in the next Radioactive Effluent Release Report.

The results of the liquid and gaseous composites analyzed for Sr-89, Sr-90, and Fe-55 for the second quarter of 1999, not included in RERR-46, are included in Revision 1 to RERR-46. The revised pages are provided as Appendix B to this report.

## **PART A. PRELIMINARY SUPPLEMENTAL INFORMATION**

### **1.0 REGULATORY LIMITS**

#### **1.1 Fission and Activation Gas Release Limits**

The dose rate due to radioactive materials released in gaseous effluents from the site (i.e. Salem Units 1 & 2, and Hope Creek) to areas at and beyond the site boundary, shall be limited to the following:

For noble gases: Less than or equal to 500 mrem/yr to the total body and less than or equal to 3000 mrem/yr to the skin.

In addition, the air dose due to noble gases released in gaseous effluents from each reactor unit to areas at and beyond the site boundary, shall be limited to the following:

During any calendar quarter: Less than or equal to 5 mrad for gamma radiation and less than or equal to 10 mrad for beta radiation and,

During any calendar year: Less than or equal to 10 mrad for gamma radiation and less than or equal to 20 mrad for beta radiation.

#### **1.2 Iodine, Particulates, and Tritium**

The dose rate due to radioactive materials released in gaseous effluents from the site to areas at and beyond the site boundary, shall be limited to the following:

For iodine-131, for tritium, and for all radionuclides in particulate form with half-lives greater than 8 days: Less than or equal to 1500 mrem/yr to any organ.

In addition, the dose to a member of the public from iodine-131, from tritium, and from all radionuclides in particulate form with half-lives greater than 8 days in gaseous effluents released, from each reactor unit, to areas at and beyond the site boundary, shall be limited to the following:

During any calendar quarter: Less than or equal to 7.5 mrem to any organ and,

During any calendar year: Less than or equal to 15 mrem to any organ.

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### **1.3 Liquid Effluents Release Limits**

The concentration of radioactive material released in liquid effluents to unrestricted areas shall be limited to the concentrations specified in 10CFR20, Appendix B, Table II, Column 2 for radionuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to 2E-04 microcuries per milliliter.

In addition, the dose or dose commitment to a member of the public from radioactive materials in liquid effluents released to unrestricted areas shall be limited to:

During any calendar quarter: Less than or equal to 1.5 mrem to the total body, and less than or equal to 5 mrem to any organ, and

During any calendar year: Less than or equal to 3 mrem to the total body, and less than or equal to 10 mrem to any organ.

### **1.4 Total Dose Limit**

The annual (calendar year) dose or dose commitment to any member of the public, due to releases of radioactivity and radiation, from uranium fuel cycle sources shall be limited to less than or equal to 25 mrem to the total body or any organ (except the thyroid, which shall be limited to less than or equal to 75 mrem).

## **2.0 MAXIMUM PERMISSIBLE CONCENTRATIONS (MPC)**

Regulatory Guide 1.21 requires that the licensee provide the MPC's used in determining allowable release rates or concentrations for radioactive releases.

- a. MPC values are not used for gaseous releases. Determination of maximum release rates for noble gases, iodines, tritium, and for all radionuclides in particulate form (with half-lives > 8 days), are based on dose rate calculations as specified in the ODCM.
- b. According to current Technical Specifications, MPC values as stated in 10CFR20, Appendix B, Table II, Column 2 are to be used for liquid effluents. Since the MPC values were removed from 10CFR20 effective 1/1/94, the MPC values are now contained in the ODCM. These MPC values are added as Appendix A of this report.
- c. The MPC value used for dissolved or entrained noble gases in liquid effluents is 2E-04 microcuries per milliliter.

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### **3.0 AVERAGE ENERGY**

Regulatory Guide 1.21 requires that the licensee provide the average energy of the radionuclide mixture in releases of fission and activation gases, if applicable.

Release limits for SGS are not based upon average energy. Therefore this section is not applicable to SGS.

### **4.0 MEASUREMENTS AND APPROXIMATIONS OF TOTAL RADIOACTIVITY**

#### **4.1 Liquid Effluents**

Liquid effluents are monitored in accordance with Table 4.11-1 of the Technical Specifications. During the period of record, all batch liquid wastes were routed to hold-up tanks for monitoring prior to release. Technical Specifications require these tanks to be uniformly mixed for sampling and analysis before being released. Batch releases are defined as releases from the waste monitor hold-up tank, and the chemical and volume control hold-up tanks. Continuous liquid releases are defined as condensate releases from intermittent blowdown of the steam generators. To determine the total liquid activity discharged in continuous releases, the specific activities from analyses were multiplied by the volume of effluent discharged.

The detection requirements of Table 4.11-1 of the Technical Specifications are achieved or exceeded. Radionuclides detected at concentrations below the Technical Specification lower limit of detection (LLD) are treated as being present. Radionuclides for which no activity was detected while meeting the required LLD's are treated as absent.

#### **4.2 Gaseous Effluents**

Gaseous effluent streams are monitored and sampled in accordance with Table 4.11-2 of the Technical Specifications. The Plant Vent is the final release point for planned gaseous effluent releases and is continuously monitored by installed radiation monitors. The vent is also continuously sampled for iodine and particulates with a charcoal cartridge and filter paper. The filter and charcoal are changed weekly, and analyzed on a multichannel analyzer.

Sampling is also performed on all gas decay tanks and containment purges prior to their release to the environment. The plant vent is sampled weekly for noble gases.

The detection requirements of Table 4.11-2 of the Technical Specifications are achieved or exceeded. Radionuclides detected at concentrations below the Technical Specification LLD are treated as being present. Radionuclides for which no activity was detected while meeting the required LLDs are treated as absent.

Continuous Mode gaseous releases are quantified by routine (monthly or weekly) sampling and isotopic analyses of the plant vent. Specific activities for each isotope detected are multiplied by the total vent flow volume for the entire sampling period in order to determine the normal continuous release of radioactivity through the plant vent.

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Slightly elevated plant vent radiation monitoring readings and containment pressure reliefs are treated as continuous releases. The monitor response is converted to "specific activity" using historical efficiency factors. The "specific activity" is multiplied by a conservative default volume of effluent discharge to determine the total activity released.

Batch Mode gaseous releases are quantified by sampling each decay tank or containment purge prior to release. Specific activities for each isotope are multiplied by the total volume of gas discharged for that batch to determine the total activity released.

Elevated plant vent radiation monitoring system readings while the channel is in an alarm state are treated as batch mode releases. If specific activity data from grab samples are not available, then the abnormal release is quantified by the use of the plant vent radiation monitors. The monitor response is converted to "specific activity" using historical efficiency factors. The "specific activity" is multiplied by the volume of effluent discharged while the channel was in an alarm state in order to determine the total activity discharged.

#### **4.3 Estimated Total Error**

The estimated total error of reported liquid and solid releases is within 25%.

The estimated total error of the reported continuous gaseous releases is within 50% when concentrations exceed detectable levels. This error is due primarily to variability of waste stream flow rates and changes in isotopic distributions of waste streams between sampling periods. The estimated total error of the reported batch gaseous releases is within 10%.

Error estimates for releases where sample activity is below the detectable concentration levels are not included since error estimates at the LLD are not defined.

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## **5.0 BATCH RELEASES**

Summaries of batch releases of gaseous and liquid effluents are provided in Tables 4A-1 and 4B-1 for Unit 1 and 4A-2 and 4B-2 for Unit 2.

## **6.0 UNPLANNED/ABNORMAL RELEASES**

During this report period, the following unplanned/abnormal releases occurred:

### **a. Liquid**

There were no unplanned/abnormal liquid releases this period.

### **b. Gaseous**

1. Number of releases: 2
2. Total activity released: 15.1 curies

#### **Salem Unit 1**

- On September 8, 1999, the 12 mixed-bed demineralizer was isolated and tagged in preparation for resin sluicing operations. While the demineralizer was being drained, operators identified that the isolation valve was leaking by, allowing about 200 gallons of reactor coolant to leak directly to the plant's radioactive waste system. Reactor coolant fission gases escaped from the liquid phase into the auxiliary building atmosphere and to the plant vent. One of the plant vent radiation monitors, 1R16, went into the alarm state. It was determined that approximately 15 curies of mixed fission product noble gases escaped through the plant vent. The activity released is included in the data provided in Tables 1A-1 and 1C-1.

#### **Salem Unit 2**

- On August 12, 1999, while performing sluicing operations, the 23 Waste Gas Decay Tank (WGDT) was inadvertently released to the Auxiliary Building via the Waste Liquid (WL) system. The gas escaped through an open drain valve on the Spent Resin Storage Tank (SRST) when the tank was allowed to completely drain to the WL system. Although the release did not exceed any radiation monitor alarm/trip setpoint, the plant vent noble gas radiation monitor 2R41 radiation levels increased from 32 uCi/sec to a peak value of 74 uCi/sec. The valve was open for about 40 minutes before being closed, terminating the release. The total activity released during this occurrence was approximately 0.1 curies of noble gases. The activity released is included in the data provided in Tables 1A-2 and 1C-2.

## 7.0 ELEVATED RADIATION MONITOR RESPONSES

During this reporting period, the following radiation monitors were in an alarm condition:

### Salem Unit 1

- The plant vent radiation monitor 1R16 as discussed in Section 6.0 above.
- On October 1, 1999, the plant vent radiation monitor 1R16 went into alarm and 1R41 went into warning (below alarm state). The alarms occurred during normal draining and venting operations of the boric acid injection tank and charging system. The elevated readings were attributed to the high noble gas inventory due to existing fuel defects. The activity associated with these elevated readings is included in Tables 1A-1 and 1C-1 of this report.
- During the Salem Unit 1 refueling outage, the containment noble gas monitor (1R12A) setpoint was lowered to two times background as required by Technical Specifications. During routine refueling operations, the 1R12A went into alarm due to the low setpoint. No abnormal radiological release occurred.

## 8.0 MODIFICATION TO PREVIOUS RADIOACTIVE EFFLUENT RELEASE REPORTS

Radioactive Effluent Release Report RERR46 was revised to include the results of composite analyses not available at the time of the original report submittal. Also, Table 2A-2 and 2A-4 from RERR-46 were revised to include continuous liquid release information from steam generator blowdown due to primary to secondary leakage on the 23 Steam Generator. The revised pages of the report are included as Appendix B to this report.

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**PART B. GASEOUS EFFLUENTS**

See Summary Tables 1A-1 through 1C for Salem Unit 1 Operations.

See Summary Tables 1A-2 through 1C for Salem Unit 2 Operations.

**PART C. LIQUID EFFLUENTS**

See Summary Tables 2A-1 through 2B for Salem Unit 1 Operations.

See Summary Tables 2A-2 through 2B for Salem Unit 2 Operations.

**PART D. SOLID WASTE**

See Summary in Table 3.

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**PART E. RADIOLOGICAL IMPACT ON MAN**

The calculated individual doses in this section are based on the controlling dose pathways and age groups as described below. The estimated dose represents the maximum radiation dose that could be received by a member of the general public. The population dose impact is based on historical site-specific data (i.e., food production, milk production, feed for milk animals and seafood production).

The doses were calculated using methods described in Regulatory Guide 1.109 and represent calculations for the 1999 calendar year. Individual doses from batch and continuous releases were calculated using the annual average historic meteorological dispersion coefficients as described in the Offsite Dose Calculation Manual. Population doses were calculated using the meteorological dispersion coefficients for the two six month reporting intervals.

**Liquid Pathways**

<u>Type</u>	<u>Age Group</u>	<u>Location</u>	<u>Pathway</u>
Total Body	Adult	Site Boundary	Seafood Ingestion
Organ	Adult	Site Boundary	Seafood Ingestion

<u>Type</u>	<u>Dose</u>	<u>Limit</u>
Total Body	1.12E-01 mrem	3 mrem
Organ Dose (Liver)	1.52E-01 mrem	10 mrem
Population (Total)	1.44E-01 Person-rem	N/A
Population (Average)	3.20E-08 mrem	N/A

**Air Pathways**

<u>Type</u>	<u>Age Group</u>	<u>Location</u>	<u>Pathway</u>
Total Body	All	Site Boundary	Direct Exposure
Skin	All	Site Boundary	Direct Exposure
Organ	Infant	4.9 mi. W.	Milk, Ground Plane, Inhalation

<u>Type</u>	<u>Dose</u>	<u>Limit</u>
Total Body	9.14E-02 mrem	500 mrem/yr *
Skin	2.17E-01 mrem	3000 mrem/yr *
Organ Dose (Thyroid)	3.58E-02 mrem	15 mrem
Population (Total)	3.00E+00 Person-rem	N/A
Population (Average)	6.67E-07 mrem	N/A

\* Dose rate limit

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**Direct Radiation**

Direct radiation may be estimated by thermoluminescent dosimetric (TLD) measurements. One method for comparing TLD measurements is by comparison with pre-operational data. It should be noted that the TLDs measure direct radiation from both the Salem and Hope Creek Generating Stations at Artificial Island, and natural background radiation.

TLD data for the six-month reporting period is given below:

<u>TLD</u>	<u>Location</u>	<u>Measurement</u>
1S-1	0.5 mi. N	4.57 mrad/month
5S-1	1.0 mi. E	3.45 mrad/month

These values are interpreted to represent natural background, since the values are within the statistical variation associated with the pre-operational program results, which are 4.1 mrad/month for location 1S-1, and 3.8 mrad/month for location 5S-1.

Since the nearest resident is 3.5 miles away, it can be concluded that the direct radiation from the operation of Salem station has not impacted the dose to members of the public in unrestricted areas.

**Total Dose**

40CFR190 limits the total dose to members of the public due to radioactivity and radiation from uranium fuel cycle sources to:

<25 mrem total body or any organ and;

<75 mrem thyroid for a calendar year.

For Artificial Island, the major sources of dose are from liquid and gaseous effluents from the Hope Creek and Salem plants.

The following doses to a "hypothetical maximum exposed individual" have been calculated for the 1999 calendar year. They are the sum of gaseous and liquid pathway doses for the Salem 1 and 2 and Hope Creek plants:

3.42E-01	mrem	Total Body
4.39E-01	mrem	Organ (GI-LLI)
3.21E-01	mrem	Thyroid

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**Dose to members of the public due to activities inside the site boundary**

Dose to members of the public is limited to 100 mrem total effective dose equivalent (TEDE) in a year in accordance with 10CFR20.1301. The members of the public that spent the most time at the NBU for July - December 1999 are various food vendors, who spent a few hours each week in front of the Security Center during lunch hours. In accordance with the requirements of Technical Specification 6.9.1.8, the dose to members of the public inside the site boundary has been calculated based on the following assumptions:

- a. The food vendors deliver Monday through Friday.
- b. They arrive at approximately 11:00 A.M. at the Security Center.
- c. The food vendors leave the site at 12:30 P.M.
- d. No deliveries are made on major holidays, making the total weeks equal 50 for the year.
- e. The dose data is based on the TLD located outside the Security Center in the vicinity of the food vendors and the calculated dose due to gaseous effluents at that location.

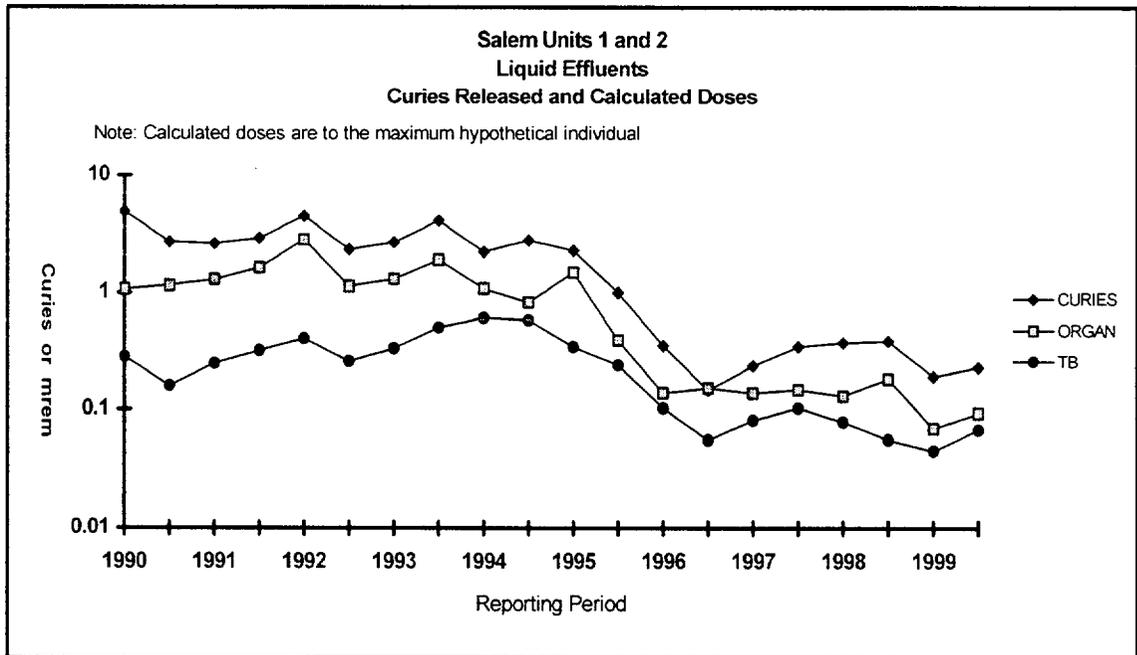
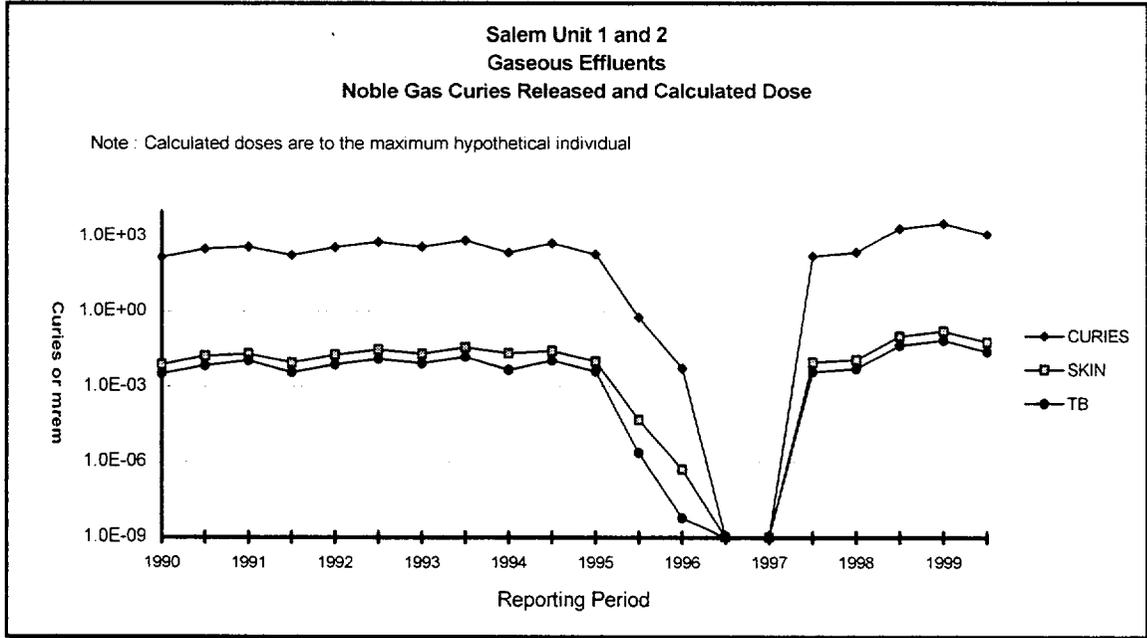
For the six-month reporting period, July 1 to December 31, 1999 the calculated doses from the operation of the Salem units are:

1.22E+00	mrem	Total Body
4.58E-03	mrem	Organ (GI-LLI)
4.73E-03	mrem	Thyroid

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**Trends**

The following two trend graphs show the total curies of gaseous and liquid effluents released for Salem from 1990 through 1999. Calculated doses in the graphs are to the maximum hypothetical individual.



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Assessment

**1. Gaseous:**

Gaseous effluents released from Salem Units 1 and 2 resulted in an insignificant projected dose to the maximum hypothetical individual. The dose for the six-month period was a small fraction of all applicable limits.

Reported gaseous effluents decreased from the previous reporting period and continue to remain well within Federal limits. Gaseous effluents released from Salem decreased principally due to the replacement of fuel that had small defects. Gaseous effluent processing equipment continues to be maintained in order to ensure that all releases of gaseous radioactivity are As-Low-As-Reasonably-Achievable (ALARA).

**2. Liquids:**

Liquid effluents released from Salem Units 1 and 2 resulted in an insignificant projected dose to the maximum hypothetical individual and were well within all applicable limits.

The amount of radioactivity in liquid effluents increased slightly from previous reporting periods due to the waste processing equipment challenges.

#### **PART F. METEOROLOGICAL DATA**

Cumulative joint wind frequency distributions by atmospheric stability class at the 33 foot elevation are provided for 1999 at the end of this report in Appendix C.

#### **PART G. OFFSITE DOSE CALCULATION MANUAL (ODCM) CHANGES**

During the report period, the Salem Offsite Dose Calculation Manual was revised twice, as follows:

- SORC approved Revision 12 of the ODCM on October 11, 1999. The revision corrected parameters associated with higher maximum steam generator blowdown flowrates. Engineering evaluations concluded that operating at higher steam generator blowdown flowrates had no detrimental effect on potential dose to the public from radioactive effluents. The revision also included approved changes to REMP sampling locations. There were several editorial changes, also. A copy of the revision summary is provided as Appendix D of this report.
- SORC approved Revision 13 of the ODCM on 12/22/99 in support of License Change Request to implement Nuclear Regulatory Commission Generic Letter 89-01. A copy of Revision 13 of the Salem ODCM is provided as Appendix E of this report.

#### **PART H. INOPERABLE MONITORS**

During this period the following effluent radiation monitors were inoperable for greater than 30 days:

- Salem Unit 2

Plant Vent Noble Gas Radiation Monitor (2R41). The monitor was declared inoperable due to frequent failures of the mid and high range sample pumps resulting in loss of sample flow. Troubleshooting determined that the pumps thermal overload protection was not adequately designed for the existing normal load condition. A new design sample pump was installed. The corrective actions were not timely due to the extensive troubleshooting required to identify the cause of frequent pump failure and the lead time to obtain a new design pump from the manufacturer.

#### **PART I. PROCESS CONTROL PROGRAM (PCP) CHANGES**

During the reporting period, there were no changes to the process control program.

#### **PART J. ENVIRONMENTAL MONITORING LOCATION CHANGES**

During the reporting period, the following changes to the Radiological Environmental Monitoring Program (REMP) were made:

- Replaced control TLD location 3H3 with 14G1 to relocate the control station as recommended by the Radiological Assessment Branch Technical Position November 1979.
- Replaced the milk sample location at 2F7 with the milk farm at 2F9. The farmer at location 2F7 went out of business.

#### **PART K. MAJOR CHANGES TO WASTE PROCESSING SYSTEMS**

During the report period, there were no major changes to the waste processing systems at Salem Unit 1 or 2.

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**SALEM GENERATING STATION  
TABLE 1A-1**

**EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 1  
GASEOUS EFFLUENTS – SUMMATION OF ALL RELEASES**

		Units	3 <sup>rd</sup> Quarter	4 <sup>th</sup> Quarter	Est. Total Error <sup>1</sup>
<b>A.</b>	<b>Fission and Activation Products</b>				
1.	Total Release	Ci	8.00E+02	2.23E+02	50%
2.	Average Release Rate For Period	μCi/sec	1.02E+02	2.83E+01	
3.	Percent of Technical Specification Limit (T.S. 3.11.2.2(a))	%	5.90E-01	1.64E-01	
<b>B.</b>	<b>Iodines</b>				
1.	Total Iodine-131	Ci	1.84E-03	1.63E-03	50%
2.	Average Release Rate For Period	μCi/sec	2.35E-04	2.07E-04	
3.	Percent of Technical Specification Limit <sup>2</sup> (T.S. 3.11.2.3(a))	%	9.10E-02	7.83E-02	
<b>C.</b>	<b>Particulates</b>				
1.	Particulates With Half-lives > 8 days	Ci	2.67E-05	6.35E-05	50%
2.	Average Release Rate For Period	μCi/sec	3.39E-06	8.06E-06	
3.	Percent of Technical Specification Limit <sup>2</sup> (T.S. 3.11.2.3(a))	%	9.10E-02	7.83E-02	
4.	Gross Alpha	Ci	0.00E+00	0.00E+00	
<b>D.</b>	<b>Tritium</b>				
1.	Total Release	Ci	1.63E+02	6.05E+01	50%
2.	Average Release Rate For Period	μCi/sec	2.08E+01	7.69E+00	
3.	Percent of Technical Specification Limit <sup>2</sup> (T.S. 3.11.2.3(a))	%	9.10E-02	7.83E-02	

1. For batch releases, the estimated overall error is 10%.
2. Iodines, Tritium, and Particulates are treated as a group.

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 1A-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT2  
GASEOUS EFFLUENTS – SUMMATION OF ALL RELEASES

		Units	3 <sup>rd</sup> Quarter	4 <sup>th</sup> Quarter	Est. Total Error <sup>1</sup>
<b>A.</b>	<b>Fission and Activation Products</b>				
1.	Total Release	Ci	5.20E+1	1.01E+02	50%
2.	Average Release Rate For Period	μCi/sec	6.62E+00	1.29E+01	
3.	Percent of Technical Specification Limit (T.S. 3.11.2.2(a))	%	3.82E-02	7.43E-02	
<b>B.</b>	<b>Iodines</b>				
1.	Total Iodine-131	Ci	2.51E-04	2.01E-04	50%
2.	Average Release Rate For Period	μCi/sec	3.19E-05	2.55E-05	
3.	Percent of Technical Specification Limit <sup>2</sup> (T.S. 3.11.2.3(a))	%	1.59E-02	1.48E-02	
<b>C.</b>	<b>Particulates</b>				
1.	Particulates With Half-lives > 8 days	Ci	4.02E-06	1.95E-05	50%
2.	Average Release Rate For Period	μCi/sec	5.11E-07	2.48E-06	
3.	Percent of Technical Specification Limit <sup>2</sup> (T.S. 3.11.2.3(a))	%	1.59E-02	1.48E-02	
4.	Gross Alpha	Ci	0.00E+00	0.00E+00	
<b>D.</b>	<b>Tritium</b>				
1.	Total Release	Ci	1.43E+02	1.30E+02	50%
2.	Average Release Rate For Period	μCi/sec	1.82E+01	1.66E+01	
3.	Percent of Technical Specification Limit <sup>2</sup> (T.S. 3.11.2.3(a))	%	1.59E-02	1.48E-02	

1. For batch releases, the estimated overall error is 10%.
2. Iodines, Tritium, and Particulates are treated as a group.

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 1B

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
GASEOUS EFFLUENTS – ELEVATED RELEASES

There were no elevated releases during this reporting period.

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 1C-1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 1  
GASEOUS EFFLUENTS – GROUND LEVEL RELEASES

Nuclides  Released	Units	<u>Continuous Mode</u>		<u>Batch Mode</u>	
		<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>	<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>
<b>1. Fission Gases</b>					
Krypton-85	Ci			6.56E+00	1.99E+00
Krypton-85m	Ci				5.94E-09
Krypton-88	Ci				3.86E-13
Xenon-131m	Ci			4.86E-01	1.56E-01
Xenon-133	Ci	6.92E+02	2.19E+02	9.98E+01	1.30E+00
Xenon-133m	Ci			7.27E-01	2.41E-03
Xenon-135	Ci			5.26E-02	2.37E-04
<b>Totals</b>	<b>Ci</b>	<b>6.92E+02</b>	<b>2.19E+02</b>	<b>1.08E+02</b>	<b>3.45E+00</b>
<b>2. Iodine</b>					
Iodine-131	Ci	1.84E-03	1.63E-03		
<b>Totals</b>	<b>Ci</b>	<b>1.84E-03</b>	<b>1.63E-03</b>	<b>0.00E+00</b>	<b>0.00E+00</b>
<b>3. Particulates</b> (Half-life >8 days)					
Cobalt-60	Ci	1.50E-06	1.05E-06		
Cobalt-58	Ci	2.36E-05	4.90E-05		
Cs-137	Ci	1.60E-06	1.34E-05		
<b>Totals</b>	<b>Ci</b>	<b>2.67E-05</b>	<b>6.35E-05</b>	<b>0.00E+00</b>	<b>0.00E+00</b>
<b>4. Tritium</b>	<b>Ci</b>	<b>1.63E+02</b>	<b>6.05E+01</b>	<b>0.00E+00</b>	<b>0.00E+00</b>

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 1C-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 2  
GASEOUS EFFLUENTS – GROUND LEVEL RELEASES

Nuclides  Released	Units	<u>Continuous Mode</u>		<u>Batch Mode</u>	
		<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>	<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>
<b>1. Fission Gases</b>					
Krypton-85	Ci			1.47E-01	2.44E-01
Xenon-131m	Ci			1.68E-02	1.43E-02
Xenon-133	Ci	5.14E+01	1.00E+02	4.61E-01	6.35E-01
Xenon-133m	Ci			2.74E-03	5.86E-03
Xenon-135	Ci			4.98E-04	8.21E-04
<b>Totals</b>	<b>Ci</b>	<b>5.14E+01</b>	<b>1.00E+02</b>	<b>6.28E-01</b>	<b>8.99E-01</b>
<b>2. Iodine</b>					
Iodine-131	Ci	2.51E-04	2.01E-04		
<b>Totals</b>	<b>Ci</b>	<b>2.51E-04</b>	<b>2.01E-04</b>	<b>0.00E+00</b>	<b>0.00E+00</b>
<b>3. Particulates</b> (Half-life >8 days)					
Manganese-54	Ci	5.16E-07			
Cobalt-58	Ci	3.50E-06	1.31E-05		
Cobalt-60	Ci		3.48E-06		
Cesium-137	Ci		2.90E-06		
<b>Totals</b>	<b>Ci</b>	<b>4.02E-06</b>	<b>1.95E-5</b>	<b>0.00E+00</b>	<b>0.00E+00</b>
<b>4. Tritium</b>	<b>Ci</b>	<b>1.43E+02</b>	<b>1.30E+02</b>	<b>0.00E+00</b>	<b>0.00E+00</b>

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 2A-1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 1  
LIQUID EFFLUENTS – SUMMATION OF ALL RELEASES

		Units	3 <sup>rd</sup> Quarter	4 <sup>th</sup> Quarter	Est. Total Error
<b>A.</b>	<b>Fission and Activation Products</b>				
1.	Total Release	Ci	7.00E-02	1.74E-02	25%
2.	Average Release Rate For Period	μCi/ml	8.97E-07	1.72E-07	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.2(a))	%	8.91E-01	3.18E-01	
<b>B.</b>	<b>Tritium</b>				
1.	Total Release	Ci	5.77E+01	9.69E+01	25%
2.	Average Release Rate For Period	μCi/ml	7.40E-04	9.58E-04	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	2.46E+01	3.19E+01	
<b>C.</b>	<b>Dissolved and Entrained Noble Gases</b>				
1.	Total Release	Ci	1.70E-02	2.22E-03	25%
2.	Average Release Rate For Period	μCi/ml	2.18E-07	2.20E-08	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	1.09E-01	1.10E-02	
<b>D.</b>	<b>Gross Alpha</b>	Ci	0.00E+00	0.00E+00	25%
<b>E.</b>	<b>Volume of Waste Release (Prior to Dilution)</b>	Liters	5.64E+05	7.72E+05	25%
<b>F.</b>	<b>Volume of Dilution Water Used During Entire Period</b>	Liters	7.80E+07	1.01E+08	25%

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 2A-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 2  
LIQUID EFFLUENTS – SUMMATION OF ALL RELEASES

		Units	3 <sup>rd</sup> Quarter	4 <sup>th</sup> Quarter	Est. Total Error
<b>A.</b>	<b>Fission and Activation Products</b>				
1.	Total Release	Ci	1.07E-01	3.34E-02	25%
2.	Average Release Rate For Period	μCi/ml	1.28E-06	3.39E-07	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.2(a))	%	1.77E+00	6.21E-01	
<b>B.</b>	<b>Tritium</b>				
1.	Total Release	Ci	5.44E+01	1.24E+02	25%
2.	Average Release Rate For Period	μCi/ml	6.47E-04	1.26E-03	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	2.16E+01	4.20E+01	
<b>C.</b>	<b>Dissolved and Entrained Noble Gases</b>				
1.	Total Release	Ci	1.68E-02	1.29E-02	25%
2.	Average Release Rate For Period	μCi/ml	2.16E-07	1.27E-07	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	1.08E-01	6.34E-02	
<b>D.</b>	<b>Gross Alpha</b>	Ci	0.00E+00	0.00E+00	25%
<b>E.</b>	<b>Volume of Waste Release (Prior to Dilution)</b>	Liters	6.89E+05	1.04E+06	25%
<b>F.</b>	<b>Volume of Dilution Water Used During Entire Period</b>	Liters	8.40E+07	9.85E+07	25%

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 2B-1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 1  
LIQUID EFFLUENTS

Nuclides	Units	<u>Continuous Mode</u>		<u>Batch Mode</u>	
		<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>	<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>
<u>Released</u>					
<b>1. Fission and Activation Products</b>					
Manganese-54	Ci			7.24E-05	1.23E-05
Iron-55	Ci			9.03E-04	
Cobalt-57	Ci				1.15E-05
Cobalt-58	Ci			4.41E-03	9.10E-03
Cobalt-60	Ci			2.18E-03	1.08E-03
Niobium-95	Ci			3.56E-05	8.88E-06
Niobium-97	Ci				9.18E-06
Antimony-122	Ci				6.37E-05
Antimony-124	Ci			2.65E-04	
Antimony-125	Ci			3.57E-03	1.30E-04
Iodine-131	Ci			3.28E-03	3.52E-04
Iodine-133	Ci			5.61E-04	
Cesium-134	Ci			1.62E-02	2.25E-03
Cesium-137	Ci			3.85E-02	4.40E-03
<b>Totals</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>7.00E-02</b>	<b>1.74E-02</b>
<b>2. Tritium</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>5.77E+01</b>	<b>9.69E+01</b>
<b>3. Dissolved and Entrained Noble Gases</b>					
Xenon-133m	Ci			1.78E-04	
Xenon-133	Ci			1.67E-02	2.22E-03
Xenon-135	Ci			1.23E-04	
<b>Totals</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>1.70E-02</b>	<b>2.22E-03</b>

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 2B-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
UNIT 2  
LIQUID EFFLUENTS

Nuclides	Units	<u>Continuous Mode</u>		<u>Batch Mode</u>	
		<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>	<u>3<sup>rd</sup> Quarter</u>	<u>4<sup>th</sup> Quarter</u>
<b>Released</b>					
<b>1. Fission and Activation Products</b>					
Chromium-51	Ci			5.04E-04	
Manganese-54	Ci			2.52E-04	7.74E-05
Iron-55	Ci			1.59E-03	
Cobalt-57	Ci			4.15E-05	2.26E-05
Cobalt-58	Ci			1.23E-02	1.55E-02
Cobalt-60	Ci			3.94E-03	9.06E-04
Niobium-95	Ci			9.26E-05	
Silver-110m	Ci				2.36E-05
Antimony-124	Ci			7.00E-04	6.53E-05
Antimony-125	Ci			9.47E-03	6.66E-04
Iodine-131	Ci			2.03E-04	1.38E-03
Cesium-134	Ci			2.36E-02	4.97E-03
Cesium-137	Ci			5.45E-02	9.80E-03
Cesium-136	Ci				1.60E-05
<b>Totals</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>1.07E-01</b>	<b>3.34E-02</b>
<b>2. Tritium</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>5.44E+01</b>	<b>1.24E+02</b>
<b>3. Dissolved and Entrained Noble Gases</b>					
Xenon-131m	Ci				2.57E-04
Xenon-133m	Ci				
Xenon-133	Ci			1.68E-02	1.26E-02
Xenon-135	Ci			1.28E-05	
<b>Totals</b>	<b>Ci</b>			<b>1.68E-02</b>	<b>1.29E-02</b>

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 3

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

SOLID RADWASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL  
(Not Irradiated Fuel)

1.	A	Type of Waste (Class A or less)	Units <sup>1</sup>	6-Month Period	Est. Total Error
a.		Spent Resins, Filters, Sludges, Evaporator Bottoms	m <sup>3</sup> Ci	1.65E+01 2.48E+00	25%
b.		Dry Compressible Waste, Contaminated Equipment	m <sup>3</sup> Ci	6.53E+02 1.68E+00	25%
c.		Irradiated Components, Control Rods	m <sup>3</sup> Ci	0.00E+00 0.00E+00	25%
d.		Others	m <sup>3</sup> Ci	0.00E+00 0.00E+00	25%

1. Volumes are measured, activities are estimated.

**2A. Estimate of Major Nuclide Composition (>1%)**

Nuclides	Resins		DAW	
	%	Ci	%	Ci
Hydrogen-3	<1%		15.71	2.64E-01
Manganese-54	1.04	2.59E-02	<1%	
Iron-55	2.84	7.05E-02	15.07	2.53E-01
Cobalt-58	60.32	1.50E+00	40.96	6.88E-01
Cobalt-60	3.47	8.60E-02	5.10	8.57E-02
Nickel-63	16.08	3.99E-01	12.6	2.12E-01
Cesium-134	5.12	1.27E-01	2.76	4.64E-02
Cesium-137	9.95	2.47E-01	6.69	1.12E-01

**3A. Solid Waste Disposal (Class A or less)**

Number of Shipments	Mode of Transportation	Destination	Type of Containers
3	Truck	Oak Ridge, TN	HIC
5	Truck	Oak Ridge, TN	Strong/Tight

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

SALEM GENERATING STATION  
TABLE 3 (Continued)

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

SOLID RADWASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL

1. B	Type of Waste (Class B)	Units <sup>1</sup>	6-Month Period	Est. Total Error
a.	Spent Resins, Filters, Sludges, Evaporator Bottoms	m <sup>3</sup> Ci	6.81E+00 2.06E+02	25%
b.	Dry Compressible Waste, Contaminated Equipment	m <sup>3</sup> Ci	0.00E+00 0.00E+00	25%
c.	Irradiated Components, Control Rods	m <sup>3</sup> Ci	0.00E+00 0.00E+00	25%
d.	Others	m <sup>3</sup> Ci	0.00E+00 0.00E+00	25%

1. Volumes are measured, activities are estimated.

**2B. Estimate of Major Nuclide Composition (>1%)**

<u>Nuclides</u>	<u>Resins</u>	
	%	Ci
Iron-55	8.30	1.71E+01
Cobalt-60	18.89	3.90E+01
Nickel-63	67.62	1.40E+02
Cesium-137	3.83	7.90E+00

**3B. Solid Waste Disposal (Class B)**

<u>Number of Shipments</u>	<u>Mode of Transportation</u>	<u>Destination</u>	<u>Type of Containers</u>
2	Truck	Barnwell, SC	Poly HIC

There were no Class C shipments made during the report period.

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION

TABLE 3 (Continued)

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

SOLID RADWASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL

**4. Irradiated Fuel Shipments (Disposition)**

<b><u>Number of Shipments</u></b>	<b><u>Mode of Transportation</u></b>	<b><u>Destination</u></b>
None	N/A	N/A

**5. Solidification Methods**

No shipments of Solid Radioactive Waste requiring solidification were made during this period.

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4A-1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT1

**BATCH RELEASES ONLY**

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1. Dates:	July 1, 1999 – September 30, 1999
2. Type of release:	Gaseous
3. Number of releases during quarter:	14
4. Total time duration for all releases of type listed above:	1.06E+04 Min.
5. Maximum duration for release of type listed above:	1.53E+03 Min.
6. Average duration for release of type listed above:	7.59E+02 Min.
7. Minimum duration for release of type listed above:	1.62E+02 Min.
8. Average stream flow (dilution flow) during period of release:	N/A

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4A-1  
(CONT'D)

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 1

**BATCH RELEASES ONLY**

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1. Dates:	October 1, 1999 – December 31, 1999
2. Type of release:	Gaseous
3. Number of releases during quarter:	22
4. Total time duration for all releases of type listed above:	1.70E+04 Min.
5. Maximum duration for release of type listed above:	2.14E+03 Min.
6. Average duration for release of type listed above:	7.73E+02 Min.
7. Minimum duration for release of type listed above:	1.83E+02 Min.
8. Average stream flow (dilution flow) during period of release:	N/A

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4A-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 2

**BATCH RELEASES ONLY**

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- |  |                                   |
|--|-----------------------------------|
| 1. Dates:  | July 1, 1999 – September 30, 1999 |
| 2. Type of release:  | Gaseous                           |
| 3. Number of releases during quarter:                            | 5                                 |
| 4. Total time duration for all releases of type listed above:    | 6.95E+02 Min.                     |
| 5. Maximum duration for release of type listed above:            | 1.55E+02 Min.                     |
| 6. Average duration for release of type listed above:            | 1.39E+02 Min.                     |
| 7. Minimum duration for release of type listed above:            | 1.28E+02 Min.                     |
| 8. Average stream flow (dilution flow) during period of release: | N/A                               |

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4A-2  
(CONT'D)

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 2

**BATCH RELEASES ONLY**

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- |  |                                     |
|--|-------------------------------------|
| 1. Dates:  | October 1, 1999 – December 31, 1999 |
| 2. Type of release:  | Gaseous                             |
| 3. Number of releases during quarter:                            | 6                                   |
| 4. Total time duration for all releases of type listed above:    | 8.88E+02 Min.                       |
| 5. Maximum duration for release of type listed above:            | 2.02E+02 Min.                       |
| 6. Average duration for release of type listed above:            | 1.48E+02 Min.                       |
| 7. Minimum duration for release of type listed above:            | 1.33E+02 Min.                       |
| 8. Average stream flow (dilution flow) during period of release: | N/A                                 |

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4B - 1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 1

**BATCH RELEASES ONLY**

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- |  |                                   |
|--|-----------------------------------|
| 1. Dates:  | July 1, 1999 – September 30, 1999 |
| 2. Type of release:  | Liquid                            |
| 3. Number of releases during quarter:                            | 10                                |
| 4. Total time duration for all releases of type listed above:    | 3144 Min.                         |
| 5. Maximum duration for release of type listed above:            | 538 Min.                          |
| 6. Average duration for release of type listed above:            | 314 Min.                          |
| 7. Minimum duration for release of type listed above:            | 193 Min.                          |
| 8. Average stream flow (dilution flow) during period of release: | 6.56E+04 GPM                      |

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4B-1  
(CONT'D)

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SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 1

**BATCH RELEASES ONLY**

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1. Dates:	October 1, 1999 – December 31, 1999
2. Type of release:	Liquid
3. Number of releases during quarter:	14
4. Total time duration for all releases of type listed above:	3896 Min.
5. Maximum duration for release of type listed above:	547 Min.
6. Average duration for release of type listed above:	278 Min.
7. Minimum duration for release of type listed above:	166 Min.
8. Average stream flow (dilution flow) during period of release:	9.62E+04 GPM

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SALEM GENERATING STATION  
TABLE 4B-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 2

**BATCH RELEASES ONLY**

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1. Dates:	July 1, 1999 – September 30, 1999
2. Type of release:	Liquid
3. Number of releases during quarter:	13
4. Total time duration for all releases of type listed above:	2816 Min.
5. Maximum duration for release of type listed above:	299 Min.
6. Average duration for release of type listed above:	217 Min.
7. Minimum duration for release of type listed above:	131 Min.
8. Average stream flow (dilution flow) during period of release:	1.02E+05 GPM

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JULY - DECEMBER 1999

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SALEM GENERATING STATION  
TABLE 4B-2  
(CONT'D)

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JULY - DECEMBER 1999  
SUMMARY SHEET FOR RADIOACTIVE EFFLUENTS RELEASED  
IN A BATCH MODE  
UNIT 2

**BATCH RELEASES ONLY**

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- |  |                                     |
|--|-------------------------------------|
| 1. Dates:  | October 1, 1999 – December 31, 1999 |
| 2. Type of release:  | Liquid                              |
| 3. Number of releases during quarter:                            | 18                                  |
| 4. Total time duration for all releases of type listed above:    | 4428 Min.                           |
| 5. Maximum duration for release of type listed above:            | 360 Min.                            |
| 6. Average duration for release of type listed above:            | 246 Min.                            |
| 7. Minimum duration for release of type listed above:            | 133 Min.                            |
| 8. Average stream flow (dilution flow) during period of release: | 1.06E+05 GPM                        |

# APPENDIX A

## **MPC DATA**

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The following radionuclide concentrations were obtained from 10 CFR 20 Appendix B, Table II, Column 2 as revised January 1, 1991.

**Maximum Permissible Concentrations**

Element	Isotope	Soluble Conc ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Actinium (89)	Ac-227	2E-6	3E-4
	Ac-228	9E-5	9E-5
Americium (95)	Am-241	4E-6	3E-5
	Am-242m	4E-6	9E-5
	Am-242	1E-4	1E-4
	Am-243	4E-6	3E-5
	Am-244	5E-3	5E-3
Antimony (51)	Sb-122	3E-5	3E-5
	Sb-124	2E-5	2E-5
	Sb-125	1E-4	1E-4
Arsenic (33)	As-73	5E-4	5E-4
	As-74	5E-5	5E-5
	As-76	2E-5	2E-5
	As-77	8E-5	8E-5
Astatine (85)	At-211	2E-6	7E-5
Barium (56)	Ba-131	2E-4	2E-4
	Ba-140	3E-5	2E-5
Berkelium (97)	Bk-249	6E-4	6E-4
	Bk-250	2E-4	2E-4
Beryllium (4)	Be-7	2E-3	2E-3
Bismuth (83)	Bi-206	4E-5	4E-5
	Bi-207	6E-5	6E-5
	Bi-210	4E-5	4E-5
	Bi-212	4E-4	4E-4
Bromine (35)	Br-82	3E-4	4E-5
Cadmium (48)	Cd-109	2E-4	2E-4
	Cd-115m	3E-5	3E-5
	Cd-115	3E-5	4E-5
Calcium (20)	Ca-45	9E-6	2E-4
	Ca-47	5E-5	3E-5
Californium (98)	Cf-249	4E-6	2E-5
	Cf-250	1E-5	3E-5
	Cf-251	4E-6	3E-5
	Cf-252	7E-6	7E-6

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Californium (98)	Cf-253	1E-4	1E-4
	Cf-254	1E-7	1E-7
Carbon (6)	C-14	8E-4	-----
Cerium (58)	Ce-141	9E-5	9E-5
	Ce-143	4E-5	4E-5
	Ce-144	1E-5	1E-5
Cesium (55)	Cs-131	2E-3	9E-4
	Cs-134m	6E-3	1E-3
	Cs-134	9E-6	4E-5
	Cs-135	1E-4	2E-4
	Cs-136	9E-5	6E-5
	Cs-137	2E-5	4E-5
Chlorine (17)	Cl-36	8E-5	6E-5
	Cl-38	4E-4	4E-4
Chromium (24)	Cr-51	2E-3	2E-3
Cobalt (27)	Co-57	5E-4	4E-4
	Co-58m	3E-3	2E-3
	Co-58	1E-4	9E-5
	Co-60	5E-5	3E-5
Copper (29)	Cu-64	3E-4	2E-4
Curium (96)	Cm-242	2E-5	2E-5
	Cm-243	5E-6	2E-5
	Cm-244	7E-6	3E-5
	Cm-245	4E-6	3E-5
	Cm-246	4E-6	3E-5
	Cm-247	4E-6	2E-5
	Cm-248	4E-7	1E-6
	Cm-249	2E-3	2E-3
Dysprosium (66)	Dy-165	4E-4	4E-4
	Dy-166	4E-5	4E-5
Einsteinium (99)	Es-253	2E-5	2E-5
	Es-254m	2E-5	2E-5
	Es-254	1E-5	1E-5
	Es-255	3E-5	3E-5
Erbium (68)	Er-169	9E-5	9E-5
	Er-171	1E-4	1E-4
Europium (63)	Eu-152 (9.2 hrs)	6E-5	6E-5
	Eu-152 (13 yrs)	8E-5	8E-5

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Europium (63)	Eu-154	2E-5	2E-5
	Eu-155	2E-4	2E-4
Fermium (100)	Fm-254	1E-4	1E-4
	Fm-255	3E-5	3E-5
	Fm-256	9E-7	9E-7
Fluorine (9)	F-18	8E-4	5E-4
Gadolinium (64)	Gd-153	2E-4	2E-4
	Gd-159	8E-5	8E-5
Gallium (31)	Ga-72	4E-5	4E-5
Germanium (32)	Ge-71	2E-3	2E-3
Gold (79)	Au-196	2E-4	1E-4
	Au-198	5E-5	5E-5
	Au-199	2E-4	2E-4
Hafnium (72)	Hf-181	7E-5	7E-5
Holmium (67)	Ho-166	3E-5	3E-5
Hydrogen (3)	H-3	3E-3	3E-3
Indium (49)	In-113m	1E-3	1E-3
	In-114m	2E-5	2E-5
	In-115m	4E-4	4E-4
	In-115	9E-5	9E-5
Iodine (53)	I-125	2E-7	2E-4
	I-126	3E-7	9E-5
	I-129	6E-8	2E-4
	I-131	3E-7	6E-5
	I-132	8E-6	2E-4
	I-133	1E-6	4E-5
	I-134	2E-5	6E-4
	I-135	4E-6	7E-5
Iridium (77)	Ir-190	2E-4	2E-4
	Ir-192	4E-5	4E-5
	Ir-194	3E-5	3E-5
Iron (26)	Fe-55	8E-4	2E-3
	Fe-59	6E-5	5E-5
Lanthanum (57)	La-140	2E-5	2E-5
Lead (82)	Pb-203	4E-4	4E-4
	Pb-210	1E-7	2E-4
	Pb-212	2E-5	2E-5
Lutetium (71)	Lu-177	1E-4	1E-4

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Manganese (25)	Mn-52	3E-5	3E-5
	Mn-54	1E-4	1E-4
	Mn-56	1E-4	1E-4
Mercury (80)	Hg-197m	2E-4	2E-4
	Hg-197	3E-4	5E-4
	Hg-203	2E-5	1E-4
Molybdenum (42)	Mo-99	2E-4	4E-5
Neodymium (60)	Nd-144	7E-5	8E-5
	Nd-147	6E-5	6E-5
	Nd-149	3E-4	3E-4
Neptunium (93)	Np-237	3E-6	3E-5
	Np-239	1E-4	1E-4
Nickel (28)	Ni-59	2E-4	2E-3
	Ni-63	3E-5	7E-4
	Ni-65	1E-4	1E-4
Niobium (41)	Nb-93m	4E-4	4E-4
	Nb-95	1E-4	1E-4
	Nb-97	9E-4	9E-4
Osmium (76)	Os-185	7E-5	7E-5
	Os-191m	3E-3	2E-3
	Os-191	2E-4	2E-4
	Os-193	6E-5	5E-5
Palladium (46)	Pd-103	3E-4	3E-4
	Pd-109	9E-5	7E-5
Phosphorus (15)	P-32	2E-5	2E-5
Platinum (78)	Pt-191	1E-4	1E-4
	Pt-193m	1E-3	1E-3
	Pt-193	9E-4	2E-3
	Pt-197m	1E-3	9E-4
	Pt-197	1E-4	1E-4
Plutonium (94)	Pu-238	5E-6	3E-5
	Pu-239	5E-6	3E-5
	Pu-240	5E-6	3E-5
	Pu-241	2E-4	1E-3
	Pu-242	5E-6	3E-5
	Pu-243	3E-4	3E-4
Polonium (84)	Po-210	7E-7	3E-5
Potassium (19)	K-42	3E-4	2E-5

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Praseodymium(59)	Pr-142	3E-5	3E-5
	Pr-143	5E-5	5E-5
Promethium (61)	Pm-147	2E-4	2E-4
	Pm-149	4E-5	4E-5
Protactinium(91)	Pa-230	2E-4	2E-4
	Pa-231	9E-7	2E-5
	Pa-233	1E-4	1E-4
Radium (88)	Ra-223	7E-7	4E-6
	Ra-224	2E-6	5E-6
	Ra-226	3E-8	3E-5
	Ra-228	3E-8	3E-5
Rhenium (75)	Re-183	6E-4	3E-4
	Re-186	9E-5	5E-5
	Re-187	3E-3	2E-3
	Re-188	6E-5	3E-5
Rhodium (45)	Rh-103m	1E-2	1E-2
	Rh-105	1E-4	1E-4
Rubidium (37)	Rb-86	7E-5	2E-5
	Rb-87	1E-4	2E-4
Ruthenium (44)	Ru-97	4E-4	3E-4
	Ru-103	8E-5	8E-5
	Ru-105	1E-4	1E-4
	Ru-106	1E-5	1E-5
Samarium (62)	Sm-147	6E-5	7E-5
	Sm-151	4E-4	4E-4
	Sm-153	8E-5	8E-5
Scandium (21)	Sc-46	4E-5	4E-5
	Sc-47	9E-5	9E-5
	Sc-48	3E-5	3E-5
Selenium (34)	Se-75	3E-4	3E-4
Silicon (14)	Si-31	9E-4	2E-4
Silver (47)	Ag-105	1E-4	1E-4
	Ag-110m	3E-5	3E-5
	Ag-111	4E-5	4E-5
Sodium (11)	Na-22	4E-5	3E-5
	Na-24	2E-4	3E-5
Strontium (38)	Sr-85m	7E-3	7E-3
	Sr-85	1E-4	2E-4

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Strontium (38)	Sr-89	3E-6	3E-5
	Sr-90	3E-7	4E-5
	Sr-91	7E-5	5E-5
	Sr-92	7E-5	6E-5
Sulfur (16)	S-35	6E-5	3E-4
Tantalum (73)	Ta-182	4E-5	4E-5
Technetium (43)	Tc-96m	1E-2	1E-2
	Tc-96	1E-4	5E-5
	Tc-97m	4E-4	2E-4
	Tc-97	2E-3	8E-4
	Tc-99m	6E-3	3E-3
	Tc-99	3E-4	2E-4
Tellurium (52)	Te-125m	2E-4	1E-4
	Te-127m	6E-5	5E-5
	Te-127	3E-4	2E-4
	Te-129m	3E-5	2E-5
	Te-129	8E-4	8E-4
	Te-131m	6E-5	4E-5
	Te-132	3E-5	2E-5
	Terbium (65)	Tb-160	4E-5
Thallium (81)	Tl-200	4E-4	2E-4
	Tl-201	3E-4	2E-4
	Tl-202	1E-4	7E-5
	Tl-204	1E-4	6E-5
Thorium (90)	Th-227	2E-5	2E-5
	Th-228	7E-6	1E-5
	Th-230	2E-6	3E-5
	Th-231	2E-4	2E-4
	Th-232	2E-6	4E-5
	Th-natural	2E-6	2E-5
	Th-234	2E-5	2E-5
Thulium (69)	Tm-170	5E-5	5E-5
	Tm-171	5E-4	5E-4
Tin (50)	Sn-113	9E-5	8E-5
	Sn-124	2E-5	2E-5
Tungsten (74)	W-181	4E-4	3E-4
	W-185	1E-4	1E-4

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Tungsten (74)	W-187	7E-5	6E-5
Uranium (92)	U-230	5E-6	5E-6
	U-232	3E-5	3E-5
	U-233	3E-5	3E-5
	U-234	3E-5	3E-5
	U-235	3E-5	3E-5
	U-236	3E-5	3E-5
	U-238	4E-5	4E-5
	U-240	3E-5	3E-5
	U-natural	3E-5	3E-5
	Vanadium (23)	V-48	3E-5
Ytterbium (70)	Yb-175	1E-4	1E-4
Yttrium	Y-90	2E-5	2E-5
	Y-91m	3E-3	3E-3
	Y-91	3E-5	3E-5
	Y-92	6E-5	6E-5
	Y-93	3E-5	3E-5
Zinc (30)	Zn-65	1E-4	2E-4
	Zn-69m	7E-5	6E-5
	Zn-69	2E-3	2E-3
Zirconium (40)	Zr-93	8E-4	8E-4
	Zr-95	6E-5	6E-5
	Zr-97	2E-5	2E-5
Any single radio-nuclide not listed above with decay mode other than alpha emission or spontaneous fission and with radio - active half-life greater than 2 hours		3E-6	3E-6
Any single radio-nuclide not listed above, which decays by alpha emission or spontaneous fission.		3E-8	3E-8

Notes:

1. If the identity of any radionuclide is not known, the limiting values for purposes of this table shall be:  $3E-8 \mu\text{Ci/ml}$ .
2. If the identity and concentration of each radionuclide are known, the limiting values should be derived as follows: Determine, for each radionuclide in the mixture, the ratio between the quantity present in the mixture and the limit otherwise established in Appendix B for the specific radionuclide not in a mixture. The sum of such ratios for all the radionuclides in the mixture may not exceed "1" (i.e. "unity").

# APPENDIX B

## **REVISED SALEM RERR 46**

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SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
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**PART E. RADIOLOGICAL IMPACT ON MAN**

The calculated individual doses in this section are based on the controlling dose pathways and age groups as described below. The estimated dose represents the maximum radiation dose that could be received by a member of the general public. The population dose impact is based on historical site-specific data (i.e., food production, milk production, feed for milk animals and seafood production).

The doses were calculated using methods described in Regulatory Guide 1.109 and represent calculations for the six-month reporting interval. Individual doses from batch and continuous releases were calculated using the annual average historic meteorological dispersion coefficients as described in the Offsite Dose Calculation Manual. Population doses were calculated using the meteorological dispersion coefficients for the six month reporting interval.

**Liquid Pathways**

<u>Type</u>	<u>Age Group</u>	<u>Location</u>	<u>Pathway</u>
Total Body	Adult	Site Boundary	Seafood Ingestion
Organ	Adult	Site Boundary	Seafood Ingestion

<u>Type</u>	<u>Dose</u>	<u>Limit</u>
Total Body	4.69E-02 mrem	3 mrem
Organ Dose (GI-LLI)	7.44E-02 mrem	10 mrem
Population (Total)	4.38E-02 Person-rem	N/A
Population (Average)	7.11E-09 mrem	N/A

**Air Pathways**

<u>Type</u>	<u>Age Group</u>	<u>Location</u>	<u>Pathway</u>
Total Body	All	Site Boundary	Direct Exposure
Skin	All	Site Boundary	Direct Exposure
Organ	Infant	4.9 mi. W.	Milk, Ground Plane, Inhalation

<u>Type</u>	<u>Dose</u>	<u>Limit</u>
Total Body	6.75E-02 mrem	500 mrem/yr
Skin	1.60E-01 mrem	3000 mrem/yr
Organ Dose (Thyroid)	1.91E-02 mrem	15 mrem
Population (Total)	1.73E+00 Person-rem	N/A
Population (Average)	3.84E-07 mrem	N/A

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SALEM GENERATING STATION

TABLE 2A-1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JANUARY – JUNE 1999

UNIT 1

LIQUID EFFLUENTS – SUMMATION OF ALL RELEASES

		Units	1 <sup>st</sup> Quarter	2 <sup>nd</sup> Quarter	Est. Total Error
<b>A.</b>	<b>Fission and Activation Products</b>				
1.	Total Release	Ci	4.26E-02	3.17E-02	25%
2.	Average Release Rate For Period	μCi/ml	2.15E-08	1.87E-08	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.2(a))	%	6.78E-01	5.43E-01	
<b>B.</b>	<b>Tritium</b>				
1.	Total Release	Ci	1.08E+02	7.16E+01	25%
2.	Average Release Rate For Period	μCi/ml	5.44E-05	4.69E-05	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	1.81E+00	1.56E+00	
<b>C.</b>	<b>Dissolved and Entrained Noble Gases</b>				
1.	Total Release	Ci	2.45E-02	1.48E-02	25%
2.	Average Release Rate For Period	μCi/ml	1.23E-08	9.70E-09	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	6.15E-03	4.85E-03	
<b>D.</b>	<b>Gross Alpha</b>	Ci	0.00E+00	0.00E+00	25%
<b>E.</b>	Volume of Waste Release (Prior to Dilution)	Liters	6.14E+05	4.94E+05	25%
<b>F.</b>	Volume of Dilution Water Used During Entire Period	Liters	1.98E+09	1.53E+09	25%

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SALEM GENERATING STATION  
TABLE 2A-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JANUARY – JUNE 1999

UNIT 2

LIQUID EFFLUENTS – SUMMATION OF ALL RELEASES

		Units	1 <sup>st</sup> Quarter	2 <sup>nd</sup> Quarter	Est. Total Error
<b>A.</b>	<b>Fission and Activation Products</b>				
1.	Total Release	Ci	6.14E-02	6.21E-02	25%
2.	Average Release Rate For Period	μCi/ml	1.78E-08	2.30E-08	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.2(a))	%	9.22E-01	1.05E+00	
<b>B.</b>	<b>Tritium</b>				
1.	Total Release	Ci	2.34E+02	1.62E+02	25%
2.	Average Release Rate For Period	μCi/ml	6.52E-05	6.26E-05	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	2.17E+00	2.09E+00	
<b>C.</b>	<b>Dissolved and Entrained Noble Gases</b>				
1.	Total Release	Ci	2.54E-02	4.77E-02	25%
2.	Average Release Rate For Period	μCi/ml	7.08E-09	1.84E-08	
3.	Percent of Technical Specification Limit (T.S. 3.11.1.1)	%	3.54E-03	9.22E-03	
<b>D.</b>	<b>Gross Alpha</b>	Ci	0.00E+00	0.00E+00	25%
<b>E.</b>	Volume of Waste Release (Prior to Dilution)	Liters	1.15E+06	1.85E+06	25%
<b>F.</b>	Volume of Dilution Water Used During Entire Period	Liters	3.59E+09	2.59E+09	25%

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JANUARY – JUNE 1999

SALEM GENERATING STATION  
TABLE 2B-1

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JANUARY – JUNE 1999  
UNIT 1  
LIQUID EFFLUENTS

Nuclides  <u>Released</u>	Units	<u>Continuous Mode</u>		<u>Batch Mode</u>	
		<u>1<sup>st</sup> Quarter</u>	<u>2<sup>nd</sup> Quarter</u>	<u>1<sup>st</sup> Quarter</u>	<u>2<sup>nd</sup> Quarter</u>
<b>1. Fission and Activation Products</b>					
Sodium-24	Ci	0.00E+00	0.00E+00	7.25E-05	0.00E+00
Manganese-54	Ci	0.00E+00	0.00E+00	1.70E-04	1.15E-04
Iron-55	Ci	0.00E+00	0.00E+00	4.12E-03	3.16E-03
Cobalt-57	Ci	0.00E+00	0.00E+00	0.00E+00	2.12E-05
Cobalt-58	Ci	0.00E+00	0.00E+00	7.83E-03	1.59E-02
Cobalt-60	Ci	0.00E+00	0.00E+00	1.11E-03	1.99E-03
Strontium-90	Ci	0.00E+00	0.00E+00	7.97E-06	0.00E+00
Niobium-95	Ci	0.00E+00	0.00E+00	0.00E+00	1.85E-05
Zirconium-95	Ci	0.00E+00	0.00E+00	0.00E+00	1.64E-05
Technicium-99m	Ci	0.00E+00	0.00E+00	0.00E+00	2.29E-05
Antimony-124	Ci	0.00E+00	0.00E+00	3.37E-03	6.70E-04
Antimony-125	Ci	0.00E+00	0.00E+00	4.37E-03	2.00E-03
Iodine-131	Ci	0.00E+00	0.00E+00	1.02E-03	2.04E-03
Iodine-133	Ci	0.00E+00	0.00E+00	6.30E-05	1.82E-04
Cesium-134	Ci	0.00E+00	0.00E+00	6.10E-03	1.73E-03
Cesium-137	Ci	0.00E+00	0.00E+00	1.44E-02	3.75E-03
Cerium-141	Ci	0.00E+00	0.00E+00	5.53E-06	0.00E+00
<b>Totals</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>4.26E-02</b>	<b>3.17E-02</b>
<b>2. Tritium</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>1.08E+02</b>	<b>7.16E+00</b>
<b>3. Dissolved and Entrained Noble Gases</b>					
Xenon-131m	Ci	0.00E+00	0.00E+00	0.00E+00	6.40E-04
Xenon-133	Ci	0.00E+00	0.00E+00	2.44E-02	1.42E-02
Xenon-135	Ci	0.00E+00	0.00E+00	5.24E-05	0.00E+00
<b>Totals</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>2.45E-02</b>	<b>1.48E-02</b>

SGS RADIOACTIVE EFFLUENTS RELEASE REPORT  
JANUARY – JUNE 1999

SALEM GENERATING STATION  
TABLE 2B-2

EFFLUENTS AND WASTE DISPOSAL ANNUAL REPORT  
JANUARY – JUNE 1999  
UNIT 2  
LIQUID EFFLUENTS

Nuclides	Units	Continuous Mode		Batch Mode	
		1 <sup>st</sup> Quarter	2 <sup>nd</sup> Quarter	1 <sup>st</sup> Quarter	2 <sup>nd</sup> Quarter
<u>Released</u>					
<b>1. Fission and Activation Products</b>					
Chromium-51	Ci	0.00E+00	0.00E+00	3.84E-05	0.00E+00
Manganese-54	Ci	0.00E+00	0.00E+00	2.80E-04	1.96E-04
Iron-55	Ci	0.00E+00	0.00E+00	2.48E-03	2.75E-03
Cobalt-57	Ci	0.00E+00	0.00E+00	0.00E+00	7.64E-04
Cobalt-58	Ci	0.00E+00	0.00E+00	9.88E-03	2.57E-02
Cobalt-60	Ci	0.00E+00	0.00E+00	3.87E-03	3.34E-03
Niobium-95	Ci	0.00E+00	0.00E+00	0.00E+00	3.50E-05
Zirconium-95	Ci	0.00E+00	0.00E+00	0.00E+00	1.92E-05
Molybdenum-99	Ci	0.00E+00	0.00E+00	3.11E-05	0.00E+00
Antimony-122	Ci	0.00E+00	0.00E+00	1.06E-05	7.57E-06
Antimony-124	Ci	0.00E+00	0.00E+00	5.96E-03	2.70E-04
Antimony-125	Ci	0.00E+00	0.00E+00	6.47E-03	2.00E-03
Iodine-131	Ci	4.93E-04	0.00E+00	4.70E-03	2.14E-03
Iodine-133	Ci	7.50E-06	0.00E+00	7.05E-05	3.12E-05
Cesium-134	Ci	0.00E+00	0.00E+00	7.96E-03	7.06E-03
Cesium-137	Ci	0.00E+00	0.00E+00	1.92E-02	1.85E-02
Cerium-144	Ci	0.00E+00	0.00E+00	0.00E+00	2.5E-05
<b>Totals</b>	<b>Ci</b>	<b>5.01E-04</b>	<b>0.00E+00</b>	<b>6.10E-02</b>	<b>6.21E-02</b>
<b>2. Tritium</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>2.34E+02</b>	<b>1.62E+02</b>
<b>3. Dissolved and Entrained Noble Gases</b>					
Xenon-131m	Ci	0.00E+00	0.00E+00	0.00E+00	5.14E-04
Xenon-133m	Ci	0.00E+00	0.00E+00	7.84E-05	0.00E+00
Xenon-133	Ci	0.00E+00	0.00E+00	2.50E-02	4.72E-02
Xenon-135	Ci	0.00E+00	0.00E+00	2.39E-04	7.09E-06
<b>Totals</b>	<b>Ci</b>	<b>0.00E+00</b>	<b>0.00E+00</b>	<b>2.53E-02</b>	<b>4.77E-02</b>

# APPENDIX C

## **MET DATA**

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ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT			
N	0	0.0	0	0.0	0	0.0	1	0.0	4	0.2	0	0.0	0	0.0	5	0.2
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
W	0	0.0	0	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	4	0.2
WNW	0	0.0	1	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	4	0.2
NW	0	0.0	0	0.0	0	0.0	1	0.0	24	1.1	5	0.2	0	0.0	30	1.4
NNW	0	0.0	0	0.0	0	0.0	0	0.0	12	0.6	4	0.2	0	0.0	16	0.7
	0	0.0	1	0.0	0	0.0	4	0.2	48	2.2	9	0.4	0	0.0	62	2.9

MEAN WIND SPEED: 15.6  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 30 FT  
DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
CLASS B

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	4	0.2	5	0.2	0	0.0	0	0.0	9	0.4
NNE	0	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	0	0.0	4	0.2
NE	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	2	0.1
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
WSW	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
W	0	0.0	0	0.0	1	0.0	0	0.0	4	0.2	3	0.1	0	0.0	8	0.4
WNW	0	0.0	0	0.0	0	0.0	1	0.0	5	0.2	2	0.1	0	0.0	8	0.4
NW	0	0.0	0	0.0	0	0.0	6	0.3	13	0.6	1	0.0	0	0.0	20	0.9
NNW	0	0.0	0	0.0	0	0.0	5	0.2	9	0.4	4	0.2	0	0.0	18	0.8
	0	0.0	0	0.0	4	0.2	23	1.1	36	1.7	10	0.5	0	0.0	73	3.4

MEAN WIND SPEED: 13.5  
MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	2	0.1	11	0.5	7	0.3	0	0.0	0	0.0	20	0.9
NNE	0	0.0	0	0.0	1	0.0	4	0.2	1	0.0	0	0.0	0	0.0	6	0.3
NE	0	0.0	0	0.0	0	0.0	4	0.2	2	0.1	0	0.0	0	0.0	6	0.3
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
WSW	0	0.0	0	0.0	3	0.1	3	0.1	1	0.0	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	1	0.0	0	0.0	6	0.3
WNW	0	0.0	0	0.0	2	0.1	1	0.0	3	0.1	1	0.0	0	0.0	7	0.3
NW	0	0.0	0	0.0	2	0.1	11	0.5	7	0.3	0	0.0	0	0.0	20	0.9
NNW	0	0.0	0	0.0	1	0.0	7	0.3	9	0.4	3	0.1	0	0.0	20	0.9
	0	0.0	0	0.0	11	0.5	42	2.0	35	1.6	5	0.2	0	0.0	93	4.3

MEAN WIND SPEED: 12.0  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	3	0.1	13	0.6	27	1.3	27	1.3	1	0.0	0	0.0	71	3.3
NNE	0	0.0	2	0.1	21	1.0	29	1.4	10	0.5	2	0.1	0	0.0	64	3.0
NE	0	0.0	1	0.0	22	1.0	22	1.0	4	0.2	0	0.0	0	0.0	49	2.3
ENE	0	0.0	4	0.2	12	0.6	8	0.4	0	0.0	0	0.0	0	0.0	24	1.1
E	0	0.0	2	0.1	4	0.2	1	0.0	0	0.0	0	0.0	0	0.0	7	0.3
ESE	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SE	0	0.0	5	0.2	0	0.0	6	0.3	7	0.3	0	0.0	0	0.0	18	0.8
SSE	0	0.0	0	0.0	2	0.1	6	0.3	3	0.1	0	0.0	0	0.0	11	0.5
S	0	0.0	1	0.0	1	0.0	0	0.0	1	0.0	0	0.0	0	0.0	3	0.1
SSW	0	0.0	2	0.1	1	0.0	1	0.0	0	0.0	1	0.0	0	0.0	5	0.2
SW	0	0.0	1	0.0	6	0.3	7	0.3	0	0.0	2	0.1	1	0.0	17	0.8
WSW	0	0.0	0	0.0	8	0.4	13	0.6	7	0.3	1	0.0	2	0.1	31	1.4
W	0	0.0	0	0.0	8	0.4	15	0.7	17	0.8	10	0.5	0	0.0	50	2.3
WNW	0	0.0	3	0.1	16	0.7	39	1.8	34	1.6	4	0.2	3	0.1	99	4.6
NW	0	0.0	3	0.1	12	0.6	51	2.4	45	2.1	10	0.5	1	0.0	122	5.7
NNW	0	0.0	3	0.1	10	0.5	24	1.1	43	2.0	5	0.2	0	0.0	85	4.0
	0	0.0	31	1.4	138	6.4	249	11.6	198	9.3	36	1.7	7	0.3	659	30.8

MEAN WIND SPEED: 11.0  
 MISSING: 6

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	4	0.2	44	2.1	46	2.1	5	0.2	0	0.0	0	0.0	99	4.6
NNE	0	0.0	4	0.2	36	1.7	12	0.6	1	0.0	0	0.0	0	0.0	53	2.5
NE	0	0.0	6	0.3	30	1.4	2	0.1	1	0.0	1	0.0	0	0.0	40	1.9
ENE	0	0.0	4	0.2	17	0.8	1	0.0	0	0.0	0	0.0	0	0.0	22	1.0
E	0	0.0	5	0.2	13	0.6	0	0.0	0	0.0	0	0.0	0	0.0	18	0.8
ESE	0	0.0	5	0.2	15	0.7	8	0.4	2	0.1	0	0.0	1	0.0	31	1.4
SE	0	0.0	4	0.2	21	1.0	10	0.5	13	0.6	8	0.4	8	0.4	64	3.0
SSE	0	0.0	2	0.1	4	0.2	10	0.5	1	0.0	1	0.0	0	0.0	18	0.8
S	0	0.0	2	0.1	14	0.7	18	0.8	8	0.4	0	0.0	1	0.0	43	2.0
SSW	0	0.0	3	0.1	15	0.7	19	0.9	11	0.5	1	0.0	0	0.0	49	2.3
SW	0	0.0	4	0.2	19	0.9	18	0.8	4	0.2	0	0.0	0	0.0	45	2.1
WSW	0	0.0	3	0.1	16	0.7	15	0.7	0	0.0	0	0.0	0	0.0	34	1.6
W	0	0.0	1	0.0	28	1.3	22	1.0	0	0.0	1	0.0	0	0.0	52	2.4
WNW	0	0.0	2	0.1	28	1.3	40	1.9	4	0.2	1	0.0	0	0.0	75	3.5
NW	0	0.0	3	0.1	29	1.4	58	2.7	26	1.2	0	0.0	0	0.0	116	5.4
NNW	0	0.0	1	0.0	12	0.6	31	1.4	22	1.0	1	0.0	0	0.0	67	3.1
	0	0.0	53	2.5	341	15.9	310	14.5	98	4.6	14	0.7	10	0.5	826	38.6

MEAN WIND SPEED: 8.7  
 MISSING: 6

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 30 FT  
DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
CLASS F

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	13	0.6	0	0.0	0	0.0	0	0.0	0	0.0	15	0.7
NNE	0	0.0	2	0.1	4	0.2	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3
NE	0	0.0	5	0.2	7	0.3	1	0.0	0	0.0	0	0.0	0	0.0	13	0.6
ENE	0	0.0	8	0.4	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	9	0.4
E	0	0.0	2	0.1	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	7	0.3
ESE	0	0.0	2	0.1	13	0.6	5	0.2	1	0.0	0	0.0	0	0.0	21	1.0
SE	0	0.0	2	0.1	18	0.8	20	0.9	11	0.5	1	0.0	1	0.0	53	2.5
SSE	0	0.0	6	0.3	14	0.7	3	0.1	3	0.1	1	0.0	0	0.0	27	1.3
S	0	0.0	2	0.1	13	0.6	9	0.4	1	0.0	1	0.0	0	0.0	26	1.2
SSW	0	0.0	1	0.0	9	0.4	7	0.3	4	0.2	2	0.1	0	0.0	23	1.1
SW	0	0.0	3	0.1	23	1.1	6	0.3	0	0.0	0	0.0	0	0.0	32	1.5
WSW	0	0.0	2	0.1	13	0.6	4	0.2	0	0.0	1	0.0	0	0.0	20	0.9
W	0	0.0	2	0.1	8	0.4	7	0.3	0	0.0	0	0.0	0	0.0	17	0.8
WNW	0	0.0	1	0.0	2	0.1	5	0.2	0	0.0	0	0.0	0	0.0	8	0.4
NW	0	0.0	2	0.1	2	0.1	3	0.1	0	0.0	0	0.0	0	0.0	7	0.3
NNW	0	0.0	1	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	4	0.2
	0	0.0	43	2.0	146	6.8	72	3.4	20	0.9	6	0.3	1	0.0	288	13.5

MEAN WIND SPEED: 7.1  
MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	5	0.2	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3
NNE	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
NE	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
ENE	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
E	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	8	0.4	1	0.0	0	0.0	0	0.0	0	0.0	9	0.4
SE	0	0.0	0	0.0	19	0.9	21	1.0	21	1.0	2	0.1	0	0.0	63	2.9
SSE	0	0.0	1	0.0	7	0.3	9	0.4	0	0.0	0	0.0	0	0.0	17	0.8
S	0	0.0	2	0.1	1	0.0	1	0.0	1	0.0	2	0.1	0	0.0	7	0.3
SSW	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
SW	0	0.0	0	0.0	7	0.3	0	0.0	0	0.0	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	7	0.3	0	0.0	0	0.0	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNW	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
	0	0.0	9	0.4	72	3.4	32	1.5	22	1.0	4	0.2	0	0.0	139	6.5

MEAN WIND SPEED: 8.4  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 30 FT  
DELTA T: (300-33FT)

ALL STABILITY CLASSES

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	10	0.5	77	3.6	89	4.2	48	2.2	1	0.0	0	0.0	225	10.5
NNE	0	0.0	8	0.4	67	3.1	50	2.3	12	0.6	2	0.1	0	0.0	139	6.5
NE	0	0.0	12	0.6	64	3.0	31	1.4	8	0.4	1	0.0	0	0.0	116	5.4
ENE	0	0.0	16	0.7	32	1.5	9	0.4	0	0.0	0	0.0	0	0.0	57	2.7
E	0	0.0	9	0.4	22	1.0	3	0.1	0	0.0	0	0.0	0	0.0	34	1.6
ESE	0	0.0	8	0.4	38	1.8	14	0.7	3	0.1	0	0.0	1	0.0	64	3.0
SE	0	0.0	11	0.5	58	2.7	57	2.7	52	2.4	11	0.5	9	0.4	198	9.3
SSE	0	0.0	9	0.4	27	1.3	28	1.3	7	0.3	2	0.1	0	0.0	73	3.4
S	0	0.0	7	0.3	29	1.4	28	1.3	11	0.5	3	0.1	1	0.0	79	3.7
SSW	0	0.0	9	0.4	28	1.3	27	1.3	15	0.7	4	0.2	0	0.0	83	3.9
SW	0	0.0	8	0.4	56	2.6	32	1.5	4	0.2	2	0.1	1	0.0	103	4.8
WSW	0	0.0	5	0.2	48	2.2	37	1.7	8	0.4	2	0.1	2	0.1	102	4.8
W	0	0.0	3	0.1	45	2.1	44	2.1	30	1.4	15	0.7	0	0.0	137	6.4
WNW	0	0.0	7	0.3	48	2.2	86	4.0	49	2.3	8	0.4	3	0.1	201	9.4
NW	0	0.0	8	0.4	46	2.1	130	6.1	115	5.4	16	0.7	1	0.0	316	14.8
NNW	0	0.0	7	0.3	27	1.3	67	3.1	95	4.4	17	0.8	0	0.0	213	10.0
	0	0.0	137	6.4	712	33.3	732	34.2	457	21.4	84	3.9	18	0.8	2140	100.0

MISSING HOURS: 20

MEAN WIND SPEED: 9.7



ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	7	0.3	0	0.0	8	0.4
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
W	0	0.0	1	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	5	0.2
WNW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	3	0.1
NW	0	0.0	0	0.0	0	0.0	0	0.0	7	0.3	15	0.7	1	0.0	23	1.1
NNW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	9	0.4	8	0.4	20	0.9
	0	0.0	1	0.0	0	0.0	2	0.1	18	0.8	32	1.5	9	0.4	62	2.9

MEAN WIND SPEED: 19.7  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	1	0.0	8	0.4	1	0.0	0	0.0	10	0.5
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	4	0.2
ENE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
WSW	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	3	0.1
W	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	2	0.1	3	0.1	8	0.4
WNW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	4	0.2	1	0.0	8	0.4
NW	0	0.0	0	0.0	0	0.0	3	0.1	6	0.3	6	0.3	0	0.0	15	0.7
NNW	0	0.0	0	0.0	0	0.0	1	0.0	11	0.5	5	0.2	5	0.2	22	1.0
	0	0.0	0	0.0	3	0.1	12	0.6	31	1.4	18	0.8	9	0.4	73	3.4

MEAN WIND SPEED: 17.1  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	2	0.1	6	0.3	10	0.5	4	0.2	1	0.0	23	1.1
NNE	0	0.0	0	0.0	0	0.0	4	0.2	1	0.0	0	0.0	0	0.0	5	0.2
NE	0	0.0	0	0.0	0	0.0	3	0.1	5	0.2	0	0.0	0	0.0	8	0.4
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	1	0.0	3	0.1	3	0.1	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0	4	0.2	1	0.0	7	0.3
WNW	0	0.0	0	0.0	2	0.1	0	0.0	1	0.0	2	0.1	1	0.0	6	0.3
NW	0	0.0	0	0.0	2	0.1	2	0.1	11	0.5	4	0.2	0	0.0	19	0.9
NNW	0	0.0	0	0.0	1	0.0	1	0.0	10	0.5	3	0.1	3	0.1	18	0.8
	0	0.0	0	0.0	9	0.4	19	0.9	42	2.0	17	0.8	6	0.3	93	4.3

MEAN WIND SPEED: 15.3  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	1	0.0	5	0.2	11	0.5	20	0.9	20	0.9	4	0.2	61	2.9
NNE	0	0.0	1	0.0	14	0.7	27	1.3	13	0.6	9	0.4	2	0.1	66	3.1
NE	0	0.0	1	0.0	15	0.7	13	0.6	20	0.9	4	0.2	0	0.0	53	2.5
ENE	0	0.0	4	0.2	10	0.5	18	0.8	6	0.3	0	0.0	0	0.0	38	1.8
E	0	0.0	1	0.0	3	0.1	0	0.0	1	0.0	0	0.0	0	0.0	5	0.2
ESE	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SE	0	0.0	1	0.0	3	0.1	0	0.0	5	0.2	8	0.4	0	0.0	17	0.8
SSE	0	0.0	0	0.0	2	0.1	5	0.2	3	0.1	1	0.0	0	0.0	11	0.5
S	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	1	0.0	0	0.0	3	0.1
SSW	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	1	0.0	4	0.2
SW	0	0.0	1	0.0	4	0.2	7	0.3	4	0.2	0	0.0	3	0.1	19	0.9
WSW	0	0.0	0	0.0	5	0.2	7	0.3	6	0.3	4	0.2	5	0.2	27	1.3
W	0	0.0	0	0.0	5	0.2	12	0.6	15	0.7	10	0.5	12	0.6	54	2.5
WNW	0	0.0	0	0.0	11	0.5	22	1.0	32	1.5	22	1.0	4	0.2	91	4.3
NW	0	0.0	1	0.0	8	0.4	24	1.1	50	2.3	29	1.4	12	0.6	124	5.8
NNW	0	0.0	0	0.0	5	0.2	11	0.5	25	1.2	25	1.2	16	0.7	82	3.8
	0	0.0	11	0.5	97	4.5	158	7.4	200	9.4	133	6.2	59	2.8	658	30.8

MEAN WIND SPEED: 14.9  
 MISSING: 7

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	6	0.3	21	1.0	37	1.7	8	0.4	0	0.0	72	3.4
NNE	0	0.0	2	0.1	9	0.4	38	1.8	17	0.8	0	0.0	0	0.0	66	3.1
NE	0	0.0	6	0.3	9	0.4	27	1.3	1	0.0	2	0.1	1	0.0	46	2.2
ENE	0	0.0	0	0.0	8	0.4	17	0.8	0	0.0	0	0.0	0	0.0	25	1.2
E	0	0.0	2	0.1	9	0.4	12	0.6	0	0.0	0	0.0	0	0.0	23	1.1
ESE	0	0.0	1	0.0	3	0.1	6	0.3	7	0.3	1	0.0	1	0.0	19	0.9
SE	0	0.0	1	0.0	4	0.2	20	0.9	9	0.4	3	0.1	27	1.3	64	3.0
SSE	0	0.0	0	0.0	8	0.4	10	0.5	3	0.1	1	0.0	1	0.0	23	1.1
S	0	0.0	3	0.1	4	0.2	14	0.7	11	0.5	3	0.1	1	0.0	36	1.7
SSW	0	0.0	3	0.1	13	0.6	15	0.7	14	0.7	8	0.4	3	0.1	56	2.6
SW	0	0.0	2	0.1	10	0.5	25	1.2	9	0.4	5	0.2	0	0.0	51	2.4
WSW	0	0.0	1	0.0	7	0.3	16	0.7	7	0.3	2	0.1	0	0.0	33	1.5
W	0	0.0	2	0.1	5	0.2	20	0.9	23	1.1	0	0.0	1	0.0	51	2.4
WNW	0	0.0	1	0.0	13	0.6	33	1.5	24	1.1	3	0.1	1	0.0	75	3.5
NW	0	0.0	0	0.0	4	0.2	37	1.7	55	2.6	22	1.0	1	0.0	119	5.6
NNW	0	0.0	0	0.0	1	0.0	6	0.3	34	1.6	21	1.0	5	0.2	67	3.1
	0	0.0	24	1.1	113	5.3	317	14.8	251	11.7	79	3.7	42	2.0	826	38.6

MEAN WIND SPEED: 13.0  
 MISSING: 6

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	0	0.0	3	0.1	4	0.2	0	0.0	0	0.0	9	0.4
NNE	0	0.0	0	0.0	2	0.1	3	0.1	0	0.0	0	0.0	0	0.0	5	0.2
NE	0	0.0	0	0.0	1	0.0	4	0.2	3	0.1	0	0.0	0	0.0	8	0.4
ENE	0	0.0	1	0.0	4	0.2	3	0.1	0	0.0	0	0.0	0	0.0	8	0.4
E	0	0.0	1	0.0	6	0.3	1	0.0	2	0.1	0	0.0	0	0.0	10	0.5
ESE	0	0.0	1	0.0	2	0.1	2	0.1	2	0.1	2	0.1	0	0.0	9	0.4
SE	0	0.0	1	0.0	12	0.6	18	0.8	13	0.6	7	0.3	7	0.3	58	2.7
SSE	0	0.0	0	0.0	8	0.4	9	0.4	6	0.3	6	0.3	1	0.0	30	1.4
S	0	0.0	2	0.1	5	0.2	8	0.4	2	0.1	1	0.0	2	0.1	20	0.9
SSW	0	0.0	0	0.0	4	0.2	6	0.3	13	0.6	5	0.2	3	0.1	31	1.4
SW	0	0.0	1	0.0	2	0.1	15	0.7	16	0.7	0	0.0	0	0.0	34	1.6
WSW	0	0.0	2	0.1	4	0.2	11	0.5	7	0.3	0	0.0	1	0.0	25	1.2
W	0	0.0	1	0.0	1	0.0	7	0.3	5	0.2	0	0.0	0	0.0	14	0.7
WNW	0	0.0	0	0.0	2	0.1	3	0.1	8	0.4	0	0.0	0	0.0	13	0.6
NW	0	0.0	1	0.0	2	0.1	0	0.0	5	0.2	0	0.0	0	0.0	8	0.4
NNW	0	0.0	1	0.0	2	0.1	1	0.0	2	0.1	0	0.0	0	0.0	6	0.3
	0	0.0	14	0.7	57	2.7	94	4.4	88	4.1	21	1.0	14	0.7	288	13.5

MEAN WIND SPEED: 12.0  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 150 FT  
DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
CLASS G

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	1	0.0	5	0.2	0	0.0	0	0.0	0	0.0	6	0.3
E	0	0.0	0	0.0	3	0.1	3	0.1	1	0.0	0	0.0	0	0.0	7	0.3
ESE	0	0.0	1	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	6	0.3
SE	0	0.0	0	0.0	1	0.0	9	0.4	9	0.4	2	0.1	3	0.1	24	1.1
SSE	0	0.0	0	0.0	0	0.0	3	0.1	13	0.6	6	0.3	16	0.7	38	1.8
S	0	0.0	1	0.0	1	0.0	2	0.1	14	0.7	1	0.0	3	0.1	22	1.0
SSW	0	0.0	0	0.0	1	0.0	3	0.1	4	0.2	0	0.0	0	0.0	8	0.4
SW	0	0.0	2	0.1	0	0.0	3	0.1	7	0.3	0	0.0	0	0.0	12	0.6
WSW	0	0.0	0	0.0	1	0.0	5	0.2	0	0.0	0	0.0	0	0.0	6	0.3
W	0	0.0	1	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	4	0.2
WNW	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
NW	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	0	0.0	2	0.1
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	7	0.3	11	0.5	40	1.9	50	2.3	9	0.4	22	1.0	139	6.5

MEAN WIND SPEED: 15.0  
MISSING: 0



JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	13	0.6	42	2.0	80	3.7	40	1.9	5	0.2	183	8.5
NNE	0	0.0	4	0.2	25	1.2	75	3.5	31	1.4	9	0.4	2	0.1	146	6.8
NE	0	0.0	7	0.3	25	1.2	50	2.3	30	1.4	7	0.3	1	0.0	120	5.6
ENE	0	0.0	5	0.2	23	1.1	44	2.1	6	0.3	0	0.0	0	0.0	78	3.6
E	0	0.0	4	0.2	21	1.0	16	0.7	4	0.2	0	0.0	0	0.0	45	2.1
ESE	0	0.0	3	0.1	9	0.4	11	0.5	10	0.5	3	0.1	1	0.0	37	1.7
SE	0	0.0	3	0.1	20	0.9	47	2.2	36	1.7	20	0.9	37	1.7	163	7.6
SSE	0	0.0	0	0.0	18	0.8	27	1.3	26	1.2	14	0.7	18	0.8	103	4.8
S	0	0.0	6	0.3	14	0.7	24	1.1	27	1.3	6	0.3	6	0.3	83	3.9
SSW	0	0.0	3	0.1	20	0.9	25	1.2	31	1.4	13	0.6	7	0.3	99	4.6
SW	0	0.0	6	0.3	17	0.8	50	2.3	36	1.7	5	0.2	3	0.1	117	5.5
WSW	0	0.0	3	0.1	20	0.9	44	2.1	23	1.1	6	0.3	6	0.3	102	4.8
W	0	0.0	5	0.2	13	0.6	42	2.0	50	2.3	16	0.7	17	0.8	143	6.7
WNW	0	0.0	2	0.1	28	1.3	59	2.8	71	3.3	31	1.4	7	0.3	198	9.2
NW	0	0.0	2	0.1	17	0.8	66	3.1	135	6.3	76	3.5	14	0.7	310	14.5
NNW	0	0.0	1	0.0	9	0.4	20	0.9	85	4.0	63	2.9	37	1.7	215	10.0
	0	0.0	57	2.7	292	13.6	642	30.0	681	31.8	309	14.4	161	7.5	2142	100.0

MISSING HOURS: 18

MEAN WIND SPEED: 14.0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	2	0.1	7	0.3
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
W	0	0.0	1	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	4	0.2
WNW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	4	0.2
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	10	0.5	1	0.0	11	0.5
NNW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	16	0.8	10	0.5	29	1.4
	0	0.0	1	0.0	0	0.0	2	0.1	8	0.4	33	1.6	13	0.6	57	2.7

MEAN WIND SPEED: 21.5  
 MISSING: 5

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	1	0.0	4	0.2	5	0.2	0	0.0	10	0.5
NNE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	4	0.2
ENE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
W	0	0.0	0	0.0	1	0.0	2	0.1	1	0.0	1	0.0	3	0.1	8	0.4
WNW	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	2	0.1	6	0.3
NW	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	11	0.5	2	0.1	16	0.8
NNW	0	0.0	0	0.0	0	0.0	2	0.1	8	0.4	6	0.3	5	0.2	21	1.0
	0	0.0	0	0.0	2	0.1	9	0.4	20	0.9	25	1.2	12	0.6	68	3.2

MEAN WIND SPEED: 18.9  
 MISSING: 5

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	2	0.1	6	0.3	6	0.3	7	0.3	2	0.1	23	1.1
NNE	0	0.0	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	4	0.2
NE	0	0.0	0	0.0	0	0.0	4	0.2	5	0.2	1	0.0	0	0.0	10	0.5
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
W	0	0.0	0	0.0	2	0.1	3	0.1	2	0.1	4	0.2	2	0.1	13	0.6
WNW	0	0.0	0	0.0	1	0.0	1	0.0	1	0.0	2	0.1	1	0.0	6	0.3
NW	0	0.0	0	0.0	1	0.0	2	0.1	6	0.3	4	0.2	3	0.1	16	0.8
NNW	0	0.0	0	0.0	1	0.0	1	0.0	8	0.4	7	0.3	1	0.0	18	0.8
	0	0.0	0	0.0	7	0.3	19	0.9	30	1.4	25	1.2	9	0.4	90	4.2

MEAN WIND SPEED: 16.7  
 MISSING: 3

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	4	0.2	9	0.4	13	0.6	13	0.6	27	1.3	67	3.2
NNE	0	0.0	0	0.0	9	0.4	17	0.8	24	1.1	4	0.2	3	0.1	57	2.7
NE	0	0.0	0	0.0	7	0.3	19	0.9	16	0.8	15	0.7	8	0.4	65	3.1
ENE	0	0.0	1	0.0	3	0.1	19	0.9	9	0.4	3	0.1	0	0.0	35	1.6
E	0	0.0	2	0.1	6	0.3	1	0.0	0	0.0	0	0.0	0	0.0	9	0.4
ESE	0	0.0	1	0.0	3	0.1	0	0.0	0	0.0	1	0.0	0	0.0	5	0.2
SE	0	0.0	1	0.0	4	0.2	0	0.0	1	0.0	6	0.3	1	0.0	13	0.6
SSE	0	0.0	0	0.0	3	0.1	4	0.2	4	0.2	1	0.0	1	0.0	13	0.6
S	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	2	0.1	0	0.0	6	0.3
SSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0	2	0.1
SW	0	0.0	0	0.0	3	0.1	6	0.3	2	0.1	0	0.0	2	0.1	13	0.6
WSW	0	0.0	0	0.0	1	0.0	6	0.3	7	0.3	2	0.1	4	0.2	20	0.9
W	0	0.0	0	0.0	7	0.3	10	0.5	10	0.5	7	0.3	8	0.4	42	2.0
WNW	0	0.0	0	0.0	10	0.5	13	0.6	39	1.8	33	1.6	14	0.7	109	5.1
NW	0	0.0	0	0.0	8	0.4	13	0.6	40	1.9	32	1.5	17	0.8	110	5.2
NNW	0	0.0	0	0.0	3	0.1	6	0.3	15	0.7	35	1.6	30	1.4	89	4.2
	0	0.0	6	0.3	72	3.4	125	5.9	182	8.6	154	7.3	116	5.5	655	30.9

MEAN WIND SPEED: 17.1  
 MISSING: 10

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	4	0.2	7	0.3	19	0.9	16	0.8	6	0.3	52	2.5
NNE	0	0.0	1	0.0	8	0.4	13	0.6	38	1.8	13	0.6	0	0.0	73	3.4
NE	0	0.0	1	0.0	4	0.2	15	0.7	23	1.1	2	0.1	0	0.0	45	2.1
ENE	0	0.0	2	0.1	2	0.1	18	0.8	7	0.3	0	0.0	2	0.1	31	1.5
E	0	0.0	1	0.0	9	0.4	12	0.6	5	0.2	0	0.0	0	0.0	27	1.3
ESE	0	0.0	0	0.0	5	0.2	4	0.2	6	0.3	3	0.1	1	0.0	19	0.9
SE	0	0.0	0	0.0	0	0.0	2	0.1	6	0.3	3	0.1	20	0.9	31	1.5
SSE	0	0.0	1	0.0	4	0.2	11	0.5	14	0.7	4	0.2	11	0.5	45	2.1
S	0	0.0	0	0.0	4	0.2	12	0.6	5	0.2	1	0.0	2	0.1	24	1.1
SSW	0	0.0	0	0.0	7	0.3	12	0.6	24	1.1	11	0.5	5	0.2	59	2.8
SW	0	0.0	1	0.0	7	0.3	8	0.4	17	0.8	10	0.5	4	0.2	47	2.2
WSW	0	0.0	0	0.0	4	0.2	20	0.9	13	0.6	1	0.0	0	0.0	38	1.8
W	0	0.0	0	0.0	10	0.5	14	0.7	19	0.9	12	0.6	1	0.0	56	2.6
WNW	0	0.0	0	0.0	8	0.4	17	0.8	19	0.9	12	0.6	3	0.1	59	2.8
NW	0	0.0	0	0.0	6	0.3	16	0.8	55	2.6	31	1.5	10	0.5	118	5.6
NNW	0	0.0	1	0.0	0	0.0	11	0.5	32	1.5	35	1.6	22	1.0	101	4.8
	0	0.0	8	0.4	82	3.9	192	9.0	302	14.2	154	7.3	87	4.1	825	38.9

MEAN WIND SPEED: 16.0  
 MISSING: 7

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	1	0.0	4	0.2	2	0.1	3	0.1	0	0.0	10	0.5
NNE	0	0.0	0	0.0	1	0.0	0	0.0	3	0.1	0	0.0	0	0.0	4	0.2
NE	0	0.0	1	0.0	2	0.1	1	0.0	2	0.1	1	0.0	0	0.0	7	0.3
ENE	0	0.0	0	0.0	2	0.1	3	0.1	1	0.0	0	0.0	0	0.0	6	0.3
E	0	0.0	1	0.0	3	0.1	3	0.1	1	0.0	2	0.1	0	0.0	10	0.5
ESE	0	0.0	0	0.0	1	0.0	2	0.1	1	0.0	0	0.0	0	0.0	4	0.2
SE	0	0.0	0	0.0	5	0.2	8	0.4	3	0.1	4	0.2	4	0.2	24	1.1
SSE	0	0.0	0	0.0	9	0.4	15	0.7	7	0.3	9	0.4	11	0.5	51	2.4
S	0	0.0	1	0.0	5	0.2	7	0.3	8	0.4	4	0.2	2	0.1	27	1.3
SSW	0	0.0	1	0.0	3	0.1	3	0.1	6	0.3	12	0.6	6	0.3	31	1.5
SW	0	0.0	1	0.0	1	0.0	8	0.4	12	0.6	8	0.4	0	0.0	30	1.4
WSW	0	0.0	1	0.0	1	0.0	3	0.1	10	0.5	11	0.5	1	0.0	27	1.3
W	0	0.0	1	0.0	1	0.0	4	0.2	4	0.2	7	0.3	0	0.0	17	0.8
WNW	0	0.0	3	0.1	2	0.1	1	0.0	3	0.1	4	0.2	2	0.1	15	0.7
NW	0	0.0	0	0.0	3	0.1	3	0.1	3	0.1	8	0.4	0	0.0	17	0.8
NNW	0	0.0	1	0.0	1	0.0	1	0.0	1	0.0	4	0.2	0	0.0	8	0.4
	0	0.0	11	0.5	41	1.9	66	3.1	67	3.2	77	3.6	26	1.2	288	13.6

MEAN WIND SPEED: 15.2  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	1	0.0	0	0.0	4	0.2
ESE	0	0.0	1	0.0	0	0.0	2	0.1	5	0.2	1	0.0	0	0.0	9	0.4
SE	0	0.0	0	0.0	2	0.1	1	0.0	2	0.1	6	0.3	2	0.1	13	0.6
SSE	0	0.0	0	0.0	0	0.0	2	0.1	3	0.1	1	0.0	11	0.5	17	0.8
S	0	0.0	1	0.0	2	0.1	3	0.1	11	0.5	7	0.3	14	0.7	38	1.8
SSW	0	0.0	0	0.0	2	0.1	2	0.1	8	0.4	5	0.2	2	0.1	19	0.9
SW	0	0.0	0	0.0	2	0.1	2	0.1	3	0.1	4	0.2	0	0.0	11	0.5
WSW	0	0.0	1	0.0	1	0.0	0	0.0	2	0.1	6	0.3	0	0.0	10	0.5
W	0	0.0	2	0.1	0	0.0	1	0.0	2	0.1	3	0.1	0	0.0	8	0.4
WNW	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	3	0.1	0	0.0	5	0.2
NW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	2	0.1
NNW	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
	0	0.0	6	0.3	12	0.6	15	0.7	39	1.8	38	1.8	29	1.4	139	6.6

MEAN WIND SPEED: 18.5  
 MISSING: 0

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT			
N	0	0.0	1	0.0	12	0.6	27	1.3	44	2.1	49	2.3	37	1.7	170	8.0
NNE	0	0.0	1	0.0	19	0.9	33	1.6	68	3.2	17	0.8	3	0.1	141	6.6
NE	0	0.0	2	0.1	13	0.6	41	1.9	48	2.3	20	0.9	8	0.4	132	6.2
ENE	0	0.0	3	0.1	7	0.3	40	1.9	18	0.8	3	0.1	2	0.1	73	3.4
E	0	0.0	4	0.2	18	0.8	17	0.8	8	0.4	3	0.1	0	0.0	50	2.4
ESE	0	0.0	2	0.1	9	0.4	8	0.4	12	0.6	5	0.2	1	0.0	37	1.7
SE	0	0.0	1	0.0	11	0.5	11	0.5	12	0.6	19	0.9	27	1.3	81	3.8
SSE	0	0.0	1	0.0	16	0.8	32	1.5	28	1.3	15	0.7	34	1.6	126	5.9
S	0	0.0	2	0.1	12	0.6	23	1.1	26	1.2	14	0.7	18	0.8	95	4.5
SSW	0	0.0	1	0.0	12	0.6	18	0.8	38	1.8	28	1.3	14	0.7	111	5.2
SW	0	0.0	2	0.1	13	0.6	24	1.1	34	1.6	22	1.0	6	0.3	101	4.8
WSW	0	0.0	2	0.1	8	0.4	29	1.4	32	1.5	20	0.9	5	0.2	96	4.5
W	0	0.0	4	0.2	21	1.0	35	1.6	40	1.9	34	1.6	14	0.7	148	7.0
WNW	0	0.0	3	0.1	22	1.0	34	1.6	66	3.1	57	2.7	22	1.0	204	9.6
NW	0	0.0	0	0.0	18	0.8	35	1.6	107	5.0	97	4.6	33	1.6	290	13.7
NNW	0	0.0	3	0.1	5	0.2	21	1.0	67	3.2	103	4.9	68	3.2	267	12.6
	0	0.0	32	1.5	216	10.2	428	20.2	648	30.5	506	23.8	292	13.8	2122	100.0
																MISSING HOURS: 38

MEAN WIND SPEED: 16.7

ARTIFICIAL ISLAND 1/99 - 3/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	12	0.6	27	1.3	44	2.1	49	2.3	37	1.7	170	8.0
NNE	0	0.0	1	0.0	19	0.9	33	1.6	68	3.2	17	0.8	3	0.1	141	6.6
NE	0	0.0	2	0.1	13	0.6	41	1.9	48	2.3	20	0.9	8	0.4	132	6.2
ENE	0	0.0	3	0.1	7	0.3	40	1.9	18	0.8	3	0.1	2	0.1	73	3.4
E	0	0.0	4	0.2	18	0.8	17	0.8	8	0.4	3	0.1	0	0.0	50	2.4
ESE	0	0.0	2	0.1	9	0.4	8	0.4	12	0.6	5	0.2	1	0.0	37	1.7
SE	0	0.0	1	0.0	11	0.5	11	0.5	12	0.6	19	0.9	27	1.3	81	3.8
SSE	0	0.0	1	0.0	17	0.8	32	1.5	28	1.3	15	0.7	34	1.6	127	6.0
S	0	0.0	3	0.1	12	0.6	23	1.1	27	1.3	14	0.7	18	0.8	97	4.6
SSW	0	0.0	1	0.0	12	0.6	18	0.8	38	1.8	28	1.3	14	0.7	111	5.2
SW	0	0.0	2	0.1	13	0.6	24	1.1	34	1.6	22	1.0	6	0.3	101	4.8
WSW	0	0.0	2	0.1	8	0.4	29	1.4	32	1.5	20	0.9	5	0.2	96	4.5
W	0	0.0	4	0.2	21	1.0	35	1.6	40	1.9	34	1.6	14	0.7	148	7.0
WNW	0	0.0	3	0.1	22	1.0	34	1.6	66	3.1	58	2.7	22	1.0	205	9.6
NW	0	0.0	0	0.0	18	0.8	35	1.6	107	5.0	97	4.6	33	1.6	290	13.6
NNW	0	0.0	3	0.1	5	0.2	21	1.0	67	3.2	103	4.8	68	3.2	267	12.6
	0	0.0	33	1.6	217	10.2	428	20.1	649	30.5	507	23.8	292	13.7	2126	100.0

MISSING HOURS: 34

MEAN WIND SPEED: 16.7

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	5	0.2
NNE	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	2	0.1
NE	0	0.0	0	0.0	1	0.0	9	0.4	4	0.2	1	0.0	0	0.0	15	0.7
ENE	0	0.0	0	0.0	0	0.0	11	0.5	5	0.2	0	0.0	0	0.0	16	0.7
E	0	0.0	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	5	0.2
ESE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	4	0.2	2	0.1	0	0.0	0	0.0	6	0.3
SSE	0	0.0	0	0.0	0	0.0	5	0.2	3	0.1	0	0.0	0	0.0	8	0.4
S	0	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	3	0.1
SSW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	3	0.1	5	0.2	0	0.0	0	0.0	0	0.0	8	0.4
WSW	0	0.0	0	0.0	1	0.0	1	0.0	3	0.1	0	0.0	0	0.0	5	0.2
W	0	0.0	0	0.0	1	0.0	11	0.5	11	0.5	0	0.0	0	0.0	23	1.1
WNW	0	0.0	0	0.0	0	0.0	6	0.3	3	0.1	0	0.0	0	0.0	9	0.4
NW	0	0.0	0	0.0	0	0.0	5	0.2	3	0.1	7	0.3	0	0.0	15	0.7
NNW	0	0.0	0	0.0	0	0.0	2	0.1	6	0.3	0	0.0	0	0.0	8	0.4
	0	0.0	0	0.0	7	0.3	72	3.3	43	2.0	8	0.4	0	0.0	130	6.0

MEAN WIND SPEED: 12.4  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	1	0.0	5	0.2	7	0.3	0	0.0	0	0.0	13	0.6
NNE	0	0.0	0	0.0	0	0.0	5	0.2	1	0.0	0	0.0	0	0.0	6	0.3
NE	0	0.0	0	0.0	0	0.0	6	0.3	2	0.1	0	0.0	0	0.0	8	0.4
ENE	0	0.0	0	0.0	2	0.1	8	0.4	0	0.0	0	0.0	0	0.0	10	0.5
E	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	3	0.1	3	0.1	0	0.0	0	0.0	6	0.3
SSE	0	0.0	0	0.0	0	0.0	4	0.2	4	0.2	0	0.0	0	0.0	8	0.4
S	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
SW	0	0.0	0	0.0	2	0.1	4	0.2	0	0.0	0	0.0	0	0.0	6	0.3
WSW	0	0.0	0	0.0	0	0.0	1	0.0	4	0.2	0	0.0	0	0.0	5	0.2
W	0	0.0	0	0.0	0	0.0	5	0.2	2	0.1	0	0.0	0	0.0	7	0.3
WNW	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
NW	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	3	0.1	0	0.0	8	0.4
NNW	0	0.0	0	0.0	0	0.0	4	0.2	4	0.2	0	0.0	0	0.0	8	0.4
	0	0.0	0	0.0	9	0.4	51	2.3	31	1.4	3	0.1	0	0.0	94	4.3

MEAN WIND SPEED: 11.6  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	6	0.3	10	0.5	3	0.1	0	0.0	0	0.0	19	0.9
NNE	0	0.0	0	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	5	0.2
NE	0	0.0	0	0.0	4	0.2	9	0.4	3	0.1	0	0.0	0	0.0	16	0.7
ENE	0	0.0	0	0.0	0	0.0	7	0.3	0	0.0	0	0.0	0	0.0	7	0.3
E	0	0.0	0	0.0	2	0.1	5	0.2	0	0.0	0	0.0	0	0.0	7	0.3
ESE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	1	0.0	4	0.2	0	0.0	0	0.0	5	0.2
SSE	0	0.0	0	0.0	3	0.1	3	0.1	4	0.2	0	0.0	0	0.0	10	0.5
S	0	0.0	0	0.0	7	0.3	1	0.0	0	0.0	0	0.0	0	0.0	8	0.4
SSW	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SW	0	0.0	0	0.0	3	0.1	8	0.4	2	0.1	0	0.0	0	0.0	13	0.6
WSW	0	0.0	0	0.0	2	0.1	3	0.1	3	0.1	0	0.0	0	0.0	8	0.4
W	0	0.0	0	0.0	0	0.0	8	0.4	2	0.1	0	0.0	0	0.0	10	0.5
WNW	0	0.0	0	0.0	2	0.1	4	0.2	2	0.1	0	0.0	0	0.0	8	0.4
NW	0	0.0	0	0.0	1	0.0	2	0.1	4	0.2	1	0.0	0	0.0	8	0.4
NNW	0	0.0	0	0.0	1	0.0	7	0.3	3	0.1	0	0.0	0	0.0	11	0.5
	0	0.0	0	0.0	35	1.6	72	3.3	31	1.4	1	0.0	0	0.0	139	6.4

MEAN WIND SPEED: 10.0  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (+300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	1	0.0	21	1.0	31	1.4	9	0.4	0	0.0	0	0.0	62	2.9
NNE	0	0.0	1	0.0	26	1.2	21	1.0	7	0.3	0	0.0	0	0.0	55	2.5
NE	0	0.0	1	0.0	32	1.5	56	2.6	8	0.4	0	0.0	0	0.0	97	4.5
ENE	0	0.0	7	0.3	43	2.0	28	1.3	1	0.0	0	0.0	0	0.0	79	3.6
E	0	0.0	6	0.3	25	1.2	22	1.0	0	0.0	0	0.0	0	0.0	53	2.4
ESE	0	0.0	3	0.1	10	0.5	17	0.8	3	0.1	0	0.0	0	0.0	33	1.5
SE	0	0.0	1	0.0	2	0.1	28	1.3	30	1.4	2	0.1	0	0.0	63	2.9
SSE	0	0.0	0	0.0	27	1.2	27	1.2	27	1.2	2	0.1	0	0.0	83	3.8
S	0	0.0	2	0.1	30	1.4	16	0.7	5	0.2	0	0.0	0	0.0	53	2.4
SSW	0	0.0	2	0.1	19	0.9	23	1.1	4	0.2	0	0.0	0	0.0	48	2.2
SW	0	0.0	1	0.0	16	0.7	15	0.7	2	0.1	0	0.0	0	0.0	34	1.6
WSW	0	0.0	1	0.0	8	0.4	18	0.8	2	0.1	0	0.0	0	0.0	29	1.3
W	0	0.0	0	0.0	7	0.3	17	0.8	7	0.3	0	0.0	0	0.0	31	1.4
WNW	0	0.0	2	0.1	7	0.3	10	0.5	4	0.2	0	0.0	0	0.0	23	1.1
NW	0	0.0	1	0.0	6	0.3	12	0.6	8	0.4	0	0.0	0	0.0	27	1.2
NNW	0	0.0	1	0.0	8	0.4	8	0.4	10	0.5	0	0.0	0	0.0	27	1.2
	0	0.0	30	1.4	287	13.2	349	16.1	127	5.8	4	0.2	0	0.0	797	36.7

MEAN WIND SPEED: 8.9  
 MISSING: 1

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 30 FT  
DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	27	1.2	20	0.9	8	0.4	0	0.0	0	0.0	58	2.7
NNE	0	0.0	1	0.0	37	1.7	24	1.1	2	0.1	0	0.0	0	0.0	64	2.9
NE	0	0.0	6	0.3	48	2.2	20	0.9	0	0.0	0	0.0	0	0.0	74	3.4
ENE	0	0.0	5	0.2	37	1.7	4	0.2	0	0.0	0	0.0	0	0.0	46	2.1
E	0	0.0	4	0.2	15	0.7	5	0.2	0	0.0	0	0.0	0	0.0	24	1.1
ESE	0	0.0	3	0.1	21	1.0	7	0.3	0	0.0	0	0.0	0	0.0	31	1.4
SE	0	0.0	6	0.3	14	0.6	26	1.2	17	0.8	0	0.0	0	0.0	63	2.9
SSE	0	0.0	0	0.0	13	0.6	22	1.0	11	0.5	0	0.0	0	0.0	46	2.1
S	0	0.0	1	0.0	13	0.6	9	0.4	2	0.1	1	0.0	0	0.0	26	1.2
SSW	0	0.0	3	0.1	25	1.2	22	1.0	0	0.0	0	0.0	0	0.0	50	2.3
SW	0	0.0	3	0.1	33	1.5	24	1.1	0	0.0	0	0.0	0	0.0	60	2.8
WSW	0	0.0	5	0.2	18	0.8	11	0.5	1	0.0	0	0.0	0	0.0	35	1.6
W	0	0.0	3	0.1	13	0.6	18	0.8	1	0.0	0	0.0	0	0.0	35	1.6
WNW	0	0.0	3	0.1	9	0.4	19	0.9	2	0.1	0	0.0	0	0.0	33	1.5
NW	0	0.0	1	0.0	23	1.1	27	1.2	5	0.2	0	0.0	0	0.0	56	2.6
NNW	0	0.0	7	0.3	18	0.8	19	0.9	0	0.0	0	0.0	0	0.0	44	2.0
	0	0.0	54	2.5	364	16.8	277	12.7	49	2.3	1	0.0	0	0.0	745	34.3

MEAN WIND SPEED: 7.4  
MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	1	0.0	8	0.4	5	0.2	0	0.0	0	0.0	0	0.0	14	0.6
NNE	0	0.0	0	0.0	11	0.5	7	0.3	0	0.0	0	0.0	0	0.0	18	0.8
NE	0	0.0	1	0.0	8	0.4	1	0.0	0	0.0	0	0.0	0	0.0	10	0.5
ENE	0	0.0	1	0.0	4	0.2	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
E	0	0.0	3	0.1	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3
ESE	0	0.0	2	0.1	9	0.4	1	0.0	0	0.0	0	0.0	0	0.0	12	0.6
SE	0	0.0	2	0.1	13	0.6	11	0.5	2	0.1	0	0.0	0	0.0	28	1.3
SSE	0	0.0	0	0.0	10	0.5	9	0.4	0	0.0	0	0.0	0	0.0	19	0.9
S	0	0.0	1	0.0	7	0.3	1	0.0	0	0.0	0	0.0	0	0.0	9	0.4
SSW	0	0.0	4	0.2	7	0.3	3	0.1	0	0.0	0	0.0	0	0.0	14	0.6
SW	0	0.0	0	0.0	7	0.3	9	0.4	0	0.0	0	0.0	0	0.0	16	0.7
WSW	0	0.0	1	0.0	12	0.6	5	0.2	0	0.0	0	0.0	0	0.0	18	0.8
W	0	0.0	2	0.1	7	0.3	5	0.2	0	0.0	0	0.0	0	0.0	14	0.6
WNW	0	0.0	2	0.1	8	0.4	8	0.4	0	0.0	0	0.0	0	0.0	18	0.8
NW	0	0.0	0	0.0	10	0.5	6	0.3	0	0.0	0	0.0	0	0.0	16	0.7
NNW	0	0.0	0	0.0	6	0.3	2	0.1	0	0.0	0	0.0	0	0.0	8	0.4
	0	0.0	20	0.9	130	6.0	73	3.4	2	0.1	0	0.0	0	0.0	225	10.4

MEAN WIND SPEED: 6.6  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
NNE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
ENE	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
E	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
ESE	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SE	0	0.0	0	0.0	9	0.4	3	0.1	1	0.0	0	0.0	0	0.0	13	0.6
SSE	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
S	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	5	0.2
WSW	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
W	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
WNW	0	0.0	1	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	4	0.2
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
	0	0.0	9	0.4	26	1.2	7	0.3	1	0.0	0	0.0	0	0.0	43	2.0
MEAN WIND SPEED:	5.5															
MISSING:	0															

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	SUM PERCENT
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	5	0.2	65	3.0	74	3.4	29	1.3	0	0.0	0	0.0	173	8.0
NNE	0	0.0	2	0.1	76	3.5	62	2.9	11	0.5	0	0.0	0	0.0	151	6.9
NE	0	0.0	8	0.4	93	4.3	102	4.7	17	0.8	1	0.0	0	0.0	221	10.2
ENE	0	0.0	14	0.6	86	4.0	58	2.7	6	0.3	0	0.0	0	0.0	164	7.5
E	0	0.0	14	0.6	45	2.1	38	1.7	1	0.0	0	0.0	0	0.0	98	4.5
ESE	0	0.0	9	0.4	43	2.0	26	1.2	4	0.2	0	0.0	0	0.0	82	3.8
SE	0	0.0	9	0.4	38	1.7	76	3.5	59	2.7	2	0.1	0	0.0	184	8.5
SSE	0	0.0	2	0.1	54	2.5	70	3.2	49	2.3	2	0.1	0	0.0	177	8.1
S	0	0.0	4	0.2	59	2.7	32	1.5	7	0.3	1	0.0	0	0.0	103	4.7
SSW	0	0.0	9	0.4	58	2.7	48	2.2	4	0.2	0	0.0	0	0.0	119	5.5
SW	0	0.0	5	0.2	67	3.1	66	3.0	4	0.2	0	0.0	0	0.0	142	6.5
WSW	0	0.0	9	0.4	41	1.9	39	1.8	13	0.6	0	0.0	0	0.0	102	4.7
W	0	0.0	5	0.2	29	1.3	65	3.0	23	1.1	0	0.0	0	0.0	122	5.6
WNW	0	0.0	8	0.4	29	1.3	48	2.2	12	0.6	0	0.0	0	0.0	97	4.5
NW	0	0.0	2	0.1	40	1.8	55	2.5	22	1.0	11	0.5	0	0.0	130	6.0
NNW	0	0.0	8	0.4	35	1.6	42	1.9	23	1.1	0	0.0	0	0.0	108	5.0
	0	0.0	113	5.2	858	39.5	901	41.5	284	13.1	17	0.8	0	0.0	2173	100.0
															MISSING HOURS: 11	
MEAN WIND SPEED:		8.5														



ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 150 FT  
DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	5	0.2
NNE	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	3	0.1
NE	0	0.0	0	0.0	0	0.0	2	0.1	9	0.4	2	0.1	1	0.0	14	0.6
ENE	0	0.0	0	0.0	0	0.0	2	0.1	12	0.6	3	0.1	0	0.0	17	0.8
E	0	0.0	0	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	4	0.2
ESE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	1	0.0	6	0.3	2	0.1	0	0.0	9	0.4
SSE	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	5	0.2
S	0	0.0	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	3	0.1
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	4	0.2	5	0.2	0	0.0	0	0.0	0	0.0	9	0.4
WSW	0	0.0	0	0.0	1	0.0	1	0.0	1	0.0	3	0.1	0	0.0	6	0.3
W	0	0.0	0	0.0	0	0.0	7	0.3	15	0.7	3	0.1	0	0.0	25	1.2
WNW	0	0.0	0	0.0	0	0.0	2	0.1	3	0.1	1	0.0	0	0.0	6	0.3
NW	0	0.0	0	0.0	0	0.0	2	0.1	4	0.2	6	0.3	4	0.2	16	0.7
NNW	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	1	0.0	0	0.0	7	0.3
	0	0.0	0	0.0	5	0.2	28	1.3	71	3.3	21	1.0	5	0.2	130	6.0

MEAN WIND SPEED: 15.1  
MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	1	0.0	2	0.1	7	0.3	1	0.0	0	0.0	11	0.5
NNE	0	0.0	0	0.0	0	0.0	4	0.2	2	0.1	0	0.0	0	0.0	6	0.3
NE	0	0.0	0	0.0	0	0.0	4	0.2	4	0.2	2	0.1	0	0.0	10	0.5
ENE	0	0.0	0	0.0	1	0.0	4	0.2	4	0.2	0	0.0	0	0.0	9	0.4
E	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	3	0.1	1	0.0	3	0.1	0	0.0	7	0.3
SSE	0	0.0	0	0.0	0	0.0	2	0.1	3	0.1	2	0.1	0	0.0	7	0.3
S	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	1	0.0	4	0.2	4	0.2	0	0.0	0	0.0	0	0.0	9	0.4
WSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	4	0.2	0	0.0	5	0.2
W	0	0.0	0	0.0	0	0.0	4	0.2	3	0.1	1	0.0	0	0.0	8	0.4
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	1	0.0	2	0.1	9	0.4
NNW	0	0.0	0	0.0	0	0.0	2	0.1	6	0.3	0	0.0	0	0.0	8	0.4
	0	0.0	1	0.0	6	0.3	33	1.5	37	1.7	15	0.7	2	0.1	94	4.3

MEAN WIND SPEED: 14.1  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 150 FT  
DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	4	0.2	9	0.4	2	0.1	2	0.1	0	0.0	17	0.8
NNE	0	0.0	0	0.0	2	0.1	3	0.1	1	0.0	0	0.0	0	0.0	6	0.3
NE	0	0.0	0	0.0	1	0.0	7	0.3	4	0.2	1	0.0	0	0.0	13	0.6
ENE	0	0.0	0	0.0	3	0.1	4	0.2	4	0.2	0	0.0	0	0.0	11	0.5
E	0	0.0	0	0.0	0	0.0	2	0.1	3	0.1	0	0.0	0	0.0	5	0.2
ESE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	1	0.0	1	0.0	1	0.0	3	0.1	1	0.0	7	0.3
SSE	0	0.0	0	0.0	3	0.1	1	0.0	5	0.2	0	0.0	0	0.0	9	0.4
S	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
SSW	0	0.0	2	0.1	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	5	0.2
SW	0	0.0	0	0.0	3	0.1	3	0.1	5	0.2	2	0.1	0	0.0	13	0.6
WSW	0	0.0	0	0.0	2	0.1	2	0.1	3	0.1	2	0.1	0	0.0	9	0.4
W	0	0.0	0	0.0	0	0.0	6	0.3	6	0.3	0	0.0	0	0.0	12	0.6
WNW	0	0.0	0	0.0	2	0.1	1	0.0	4	0.2	0	0.0	0	0.0	7	0.3
NW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	1	0.0	6	0.3
NNW	0	0.0	0	0.0	0	0.0	10	0.5	2	0.1	2	0.1	0	0.0	14	0.6
	0	0.0	2	0.1	26	1.2	51	2.3	44	2.0	14	0.6	2	0.1	139	6.4

MEAN WIND SPEED: 12.2  
MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	12	0.6	22	1.0	16	0.7	6	0.3	0	0.0	58	2.7
NNE	0	0.0	0	0.0	20	0.9	22	1.0	7	0.3	4	0.2	0	0.0	53	2.4
NE	0	0.0	0	0.0	17	0.8	46	2.1	30	1.4	10	0.5	0	0.0	103	4.7
ENE	0	0.0	4	0.2	21	1.0	43	2.0	15	0.7	2	0.1	0	0.0	85	3.9
E	0	0.0	1	0.0	17	0.8	22	1.0	8	0.4	0	0.0	0	0.0	48	2.2
ESE	0	0.0	1	0.0	6	0.3	11	0.5	13	0.6	1	0.0	0	0.0	32	1.5
SE	0	0.0	1	0.0	6	0.3	11	0.5	29	1.3	22	1.0	2	0.1	71	3.3
SSE	0	0.0	2	0.1	13	0.6	14	0.6	30	1.4	13	0.6	0	0.0	72	3.3
S	0	0.0	4	0.2	16	0.7	21	1.0	9	0.4	0	0.0	0	0.0	50	2.3
SSW	0	0.0	2	0.1	18	0.8	22	1.0	12	0.6	1	0.0	0	0.0	55	2.5
SW	0	0.0	4	0.2	8	0.4	8	0.4	13	0.6	1	0.0	0	0.0	34	1.6
WSW	0	0.0	1	0.0	3	0.1	11	0.5	7	0.3	1	0.0	0	0.0	23	1.1
W	0	0.0	0	0.0	7	0.3	11	0.5	14	0.6	3	0.1	0	0.0	35	1.6
WNW	0	0.0	0	0.0	6	0.3	7	0.3	7	0.3	1	0.0	0	0.0	21	1.0
NW	0	0.0	1	0.0	5	0.2	5	0.2	13	0.6	6	0.3	0	0.0	30	1.4
NNW	0	0.0	1	0.0	4	0.2	10	0.5	3	0.1	8	0.4	1	0.0	27	1.2
	0	0.0	24	1.1	179	8.2	286	13.2	226	10.4	79	3.6	3	0.1	797	36.7

MEAN WIND SPEED: 11.4  
 MISSING: 1

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	5	0.2	19	0.9	18	0.8	10	0.5	0	0.0	53	2.4
NNE	0	0.0	0	0.0	14	0.6	22	1.0	16	0.7	0	0.0	0	0.0	52	2.4
NE	0	0.0	0	0.0	5	0.2	40	1.8	25	1.2	0	0.0	0	0.0	70	3.2
ENE	0	0.0	1	0.0	17	0.8	36	1.7	6	0.3	0	0.0	0	0.0	60	2.8
E	0	0.0	2	0.1	10	0.5	15	0.7	3	0.1	0	0.0	0	0.0	30	1.4
ESE	0	0.0	1	0.0	10	0.5	10	0.5	8	0.4	0	0.0	0	0.0	29	1.3
SE	0	0.0	1	0.0	7	0.3	19	0.9	24	1.1	15	0.7	0	0.0	66	3.0
SSE	0	0.0	3	0.1	6	0.3	16	0.7	9	0.4	6	0.3	0	0.0	40	1.8
S	0	0.0	0	0.0	12	0.6	9	0.4	4	0.2	1	0.0	1	0.0	27	1.2
SSW	0	0.0	3	0.1	14	0.6	19	0.9	14	0.6	0	0.0	0	0.0	50	2.3
SW	0	0.0	2	0.1	11	0.5	34	1.6	15	0.7	0	0.0	0	0.0	62	2.9
WSW	0	0.0	3	0.1	9	0.4	18	0.8	4	0.2	1	0.0	0	0.0	35	1.6
W	0	0.0	2	0.1	9	0.4	18	0.8	12	0.6	3	0.1	0	0.0	44	2.0
WNW	0	0.0	5	0.2	5	0.2	10	0.5	11	0.5	0	0.0	0	0.0	31	1.4
NW	0	0.0	0	0.0	6	0.3	23	1.1	28	1.3	6	0.3	0	0.0	63	2.9
NNW	0	0.0	0	0.0	4	0.2	12	0.6	15	0.7	2	0.1	0	0.0	33	1.5
	0	0.0	24	1.1	144	6.6	320	14.7	212	9.8	44	2.0	1	0.0	745	34.3

MEAN WIND SPEED: 11.1  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	2	0.1	2	0.1	8	0.4	0	0.0	0	0.0	12	0.6
NNE	0	0.0	0	0.0	3	0.1	9	0.4	4	0.2	0	0.0	0	0.0	16	0.7
NE	0	0.0	0	0.0	0	0.0	4	0.2	6	0.3	0	0.0	0	0.0	10	0.5
ENE	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	5	0.2
E	0	0.0	0	0.0	5	0.2	4	0.2	0	0.0	0	0.0	0	0.0	9	0.4
ESE	0	0.0	1	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	6	0.3
SE	0	0.0	1	0.0	2	0.1	11	0.5	4	0.2	1	0.0	0	0.0	19	0.9
SSE	0	0.0	0	0.0	3	0.1	4	0.2	10	0.5	3	0.1	0	0.0	20	0.9
S	0	0.0	1	0.0	3	0.1	5	0.2	2	0.1	0	0.0	0	0.0	11	0.5
SSW	0	0.0	0	0.0	3	0.1	9	0.4	4	0.2	0	0.0	0	0.0	16	0.7
SW	0	0.0	2	0.1	4	0.2	15	0.7	10	0.5	0	0.0	0	0.0	31	1.4
WSW	0	0.0	1	0.0	2	0.1	7	0.3	4	0.2	0	0.0	0	0.0	14	0.6
W	0	0.0	0	0.0	2	0.1	11	0.5	6	0.3	0	0.0	0	0.0	19	0.9
WNW	0	0.0	0	0.0	1	0.0	5	0.2	4	0.2	0	0.0	0	0.0	10	0.5
NW	0	0.0	0	0.0	2	0.1	10	0.5	10	0.5	0	0.0	0	0.0	22	1.0
NNW	0	0.0	0	0.0	1	0.0	2	0.1	2	0.1	0	0.0	0	0.0	5	0.2
	0	0.0	6	0.3	37	1.7	103	4.7	75	3.5	4	0.2	0	0.0	225	10.4

MEAN WIND SPEED: 10.8  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 150 FT  
DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
CLASS G

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	3	0.1	0	0.0	6	0.3
SSE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
S	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	5	0.2
SW	0	0.0	1	0.0	4	0.2	5	0.2	2	0.1	0	0.0	0	0.0	12	0.6
WSW	0	0.0	1	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	4	0.2
W	0	0.0	0	0.0	1	0.0	3	0.1	0	0.0	0	0.0	0	0.0	4	0.2
WNW	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	3	0.1
NW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNW	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
	0	0.0	2	0.1	11	0.5	20	0.9	7	0.3	3	0.1	0	0.0	43	2.0

MEAN WIND SPEED: 10.3  
MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 150 FT  
DELTA T: (300-33FT)

ALL STABILITY CLASSES

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT		
N	0	0.0	3	0.1	24	1.1	54	2.5	56	2.6	19	0.9	0	0.0	156	7.2
NNE	0	0.0	0	0.0	39	1.8	62	2.9	32	1.5	4	0.2	0	0.0	137	6.3
NE	0	0.0	0	0.0	23	1.1	103	4.7	79	3.6	15	0.7	1	0.0	221	10.2
ENE	0	0.0	5	0.2	45	2.1	91	4.2	41	1.9	5	0.2	0	0.0	187	8.6
E	0	0.0	3	0.1	32	1.5	44	2.0	19	0.9	0	0.0	0	0.0	98	4.5
ESE	0	0.0	3	0.1	17	0.8	25	1.2	25	1.2	1	0.0	0	0.0	71	3.3
SE	0	0.0	3	0.1	16	0.7	47	2.2	67	3.1	49	2.3	3	0.1	185	8.5
SSE	0	0.0	5	0.2	26	1.2	40	1.8	59	2.7	24	1.1	0	0.0	154	7.1
S	0	0.0	5	0.2	34	1.6	41	1.9	16	0.7	1	0.0	1	0.0	98	4.5
SSW	0	0.0	7	0.3	40	1.8	53	2.4	30	1.4	1	0.0	0	0.0	131	6.0
SW	0	0.0	10	0.5	38	1.7	74	3.4	45	2.1	3	0.1	0	0.0	170	7.8
WSW	0	0.0	6	0.3	18	0.8	42	1.9	19	0.9	11	0.5	0	0.0	96	4.4
W	0	0.0	2	0.1	19	0.9	60	2.8	56	2.6	10	0.5	0	0.0	147	6.8
WNW	0	0.0	5	0.2	15	0.7	27	1.2	29	1.3	3	0.1	0	0.0	79	3.6
NW	0	0.0	1	0.0	13	0.6	41	1.9	64	2.9	21	1.0	7	0.3	147	6.8
NNW	0	0.0	1	0.0	9	0.4	37	1.7	35	1.6	13	0.6	1	0.0	96	4.4
	0	0.0	59	2.7	408	18.8	841	38.7	672	30.9	180	8.3	13	0.6	2173	100.0

MISSING HOURS: 11

MEAN WIND SPEED: 11.6

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	24	1.1	54	2.5	56	2.6	19	0.9	0	0.0	156	7.1
NNE	0	0.0	0	0.0	39	1.8	62	2.8	32	1.5	4	0.2	0	0.0	137	6.3
NE	0	0.0	0	0.0	23	1.1	104	4.8	79	3.6	15	0.7	1	0.0	222	10.2
ENE	0	0.0	5	0.2	45	2.1	91	4.2	41	1.9	5	0.2	0	0.0	187	8.6
E	0	0.0	3	0.1	32	1.5	44	2.0	19	0.9	0	0.0	0	0.0	98	4.5
ESE	0	0.0	3	0.1	17	0.8	25	1.1	25	1.1	1	0.0	0	0.0	71	3.3
SE	0	0.0	3	0.1	16	0.7	47	2.2	67	3.1	49	2.2	3	0.1	185	8.5
SSE	0	0.0	5	0.2	26	1.2	40	1.8	59	2.7	24	1.1	0	0.0	154	7.1
S	0	0.0	5	0.2	34	1.6	41	1.9	16	0.7	1	0.0	1	0.0	98	4.5
SSW	0	0.0	7	0.3	40	1.8	53	2.4	30	1.4	1	0.0	0	0.0	131	6.0
SW	0	0.0	10	0.5	38	1.7	74	3.4	45	2.1	3	0.1	0	0.0	170	7.8
WSW	0	0.0	6	0.3	18	0.8	43	2.0	20	0.9	11	0.5	0	0.0	98	4.5
W	0	0.0	2	0.1	20	0.9	60	2.7	61	2.8	10	0.5	0	0.0	153	7.0
WNW	0	0.0	5	0.2	15	0.7	27	1.2	30	1.4	3	0.1	0	0.0	80	3.7
NW	0	0.0	1	0.0	13	0.6	41	1.9	64	2.9	21	1.0	7	0.3	147	6.7
NNW	0	0.0	1	0.0	9	0.4	37	1.7	35	1.6	13	0.6	1	0.0	96	4.4
	0	0.0	59	2.7	409	18.7	843	38.6	679	31.1	180	8.2	13	0.6	2183	100.0

MISSING HOURS: 1

MEAN WIND SPEED: 11.6

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	4	0.2
NNE	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	5	0.2
NE	0	0.0	0	0.0	0	0.0	1	0.0	8	0.4	3	0.1	2	0.1	14	0.7
ENE	0	0.0	0	0.0	0	0.0	1	0.0	12	0.6	2	0.1	0	0.0	15	0.7
E	0	0.0	0	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	4	0.2
ESE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	3	0.1
SSE	0	0.0	0	0.0	0	0.0	3	0.1	4	0.2	2	0.1	0	0.0	9	0.4
S	0	0.0	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	3	0.1
SSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	3	0.1	3	0.1	1	0.0	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	1	0.0	3	0.1	0	0.0	1	0.0	2	0.1	7	0.3
W	0	0.0	0	0.0	0	0.0	2	0.1	10	0.5	4	0.2	0	0.0	16	0.7
WNW	0	0.0	0	0.0	0	0.0	1	0.0	5	0.2	1	0.0	0	0.0	7	0.3
NW	0	0.0	0	0.0	0	0.0	2	0.1	11	0.5	2	0.1	3	0.1	18	0.8
NNW	0	0.0	0	0.0	0	0.0	0	0.0	7	0.3	2	0.1	6	0.3	15	0.7
	0	0.0	0	0.0	4	0.2	20	0.9	73	3.4	19	0.9	13	0.6	129	6.0

MEAN WIND SPEED: 16.4  
 MISSING: 1

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)															
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	1	0.0	0	0.0	7	0.3
NNE	0	0.0	0	0.0	1	0.0	4	0.2	1	0.0	0	0.0	0	0.0	6	0.3
NE	0	0.0	0	0.0	0	0.0	2	0.1	4	0.2	1	0.0	1	0.0	8	0.4
ENE	0	0.0	0	0.0	1	0.0	3	0.1	5	0.2	0	0.0	0	0.0	9	0.4
E	0	0.0	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	3	0.1
ESE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	0	0.0	4	0.2
SSE	0	0.0	0	0.0	0	0.0	3	0.1	3	0.1	3	0.1	0	0.0	9	0.4
S	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	2	0.1	3	0.1	2	0.1	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1	2	0.1	6	0.3
W	0	0.0	0	0.0	1	0.0	4	0.2	2	0.1	2	0.1	0	0.0	9	0.4
WNW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	2	0.1
NW	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	1	0.0	0	0.0	7	0.3
NNW	0	0.0	0	0.0	0	0.0	4	0.2	5	0.2	3	0.1	3	0.1	15	0.7
	0	0.0	0	0.0	7	0.3	29	1.4	36	1.7	16	0.7	6	0.3	94	4.4

MEAN WIND SPEED: 15.0  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	8	0.4	2	0.1	2	0.1	0	0.0	12	0.6
NNE	0	0.0	0	0.0	1	0.0	6	0.3	2	0.1	0	0.0	0	0.0	9	0.4
NE	0	0.0	0	0.0	1	0.0	5	0.2	6	0.3	1	0.0	0	0.0	13	0.6
ENE	0	0.0	0	0.0	2	0.1	3	0.1	5	0.2	0	0.0	0	0.0	10	0.5
E	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SE	0	0.0	0	0.0	2	0.1	1	0.0	1	0.0	1	0.0	0	0.0	5	0.2
SSE	0	0.0	0	0.0	1	0.0	1	0.0	5	0.2	2	0.1	0	0.0	9	0.4
S	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
SSW	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SW	0	0.0	0	0.0	2	0.1	3	0.1	4	0.2	2	0.1	0	0.0	11	0.5
WSW	0	0.0	0	0.0	2	0.1	2	0.1	1	0.0	4	0.2	0	0.0	9	0.4
W	0	0.0	1	0.0	2	0.1	4	0.2	3	0.1	1	0.0	0	0.0	11	0.5
WNW	0	0.0	0	0.0	2	0.1	1	0.0	6	0.3	0	0.0	0	0.0	9	0.4
NW	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	2	0.1	2	0.1	10	0.5
NNW	0	0.0	0	0.0	0	0.0	12	0.6	5	0.2	2	0.1	1	0.0	20	0.9
	0	0.0	1	0.0	20	0.9	49	2.3	48	2.2	17	0.8	3	0.1	138	6.4

MEAN WIND SPEED: 12.9  
 MISSING: 1

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	11	0.5	22	1.0	17	0.8	7	0.3	1	0.0	58	2.7
NNE	0	0.0	0	0.0	13	0.6	14	0.7	13	0.6	9	0.4	2	0.1	51	2.4
NE	0	0.0	0	0.0	7	0.3	24	1.1	37	1.7	4	0.2	1	0.0	73	3.4
ENE	0	0.0	1	0.0	18	0.8	42	2.0	27	1.3	2	0.1	2	0.1	92	4.3
E	0	0.0	1	0.0	9	0.4	22	1.0	10	0.5	0	0.0	1	0.0	43	2.0
ESE	0	0.0	1	0.0	6	0.3	10	0.5	9	0.4	7	0.3	0	0.0	33	1.5
SE	0	0.0	0	0.0	10	0.5	9	0.4	21	1.0	13	0.6	2	0.1	55	2.6
SSE	0	0.0	1	0.0	11	0.5	16	0.7	25	1.2	18	0.8	2	0.1	73	3.4
S	0	0.0	3	0.1	16	0.7	23	1.1	13	0.6	1	0.0	0	0.0	56	2.6
SSW	0	0.0	0	0.0	8	0.4	16	0.7	16	0.7	8	0.4	0	0.0	48	2.2
SW	0	0.0	1	0.0	8	0.4	8	0.4	15	0.7	1	0.0	0	0.0	33	1.5
WSW	0	0.0	1	0.0	10	0.5	7	0.3	4	0.2	4	0.2	0	0.0	26	1.2
W	0	0.0	1	0.0	6	0.3	11	0.5	12	0.6	4	0.2	0	0.0	34	1.6
WNW	0	0.0	1	0.0	5	0.2	6	0.3	7	0.3	7	0.3	0	0.0	26	1.2
NW	0	0.0	0	0.0	6	0.3	10	0.5	15	0.7	11	0.5	1	0.0	43	2.0
NNW	0	0.0	2	0.1	6	0.3	14	0.7	4	0.2	10	0.5	3	0.1	39	1.8
	0	0.0	13	0.6	150	7.0	254	11.9	245	11.4	106	5.0	15	0.7	783	36.6

MEAN WIND SPEED: 12.5  
 MISSING: 15

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 300 FT  
DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	5	0.2	11	0.5	22	1.0	13	0.6	4	0.2	55	2.6
NNE	0	0.0	0	0.0	2	0.1	8	0.4	22	1.0	11	0.5	1	0.0	44	2.1
NE	0	0.0	0	0.0	3	0.1	17	0.8	28	1.3	9	0.4	0	0.0	57	2.7
ENE	0	0.0	0	0.0	10	0.5	25	1.2	18	0.8	2	0.1	0	0.0	55	2.6
E	0	0.0	2	0.1	11	0.5	19	0.9	12	0.6	1	0.0	0	0.0	45	2.1
ESE	0	0.0	0	0.0	5	0.2	15	0.7	6	0.3	1	0.0	0	0.0	27	1.3
SE	0	0.0	2	0.1	3	0.1	9	0.4	16	0.7	11	0.5	3	0.1	44	2.1
SSE	0	0.0	2	0.1	6	0.3	14	0.7	12	0.6	7	0.3	2	0.1	43	2.0
S	0	0.0	0	0.0	6	0.3	10	0.5	8	0.4	0	0.0	0	0.0	24	1.1
SSW	0	0.0	0	0.0	6	0.3	11	0.5	22	1.0	9	0.4	1	0.0	49	2.3
SW	0	0.0	0	0.0	9	0.4	12	0.6	32	1.5	6	0.3	0	0.0	59	2.8
WSW	0	0.0	5	0.2	8	0.4	15	0.7	13	0.6	1	0.0	0	0.0	42	2.0
W	0	0.0	0	0.0	10	0.5	11	0.5	14	0.7	5	0.2	0	0.0	40	1.9
WNW	0	0.0	0	0.0	3	0.1	4	0.2	17	0.8	4	0.2	0	0.0	28	1.3
NW	0	0.0	2	0.1	5	0.2	17	0.8	32	1.5	13	0.6	2	0.1	71	3.3
NNW	0	0.0	1	0.0	0	0.0	8	0.4	23	1.1	14	0.7	2	0.1	48	2.2
	0	0.0	14	0.7	92	4.3	206	9.6	297	13.9	107	5.0	15	0.7	731	34.1

MEAN WIND SPEED: 13.6  
MISSING: 14

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 300 FT  
DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
CLASS F

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	3	0.1	6	0.3	2	0.1	0	0.0	11	0.5
NNE	0	0.0	0	0.0	1	0.0	5	0.2	5	0.2	4	0.2	0	0.0	15	0.7
NE	0	0.0	0	0.0	1	0.0	1	0.0	3	0.1	4	0.2	0	0.0	9	0.4
ENE	0	0.0	0	0.0	2	0.1	1	0.0	1	0.0	1	0.0	0	0.0	5	0.2
E	0	0.0	0	0.0	1	0.0	2	0.1	1	0.0	1	0.0	0	0.0	5	0.2
ESE	0	0.0	0	0.0	2	0.1	2	0.1	2	0.1	0	0.0	0	0.0	6	0.3
SE	0	0.0	0	0.0	1	0.0	5	0.2	5	0.2	1	0.0	0	0.0	12	0.6
SSE	0	0.0	2	0.1	2	0.1	6	0.3	6	0.3	1	0.0	0	0.0	17	0.8
S	0	0.0	0	0.0	2	0.1	0	0.0	4	0.2	0	0.0	0	0.0	6	0.3
SSW	0	0.0	2	0.1	3	0.1	5	0.2	5	0.2	4	0.2	0	0.0	19	0.9
SW	0	0.0	0	0.0	3	0.1	6	0.3	9	0.4	9	0.4	0	0.0	27	1.3
WSW	0	0.0	0	0.0	4	0.2	8	0.4	6	0.3	3	0.1	0	0.0	21	1.0
W	0	0.0	0	0.0	1	0.0	2	0.1	11	0.5	2	0.1	0	0.0	16	0.7
WNW	0	0.0	0	0.0	1	0.0	2	0.1	9	0.4	6	0.3	0	0.0	18	0.8
NW	0	0.0	0	0.0	2	0.1	3	0.1	10	0.5	5	0.2	0	0.0	20	0.9
NNW	0	0.0	0	0.0	0	0.0	3	0.1	9	0.4	4	0.2	0	0.0	16	0.7
	0	0.0	4	0.2	26	1.2	54	2.5	92	4.3	47	2.2	0	0.0	223	10.4

MEAN WIND SPEED: 14.3  
MISSING: 2

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT
N	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0	2	0.1	0	0.0	4	0.2
SSE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	2	0.1
S	0	0.0	0	0.0	0	0.0	2	0.1	2	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	0	0.0	0	0.0	4	0.2
SW	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	3	0.1	0	0.0	5	0.2
WSW	0	0.0	0	0.0	0	0.0	4	0.2	1	0.0	0	0.0	0	0.0	5	0.2
W	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	2	0.1	0	0.0	7	0.3
WNW	0	0.0	0	0.0	2	0.1	3	0.1	1	0.0	0	0.0	0	0.0	6	0.3
NW	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	3	0.1
NNW	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1
	0	0.0	0	0.0	4	0.2	15	0.7	15	0.7	8	0.4	1	0.0	43	2.0

MEAN WIND SPEED: 13.9  
 MISSING: 0

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT			
N	0	0.0	0	0.0	16	0.7	44	2.1	56	2.6	27	1.3	5	0.2	148	6.9
NNE	0	0.0	0	0.0	18	0.8	38	1.8	48	2.2	24	1.1	3	0.1	131	6.1
NE	0	0.0	0	0.0	12	0.6	50	2.3	86	4.0	22	1.0	4	0.2	174	8.1
ENE	0	0.0	1	0.0	33	1.5	75	3.5	68	3.2	7	0.3	3	0.1	187	8.7
E	0	0.0	3	0.1	21	1.0	46	2.1	29	1.4	2	0.1	1	0.0	102	4.8
ESE	0	0.0	1	0.0	13	0.6	28	1.3	19	0.9	8	0.4	0	0.0	69	3.2
SE	0	0.0	2	0.1	17	0.8	26	1.2	47	2.2	30	1.4	5	0.2	127	5.9
SSE	0	0.0	5	0.2	20	0.9	44	2.1	55	2.6	34	1.6	4	0.2	162	7.6
S	0	0.0	3	0.1	27	1.3	39	1.8	26	1.2	1	0.0	0	0.0	96	4.5
SSW	0	0.0	2	0.1	20	0.9	35	1.6	45	2.1	21	1.0	1	0.0	124	5.8
SW	0	0.0	1	0.0	27	1.3	37	1.7	63	2.9	21	1.0	0	0.0	149	7.0
WSW	0	0.0	6	0.3	27	1.3	39	1.8	25	1.2	15	0.7	4	0.2	116	5.4
W	0	0.0	2	0.1	20	0.9	34	1.6	57	2.7	20	0.9	0	0.0	133	6.2
WNW	0	0.0	1	0.0	13	0.6	18	0.8	45	2.1	19	0.9	0	0.0	96	4.5
NW	0	0.0	2	0.1	13	0.6	33	1.5	82	3.8	34	1.6	8	0.4	172	8.0
NNW	0	0.0	3	0.1	6	0.3	41	1.9	55	2.6	35	1.6	15	0.7	155	7.2
	0	0.0	32	1.5	303	14.2	627	29.3	806	37.6	320	14.9	53	2.5	2141	100.0

MISSING HOURS: 43

MEAN WIND SPEED: 13.5

ARTIFICIAL ISLAND 4/99 - 6/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	16	0.7	44	2.0	56	2.6	27	1.3	5	0.2	148	6.9
NNE	0	0.0	0	0.0	18	0.8	38	1.8	48	2.2	24	1.1	3	0.1	131	6.1
NE	0	0.0	0	0.0	12	0.6	50	2.3	87	4.0	22	1.0	4	0.2	175	8.1
ENE	0	0.0	1	0.0	33	1.5	75	3.5	68	3.2	7	0.3	3	0.1	187	8.7
E	0	0.0	3	0.1	21	1.0	46	2.1	29	1.3	2	0.1	1	0.0	102	4.7
ESE	0	0.0	1	0.0	13	0.6	28	1.3	19	0.9	8	0.4	0	0.0	69	3.2
SE	0	0.0	2	0.1	17	0.8	26	1.2	47	2.2	30	1.4	5	0.2	127	5.9
SSE	0	0.0	5	0.2	20	0.9	44	2.0	55	2.6	34	1.6	4	0.2	162	7.5
S	0	0.0	3	0.1	27	1.3	39	1.8	26	1.2	1	0.0	0	0.0	96	4.5
SSW	0	0.0	2	0.1	20	0.9	35	1.6	45	2.1	21	1.0	1	0.0	124	5.8
SW	0	0.0	1	0.0	27	1.3	37	1.7	63	2.9	21	1.0	0	0.0	149	6.9
WSW	0	0.0	6	0.3	27	1.3	39	1.8	25	1.2	15	0.7	4	0.2	116	5.4
W	0	0.0	2	0.1	20	0.9	36	1.7	62	2.9	21	1.0	0	0.0	141	6.6
WNW	0	0.0	1	0.0	13	0.6	18	0.8	46	2.1	19	0.9	0	0.0	97	4.5
NW	0	0.0	2	0.1	13	0.6	33	1.5	82	3.8	34	1.6	8	0.4	172	8.0
NNW	0	0.0	3	0.1	6	0.3	41	1.9	55	2.6	35	1.6	15	0.7	155	7.2
	0	0.0	32	1.5	303	14.1	629	29.2	813	37.8	321	14.9	53	2.5	2151	100.0

MISSING HOURS: 33

MEAN WIND SPEED: 13.5

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)												SUM PERCENT					
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5				GE 24.6			
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT			
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	18	0.8
SE	0	0.0	0	0.0	1	0.0	7	0.3	10	0.5	0	0.0	0	0.0	0	0.0	14	0.6
SSE	0	0.0	0	0.0	1	0.0	9	0.4	4	0.2	0	0.0	0	0.0	0	0.0	4	0.2
S	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	4	0.2
WSW	0	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
W	0	0.0	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	0	0.0	4	0.2	26	1.2	15	0.7	0	0.0	0	0.0	45	2.0		

MEAN WIND SPEED: 11.2  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	2	0.1	0	0.0	0	0.0
S	0	0.0	0	0.0	4	0.2	3	0.1	4	0.2	0	0.0	0	0.0	7	0.3
SSW	0	0.0	0	0.0	7	0.3	0	0.0	0	0.0	0	0.0	0	0.0	11	0.5
SW	0	0.0	0	0.0	7	0.3	2	0.1	0	0.0	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	5	0.2	2	0.1	0	0.0	0	0.0	0	0.0	9	0.4
W	0	0.0	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	0	0.0	7	0.3
WNW	0	0.0	0	0.0	0	0.0	5	0.2	1	0.0	0	0.0	0	0.0	4	0.2
NW	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	6	0.3
NNW	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	0	0.0	0	0.0	2	0.1
	0	0.0	0	0.0	1	0.0	0	0.0	2	0.1	0	0.0	0	0.0	6	0.3
															3	0.1
	0	0.0	0	0.0	25	1.1	21	1.0	15	0.7	2	0.1	0	0.0	63	2.9
MEAN WIND SPEED:	9.9															
MISSING:	0															

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)												SUM PERCENT			
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5				GE 24.6	
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	
N	0	0.0	0	0.0	7	0.3	10	0.5	2	0.1	0	0.0	0	0.0	19	0.9
NNE	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	3	0.1
NE	0	0.0	0	0.0	2	0.1	7	0.3	3	0.1	0	0.0	0	0.0	12	0.5
ENE	0	0.0	0	0.0	3	0.1	3	0.1	0	0.0	0	0.0	0	0.0	6	0.3
E	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
ESE	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SE	0	0.0	1	0.0	2	0.1	10	0.5	5	0.2	2	0.1	0	0.0	20	0.9
SSE	0	0.0	0	0.0	5	0.2	9	0.4	5	0.2	0	0.0	0	0.0	19	0.9
S	0	0.0	0	0.0	15	0.7	6	0.3	0	0.0	0	0.0	0	0.0	21	1.0
SSW	0	0.0	1	0.0	4	0.2	2	0.1	0	0.0	0	0.0	0	0.0	7	0.3
SW	0	0.0	0	0.0	11	0.5	1	0.0	1	0.0	0	0.0	0	0.0	13	0.6
WSW	0	0.0	1	0.0	3	0.1	5	0.2	1	0.0	0	0.0	0	0.0	10	0.5
W	0	0.0	0	0.0	4	0.2	5	0.2	0	0.0	0	0.0	0	0.0	9	0.4
WNW	0	0.0	1	0.0	2	0.1	5	0.2	1	0.0	0	0.0	0	0.0	9	0.4
NW	0	0.0	0	0.0	3	0.1	4	0.2	5	0.2	0	0.0	0	0.0	12	0.5
NNW	0	0.0	0	0.0	2	0.1	6	0.3	1	0.0	0	0.0	0	0.0	9	0.4
	0	0.0	4	0.2	67	3.0	76	3.4	24	1.1	2	0.1	0	0.0	173	7.8

MEAN WIND SPEED: 8.8  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	6	0.3	24	1.1	29	1.3	11	0.5	0	0.0	2	0.1	72	3.3
NNE	0	0.0	7	0.3	14	0.6	28	1.3	1	0.0	1	0.0	0	0.0	51	2.3
NE	0	0.0	6	0.3	12	0.5	35	1.6	24	1.1	2	0.1	0	0.0	79	3.6
ENE	0	0.0	1	0.0	16	0.7	16	0.7	5	0.2	0	0.0	0	0.0	38	1.7
E	0	0.0	1	0.0	15	0.7	17	0.8	1	0.0	0	0.0	0	0.0	34	1.5
ESE	0	0.0	0	0.0	5	0.2	11	0.5	2	0.1	0	0.0	0	0.0	18	0.8
SE	0	0.0	3	0.1	4	0.2	36	1.6	48	2.2	8	0.4	0	0.0	99	4.5
SSE	0	0.0	2	0.1	30	1.4	48	2.2	48	2.2	5	0.2	0	0.0	133	6.0
S	0	0.0	2	0.1	29	1.3	37	1.7	25	1.1	2	0.1	0	0.0	95	4.3
SSW	0	0.0	3	0.1	32	1.5	32	1.5	9	0.4	2	0.1	0	0.0	78	3.5
SW	0	0.0	0	0.0	27	1.2	28	1.3	9	0.4	0	0.0	0	0.0	64	2.9
WSW	0	0.0	2	0.1	13	0.6	14	0.6	5	0.2	0	0.0	0	0.0	34	1.5
W	0	0.0	0	0.0	12	0.5	33	1.5	8	0.4	0	0.0	0	0.0	53	2.4
WNW	0	0.0	0	0.0	9	0.4	26	1.2	4	0.2	1	0.0	0	0.0	40	1.8
NW	0	0.0	4	0.2	12	0.5	20	0.9	7	0.3	6	0.3	2	0.1	51	2.3
NNW	0	0.0	4	0.2	14	0.6	16	0.7	8	0.4	0	0.0	1	0.0	43	1.9
	0	0.0	41	1.9	268	12.1	426	19.3	215	9.7	27	1.2	5	0.2	982	44.5
MEAN WIND SPEED:	9.9															
MISSING:	0															

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	15	0.7	17	0.8	3	0.1	2	0.1	0	0.0	40	1.8
NNE	0	0.0	6	0.3	29	1.3	29	1.3	6	0.3	0	0.0	0	0.0	70	3.2
NE	0	0.0	4	0.2	29	1.3	24	1.1	2	0.1	2	0.1	0	0.0	61	2.8
ENE	0	0.0	7	0.3	25	1.1	5	0.2	0	0.0	0	0.0	0	0.0	37	1.7
E	0	0.0	8	0.4	23	1.0	8	0.4	1	0.0	0	0.0	0	0.0	40	1.8
ESE	0	0.0	0	0.0	25	1.1	3	0.1	0	0.0	0	0.0	0	0.0	28	1.3
SE	0	0.0	1	0.0	14	0.6	25	1.1	9	0.4	0	0.0	0	0.0	49	2.2
SSE	0	0.0	0	0.0	8	0.4	17	0.8	8	0.4	1	0.0	0	0.0	34	1.5
S	0	0.0	1	0.0	13	0.6	14	0.6	5	0.2	0	0.0	0	0.0	33	1.5
SSW	0	0.0	0	0.0	15	0.7	27	1.2	1	0.0	0	0.0	0	0.0	43	1.9
SW	0	0.0	1	0.0	31	1.4	32	1.5	2	0.1	0	0.0	0	0.0	66	3.0
WSW	0	0.0	2	0.1	24	1.1	19	0.9	1	0.0	0	0.0	0	0.0	46	2.1
W	0	0.0	5	0.2	20	0.9	8	0.4	0	0.0	0	0.0	0	0.0	33	1.5
WNW	0	0.0	2	0.1	26	1.2	20	0.9	0	0.0	0	0.0	0	0.0	48	2.2
NW	0	0.0	3	0.1	30	1.4	28	1.3	2	0.1	0	0.0	0	0.0	63	2.9
NNW	0	0.0	4	0.2	21	1.0	17	0.8	1	0.0	0	0.0	1	0.0	44	2.0
	0	0.0	47	2.1	348	15.8	293	13.3	41	1.9	5	0.2	1	0.0	735	33.3

MEAN WIND SPEED: 7.6  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	1	0.0	9	0.4	15	0.7	0	0.0	0	0.0	0	0.0	25	1.1
NNE	0	0.0	2	0.1	21	1.0	8	0.4	0	0.0	0	0.0	0	0.0	31	1.4
NE	0	0.0	6	0.3	9	0.4	3	0.1	0	0.0	0	0.0	0	0.0	18	0.8
ENE	0	0.0	4	0.2	7	0.3	0	0.0	0	0.0	0	0.0	0	0.0	11	0.5
E	0	0.0	5	0.2	6	0.3	0	0.0	0	0.0	0	0.0	0	0.0	11	0.5
ESE	0	0.0	1	0.0	14	0.6	0	0.0	0	0.0	0	0.0	0	0.0	15	0.7
SE	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SSE	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	5	0.2
S	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
SW	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	0	0.0	1	0.0
WSW	0	0.0	1	0.0	13	0.6	2	0.1	0	0.0	0	0.0	0	0.0	4	0.2
W	0	0.0	0	0.0	11	0.5	1	0.0	0	0.0	0	0.0	0	0.0	16	0.7
WNW	0	0.0	0	0.0	6	0.3	6	0.3	0	0.0	0	0.0	0	0.0	12	0.5
NW	0	0.0	1	0.0	7	0.3	2	0.1	0	0.0	0	0.0	0	0.0	12	0.5
NNW	0	0.0	2	0.1	14	0.6	8	0.4	0	0.0	0	0.0	0	0.0	10	0.5
	0	0.0	23	1.0	125	5.7	50	2.3	1	0.0	0	0.0	0	0.0	199	9.0

MEAN WIND SPEED: 6.2  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ENE	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
E	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
W	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	1	0.0	8	0.4	0	0.0	0	0.0	0	0.0	0	0.0	9	0.4

MEAN WIND SPEED: 5.2  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	10	0.5	56	2.5	71	3.2	16	0.7	2	0.1	2	0.1	157	7.1
NNE	0	0.0	15	0.7	65	2.9	67	3.0	7	0.3	1	0.0	0	0.0	155	7.0
NE	0	0.0	17	0.8	53	2.4	69	3.1	29	1.3	4	0.2	0	0.0	172	7.8
ENE	0	0.0	12	0.5	56	2.5	24	1.1	5	0.2	0	0.0	0	0.0	97	4.4
E	0	0.0	14	0.6	46	2.1	26	1.2	2	0.1	0	0.0	0	0.0	88	4.0
ESE	0	0.0	1	0.0	47	2.1	14	0.6	2	0.1	0	0.0	0	0.0	64	2.9
SE	0	0.0	5	0.2	21	1.0	82	3.7	75	3.4	12	0.5	0	0.0	195	8.8
SSE	0	0.0	2	0.1	51	2.3	88	4.0	69	3.1	6	0.3	0	0.0	216	9.8
S	0	0.0	3	0.1	68	3.1	59	2.7	30	1.4	2	0.1	0	0.0	162	7.3
SSW	0	0.0	4	0.2	59	2.7	64	2.9	10	0.5	2	0.1	0	0.0	139	6.3
SW	0	0.0	1	0.0	76	3.4	66	3.0	12	0.5	0	0.0	0	0.0	155	7.0
WSW	0	0.0	6	0.3	53	2.4	48	2.2	7	0.3	0	0.0	0	0.0	114	5.2
W	0	0.0	5	0.2	47	2.1	54	2.4	10	0.5	0	0.0	0	0.0	116	5.3
WNW	0	0.0	3	0.1	43	1.9	59	2.7	5	0.2	1	0.0	0	0.0	111	5.0
NW	0	0.0	8	0.4	52	2.4	54	2.4	20	0.9	6	0.3	2	0.1	142	6.4
NNW	0	0.0	10	0.5	52	2.4	47	2.1	12	0.5	0	0.0	2	0.1	123	5.6
	0	0.0	116	5.3	845	38.3	892	40.4	311	14.1	36	1.6	6	0.3	2206	100.0
MEAN WIND SPEED:	8.7															
															MISSING HOURS:	2

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)												SUM PERCENT			
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	10	0.5	56	2.5	71	3.2	16	0.7	2	0.1	2	0.1	157	7.1
NNE	0	0.0	15	0.7	65	2.9	67	3.0	7	0.3	1	0.0	0	0.0	155	7.0
NE	0	0.0	17	0.8	53	2.4	69	3.1	29	1.3	4	0.2	0	0.0	172	7.8
ENE	0	0.0	12	0.5	56	2.5	24	1.1	5	0.2	0	0.0	0	0.0	97	4.4
E	0	0.0	14	0.6	46	2.1	26	1.2	2	0.1	0	0.0	0	0.0	88	4.0
ESE	0	0.0	1	0.0	47	2.1	14	0.6	2	0.1	0	0.0	0	0.0	64	2.9
SE	0	0.0	5	0.2	21	1.0	82	3.7	75	3.4	12	0.5	0	0.0	195	8.8
SSE	0	0.0	2	0.1	51	2.3	88	4.0	69	3.1	6	0.3	0	0.0	216	9.8
S	0	0.0	3	0.1	68	3.1	60	2.7	30	1.4	2	0.1	0	0.0	163	7.4
SSW	0	0.0	4	0.2	60	2.7	64	2.9	10	0.5	2	0.1	0	0.0	140	6.3
SW	0	0.0	1	0.0	76	3.4	66	3.0	12	0.5	0	0.0	0	0.0	155	7.0
WSW	0	0.0	6	0.3	53	2.4	48	2.2	7	0.3	0	0.0	0	0.0	114	5.2
W	0	0.0	5	0.2	47	2.1	54	2.4	10	0.5	0	0.0	0	0.0	116	5.3
WNW	0	0.0	3	0.1	43	1.9	59	2.7	5	0.2	1	0.0	0	0.0	111	5.0
NW	0	0.0	8	0.4	52	2.4	54	2.4	20	0.9	6	0.3	2	0.1	142	6.4
NNW	0	0.0	10	0.5	52	2.4	47	2.1	12	0.5	0	0.0	2	0.1	123	5.6
	0	0.0	116	5.3	846	38.3	893	40.4	311	14.1	36	1.6	6	0.3	2208	100.0

MISSING HOURS: 0

MEAN WIND SPEED: 8.7

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	11	0.5	4	0.2	0	0.0	22	1.0
SE	0	0.0	0	0.0	0	0.0	7	0.3	5	0.2	2	0.1	0	0.0	10	0.5
SSE	0	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	4	0.2
S	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
WSW	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	3	0.1
W	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	0	0.0	2	0.1	15	0.7	22	1.0	6	0.3	0	0.0	45	2.1

MEAN WIND SPEED: 13.8  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	
N	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1	10	0.5
SE	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	2	0.1	0	0.0	9	0.4
SSE	0	0.0	0	0.0	4	0.2	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
S	0	0.0	0	0.0	4	0.2	0	0.0	0	0.0	0	0.0	0	0.0	7	0.3
SSW	0	0.0	0	0.0	4	0.2	2	0.1	1	0.0	0	0.0	0	0.0	11	0.5
SW	0	0.0	0	0.0	8	0.4	3	0.1	0	0.0	0	0.0	0	0.0	4	0.2
WSW	0	0.0	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	0	0.0	5	0.2	2	0.1	0	0.0	0	0.0	2	0.1
WNW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	3	0.1
NW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	3	0.1
NNW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	2	0.1	0	0.0	3	0.1
	0	0.0	0	0.0	21	1.0	16	0.7	11	0.5	10	0.5	3	0.1	61	2.8

MEAN WIND SPEED: 11.8  
 MISSING: 2

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	4	0.2	12	0.6	0	0.0	1	0.0	0	0.0	17	0.8
NNE	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
NE	0	0.0	0	0.0	2	0.1	5	0.2	5	0.2	1	0.0	0	0.0	13	0.6
ENE	0	0.0	0	0.0	2	0.1	3	0.1	0	0.0	0	0.0	0	0.0	5	0.2
E	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
ESE	0	0.0	1	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
SE	0	0.0	1	0.0	3	0.1	6	0.3	9	0.4	4	0.2	3	0.1	26	1.2
SSE	0	0.0	0	0.0	2	0.1	5	0.2	3	0.1	2	0.1	0	0.0	12	0.6
S	0	0.0	0	0.0	2	0.1	6	0.3	0	0.0	0	0.0	0	0.0	15	0.7
SSW	0	0.0	0	0.0	9	0.4	6	0.3	0	0.0	0	0.0	0	0.0	11	0.5
S	0	0.0	1	0.0	8	0.4	1	0.0	1	0.0	0	0.0	0	0.0	13	0.6
SSW	0	0.0	1	0.0	6	0.3	4	0.2	0	0.0	2	0.1	0	0.0	12	0.6
SW	0	0.0	0	0.0	5	0.2	5	0.2	2	0.1	0	0.0	0	0.0	10	0.5
WSW	0	0.0	0	0.0	2	0.1	6	0.3	2	0.1	0	0.0	0	0.0	9	0.4
W	0	0.0	0	0.0	2	0.1	5	0.2	0	0.0	1	0.0	0	0.0	10	0.5
WNW	0	0.0	1	0.0	2	0.1	4	0.2	0	0.0	4	0.2	0	0.0	10	0.5
NW	0	0.0	0	0.0	2	0.1	4	0.2	0	0.0	4	0.2	0	0.0	12	0.6
NNW	0	0.0	0	0.0	1	0.0	6	0.3	3	0.1	2	0.1	0	0.0	12	0.6
	0	0.0	5	0.2	51	2.3	71	3.3	25	1.1	17	0.8	3	0.1	172	7.9

MEAN WIND SPEED: 10.6  
 MISSING: 1

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	4	0.2	14	0.6	30	1.4	14	0.6	8	0.4	0	0.0	70	3.2
NNE	0	0.0	1	0.0	16	0.7	21	1.0	7	0.3	1	0.0	0	0.0	46	2.1
NE	0	0.0	3	0.1	6	0.3	22	1.0	35	1.6	11	0.5	1	0.0	78	3.6
ENE	0	0.0	1	0.0	7	0.3	13	0.6	16	0.7	1	0.0	0	0.0	38	1.7
E	0	0.0	0	0.0	9	0.4	9	0.4	14	0.6	0	0.0	0	0.0	32	1.5
ESE	0	0.0	0	0.0	4	0.2	8	0.4	5	0.2	2	0.1	0	0.0	19	0.9
SE	0	0.0	2	0.1	2	0.1	6	0.3	38	1.7	35	1.6	14	0.6	97	4.4
SSE	0	0.0	1	0.0	26	1.2	27	1.2	58	2.7	20	0.9	5	0.2	137	6.3
S	0	0.0	3	0.1	18	0.8	33	1.5	32	1.5	11	0.5	0	0.0	97	4.4
SSW	0	0.0	2	0.1	19	0.9	34	1.6	12	0.6	10	0.5	1	0.0	78	3.6
SW	0	0.0	2	0.1	15	0.7	20	0.9	18	0.8	3	0.1	0	0.0	58	2.7
WSW	0	0.0	0	0.0	7	0.3	16	0.7	10	0.5	1	0.0	0	0.0	34	1.6
W	0	0.0	1	0.0	10	0.5	28	1.3	24	1.1	1	0.0	0	0.0	64	2.9
WNW	0	0.0	2	0.1	4	0.2	16	0.7	9	0.4	2	0.1	1	0.0	34	1.6
NW	0	0.0	2	0.1	10	0.5	13	0.6	15	0.7	4	0.2	0	0.0	44	2.0
NNW	0	0.0	0	0.0	15	0.7	16	0.7	4	0.2	5	0.2	0	0.0	40	1.8
	0	0.0	24	1.1	182	8.3	312	14.3	311	14.3	115	5.3	22	1.0	966	44.3

MEAN WIND SPEED: 12.4  
 MISSING: 16

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	3	0.1	10	0.5	15	0.7	5	0.2	0	0.0	33	1.5
NNE	0	0.0	1	0.0	13	0.6	18	0.8	24	1.1	1	0.0	0	0.0	57	2.6
NE	0	0.0	3	0.1	11	0.5	25	1.1	26	1.2	2	0.1	2	0.1	69	3.2
ENE	0	0.0	0	0.0	7	0.3	22	1.0	6	0.3	0	0.0	0	0.0	35	1.6
E	0	0.0	1	0.0	9	0.4	17	0.8	7	0.3	1	0.0	0	0.0	35	1.6
ESE	0	0.0	2	0.1	7	0.3	11	0.5	4	0.2	0	0.0	0	0.0	24	1.1
SE	0	0.0	1	0.0	3	0.1	29	1.3	21	1.0	6	0.3	0	0.0	60	2.8
SSE	0	0.0	1	0.0	8	0.4	10	0.5	9	0.4	3	0.1	1	0.0	32	1.5
S	0	0.0	0	0.0	6	0.3	11	0.5	10	0.5	4	0.2	0	0.0	31	1.4
SSW	0	0.0	0	0.0	6	0.3	31	1.4	13	0.6	1	0.0	0	0.0	51	2.3
SW	0	0.0	0	0.0	9	0.4	38	1.7	21	1.0	2	0.1	0	0.0	70	3.2
WSW	0	0.0	2	0.1	11	0.5	26	1.2	4	0.2	0	0.0	0	0.0	43	2.0
W	0	0.0	0	0.0	17	0.8	28	1.3	0	0.0	1	0.0	0	0.0	46	2.1
WNW	0	0.0	1	0.0	8	0.4	27	1.2	9	0.4	0	0.0	0	0.0	45	2.1
NW	0	0.0	1	0.0	9	0.4	24	1.1	22	1.0	0	0.0	0	0.0	56	2.6
NNW	0	0.0	0	0.0	10	0.5	13	0.6	15	0.7	3	0.1	0	0.0	41	1.9
	0	0.0	13	0.6	137	6.3	340	15.6	206	9.4	29	1.3	3	0.1	728	33.4

MEAN WIND SPEED: 10.9  
 MISSING: 7

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	2	0.1	4	0.2	11	0.5	2	0.1	0	0.0	19	0.9
NNE	0	0.0	1	0.0	2	0.1	17	0.8	8	0.4	0	0.0	0	0.0	28	1.3
NE	0	0.0	0	0.0	0	0.0	4	0.2	9	0.4	0	0.0	0	0.0	13	0.6
ENE	0	0.0	0	0.0	3	0.1	5	0.2	2	0.1	0	0.0	0	0.0	10	0.5
E	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	1	0.0	7	0.3	12	0.6	1	0.0	0	0.0	0	0.0	21	1.0
SE	0	0.0	2	0.1	1	0.0	5	0.2	2	0.1	0	0.0	0	0.0	10	0.5
SSE	0	0.0	0	0.0	1	0.0	4	0.2	2	0.1	0	0.0	0	0.0	7	0.3
S	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	3	0.1
SSW	0	0.0	1	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SW	0	0.0	1	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	6	0.3
WSW	0	0.0	0	0.0	2	0.1	7	0.3	3	0.1	0	0.0	0	0.0	12	0.6
W	0	0.0	1	0.0	2	0.1	11	0.5	2	0.1	0	0.0	0	0.0	16	0.7
WNW	0	0.0	0	0.0	4	0.2	10	0.5	4	0.2	0	0.0	0	0.0	18	0.8
NW	0	0.0	0	0.0	1	0.0	4	0.2	1	0.0	0	0.0	0	0.0	6	0.3
NNW	0	0.0	0	0.0	3	0.1	14	0.6	8	0.4	0	0.0	0	0.0	25	1.1
	0	0.0	7	0.3	32	1.5	105	4.8	53	2.4	2	0.1	0	0.0	199	9.1

MEAN WIND SPEED: 10.4  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT			
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6					
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT				
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
ESE	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	5	0.2
SE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
W	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	0	0.0	0	0.0	7	0.3	2	0.1	0	0.0	0	0.0	9	0.4		

MEAN WIND SPEED: 10.5  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	4	0.2	23	1.1	57	2.6	40	1.8	16	0.7	0	0.0	140	6.4
NNE	0	0.0	3	0.1	32	1.5	57	2.6	39	1.8	2	0.1	0	0.0	133	6.1
NE	0	0.0	6	0.3	19	0.9	57	2.6	75	3.4	14	0.6	3	0.1	174	8.0
ENE	0	0.0	1	0.0	19	0.9	43	2.0	24	1.1	1	0.0	0	0.0	88	4.0
E	0	0.0	1	0.0	20	0.9	30	1.4	21	1.0	1	0.0	0	0.0	73	3.3
ESE	0	0.0	4	0.2	20	0.9	35	1.6	12	0.6	2	0.1	0	0.0	73	3.3
SE	0	0.0	6	0.3	10	0.5	54	2.5	83	3.8	52	2.4	20	0.9	225	10.3
SSE	0	0.0	2	0.1	41	1.9	50	2.3	79	3.6	29	1.3	6	0.3	207	9.5
S	0	0.0	3	0.1	40	1.8	54	2.5	42	1.9	15	0.7	0	0.0	154	7.1
SSW	0	0.0	4	0.2	38	1.7	70	3.2	27	1.2	11	0.5	1	0.0	151	6.9
SW	0	0.0	4	0.2	38	1.7	71	3.3	39	1.8	7	0.3	0	0.0	159	7.3
WSW	0	0.0	2	0.1	25	1.1	57	2.6	24	1.1	1	0.0	0	0.0	109	5.0
W	0	0.0	2	0.1	31	1.4	78	3.6	33	1.5	2	0.1	0	0.0	146	6.7
WNW	0	0.0	4	0.2	18	0.8	58	2.7	23	1.1	4	0.2	1	0.0	108	5.0
NW	0	0.0	3	0.1	22	1.0	45	2.1	39	1.8	10	0.5	0	0.0	119	5.5
NNW	0	0.0	0	0.0	29	1.3	50	2.3	30	1.4	12	0.6	0	0.0	121	5.6
	0	0.0	49	2.2	425	19.5	866	39.7	630	28.9	179	8.2	31	1.4	2180	100.0

MISSING HOURS: 28

MEAN WIND SPEED: 11.6

Artificial Island

Joint Frequencies

7/1/99 – 9/30/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	4	0.2	23	1.1	57	2.6	40	1.8	16	0.7	0	0.0	140	6.4
NNE	0	0.0	3	0.1	32	1.5	57	2.6	39	1.8	2	0.1	0	0.0	133	6.1
NE	0	0.0	6	0.3	19	0.9	57	2.6	75	3.4	14	0.6	3	0.1	174	8.0
ENE	0	0.0	1	0.0	19	0.9	43	2.0	24	1.1	1	0.0	0	0.0	88	4.0
E	0	0.0	1	0.0	20	0.9	30	1.4	21	1.0	1	0.0	0	0.0	73	3.3
ESE	0	0.0	4	0.2	20	0.9	35	1.6	12	0.5	2	0.1	0	0.0	73	3.3
SE	0	0.0	6	0.3	10	0.5	54	2.5	83	3.8	52	2.4	20	0.9	225	10.3
SSE	0	0.0	2	0.1	41	1.9	50	2.3	79	3.6	29	1.3	6	0.3	207	9.5
S	0	0.0	3	0.1	41	1.9	54	2.5	42	1.9	15	0.7	0	0.0	155	7.1
SSW	0	0.0	4	0.2	39	1.8	70	3.2	27	1.2	11	0.5	1	0.0	152	7.0
SW	0	0.0	4	0.2	38	1.7	71	3.3	39	1.8	7	0.3	0	0.0	159	7.3
WSW	0	0.0	2	0.1	25	1.1	57	2.6	24	1.1	1	0.0	0	0.0	109	5.0
W	0	0.0	2	0.1	31	1.4	78	3.6	33	1.5	2	0.1	0	0.0	146	6.7
WNW	0	0.0	4	0.2	18	0.8	58	2.7	23	1.1	4	0.2	1	0.0	108	4.9
NW	0	0.0	3	0.1	22	1.0	45	2.1	39	1.8	10	0.5	0	0.0	119	5.5
NNW	0	0.0	0	0.0	29	1.3	50	2.3	30	1.4	12	0.5	0	0.0	121	5.5
	0	0.0	49	2.2	427	19.6	866	39.7	630	28.9	179	8.2	31	1.4	2182	100.0

MISSING HOURS: 26

MEAN WIND SPEED: 11.6

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT			
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6					
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	8	0.4	3	0.1	3	0.1	1	0.0	0	0.0	0	0.0
SSE	0	0.0	0	0.0	1	0.0	4	0.2	12	0.5	2	0.1	0	0.0	0	0.0	15	0.7
S	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	19	0.9
SSW	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
WSW	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	1	0.0
W	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	2	0.1
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	0	0.0	2	0.1	14	0.6	23	1.0	5	0.2	1	0.0	45	2.0		

MEAN WIND SPEED: 13.7  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
BY ATMOSPHERIC STABILITY CLASS

WIND: 300 FT  
DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
CLASS B

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	1	0.0	3	0.1	8	0.4
SSE	0	0.0	0	0.0	4	0.2	1	0.0	2	0.1	4	0.2	0	0.0	11	0.5
S	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	3	0.1	1	0.0	1	0.0	0	0.0	0	0.0	5	0.2
SW	0	0.0	0	0.0	7	0.3	5	0.2	0	0.0	0	0.0	0	0.0	12	0.5
WSW	0	0.0	0	0.0	4	0.2	1	0.0	2	0.1	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	0	0.0	3	0.1	4	0.2	0	0.0	0	0.0	7	0.3
WNW	0	0.0	0	0.0	0	0.0	1	0.0	2	0.1	1	0.0	0	0.0	4	0.2
NW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	3	0.1	0	0.0	4	0.2
NNW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	2	0.1	0	0.0	3	0.1
	0	0.0	1	0.0	20	0.9	14	0.6	14	0.6	11	0.5	3	0.1	63	2.9

MEAN WIND SPEED: 12.2  
MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	5	0.2	11	0.5	0	0.0	1	0.0	0	0.0	17	0.8
NNE	0	0.0	0	0.0	1	0.0	2	0.1	2	0.1	1	0.0	0	0.0	6	0.3
NE	0	0.0	0	0.0	1	0.0	4	0.2	3	0.1	1	0.0	0	0.0	9	0.4
ENE	0	0.0	0	0.0	2	0.1	2	0.1	0	0.0	0	0.0	0	0.0	4	0.2
E	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
ESE	0	0.0	2	0.1	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	5	0.2
SE	0	0.0	0	0.0	2	0.1	2	0.1	3	0.1	3	0.1	4	0.2	14	0.6
SSE	0	0.0	2	0.1	4	0.2	9	0.4	8	0.4	3	0.1	0	0.0	26	1.2
S	0	0.0	0	0.0	2	0.1	4	0.2	1	0.0	0	0.0	0	0.0	7	0.3
SSW	0	0.0	0	0.0	6	0.3	2	0.1	2	0.1	0	0.0	0	0.0	10	0.5
SW	0	0.0	2	0.1	9	0.4	4	0.2	0	0.0	1	0.0	0	0.0	16	0.7
WSW	0	0.0	1	0.0	5	0.2	5	0.2	1	0.0	1	0.0	0	0.0	13	0.6
W	0	0.0	0	0.0	3	0.1	2	0.1	6	0.3	0	0.0	0	0.0	11	0.5
WNW	0	0.0	1	0.0	1	0.0	5	0.2	1	0.0	0	0.0	0	0.0	8	0.4
NW	0	0.0	0	0.0	3	0.1	5	0.2	0	0.0	6	0.3	0	0.0	14	0.6
NNW	0	0.0	0	0.0	1	0.0	7	0.3	2	0.1	2	0.1	0	0.0	12	0.5
	0	0.0	8	0.4	47	2.1	66	3.0	29	1.3	19	0.9	4	0.2	173	7.8

MEAN WIND SPEED: 10.9  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	11	0.5	31	1.4	12	0.5	11	0.5	0	0.0	66	3.0
NNE	0	0.0	3	0.1	14	0.6	13	0.6	17	0.8	8	0.4	4	0.2	59	2.7
NE	0	0.0	1	0.0	4	0.2	9	0.4	33	1.5	18	0.8	1	0.0	66	3.0
ENE	0	0.0	1	0.0	5	0.2	13	0.6	12	0.5	4	0.2	0	0.0	35	1.6
E	0	0.0	0	0.0	8	0.4	9	0.4	13	0.6	1	0.0	0	0.0	31	1.4
ESE	0	0.0	1	0.0	4	0.2	2	0.1	5	0.2	4	0.2	1	0.0	17	0.8
SE	0	0.0	4	0.2	1	0.0	5	0.2	16	0.7	36	1.6	15	0.7	77	3.5
SSE	0	0.0	7	0.3	11	0.5	22	1.0	69	3.1	21	1.0	8	0.4	138	6.3
S	0	0.0	4	0.2	19	0.9	29	1.3	32	1.5	11	0.5	3	0.1	98	4.4
SSW	0	0.0	2	0.1	22	1.0	37	1.7	17	0.8	8	0.4	5	0.2	91	4.1
SW	0	0.0	1	0.0	11	0.5	14	0.6	20	0.9	7	0.3	1	0.0	54	2.4
WSW	0	0.0	2	0.1	7	0.3	15	0.7	11	0.5	3	0.1	1	0.0	39	1.8
W	0	0.0	2	0.1	8	0.4	24	1.1	25	1.1	3	0.1	0	0.0	62	2.8
WNW	0	0.0	2	0.1	6	0.3	19	0.9	14	0.6	3	0.1	3	0.1	47	2.1
NW	0	0.0	3	0.1	11	0.5	11	0.5	20	0.9	8	0.4	7	0.3	60	2.7
NNW	0	0.0	0	0.0	9	0.4	18	0.8	6	0.3	7	0.3	2	0.1	42	1.9
	0	0.0	34	1.5	151	6.8	271	12.3	322	14.6	153	6.9	51	2.3	982	44.5

MEAN WIND SPEED: 13.5  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	5	0.2	12	0.5	12	0.5	10	0.5	3	0.1	44	2.0
NNE	0	0.0	0	0.0	8	0.4	10	0.5	10	0.5	28	1.3	1	0.0	57	2.6
NE	0	0.0	1	0.0	2	0.1	10	0.5	24	1.1	15	0.7	2	0.1	54	2.4
ENE	0	0.0	1	0.0	4	0.2	14	0.6	18	0.8	0	0.0	0	0.0	37	1.7
E	0	0.0	1	0.0	8	0.4	11	0.5	13	0.6	0	0.0	0	0.0	33	1.5
ESE	0	0.0	0	0.0	5	0.2	7	0.3	6	0.3	3	0.1	0	0.0	21	1.0
SE	0	0.0	1	0.0	3	0.1	16	0.7	18	0.8	2	0.1	0	0.0	40	1.8
SSE	0	0.0	2	0.1	9	0.4	12	0.5	16	0.7	10	0.5	1	0.0	50	2.3
S	0	0.0	1	0.0	8	0.4	11	0.5	8	0.4	5	0.2	0	0.0	33	1.5
SSW	0	0.0	1	0.0	6	0.3	7	0.3	34	1.5	3	0.1	0	0.0	51	2.3
SW	0	0.0	0	0.0	5	0.2	18	0.8	37	1.7	9	0.4	0	0.0	69	3.1
WSW	0	0.0	1	0.0	3	0.1	16	0.7	20	0.9	4	0.2	0	0.0	44	2.0
W	0	0.0	0	0.0	19	0.9	21	1.0	11	0.5	1	0.0	0	0.0	52	2.4
WNW	0	0.0	0	0.0	9	0.4	18	0.8	12	0.5	2	0.1	0	0.0	41	1.9
NW	0	0.0	0	0.0	3	0.1	15	0.7	29	1.3	10	0.5	0	0.0	57	2.6
NNW	0	0.0	0	0.0	5	0.2	18	0.8	21	1.0	5	0.2	3	0.1	52	2.4
	0	0.0	11	0.5	102	4.6	216	9.8	289	13.1	107	4.9	10	0.5	735	33.3

MEAN WIND SPEED: 13.2  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	2	0.1	4	0.2	12	0.5	4	0.2	0	0.0	22	1.0
NNE	0	0.0	0	0.0	0	0.0	2	0.1	13	0.6	6	0.3	0	0.0	21	1.0
NE	0	0.0	0	0.0	1	0.0	1	0.0	4	0.2	11	0.5	0	0.0	17	0.8
ENE	0	0.0	0	0.0	1	0.0	2	0.1	2	0.1	1	0.0	0	0.0	6	0.3
E	0	0.0	1	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	6	0.3
ESE	0	0.0	0	0.0	2	0.1	2	0.1	1	0.0	0	0.0	0	0.0	5	0.2
SE	0	0.0	0	0.0	1	0.0	6	0.3	8	0.4	1	0.0	0	0.0	16	0.7
SSE	0	0.0	0	0.0	5	0.2	3	0.1	1	0.0	1	0.0	0	0.0	10	0.5
S	0	0.0	1	0.0	3	0.1	1	0.0	2	0.1	0	0.0	0	0.0	7	0.3
SSW	0	0.0	1	0.0	2	0.1	3	0.1	1	0.0	0	0.0	0	0.0	7	0.3
SW	0	0.0	0	0.0	1	0.0	0	0.0	2	0.1	0	0.0	0	0.0	3	0.1
WSW	0	0.0	1	0.0	0	0.0	1	0.0	6	0.3	1	0.0	0	0.0	9	0.4
W	0	0.0	0	0.0	3	0.1	8	0.4	8	0.4	2	0.1	0	0.0	21	1.0
WNW	0	0.0	1	0.0	0	0.0	3	0.1	8	0.4	2	0.1	0	0.0	14	0.6
NW	0	0.0	0	0.0	0	0.0	4	0.2	7	0.3	2	0.1	0	0.0	13	0.6
NNW	0	0.0	0	0.0	0	0.0	5	0.2	16	0.7	1	0.0	0	0.0	22	1.0
	0	0.0	5	0.2	24	1.1	47	2.1	91	4.1	32	1.5	0	0.0	199	9.0

MEAN WIND SPEED: 13.5  
 MISSING: 0

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	23	1.0	59	2.7	36	1.6	26	1.2	3	0.1	150	6.8
NNE	0	0.0	3	0.1	23	1.0	28	1.3	42	1.9	43	1.9	5	0.2	144	6.5
NE	0	0.0	2	0.1	8	0.4	24	1.1	64	2.9	45	2.0	3	0.1	146	6.6
ENE	0	0.0	2	0.1	12	0.5	31	1.4	32	1.5	5	0.2	0	0.0	82	3.7
E	0	0.0	2	0.1	19	0.9	23	1.0	26	1.2	1	0.0	0	0.0	71	3.2
ESE	0	0.0	3	0.1	13	0.6	15	0.7	12	0.5	7	0.3	1	0.0	51	2.3
SE	0	0.0	5	0.2	8	0.4	40	1.8	52	2.4	47	2.1	23	1.0	175	7.9
SSE	0	0.0	11	0.5	34	1.5	51	2.3	108	4.9	41	1.9	9	0.4	254	11.5
S	0	0.0	7	0.3	32	1.5	45	2.0	44	2.0	16	0.7	3	0.1	147	6.7
SSW	0	0.0	4	0.2	40	1.8	51	2.3	55	2.5	11	0.5	5	0.2	166	7.5
SW	0	0.0	3	0.1	33	1.5	42	1.9	59	2.7	17	0.8	1	0.0	155	7.0
WSW	0	0.0	5	0.2	19	0.9	38	1.7	42	1.9	9	0.4	1	0.0	114	5.2
W	0	0.0	2	0.1	33	1.5	58	2.6	59	2.7	6	0.3	0	0.0	158	7.2
WNW	0	0.0	4	0.2	16	0.7	46	2.1	37	1.7	8	0.4	3	0.1	114	5.2
NW	0	0.0	3	0.1	17	0.8	35	1.6	57	2.6	29	1.3	7	0.3	148	6.7
NNW	0	0.0	0	0.0	16	0.7	48	2.2	45	2.0	17	0.8	5	0.2	131	5.9
	0	0.0	59	2.7	346	15.7	634	28.7	770	34.9	328	14.9	69	3.1	2206	100.0

MISSING HOURS: 2

MEAN WIND SPEED: 13.2

ARTIFICIAL ISLAND 7/99 - 9/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	23	1.0	59	2.7	36	1.6	26	1.2	3	0.1	150	6.8
NNE	0	0.0	3	0.1	23	1.0	28	1.3	42	1.9	43	1.9	5	0.2	144	6.5
NE	0	0.0	2	0.1	8	0.4	24	1.1	64	2.9	45	2.0	3	0.1	146	6.6
ENE	0	0.0	2	0.1	12	0.5	31	1.4	32	1.4	5	0.2	0	0.0	82	3.7
E	0	0.0	2	0.1	19	0.9	23	1.0	26	1.2	1	0.0	0	0.0	71	3.2
ESE	0	0.0	3	0.1	13	0.6	15	0.7	12	0.5	7	0.3	1	0.0	51	2.3
SE	0	0.0	5	0.2	8	0.4	40	1.8	52	2.4	47	2.1	23	1.0	175	7.9
SSE	0	0.0	11	0.5	34	1.5	51	2.3	109	4.9	41	1.9	9	0.4	255	11.6
S	0	0.0	7	0.3	32	1.4	45	2.0	44	2.0	16	0.7	3	0.1	147	6.7
SSW	0	0.0	4	0.2	40	1.8	51	2.3	55	2.5	11	0.5	5	0.2	166	7.5
SW	0	0.0	3	0.1	33	1.5	42	1.9	59	2.7	17	0.8	1	0.0	155	7.0
WSW	0	0.0	5	0.2	19	0.9	38	1.7	42	1.9	9	0.4	1	0.0	114	5.2
W	0	0.0	2	0.1	33	1.5	58	2.6	59	2.7	6	0.3	0	0.0	158	7.2
WNW	0	0.0	4	0.2	16	0.7	46	2.1	37	1.7	8	0.4	3	0.1	114	5.2
NW	0	0.0	3	0.1	17	0.8	35	1.6	57	2.6	29	1.3	7	0.3	148	6.7
NNW	0	0.0	0	0.0	16	0.7	48	2.2	45	2.0	17	0.8	5	0.2	131	5.9
	0	0.0	59	2.7	346	15.7	634	28.7	771	34.9	328	14.9	69	3.1	2207	100.0

MISSING HOURS: 1

MEAN WIND SPEED: 13.2

**Artificial Island**

**Joint Frequencies**

**10/1/99 – 12/31/99**

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	3	0.1	3	0.1	0	0.0	0	0.0	6	0.3
SSE	0	0.0	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	3	0.1
S	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SW	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	2	0.1
WSW	0	0.0	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	0	0.0	5	0.2
W	0	0.0	0	0.0	0	0.0	4	0.2	2	0.1	0	0.0	0	0.0	6	0.3
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	1	0.0	0	0.0	7	0.3
NNW	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	2	0.1	0	0.0	7	0.3
	0	0.0	0	0.0	3	0.1	18	0.8	19	0.9	3	0.1	0	0.0	43	2.0

MEAN WIND SPEED: 13.2  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	6	0.3	3	0.1	0	0.0	0	0.0	9	0.4
NNE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	2	0.1
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SSE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
S	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SW	0	0.0	0	0.0	3	0.1	4	0.2	0	0.0	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	1	0.0	6	0.3	0	0.0	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	5	0.2	8	0.4	1	0.0	0	0.0	0	0.0	14	0.6
WNW	0	0.0	0	0.0	1	0.0	1	0.0	5	0.2	0	0.0	0	0.0	7	0.3
NW	0	0.0	0	0.0	0	0.0	5	0.2	10	0.5	1	0.0	0	0.0	16	0.7
NNW	0	0.0	0	0.0	1	0.0	15	0.7	11	0.5	2	0.1	0	0.0	29	1.3
	0	0.0	0	0.0	13	0.6	48	2.2	33	1.5	3	0.1	0	0.0	97	4.5

MEAN WIND SPEED: 11.8  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	3	0.1	6	0.3	7	0.3	0	0.0	0	0.0	17	0.8
NNE	0	0.0	0	0.0	3	0.1	1	0.0	1	0.0	0	0.0	0	0.0	5	0.2
NE	0	0.0	0	0.0	5	0.2	1	0.0	0	0.0	0	0.0	0	0.0	6	0.3
ENE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
E	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SSE	0	0.0	0	0.0	5	0.2	1	0.0	1	0.0	0	0.0	0	0.0	7	0.3
S	0	0.0	0	0.0	2	0.1	1	0.0	2	0.1	0	0.0	0	0.0	5	0.2
SSW	0	0.0	1	0.0	2	0.1	1	0.0	1	0.0	0	0.0	0	0.0	5	0.2
SW	0	0.0	0	0.0	4	0.2	3	0.1	0	0.0	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
W	0	0.0	0	0.0	2	0.1	5	0.2	6	0.3	1	0.0	0	0.0	14	0.6
WNW	0	0.0	0	0.0	2	0.1	2	0.1	3	0.1	0	0.0	0	0.0	7	0.3
NW	0	0.0	0	0.0	2	0.1	8	0.4	3	0.1	1	0.0	0	0.0	14	0.6
NNW	0	0.0	0	0.0	4	0.2	10	0.5	5	0.2	1	0.0	0	0.0	20	0.9
	0	0.0	3	0.1	37	1.7	40	1.8	30	1.4	3	0.1	0	0.0	113	5.2

MEAN WIND SPEED: 10.2  
 MISSING: 0

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	17	0.8	20	0.9	23	1.1	2	0.1	0	0.0	64	2.9
NNE	0	0.0	1	0.0	11	0.5	17	0.8	4	0.2	0	0.0	0	0.0	33	1.5
NE	0	0.0	2	0.1	23	1.1	29	1.3	2	0.1	0	0.0	0	0.0	56	2.6
ENE	0	0.0	2	0.1	14	0.6	6	0.3	3	0.1	0	0.0	0	0.0	25	1.1
E	0	0.0	2	0.1	6	0.3	2	0.1	1	0.0	0	0.0	0	0.0	11	0.5
ESE	0	0.0	0	0.0	6	0.3	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3
SE	0	0.0	0	0.0	3	0.1	5	0.2	6	0.3	0	0.0	0	0.0	14	0.6
SSE	0	0.0	1	0.0	15	0.7	24	1.1	3	0.1	0	0.0	0	0.0	43	2.0
S	0	0.0	0	0.0	12	0.6	23	1.1	17	0.8	0	0.0	0	0.0	52	2.4
SSW	0	0.0	3	0.1	15	0.7	17	0.8	15	0.7	0	0.0	0	0.0	50	2.3
SW	0	0.0	0	0.0	15	0.7	18	0.8	1	0.0	0	0.0	0	0.0	34	1.6
WSW	0	0.0	1	0.0	8	0.4	20	0.9	5	0.2	0	0.0	0	0.0	34	1.6
W	0	0.0	0	0.0	10	0.5	31	1.4	24	1.1	2	0.1	0	0.0	67	3.1
WNW	0	0.0	2	0.1	11	0.5	23	1.1	35	1.6	5	0.2	0	0.0	76	3.5
NW	0	0.0	2	0.1	13	0.6	30	1.4	32	1.5	2	0.1	0	0.0	79	3.6
NNW	0	0.0	1	0.0	10	0.5	45	2.1	22	1.0	3	0.1	0	0.0	81	3.7
	0	0.0	19	0.9	189	8.7	310	14.2	193	8.9	14	0.6	0	0.0	725	33.3

MEAN WIND SPEED: 10.2  
 MISSING: 1

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	14	0.6	21	1.0	1	0.0	2	0.1	0	0.0	41	1.9
NNE	0	0.0	5	0.2	21	1.0	13	0.6	1	0.0	0	0.0	0	0.0	40	1.8
NE	0	0.0	17	0.8	20	0.9	15	0.7	0	0.0	0	0.0	0	0.0	52	2.4
ENE	0	0.0	7	0.3	11	0.5	1	0.0	0	0.0	0	0.0	0	0.0	19	0.9
E	0	0.0	3	0.1	8	0.4	0	0.0	0	0.0	0	0.0	0	0.0	11	0.5
ESE	0	0.0	1	0.0	9	0.4	0	0.0	0	0.0	0	0.0	0	0.0	10	0.5
SE	0	0.0	8	0.4	25	1.1	14	0.6	2	0.1	5	0.2	2	0.1	56	2.6
SSE	0	0.0	6	0.3	23	1.1	19	0.9	1	0.0	0	0.0	1	0.0	50	2.3
S	0	0.0	5	0.2	19	0.9	25	1.1	12	0.6	0	0.0	0	0.0	61	2.8
SSW	0	0.0	6	0.3	21	1.0	36	1.7	13	0.6	2	0.1	0	0.0	78	3.6
SW	0	0.0	3	0.1	25	1.1	25	1.1	1	0.0	0	0.0	0	0.0	54	2.5
WSW	0	0.0	4	0.2	28	1.3	18	0.8	0	0.0	0	0.0	0	0.0	50	2.3
W	0	0.0	6	0.3	22	1.0	20	0.9	1	0.0	0	0.0	0	0.0	49	2.2
WNW	0	0.0	3	0.1	15	0.7	25	1.1	1	0.0	0	0.0	0	0.0	44	2.0
NW	0	0.0	7	0.3	43	2.0	42	1.9	11	0.5	1	0.0	0	0.0	104	4.8
NNW	0	0.0	1	0.0	33	1.5	55	2.5	11	0.5	1	0.0	0	0.0	101	4.6
	0	0.0	85	3.9	337	15.5	329	15.1	55	2.5	11	0.5	3	0.1	820	37.6

MEAN WIND SPEED: 7.8  
 MISSING: 5



JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED -  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 30 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	7	0.3	45	2.0	63	2.9	35	1.6	4	0.2	0	0.0	154	7.0
NNE	0	0.0	9	0.4	57	2.6	34	1.5	7	0.3	0	0.0	0	0.0	107	4.9
NE	0	0.0	24	1.1	67	3.1	46	2.1	2	0.1	0	0.0	0	0.0	139	6.3
ENE	0	0.0	14	0.6	37	1.7	9	0.4	3	0.1	0	0.0	0	0.0	63	2.9
E	0	0.0	13	0.6	23	1.0	2	0.1	1	0.0	0	0.0	0	0.0	39	1.8
ESE	0	0.0	3	0.1	31	1.4	2	0.1	0	0.0	0	0.0	0	0.0	36	1.6
SE	0	0.0	13	0.6	72	3.3	39	1.8	18	0.8	5	0.2	2	0.1	149	6.8
SSE	0	0.0	10	0.5	75	3.4	64	2.9	12	0.5	0	0.0	1	0.0	162	7.4
S	0	0.0	10	0.5	42	1.9	55	2.5	32	1.5	0	0.0	0	0.0	139	6.3
SSW	0	0.0	15	0.7	46	2.1	60	2.7	30	1.4	2	0.1	0	0.0	153	7.0
SW	0	0.0	5	0.2	60	2.7	58	2.6	2	0.1	0	0.0	0	0.0	125	5.7
WSW	0	0.0	6	0.3	59	2.7	59	2.7	5	0.2	0	0.0	0	0.0	129	5.9
W	0	0.0	9	0.4	45	2.0	75	3.4	36	1.6	3	0.1	0	0.0	168	7.7
WNW	0	0.0	6	0.3	35	1.6	52	2.4	52	2.4	5	0.2	0	0.0	150	6.8
NW	0	0.0	10	0.5	65	3.0	89	4.1	62	2.8	6	0.3	0	0.0	232	10.6
NNW	0	0.0	6	0.3	54	2.5	128	5.8	54	2.5	9	0.4	0	0.0	251	11.4
	0	0.0	160	7.3	813	37.0	835	38.0	351	16.0	34	1.5	3	0.1	2196	100.0

MISSING HOURS: 12

MEAN WIND SPEED: 8.8

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: LE -1.9 DEG C/100M  
 CLASS A

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	3	0.1	1	0.0	3	0.1	0	0.0	7	0.3
SSE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	2	0.1
S	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	3	0.1
SW	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1
WSW	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	5	0.2
W	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	1	0.0	0	0.0	6	0.3
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	6	0.3	1	0.0	7	0.3
NNW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	4	0.2	2	0.1	7	0.3
	0	0.0	0	0.0	1	0.0	12	0.6	12	0.6	15	0.7	3	0.1	43	2.0

MEAN WIND SPEED: 16.6  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.8 TO -1.7 DEG C/100M  
 CLASS B

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	3	0.1	6	0.3	1	0.0	0	0.0	10	0.5
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SSE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
S	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SW	0	0.0	0	0.0	3	0.1	2	0.1	2	0.1	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	0	0.0	5	0.2	1	0.0	0	0.0	0	0.0	6	0.3
W	0	0.0	0	0.0	3	0.1	4	0.2	6	0.3	1	0.0	0	0.0	14	0.7
WNW	0	0.0	0	0.0	1	0.0	0	0.0	4	0.2	1	0.0	0	0.0	6	0.3
NW	0	0.0	0	0.0	0	0.0	4	0.2	9	0.4	8	0.4	1	0.0	22	1.0
NNW	0	0.0	0	0.0	0	0.0	6	0.3	8	0.4	8	0.4	2	0.1	24	1.1
	0	0.0	0	0.0	9	0.4	25	1.2	40	1.9	19	0.9	3	0.1	96	4.5

MEAN WIND SPEED: 14.6  
 MISSING: 1

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.6 TO -1.5 DEG C/100M  
 CLASS C

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	1	0.0	2	0.1	4	0.2	9	0.4	3	0.1	0	0.0	19	0.9
NNE	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
NE	0	0.0	0	0.0	2	0.1	2	0.1	1	0.0	0	0.0	0	0.0	5	0.2
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	2	0.1	0	0.0	3	0.1
SSE	0	0.0	0	0.0	5	0.2	0	0.0	1	0.0	0	0.0	0	0.0	6	0.3
S	0	0.0	0	0.0	2	0.1	0	0.0	3	0.1	0	0.0	0	0.0	5	0.2
SSW	0	0.0	1	0.0	1	0.0	0	0.0	3	0.1	0	0.0	0	0.0	5	0.2
SW	0	0.0	0	0.0	2	0.1	1	0.0	2	0.1	0	0.0	0	0.0	5	0.2
WSW	0	0.0	0	0.0	1	0.0	1	0.0	1	0.0	0	0.0	0	0.0	3	0.1
W	0	0.0	0	0.0	2	0.1	1	0.0	8	0.4	2	0.1	1	0.0	14	0.7
WNW	0	0.0	0	0.0	2	0.1	0	0.0	3	0.1	1	0.0	0	0.0	6	0.3
NW	0	0.0	0	0.0	3	0.1	3	0.1	7	0.3	4	0.2	1	0.0	18	0.8
NNW	0	0.0	0	0.0	2	0.1	6	0.3	5	0.2	3	0.1	1	0.0	17	0.8
	0	0.0	2	0.1	30	1.4	19	0.9	43	2.0	15	0.7	3	0.1	112	5.3

MEAN WIND SPEED: 12.5  
 MISSING: 1

ARTIFICIAL ISLAND 10/99-12/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -1.4 TO -0.5 DEG C/100M  
 CLASS D

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	6	0.3	7	0.3	28	1.3	10	0.5	1	0.0	54	2.5
NNE	0	0.0	1	0.0	8	0.4	18	0.8	8	0.4	2	0.1	0	0.0	37	1.7
NE	0	0.0	2	0.1	15	0.7	20	0.9	21	1.0	2	0.1	0	0.0	60	2.8
ENE	0	0.0	1	0.0	9	0.4	11	0.5	3	0.1	1	0.0	3	0.1	28	1.3
E	0	0.0	1	0.0	6	0.3	1	0.0	0	0.0	0	0.0	0	0.0	8	0.4
ESE	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SE	0	0.0	2	0.1	4	0.2	3	0.1	5	0.2	2	0.1	3	0.1	19	0.9
SSE	0	0.0	0	0.0	13	0.6	11	0.5	14	0.7	3	0.1	0	0.0	41	1.9
S	0	0.0	0	0.0	4	0.2	17	0.8	25	1.2	2	0.1	0	0.0	48	2.3
SSW	0	0.0	1	0.0	4	0.2	16	0.8	17	0.8	4	0.2	0	0.0	42	2.0
SW	0	0.0	2	0.1	11	0.5	21	1.0	7	0.3	1	0.0	0	0.0	42	2.0
WSW	0	0.0	1	0.0	4	0.2	17	0.8	10	0.5	3	0.1	1	0.0	36	1.7
W	0	0.0	1	0.0	3	0.1	17	0.8	29	1.4	19	0.9	1	0.0	70	3.3
WNW	0	0.0	1	0.0	6	0.3	10	0.5	30	1.4	16	0.8	5	0.2	68	3.2
NW	0	0.0	2	0.1	5	0.2	19	0.9	39	1.8	21	1.0	2	0.1	88	4.2
NNW	0	0.0	0	0.0	5	0.2	23	1.1	35	1.7	12	0.6	4	0.2	79	3.7
	0	0.0	17	0.8	105	5.0	212	10.0	271	12.8	98	4.6	20	0.9	723	34.1

MEAN WIND SPEED: 13.3  
 MISSING: 3

ARTIFICIAL ISLAND 10/99-12/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: -0.4 TO 1.5 DEG C/100M  
 CLASS E

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	3	0.1	5	0.2	14	0.7	1	0.0	3	0.1	26	1.2
NNE	0	0.0	2	0.1	4	0.2	26	1.2	7	0.3	0	0.0	0	0.0	39	1.8
NE	0	0.0	1	0.0	13	0.6	17	0.8	10	0.5	0	0.0	0	0.0	41	1.9
ENE	0	0.0	3	0.1	13	0.6	7	0.3	3	0.1	0	0.0	0	0.0	26	1.2
E	0	0.0	2	0.1	9	0.4	3	0.1	0	0.0	0	0.0	0	0.0	14	0.7
ESE	0	0.0	1	0.0	7	0.3	4	0.2	1	0.0	0	0.0	0	0.0	13	0.6
SE	0	0.0	0	0.0	2	0.1	18	0.8	7	0.3	3	0.1	7	0.3	37	1.7
SSE	0	0.0	3	0.1	6	0.3	31	1.5	10	0.5	2	0.1	1	0.0	53	2.5
S	0	0.0	3	0.1	10	0.5	27	1.3	21	1.0	3	0.1	1	0.0	65	3.1
SSW	0	0.0	1	0.0	18	0.8	25	1.2	20	0.9	8	0.4	1	0.0	73	3.4
SW	0	0.0	2	0.1	19	0.9	28	1.3	16	0.8	1	0.0	0	0.0	66	3.1
WSW	0	0.0	6	0.3	8	0.4	26	1.2	9	0.4	0	0.0	0	0.0	49	2.3
W	0	0.0	3	0.1	7	0.3	32	1.5	10	0.5	1	0.0	0	0.0	53	2.5
WNW	0	0.0	1	0.0	10	0.5	11	0.5	19	0.9	2	0.1	0	0.0	43	2.0
NW	0	0.0	3	0.1	12	0.6	40	1.9	47	2.2	8	0.4	1	0.0	111	5.2
NNW	0	0.0	0	0.0	6	0.3	43	2.0	42	2.0	5	0.2	5	0.2	101	4.8
	0	0.0	31	1.5	147	6.9	343	16.2	236	11.1	34	1.6	19	0.9	810	38.2

MEAN WIND SPEED: 11.5  
 MISSING: 15

ARTIFICIAL ISLAND 10/99-12/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: 1.6 TO 4.0 DEG C/100M  
 CLASS F

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	2	0.1	9	0.4	10	0.5	0	0.0	0	0.0	21	1.0
NNE	0	0.0	0	0.0	3	0.1	15	0.7	1	0.0	0	0.0	0	0.0	19	0.9
NE	0	0.0	0	0.0	0	0.0	11	0.5	1	0.0	0	0.0	0	0.0	12	0.6
ENE	0	0.0	0	0.0	2	0.1	9	0.4	1	0.0	0	0.0	0	0.0	12	0.6
E	0	0.0	0	0.0	6	0.3	1	0.0	0	0.0	0	0.0	0	0.0	7	0.3
ESE	0	0.0	0	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	5	0.2
SE	0	0.0	1	0.0	5	0.2	12	0.6	8	0.4	2	0.1	0	0.0	28	1.3
SSE	0	0.0	3	0.1	10	0.5	18	0.8	9	0.4	7	0.3	0	0.0	47	2.2
S	0	0.0	0	0.0	9	0.4	9	0.4	5	0.2	1	0.0	0	0.0	24	1.1
SSW	0	0.0	0	0.0	6	0.3	6	0.3	4	0.2	1	0.0	0	0.0	17	0.8
SW	0	0.0	5	0.2	11	0.5	12	0.6	6	0.3	0	0.0	0	0.0	34	1.6
WSW	0	0.0	1	0.0	5	0.2	14	0.7	15	0.7	0	0.0	0	0.0	35	1.7
W	0	0.0	1	0.0	1	0.0	5	0.2	5	0.2	0	0.0	0	0.0	12	0.6
WNW	0	0.0	0	0.0	1	0.0	4	0.2	0	0.0	0	0.0	0	0.0	5	0.2
NW	0	0.0	0	0.0	3	0.1	5	0.2	4	0.2	0	0.0	0	0.0	12	0.6
NNW	0	0.0	0	0.0	1	0.0	6	0.3	3	0.1	0	0.0	0	0.0	10	0.5
	0	0.0	11	0.5	66	3.1	139	6.6	73	3.4	11	0.5	0	0.0	300	14.2

MEAN WIND SPEED: 10.2  
 MISSING: 31

ARTIFICIAL ISLAND 10/99-12/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	0	0.0	2	0.1
E	0	0.0	0	0.0	2	0.1	3	0.1	0	0.0	0	0.0	0	0.0	5	0.2
ESE	0	0.0	0	0.0	4	0.2	3	0.1	0	0.0	0	0.0	0	0.0	7	0.3
SE	0	0.0	1	0.0	0	0.0	3	0.1	1	0.0	1	0.0	0	0.0	6	0.3
SSE	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	4	0.2	6	0.3
S	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	3	0.1
WSW	0	0.0	1	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
W	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NNW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
	0	0.0	2	0.1	12	0.6	13	0.6	3	0.1	1	0.0	4	0.2	35	1.7

MEAN WIND SPEED: 10.7  
 MISSING: 21

ARTIFICIAL ISLAND 10/99-12/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	3	0.1	13	0.6	29	1.4	69	3.3	15	0.7	4	0.2	133	6.3
NNE	0	0.0	3	0.1	19	0.9	61	2.9	16	0.8	2	0.1	0	0.0	101	4.8
NE	0	0.0	3	0.1	30	1.4	50	2.4	33	1.6	2	0.1	0	0.0	118	5.6
ENE	0	0.0	4	0.2	25	1.2	27	1.3	10	0.5	1	0.0	3	0.1	70	3.3
E	0	0.0	3	0.1	25	1.2	8	0.4	0	0.0	0	0.0	0	0.0	36	1.7
ESE	0	0.0	1	0.0	14	0.7	11	0.5	2	0.1	0	0.0	0	0.0	28	1.3
SE	0	0.0	4	0.2	12	0.6	39	1.8	23	1.1	13	0.6	10	0.5	101	4.8
SSE	0	0.0	6	0.3	35	1.7	62	2.9	35	1.7	13	0.6	5	0.2	156	7.4
S	0	0.0	3	0.1	26	1.2	54	2.5	56	2.6	6	0.3	1	0.0	146	6.9
SSW	0	0.0	3	0.1	30	1.4	50	2.4	45	2.1	13	0.6	1	0.0	142	6.7
SW	0	0.0	9	0.4	47	2.2	64	3.0	35	1.7	2	0.1	0	0.0	157	7.4
WSW	0	0.0	9	0.4	20	0.9	66	3.1	38	1.8	3	0.1	1	0.0	137	6.5
W	0	0.0	5	0.2	16	0.8	62	2.9	60	2.8	24	1.1	2	0.1	169	8.0
WNW	0	0.0	2	0.1	20	0.9	25	1.2	56	2.6	20	0.9	5	0.2	128	6.0
NW	0	0.0	5	0.2	24	1.1	71	3.4	106	5.0	47	2.2	6	0.3	259	12.2
NNW	0	0.0	0	0.0	14	0.7	84	4.0	94	4.4	32	1.5	14	0.7	238	11.2
	0	0.0	63	3.0	370	17.5	763	36.0	678	32.0	193	9.1	52	2.5	2119	100.0

MISSING HOURS: 89

MEAN WIND SPEED: 12.2

ARTIFICIAL ISLAND 10/99-12/99

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 150 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT		SUM PERCENT			
N	0	0.0	3	0.1	13	0.6	29	1.4	69	3.2	15	0.7	4	0.2	133	6.2
NNE	0	0.0	3	0.1	19	0.9	61	2.9	16	0.7	2	0.1	0	0.0	101	4.7
NE	0	0.0	3	0.1	30	1.4	50	2.3	33	1.5	2	0.1	0	0.0	118	5.5
ENE	0	0.0	4	0.2	25	1.2	27	1.3	10	0.5	1	0.0	3	0.1	70	3.3
E	0	0.0	3	0.1	25	1.2	8	0.4	0	0.0	0	0.0	0	0.0	36	1.7
ESE	0	0.0	1	0.0	14	0.7	11	0.5	2	0.1	0	0.0	0	0.0	28	1.3
SE	0	0.0	4	0.2	12	0.6	39	1.8	23	1.1	13	0.6	10	0.5	101	4.7
SSE	0	0.0	6	0.3	35	1.6	63	2.9	35	1.6	13	0.6	5	0.2	157	7.4
S	0	0.0	3	0.1	26	1.2	55	2.6	56	2.6	6	0.3	1	0.0	147	6.9
SSW	0	0.0	3	0.1	30	1.4	51	2.4	45	2.1	13	0.6	1	0.0	143	6.7
SW	0	0.0	9	0.4	47	2.2	65	3.0	37	1.7	2	0.1	0	0.0	160	7.5
WSW	0	0.0	9	0.4	20	0.9	67	3.1	38	1.8	3	0.1	1	0.0	138	6.5
W	0	0.0	5	0.2	16	0.7	62	2.9	62	2.9	25	1.2	3	0.1	173	8.1
WNW	0	0.0	2	0.1	20	0.9	25	1.2	59	2.8	23	1.1	5	0.2	134	6.3
NW	0	0.0	5	0.2	24	1.1	71	3.3	106	5.0	47	2.2	6	0.3	259	12.1
NNW	0	0.0	0	0.0	14	0.7	84	3.9	94	4.4	32	1.5	14	0.7	238	11.1
	0	0.0	63	2.9	370	17.3	768	36.0	685	32.1	197	9.2	53	2.5	2136	100.0

MISSING HOURS: 72

MEAN WIND SPEED: 12.2

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	5	0.2
SSE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	3	0.1	0	0.0	4	0.2
S	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SSW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SW	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	5	0.2
WSW	0	0.0	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	4	0.2
W	0	0.0	0	0.0	0	0.0	3	0.1	2	0.1	1	0.0	0	0.0	6	0.3
WNW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	8	0.4	1	0.0	9	0.4
NNW	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	2	0.1	2	0.1	6	0.3
	0	0.0	0	0.0	0	0.0	13	0.6	12	0.5	15	0.7	3	0.1	43	2.0

MEAN WIND SPEED: 17.0  
MISSING: 0

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	0	0.0	3	0.1	3	0.1	2	0.1	1	0.0	9	0.4
NNE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ENE	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SSE	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
S	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
SW	0	0.0	0	0.0	1	0.0	3	0.1	3	0.1	0	0.0	0	0.0	7	0.3
WSW	0	0.0	0	0.0	2	0.1	4	0.2	1	0.0	0	0.0	0	0.0	7	0.3
W	0	0.0	0	0.0	2	0.1	6	0.3	6	0.3	1	0.0	0	0.0	15	0.7
WNW	0	0.0	0	0.0	1	0.0	0	0.0	4	0.2	1	0.0	0	0.0	6	0.3
NW	0	0.0	0	0.0	0	0.0	3	0.1	11	0.5	8	0.4	4	0.2	26	1.2
NNW	0	0.0	0	0.0	0	0.0	6	0.3	7	0.3	6	0.3	2	0.1	21	1.0
	0	0.0	0	0.0	8	0.4	26	1.2	38	1.7	18	0.8	7	0.3	97	4.4

MEAN WIND SPEED: 15.2  
 MISSING: 0

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	0	0.0	3	0.1	5	0.2	4	0.2	7	0.3	1	0.0	20	0.9
NNE	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
NE	0	0.0	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	4	0.2
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1
ESE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
SE	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	1	0.0	0	0.0	4	0.2
SSE	0	0.0	0	0.0	3	0.1	2	0.1	0	0.0	0	0.0	0	0.0	6	0.3
S	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
SSW	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2	0	0.0	0	0.0	7	0.3
SW	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	0	0.0	0	0.0	5	0.2
SSW	0	0.0	0	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	4	0.2
WSW	0	0.0	1	0.0	1	0.0	0	0.0	2	0.1	0	0.0	0	0.0	13	0.6
W	0	0.0	0	0.0	2	0.1	2	0.1	4	0.2	4	0.2	1	0.0	9	0.4
WNW	0	0.0	0	0.0	3	0.1	0	0.0	4	0.2	2	0.1	0	0.0	21	1.0
NNW	0	0.0	1	0.0	2	0.1	4	0.2	8	0.4	5	0.2	1	0.0	13	0.6
NNW	0	0.0	0	0.0	2	0.1	3	0.1	5	0.2	2	0.1	1	0.0	13	0.6
	0	0.0	2	0.1	27	1.2	23	1.0	35	1.6	22	1.0	4	0.2	113	5.2

MEAN WIND SPEED: 13.1  
 MISSING: 0

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	SUM PERCENT
	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT	SUM PERCENT				
N	0	0.0	2	0.1	5	0.2	3	0.1	16	0.7	9	0.4	17	0.8	52	2.4
NNE	0	0.0	3	0.1	7	0.3	6	0.3	16	0.7	2	0.1	0	0.0	34	1.6
NE	0	0.0	1	0.0	11	0.5	14	0.6	27	1.2	6	0.3	0	0.0	59	2.7
ENE	0	0.0	1	0.0	10	0.5	11	0.5	4	0.2	2	0.1	3	0.1	31	1.4
E	0	0.0	1	0.0	4	0.2	2	0.1	1	0.0	1	0.0	0	0.0	9	0.4
ESE	0	0.0	0	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	4	0.2
SE	0	0.0	1	0.0	7	0.3	1	0.0	3	0.1	1	0.0	2	0.1	15	0.7
SSE	0	0.0	0	0.0	4	0.2	10	0.5	19	0.9	4	0.2	0	0.0	37	1.7
S	0	0.0	2	0.1	2	0.1	11	0.5	22	1.0	3	0.1	0	0.0	40	1.8
SSW	0	0.0	1	0.0	4	0.2	19	0.9	14	0.6	10	0.5	0	0.0	48	2.2
SW	0	0.0	2	0.1	8	0.4	17	0.8	11	0.5	4	0.2	0	0.0	42	1.9
WSW	0	0.0	1	0.0	6	0.3	15	0.7	12	0.5	1	0.0	1	0.0	36	1.6
W	0	0.0	0	0.0	1	0.0	18	0.8	23	1.0	19	0.9	5	0.2	66	3.0
WNW	0	0.0	2	0.1	3	0.1	14	0.6	28	1.3	30	1.4	5	0.2	82	3.7
NW	0	0.0	1	0.0	3	0.1	16	0.7	34	1.6	32	1.5	12	0.5	98	4.5
NNW	0	0.0	0	0.0	5	0.2	12	0.5	34	1.6	16	0.7	6	0.3	73	3.3
	0	0.0	18	0.8	83	3.8	170	7.8	264	12.0	140	6.4	51	2.3	726	33.1

MEAN WIND SPEED: 14.6  
 MISSING: 0

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	2	0.1	10	0.5	13	0.6	2	0.1	3	0.1	30	1.4
NNE	0	0.0	2	0.1	1	0.0	5	0.2	15	0.7	3	0.1	0	0.0	26	1.2
NE	0	0.0	0	0.0	7	0.3	10	0.5	19	0.9	8	0.4	0	0.0	44	2.0
FNE	0	0.0	1	0.0	10	0.5	11	0.5	6	0.3	1	0.0	0	0.0	29	1.3
E	0	0.0	2	0.1	8	0.4	5	0.2	0	0.0	0	0.0	0	0.0	15	0.7
ESE	0	0.0	0	0.0	5	0.2	4	0.2	1	0.0	0	0.0	0	0.0	10	0.5
SE	0	0.0	0	0.0	6	0.3	5	0.2	8	0.4	2	0.1	4	0.2	25	1.1
SSE	0	0.0	0	0.0	5	0.2	23	1.0	12	0.5	8	0.4	5	0.2	53	2.4
S	0	0.0	1	0.0	3	0.1	20	0.9	31	1.4	5	0.2	1	0.0	61	2.8
SSW	0	0.0	2	0.1	10	0.5	15	0.7	35	1.6	25	1.1	1	0.0	88	4.0
SW	0	0.0	1	0.0	11	0.5	16	0.7	31	1.4	10	0.5	0	0.0	69	3.1
WSW	0	0.0	2	0.1	9	0.4	19	0.9	24	1.1	3	0.1	0	0.0	57	2.6
W	0	0.0	2	0.1	3	0.1	23	1.0	26	1.2	2	0.1	0	0.0	56	2.6
WNW	0	0.0	2	0.1	6	0.3	14	0.6	20	0.9	5	0.2	1	0.0	48	2.2
NW	0	0.0	1	0.0	8	0.4	27	1.2	66	3.0	32	1.5	7	0.3	141	6.4
NNW	0	0.0	1	0.0	3	0.1	14	0.6	38	1.7	15	0.7	2	0.1	73	3.3
	0	0.0	17	0.8	97	4.4	221	10.1	345	15.7	121	5.5	24	1.1	825	37.7

MEAN WIND SPEED: 13.9  
 MISSING: 0

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	0	0.0	3	0.1	10	0.5	10	0.5	1	0.0	0	0.0	24	1.1
NNE	0	0.0	0	0.0	1	0.0	3	0.1	14	0.6	0	0.0	0	0.0	18	0.8
NE	0	0.0	0	0.0	0	0.0	2	0.1	11	0.5	0	0.0	0	0.0	13	0.6
ENE	0	0.0	0	0.0	2	0.1	5	0.2	6	0.3	0	0.0	0	0.0	13	0.6
E	0	0.0	1	0.0	3	0.1	1	0.0	0	0.0	0	0.0	0	0.0	5	0.2
ESE	0	0.0	0	0.0	2	0.1	1	0.0	0	0.0	0	0.0	0	0.0	3	0.1
SE	0	0.0	0	0.0	2	0.1	7	0.3	5	0.2	2	0.1	0	0.0	16	0.7
SSE	0	0.0	1	0.0	6	0.3	10	0.5	9	0.4	4	0.2	4	0.2	34	1.6
S	0	0.0	2	0.1	6	0.3	10	0.5	9	0.4	10	0.5	1	0.0	38	1.7
SSW	0	0.0	1	0.0	5	0.2	13	0.6	9	0.4	5	0.2	0	0.0	33	1.5
SW	0	0.0	0	0.0	8	0.4	5	0.2	18	0.8	2	0.1	0	0.0	33	1.5
WSW	0	0.0	0	0.0	11	0.5	11	0.5	16	0.7	14	0.6	0	0.0	52	2.4
W	0	0.0	1	0.0	1	0.0	4	0.2	8	0.4	5	0.2	0	0.0	19	0.9
WNW	0	0.0	0	0.0	0	0.0	2	0.1	3	0.1	2	0.1	0	0.0	7	0.3
NW	0	0.0	1	0.0	1	0.0	5	0.2	7	0.3	1	0.0	0	0.0	15	0.7
NNW	0	0.0	0	0.0	2	0.1	2	0.1	3	0.1	1	0.0	0	0.0	8	0.4
	0	0.0	7	0.3	53	2.4	91	4.2	128	5.8	47	2.1	5	0.2	331	15.1

MEAN WIND SPEED: 13.0  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

LAPSE RATE: GT 4.0 DEG C/100M  
 CLASS G

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NNE	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NE	0	0.0	0	0.0	0	0.0	0	0.0	2	0.1	0	0.0	0	0.0	2	0.1
ENE	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
E	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
ESE	0	0.0	0	0.0	1	0.0	3	0.1	0	0.0	0	0.0	0	0.0	4	0.2
SE	0	0.0	1	0.0	2	0.1	6	0.3	1	0.0	0	0.0	0	0.0	10	0.5
SSE	0	0.0	0	0.0	1	0.0	1	0.0	2	0.1	1	0.0	4	0.2	9	0.4
S	0	0.0	0	0.0	0	0.0	3	0.1	3	0.1	7	0.3	1	0.0	14	0.6
SSW	0	0.0	0	0.0	0	0.0	1	0.0	1	0.0	0	0.0	0	0.0	2	0.1
SW	0	0.0	0	0.0	0	0.0	3	0.1	0	0.0	0	0.0	0	0.0	3	0.1
WSW	0	0.0	0	0.0	0	0.0	6	0.3	0	0.0	0	0.0	0	0.0	6	0.3
W	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0	0	0.0
WNW	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0
NW	0	0.0	0	0.0	0	0.0	0	0.0	1	0.0	0	0.0	0	0.0	1	0.0
NNW	0	0.0	1	0.0	0	0.0	1	0.0	0	0.0	0	0.0	0	0.0	2	0.1
	0	0.0	2	0.1	5	0.2	26	1.2	10	0.5	8	0.4	5	0.2	56	2.6

MEAN WIND SPEED: 13.5  
 MISSING: 0

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

ALL STABILITY CLASSES

WIND SPEED GROUPS (MPH)

DIRECTION	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6		SUM PERCENT	
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT		
N	0	0.0	2	0.1	13	0.6	32	1.5	46	2.1	22	1.0	22	1.0	137	6.3
NNE	0	0.0	5	0.2	12	0.5	16	0.7	45	2.1	5	0.2	0	0.0	83	3.8
NE	0	0.0	1	0.0	18	0.8	29	1.3	60	2.7	14	0.6	0	0.0	122	5.6
ENE	0	0.0	2	0.1	22	1.0	27	1.2	18	0.8	3	0.1	3	0.1	75	3.4
E	0	0.0	4	0.2	17	0.8	8	0.4	1	0.0	1	0.0	0	0.0	31	1.4
ESE	0	0.0	0	0.0	11	0.5	9	0.4	1	0.0	0	0.0	0	0.0	21	1.0
SE	0	0.0	2	0.1	20	0.9	22	1.0	20	0.9	6	0.3	6	0.3	76	3.5
SSE	0	0.0	1	0.0	20	0.9	46	2.1	43	2.0	21	1.0	13	0.6	144	6.6
S	0	0.0	5	0.2	12	0.5	45	2.1	67	3.1	25	1.1	3	0.1	157	7.2
SSW	0	0.0	4	0.2	21	1.0	49	2.2	64	2.9	40	1.8	1	0.0	179	8.2
SW	0	0.0	3	0.1	29	1.3	50	2.3	66	3.0	16	0.7	0	0.0	164	7.5
WSW	0	0.0	4	0.2	29	1.3	58	2.6	56	2.6	18	0.8	1	0.0	166	7.6
W	0	0.0	3	0.1	9	0.4	56	2.6	69	3.1	32	1.5	6	0.3	175	8.0
WNW	0	0.0	4	0.2	14	0.6	30	1.4	60	2.7	40	1.8	6	0.3	154	7.0
NW	0	0.0	4	0.2	14	0.6	55	2.5	127	5.8	86	3.9	25	1.1	311	14.2
NNW	0	0.0	2	0.1	12	0.5	38	1.7	89	4.1	42	1.9	13	0.6	196	8.9

0 0.0 46 2.1 273 12.5 570 26.0 832 38.0 371 16.9 99 4.5 2191 100.0

MISSING HOURS: 17

MEAN WIND SPEED: 14.1

JOINT DISTRIBUTION OF WIND DIRECTION AND SPEED  
 BY ATMOSPHERIC STABILITY CLASS  
 WIND: 300 FT  
 DELTA T: (300-33FT)

DIRECTION VS SPEED ONLY

DIRECTION	WIND SPEED GROUPS (MPH)														SUM PERCENT	
	0.0-0.5		0.6-3.5		3.6-7.5		7.6-12.5		12.6-18.5		18.6-24.5		GE 24.6			
	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT	SUM	PERCENT
N	0	0.0	2	0.1	13	0.6	32	1.4	46	2.1	22	1.0	22	1.0	137	6.2
NNE	0	0.0	5	0.2	12	0.5	16	0.7	45	2.0	5	0.2	0	0.0	83	3.8
NE	0	0.0	1	0.0	18	0.8	29	1.3	60	2.7	14	0.6	0	0.0	122	5.5
ENE	0	0.0	2	0.1	22	1.0	27	1.2	18	0.8	3	0.1	3	0.1	75	3.4
E	0	0.0	4	0.2	17	0.8	8	0.4	1	0.0	1	0.0	0	0.0	31	1.4
ESE	0	0.0	0	0.0	11	0.5	9	0.4	1	0.0	0	0.0	0	0.0	21	1.0
SE	0	0.0	2	0.1	20	0.9	22	1.0	20	0.9	6	0.3	6	0.3	76	3.4
SSE	0	0.0	1	0.0	20	0.9	46	2.1	43	1.9	21	1.0	13	0.6	144	6.5
S	0	0.0	5	0.2	12	0.5	46	2.1	67	3.0	25	1.1	3	0.1	158	7.2
SSW	0	0.0	4	0.2	21	1.0	49	2.2	65	2.9	40	1.8	1	0.0	180	8.2
SW	0	0.0	3	0.1	29	1.3	50	2.3	67	3.0	17	0.8	0	0.0	166	7.5
WSW	0	0.0	4	0.2	29	1.3	59	2.7	57	2.6	18	0.8	1	0.0	166	7.6
W	0	0.0	3	0.1	9	0.4	56	2.5	73	3.3	37	1.7	6	0.3	184	8.3
WNW	0	0.0	4	0.2	14	0.6	30	1.4	61	2.8	40	1.8	6	0.3	155	7.0
NW	0	0.0	4	0.2	14	0.6	55	2.5	127	5.8	86	3.9	25	1.1	311	14.1
NNW	0	0.0	2	0.1	12	0.5	38	1.7	89	4.0	42	1.9	13	0.6	196	8.9
	0	0.0	46	2.1	273	12.4	572	25.9	840	38.1	377	17.1	99	4.5	2207	100.0

MISSING HOURS: 1

MEAN WIND SPEED: 14.1

# APPENDIX D

## **SALEM ODCM REVISION 12**

---

### Revision Summary:

The following revisions were made to address increased Steam Generator Blowdown flowrates:

- Section 1.2.1 – Revised Equation 1.2 by adding an Allocation Factor (AF). The allocation factor is applicable to steam generator blowdown radiation monitors as a precaution to prevent exceeding the MPC limit should there be simultaneous primary-to-secondary leakage at both Units.
- Section 1.2.2 – Added description of the allocation factor used in determining conservative default setpoints
- Tables 1-1 and 1-2 – Revised the Steam Generator Blowdown Flow to 250 gpm per engineering evaluation S-C-GBD-MEE-1331 and S-C-GBD-MEE-1330. Included the Allocation Factor applicable to the Steam Generator Blowdown monitors.

Revised release data to reflect recent operations:

- Appendix A – Revised Tables A-1 and A-2 to update the release data. Included 1998 data.
- Appendix B – Revised Tables B-1 and B-2 to include calculations for 1998 liquid release data.

Revised Table E-1 to correct the REMP sampling locations as follows:

- Added control TLD Location 14G1 to co-locate with Air Sampling control at 14G1
- Deleted control TLD Location 3H3 – replaced by 14G1
- Deleted Milk Sampling Location 2F7 – owner went out of business
- Added Milk Sampling Location 2F9 as a replacement for 2F7
- Added Water Sediment Sample Location 6S2 to be consistent with REMP program as applied

The following editorial changes were made:

- Revised INTRODUCTION section to be more concise
- Revised format of overall document to improve readability
- Added reference to Appendix F for MPC values throughout the ODCM as appropriate
- Throughout the document added the “range” term to the Summation Symbol
- Section 1.1 – Corrected references to the Figures 1-1, 1-2, and 1-3
- Section 1.2.1 – Revised Equation 1.3 to indicate the MPC<sub>e</sub> is determined using gamma emitters
- Section 1.4.1 – Corrected the subscript for the dose conversion factor to reflect that the factor is organ specific
- Section 1.5 – Deleted the term “significant” for potential releases from the secondary side.
- Section 2.1 – Revised last paragraph to correct references to Figures 2-1 and 2-2
- Section 2.3.2 and 2.5 – Added “tritium” in definition of Q<sub>i</sub>
- Section 2.5, Appendix D – Clarified the use of controlling age group and pathways in Table 2-4
- Section 2.6 – Corrected the value for the partitioning factor (PF) for all other particulates to 0.001
- Section 2.7 – Corrected the references to the Figures 2-1 and 2-2
- Section 4.2 – Corrected the reference to the Technical Specification for the interlaboratory comparison program
- Figures 1-1, 1-2, 1-3, 2-1, and 2-2 – Revised the figures to be more easily read and understood.
- Table 1-2 – Corrected the table note by adding the R19 monitor to this note
- Appendix A – Revised the equation to more clearly demonstrate that it applies to gamma emitters
- Appendix E-1 – Revised wording under section for groundwater sampling to be more accurate

**APPENDIX E**

**SALEM ODCM**

**REVISION 13**

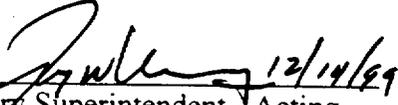
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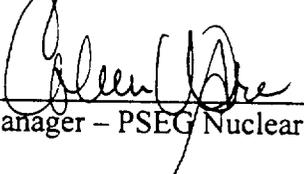
**OFFSITE DOSE CALCULATION MANUAL**  
**FOR**  
**PSEG NUCLEAR**  
**SALEM GENERATING STATION**

**Revision 13**

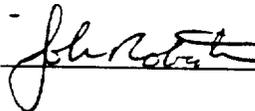
Prepared by: Vince Ciarlante   
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Approved by: Coleen Ware  12/14/99  
Chemistry Manager – PSEG Nuclear

Accepted by:

SORC Chairman:  Date: 12/22/99 Mtg. # S99-115

## Revision Summary:

PART I Added PART I, Radiological Effluent Controls, in preparation for implementation of NRC Generic Letter 89-01. Part I includes the Radiological Effluent Controls that will replace the Radiological Effluent Technical Specifications upon NRC approval of the License Change Request.

The following revisions to the current RETS are included in the ODCM PART I:

1. DEFINITION: WASTE GAS HOLDUP SYSTEM is included in the ODCM. This definition is not in either Salem U1 or U2 Tech Specs, but is provided in NUREG 1301 (Supplement to GL89-01).
2. ODCM Control 3.0.3: "This Control is not applicable in MODE 5 or 6" is included in the ODCM. This statement is not in either Salem U1 or U2 Tech Specs, but is provided in NUREG 1301.
3. ODCM Table 3/4.12-1, REMP: Revised table from U1 and U2 Technical Specifications to conform to NUREG 1301. Made the REMP Tables consistent with Hope Creek REMP. Both programs are conducted as one program. The most limiting sampling requirements and frequencies are chosen to be applicable at both stations. The program conforms to the Radiological Assessment Branch Technical Position on the REMP.
4. ODCM Section 6.9.1.8, Radioactive Effluent Release Report (RERR): Revised the reporting period to annual to conform to most recent Regulatory requirement in 10CFR50.36a.

The following differences between Salem Unit 1 and Unit 2 Technical Specifications are included in the ODCM PART I:

1. ODCM Control Table 3.3.12, Instrument 2.a.: Identified the Minimum Channels Operable for each Unit's Containment Fan Coolers radiation monitors.
2. ODCM Control Table 3.3.12, Instrument 2.b.: Included the Chemical Waste Basin radiation monitor as applicable to both stations.
3. ODCM Control Table 3.3-12, ACTION 28: ACTION 28 a. is only applicable to Unit 2 per the current Technical Specifications.
4. ODCM Control TABLE 4.3-12: Table Notation (2) conditions 3 and 4: Statements in parentheses concerning indication in control equipment room or instruments with operate mode switches are applicable to Unit 2 per the current Technical Specifications
5. ODCM Control Table 4.3-13: Table Notation (1), condition 3 and (2), conditions 3 and 4: Statements in parentheses concerning indication in control equipment room or instruments with operate mode switches are applicable to Unit 1 per the current Technical Specifications.

Revision Summary (continued):

6. ODCM BASES Sections 3.3.3.8 and 3.3.3.9: Included both Units' Bases with no changes to the current Technical Specification Bases.

PART II Revised the previous revision of the ODCM to become PART II, Computational Methodologies.

Revised the term "Safety Factor" related to liquid effluent setpoint calculations to "Correction Factor".

Corrected typographical error in Table 2-5. Corrected the I-133 Pathway Dose Factor for the Grass-Cow-Milk-INFANT pathway for the Bone from  $3.27E+7$  to  $3.72E+7$ .

Corrected editorial errors in Tables B-1 and B-2.

Added "CONTROL" to Technical Specifications referenced throughout the ODCM in preparation to NRC approval of Generic Letter 89-01 submittal (LCR S99-019).

Changed reference to "Semi-annual Radioactive Effluent Release Report" to "Radioactive Effluent Release Report" to prepare for change to annual reporting (LCR S99-019).

Provided an example calculation for assessing dose to MEMBERS OF THE PUBLIC due to activities inside the SITE BOUNDARY in Section 3.1. This is in accordance with Salem Technical Specification BASES Section 3/4.11.2.1.

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<b>APPENDIX F</b>	Maximum Permissible Concentrations – Liquid Effluents

## SALEM NUCLEAR GENERATING STATION OFFSITE DOSE CALCULATION MANUAL

### INTRODUCTION

The Salem Offsite Dose Calculation Manual (ODCM) is a supporting document to the Salem Units 1 and 2 Technical Specifications. The previous Limiting Conditions for Operations that were contained in the Radiological Effluent Technical Specifications (RETS) are now included in the ODCM as Radiological Effluent Controls (REC). The ODCM contains two parts: Part I – Radiological Effluent Controls, and Part II – Calculational Methodologies.

Part I includes the following:

- The Radiological Effluent Controls and the Radiological Environmental Monitoring Programs required by Technical Specifications 6.8.4
- Descriptions of the information that should be included in the Annual Radiological Environmental Operating Report and the Annual Radioactive Effluent Release Report required by Technical Specifications 6.9.1.7 and 6.9.1.8, respectively.

Part II describes methodologies and parameters used for:

- the calculation of radioactive liquid and gaseous effluent monitoring instrumentation alarm/trip setpoints; and
- the calculation of radioactive liquid and gaseous concentrations, dose rates, cumulative quarterly and yearly doses, and projected doses.

Part II also contains a list and graphical description of the specific sample locations for the radiological environmental monitoring program (REMP), and the liquid and gaseous waste treatment systems.

Revisions to the ODCM shall be made in accordance with the Technical Specifications Section 6.14.

The current licensing basis applies Maximum Permissible Concentrations (MPCs) for radioactive liquid effluent concentration limits. Since the MPC values were removed from 10CFR20 effective 1/1/94, the MPC values are provided as Appendix F to the ODCM.

Until the Salem Technical Specifications are revised to delete the Radiological Effluent Technical Specifications, the ODCM Part I will only be used for information. The Technical Specifications with LCOs and Surveillance Requirements will remain the controlling document. Part I of the ODCM will become the controlling document for Radiological Effluent Control upon NRC approval of LCR S99-19.

**PART I - RADIOLOGICAL EFFLUENT CONTROLS**

SECTION 1.0  
DEFINITIONS

## 1.0 DEFINITIONS

---

### DEFINED TERMS

1.1 The DEFINED TERMS of this section appear in capitalized type and are applicable throughout these CONTROLS.

### ACTION

1.2 ACTION shall be that part of a CONTROL which prescribes remedial measures required under designated conditions.

### CHANNEL CALIBRATION

1.4 A CHANNEL CALIBRATION shall be the adjustment, as necessary, of the channel output such that it responds with the necessary range and accuracy to known values of the parameter that the channel monitors. The CHANNEL CALIBRATION shall encompass the entire channel, including the required sensor, alarm, display, and trip functions, and shall include the CHANNEL FUNCTIONAL TEST. The CHANNEL CALIBRATION may be performed by means of any series of sequential, overlapping, or total channel steps so that the entire channel is calibrated.

### CHANNEL CHECK

1.5 A CHANNEL CHECK shall be the qualitative assessment of channel behavior during operation by observation. This determination shall include, where possible, comparison of the channel indication and/or status with other indications and/or status derived from independent instrument channels measuring the same parameter.

### CHANNEL FUNCTIONAL TEST

1.6 A CHANNEL FUNCTIONAL TEST shall be the injection of a simulated signal into the channel as close to the primary sensor as practicable to verify OPERABILITY including alarm and/or trip functions.

### CONTROL

1.10 The present Limiting Conditions for Operation (LCOs) that are contained in the Radiological Effluent Technical Specifications are being transferred to the OFFSITE DOSE CALCULATION MANUAL (ODCM) and are being renamed CONTROLS. This is to distinguish between those LCOs which are being retained in the Technical Specifications and those LCOs or CONTROLS that are being transferred to the ODCM.

## DEFINITIONS

---

### DOSE EQUIVALENT I-131

1.11 DOSE EQUIVALENT I-131 shall be that concentration of I-131 (microcuries per gram), which alone would produce the same thyroid dose as the quantity, and isotopic mixture of I-131, I-132, I-133, I-134, and I-135 actually present. The thyroid dose conversion factors used for this calculation shall be those listed in Table III of TID-14844 "Calculation of Distance Factors for Power and Test Reactor Sites."

### FREQUENCY NOTATION

1.13 The FREQUENCY NOTATION specified for the performance of Surveillance Requirements shall correspond to the intervals defined in Table 1.2.

### GASEOUS RADWASTE TREATMENT SYSTEM

1.14 A GASEOUS RADWASTE TREATMENT SYSTEM is any system designed and installed to reduce radioactive gaseous effluents by collecting primary coolant system offgases from the primary system and providing for delay or holdup for the purpose of reducing the total radioactivity prior to release to the environment.

### MEMBER(S) OF THE PUBLIC

1.16 MEMBER(S) OF THE PUBLIC shall be all those persons who are not occupationally associated with the plant. This category does not include employees of PSE&G, its contractors, or vendors. Also excluded from this category are persons who enter the site to service equipment or to make deliveries. This category does include persons who use portions of the site for recreational, occupational, or other purposes not associated with the plant.

### OFFSITE DOSE CALCULATION MANUAL (ODCM)

1.17 The OFFSITE DOSE CALCULATION MANUAL (ODCM) shall contain the methodology and parameters used in the calculation of offsite doses due to radioactive gaseous and liquid effluents, in the calculation of gaseous and liquid effluent monitoring alarm/trip setpoints, and in the conduct of the environmental radiological monitoring program. The ODCM shall also contain (1) the Radioactive Effluent Controls and Radiological Environmental Monitoring Programs required by Technical Specification Section 6.8.4 and (2) descriptions of the information that should be included in the Annual Radiological Environmental Operating and the Radioactive Effluent Release Reports required by Technical Specification Sections 6.9.1.7 and 6.9.1.8, respectively.

DEFINITIONSOPERABLE - OPERABILITY

1.18 A system, subsystem, train, component or device shall be OPERABLE or have OPERABILITY when it is capable of performing its specified function(s), and when all necessary attendant instrumentation, controls, a normal and an emergency electrical power source, cooling or seal water, lubrication or other auxiliary equipment that are required for the system, subsystem, train, component or device to perform its function(s) are also capable of performing their related support function(s).

OPERATIONAL MODE - MODE

1.19 An OPERATIONAL MODE (i.e., MODE) shall correspond to any one inclusive combination of core reactivity condition, power level and average reactor coolant temperature specified in Table 1.1.

PURGE - PURGING

1.23 PURGE or PURGING shall be the controlled process of discharging air or gas from a confinement to maintain temperature, pressure, humidity, concentration, or other operating condition, in such a manner that replacement air or gas is required to purify the confinement.

RATED THERMAL POWER

1.25 RATED THERMAL POWER shall be a total reactor core heat transfer rate to the reactor coolant of 3411 MWt.

REPORTABLE EVENT

1.27 A REPORTABLE EVENT shall be any of those conditions specified in Section 50.73 to 10CFR Part 50.

SITE BOUNDARY

1.29 The SITE BOUNDARY shall be that line beyond which the land is not owned, leased, or otherwise controlled by the licensee, as shown in Figure 5.1-3.

SOURCE CHECK

1.31 SOURCE CHECK shall be the qualitative assessment of channel response when the channel sensor is exposed to a source of increased radioactivity.

DEFINITIONSTHERMAL POWER

1.33 THERMAL POWER shall be the total reactor core heat transfer rate to the reactor coolant.

UNRESTRICTED AREA

1.35 An UNRESTRICTED AREA shall be any area at or beyond the SITE BOUNDARY, access to which is not controlled by the licensee for purposes of protection of individuals from exposure to radiation and radioactive materials, or any area within the SITE BOUNDARY used for residential quarters or industrial, commercial, institutional, and/or recreational purposes.

VENTILATION EXHAUST TREATMENT SYSTEM

1.36 A VENTILATION EXHAUST TREATMENT SYSTEM shall be any system designed and installed to reduce gaseous radioiodine and radioactive material in particulate form in effluents by passing ventilation or vent exhaust gases through charcoal adsorbers and/or HEPA filters for the purpose of removing iodines or particulates from the gaseous exhaust stream prior to the release to the environment (such a system is not considered to have any effect on noble gas effluents). Engineered Safety Feature (ESF) atmospheric cleanup systems are not considered to be VENTILATION EXHAUST TREATMENT SYSTEM components.

VENTING

1.37 VENTING shall be the controlled process of discharging air or gas from a confinement to maintain temperature, pressure, humidity, concentration, or other operating condition, in such a manner that replacement air or gas is not provided or required during VENTING. Vent, used in system names, does not imply a VENTING process.

WASTE GAS HOLDUP SYSTEM

1.41 A WASTE GAS HOLDUP SYSTEM shall be any system designed and installed to reduce radioactive gaseous effluents by collecting Reactor Coolant System offgases from the Reactor Coolant System and providing for delay or holdup for the purpose of reducing the total radioactivity prior to release to the environment.

DEFINITIONS

TABLE 1.1  
OPERATIONAL MODES

<u>MODE</u>	<u>REACTIVITY CONDITION, <math>K_{eff}</math></u>	<u>THERMAL POWER*</u>	<u>AVERAGE COOLANT TEMPERATURE</u>
1. POWER OPERATION	$\geq 0.99$	$> 5\%$	$\geq 350^{\circ}\text{F}$
2. STARTUP	$\geq 0.99$	$\leq 5\%$	$\geq 350^{\circ}\text{F}$
3. HOT STANDBY	$< 0.99$	0	$\geq 350^{\circ}\text{F}$
4. HOT SHUTDOWN	$< 0.99$	0	$350^{\circ}\text{F} > T_{avg}$ $> 200^{\circ}\text{F}$
5. COLD SHUTDOWN	$< 0.99$	0	$\leq 200^{\circ}\text{F}$
6. REFUELING**	$\leq 0.95$	0	$\leq 140^{\circ}\text{F}$

\* Excluding decay heat.

\*\* Fuel in the reactor vessel with the vessel head closure bolts less than fully tensioned or with the head removed.

DEFINITIONS

TABLE 1.2  
FREQUENCY NOTATION

<u>NOTATION</u>	<u>FREQUENCY</u>
S	At least once per 12 hours.
D	At least once per 24 hours.
W	At least once per 7 days.
M	At least once per 31 days.
Q	At least once per 92 days.
SA	At least once per 6 months.
R	At least once per 18 months.
S/U	Prior to each reactor startup.
P	Prior to each release.
N.A.	Not applicable.

SECTIONS 3.0 AND 4.0  
CONTROLS  
AND  
SURVEILLANCE REQUIREMENTS

### 3/4 CONTROLS AND SURVEILLANCE REQUIREMENTS

#### 3/4.0 APPLICABILITY

#### CONTROLS

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3.0.1 Compliance with the CONTROLS contained in the succeeding CONTROLS is required during the OPERATIONAL MODES or other conditions specified therein; except that upon failure to meet the CONTROL, the associated ACTION requirements shall be met.

3.0.2 Noncompliance with a CONTROL shall exist when the requirements of the CONTROLS and associated ACTION requirements are not met within the specified time intervals. If the CONTROL is restored prior to expiration of the specified time intervals, completion of the ACTION requirements is not required.

3.0.3 When a CONTROL is not met except as provided in the associated ACTION requirements, within one hour action shall be initiated to place the unit in a MODE in which the CONTROL does not apply by placing it, as applicable, in:

1. At least HOT STANDBY within the next 6 hours,
2. At least HOT SHUTDOWN within the following 6 hours, and
3. At least COLD SHUTDOWN within the subsequent 24 hours.

Where corrective measures are completed that permit operation under the ACTION requirements, the ACTION may be taken in accordance with the specified time limits as measured from the time of failure to meet the CONTROL. Exceptions to these requirements are stated in the individual CONTROLS.

This CONTROL is not applicable in MODE 5 or 6.

3.0.4 Entry into an OPERATIONAL MODE or other specified condition:

(a) shall not be made when the conditions of the CONTROL are not met and the associated ACTION requires a shutdown if they are not met within a specified time interval.

(b) may be made in accordance with ACTION requirements when conformance to them permits continued operation of the facility for an unlimited period of time.

This provision shall not prevent passage through or to OPERATIONAL MODES as required to comply with ACTION requirements. Exceptions to these requirements are stated in the individual CONTROLS.

APPLICABILITY

SURVEILLANCE REQUIREMENTS

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4.0.1 Surveillance Requirements shall be met during the OPERATIONAL MODES or other conditions specified for individual CONTROLS unless otherwise stated in an individual Surveillance Requirement.

4.0.2 Each Surveillance Requirement shall be performed within the specified surveillance interval with a maximum allowable extension not to exceed 25 percent of the specified surveillance interval.

4.0.3 Failure to perform a Surveillance Requirement within the allowed surveillance interval, defined by CONTROL 4.0.2, shall constitute a failure to meet the OPERABILITY requirements for a CONTROL. The time limits of the ACTION requirements are applicable at the time it is identified that a Surveillance Requirement has not been performed. The ACTION requirements may be delayed for up to 24 hours to permit the completion of the surveillance when the allowed outage time limits of the ACTION requirements are less than 24 hours. Surveillance Requirements do not have to be performed on inoperable equipment.

4.0.4 Entry into an OPERATIONAL MODE or other specified condition shall not be made unless the Surveillance Requirement(s) associated with the CONTROL has been performed within the stated surveillance interval or as otherwise specified. This provision shall not prevent passage through or to OPERATIONAL MODES as required to comply with ACTION requirements.

### 3/4.3 INSTRUMENTATION

#### 3/ 4.3.3.8 RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

##### CONTROLS

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3.3.3.8 In accordance with Salem Units 1 and 2 Technical Specifications 6.8.4.g.1, the radioactive liquid effluent monitoring instrumentation channels shown in Table 3.3-12 shall be OPERABLE with their alarm/trip setpoints set to ensure that the limits of CONTROL 3.11.1.1 are not exceeded. The alarm/trip setpoints of these channels shall be determined in accordance with the OFFSITE DOSE CALCULATION MANUAL (ODCM).

APPLICABILITY: At all times.

##### ACTION:

- a. With a radioactive liquid effluent monitoring instrumentation channel alarm/trip setpoint less conservative than required by the above CONTROL, without delay suspend the release of radioactive liquid effluents monitored by the affected channel or declare the channel inoperable or change the setpoint so it is acceptably conservative.
- b. With less than the minimum number of radioactive liquid effluent monitoring instrumentation channels OPERABLE, take the ACTION shown in Table 3.3-12. Exert best efforts to return the instrument to OPERABLE status within 30 days and, if unsuccessful, explain in the next radioactive effluent release report why the inoperability was not corrected in a timely manner.
- c. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

##### SURVEILLANCE REQUIREMENTS

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4.3.3.8 Each radioactive liquid effluent monitoring instrumentation channel shall be demonstrated OPERABLE by performance of the CHANNEL CHECK, SOURCE CHECK, CHANNEL CALIBRATION, and CHANNEL FUNCTIONAL TEST operations at the frequencies shown in Table 4.3-12.

TABLE 3.3-12

RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

<u>INSTRUMENT</u>	<u>MINIMUM CHANNELS OPERABLE</u>	<u>ACTION</u>
1. GROSS RADIOACTIVITY MONITORS PROVIDING AUTOMATIC TERMINATION OF RELEASE		
a. Liquid Radwaste Effluent Line	1	26
b. Steam Generator Blowdown Line	4	27
2. GROSS RADIOACTIVITY MONITORS NOT PROVIDING AUTOMATIC TERMINATION OF RELEASE		
a. Containment Fan Coolers - Service Water Line Discharge	5 (Unit 1) 3 (Unit 2)	28
b. Chemical Waste Basin	1	31
3. FLOW RATE MEASUREMENT DEVICES		
a. Liquid Radwaste Effluent Line	1	29
b. Steam Generator Blowdown Line	4	29

TABLE 3.3-12 (Continued)TABLE NOTATION

ACTION 26 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases may continue provided that prior to initiating a release:

- a. At least two independent samples are analyzed in accordance with CONTROL 4.11.1.1.1, and
- b. At least two technically qualified members of the Facility Staff independently verify the release rate calculations and discharge line valving;

Otherwise, suspend release of radioactive effluents via this pathway.

ACTION 27 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided grab samples are analyzed for gross radioactivity (beta or gamma) at a limit of detection of at least  $10^{-7}$  microcuries/gram:

- a. At least once per 8 hours when the specific activity of the secondary coolant is greater than 0.01 microcuries/gram DOSE EQUIVALENT I-131, or
- b. At least once per 24 hours when the specific activity of the secondary coolant is less than or equal to 0.01 microcuries/gram DOSE EQUIVALENT I-131.

ACTION 28 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided that:

- a. At least once per 8 hours, local monitor readouts for the affected channels are verified to be below their alarm setpoints, or **(Unit 2)**
- b. With a Service Water System leak on the Containment Fan Coil Unit associated with the inoperable monitor either:
  1. Grab samples are to be collected and analyzed for gross radioactivity (beta or gamma) at a limit of detection of at least  $10^{-7}$   $\mu\text{Ci}/\text{gram}$  at least once per 8 hours, or
  2. Isolate the release pathway.
- c. With no identified service water leakage on the Containment Fan Coil Unit associated with the inoperable monitor collect grab samples and analyze for gross radioactivity (beta or gamma) at a limit of detection of at least  $10^{-7}$   $\mu\text{Ci}/\text{gram}$  at least once per 24 hours.

TABLE 3.3-12 (Continued)

TABLE NOTATION

ACTION 29 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided the flow rate is estimated at least once per 4 hours during actual releases. Pump performance curves may be used to estimate flow.

ACTION 31 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided that sampling is conducted in accordance with the following table:

<u>Frequency</u>	<u>Condition</u>
1 per week	During normal operation (all MODES)
1 per day	During operation with an identified primary to secondary leak on either Salem Unit

TABLE 4.3-12

RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION  
SURVEILLANCE REQUIREMENTS

<u>INSTRUMENT</u>	<u>CHANNEL CHECK</u>	<u>SOURCE CHECK</u>	<u>CHANNEL CALIBRATION</u>	<u>CHANNEL FUNCTIONAL TEST</u>
<b>1. GROSS RADIOACTIVITY MONITORS PROVIDING ALARM AND AUTOMATIC TERMINATION OF RELEASE</b>				
a. Liquid Radwaste Effluent Line	D	P#	R(3)	Q(1)
b. Steam Generator Blowdown Line	D	M	R(3)	Q(1)
<b>2. GROSS RADIOACTIVITY MONITORS PROVIDING ALARM BUT NOT PROVIDING AUTOMATIC TERMINATION OF RELEASE</b>				
a. Containment Fan Coolers - Service Water Line Discharge	D	M	R(3)	Q(2)
b. Chemical Waste Basin Line	D	M	R(3)	Q(2)
<b>3. FLOW RATE MEASUREMENT DEVICES</b>				
a. Liquid Radwaste Effluent Line	D(4)	N.A.	R	N.A.
b. Steam Generator Blowdown Line	D(4)	N.A.	R	N.A.

TABLE 4.3-12 (Continued)TABLE NOTATION

- (1) The CHANNEL FUNCTIONAL TEST shall also demonstrate that automatic isolation of this pathway and control room alarm annunciation occurs if any of the following conditions exist:
1. Instrument indicates measured levels at or above the alarm/trip setpoint.
  2. Circuit failure. (Loss of Power)
  3. Instrument indicates a downscale failure. (Indication on instrument drawer in Control Equipment Room only)
- (2) The CHANNEL FUNCTIONAL TEST shall also demonstrate that control room alarm annunciation occurs if any of the following conditions exist:
1. Instrument indicates measured levels at or above the alarm/trip setpoint.
  2. Circuit failure. (Loss of Power)
  3. Instrument indicates a downscale failure. (Indication on instrument drawer in Control Equipment Room only {Unit 2})
  4. Instrument controls not set in operate mode. (On instruments equipped with operate mode switches only {Unit 2})
- (3) The initial CHANNEL CALIBRATION was performed using appropriate liquid or gaseous calibration sources obtained from reputable suppliers. The activity of the calibration sources were reconfirmed using a multi-channel analyzer which was calibrated using one or more NBS (now NIST) standards.
- (4) CHANNEL CHECK shall consist of verifying indication of flow during periods of release. CHANNEL CHECK shall be made at least once per 24 hours on days on which continuous, periodic, or batch releases are made.
- # The 1R18 channel is an in-line channel which requires periodic decontamination. Any count rate indication above 10,000 cpm constitutes a CHANNEL CHECK for compliance purposes.
- # The 2R18 channel is an off-line channel which requires periodic decontamination. Any count rate indication above 10,000 cpm constitutes a CHANNEL CHECK for compliance purposes.

### 3/4.3 INSTRUMENTATION

#### 3/4.3.3.9 RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION

##### CONTROLS

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3.3.3.9 In accordance with Salem Units 1 and 2 Technical Specifications 6.8.4.g.1, the radioactive gaseous effluent monitoring instrumentation channels shown in Table 3.3-13 shall be OPERABLE with their alarm/trip setpoints set to ensure that the limits of CONTROL 3.11.2.1 are not exceeded. The alarm/trip setpoints of these channels shall be determined in accordance with the ODCM.

APPLICABILITY: As shown in Table 3.3-13

##### ACTION:

- a. With a radioactive gaseous effluent monitoring instrumentation channel alarm/trip setpoint less conservative than required by the above CONTROL, without delay suspend the release of radioactive gaseous effluents monitored by the affected channel or declare the channel inoperable or change the setpoint so it is acceptably conservative.
- b. With less than the minimum number of radioactive gaseous effluent monitoring instrumentation channels OPERABLE, take the ACTION shown in Table 3.3-13. Exert best efforts to return the instrument to OPERABLE status within 30 days and, if unsuccessful, explain in the next radioactive effluent release report why the inoperability was not corrected in a timely manner.
- c. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

##### SURVEILLANCE REQUIREMENTS

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4.3.3.9 Each radioactive gaseous effluent monitoring instrumentation channel shall be demonstrated OPERABLE by performance of the CHANNEL CHECK, SOURCE CHECK, CHANNEL CALIBRATION, and CHANNEL FUNCTIONAL TEST operations at the frequencies shown in Table 4.3-13.

TABLE 3.3-13

RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION

<u>INSTRUMENT</u>	<u>MINIMUM CHANNELS OPERABLE</u>	<u>APPLICABILITY</u>	<u>ACTION</u>
1. WASTE GAS HOLDUP SYSTEM			
a. Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release	1	*	31
2. CONTAINMENT PURGE AND PRESSURE - VACUUM RELIEF			
a. Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release	1	***	34#
3. PLANT VENT HEADER SYSTEM##			
a. Noble Gas Activity Monitor	1	*	33
b. Iodine Sampler	1	*	36
c. Particulate Sampler	1	*	36
d. Flow Rate Monitor	1	*	32
e. Sampler Flow Rate Monitor	1	*	32

# Action item #34 applies to the purging of the containment only.

## The following process streams are routed to the plant vent where they are effectively monitored by the instruments described:

- (a) Condenser Air Removal System
- (b) Auxiliary Building Ventilation System
- (c) Fuel Handling Building Ventilation System
- (d) Radwaste Area Ventilation System
- (e) Containment Purges

TABLE 3.3-13 (Continued)TABLE NOTATION

- ACTION 31 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, the contents of the tank(s) may be released to the environment provided that prior to initiating the release:
- a. At least two independent samples of the tank's contents are analyzed, and
  - b. At least two technically qualified members of the Facility Staff independently verify the release rate calculations and discharge valving lineup;
- Otherwise, suspend release of radioactive effluents via this pathway.
- ACTION 32 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided the flow rate is estimated at least once per 4 hours.
- ACTION 33 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided grab samples are taken at least once per 8 hours and these samples are analyzed for gross activity within 24 hours.
- ACTION 34 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, immediately suspend PURGING of radioactive effluents via this pathway.
- ACTION 36 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue provided samples are continuously collected with auxiliary sampling equipment as required in Table 4.11-2.

\* At all times, other than when the line is valved out and locked.

\*\*\* During containment purges or containment pressure - vacuum reliefs.

TABLE 4.3-13

RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION  
SURVEILLANCE REQUIREMENTS

<u>INSTRUMENT</u>	<u>CHANNEL CHECK</u>	<u>SOURCE CHECK</u>	<u>CHANNEL CALIBRATION</u>	<u>CHANNEL FUNCTIONAL TEST</u>	<u>MODES IN WHICH SURVEILLANCE REQUIRED</u>
1. WASTE GAS HOLDUP SYSTEM					
a. Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release	P	P	R(3)	Q(1)	*
2. CONTAINMENT PURGE AND PRESSURE - VACUUM RELIEF					
a. Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release	P	P	R(3)	Q(1)	***
3. PLANT VENT HEADER SYSTEM#					
a. Noble Gas Activity Monitor	D	M	R(3)	Q(2)	*
b. Iodine Sampler	W	N.A.	N.A.	N.A.	*
c. Particulate Sampler	W	N.A.	N.A.	N.A.	*
d. Flow Rate Monitor	D	N.A.	R	N.A.	*
e. Sampler Flow Rate Monitor	W	N.A.	R	N.A.	*

# The following process streams are routed to the plant vent where they are effectively monitored by the instruments described:

- (a) Condenser Air Removal System
- (b) Auxiliary Building Ventilation System
- (c) Fuel Handling Building Ventilation System
- (d) Radwaste Area Ventilation System
- (e) Containment Purges

TABLE 4.3-13 (Continued)TABLE NOTATION

- (1) The CHANNEL FUNCTIONAL TEST shall also demonstrate that automatic isolation of this pathway and control room alarm annunciation occurs if any of the following conditions exist:
1. Instrument indicates measured levels above the alarm/trip setpoint.
  2. Circuit failure. (Loss of Power)
  3. Instrument indicates a downscale failure. (Alarm Only) (Indication on instrument drawer in Control Equipment Room only for 1-R12A {Unit 1})
- (2) The CHANNEL FUNCTIONAL TEST shall also demonstrate that control room alarm annunciation occurs if any of the following conditions exist:
1. Instrument indicates measured levels at or above the alarm/trip setpoint.
  2. Circuit failure. (Loss of Power)
  3. Instrument indicates a downscale failure. (Indication on instrument drawer in Control Equipment Room only for 1-R16 {Unit 1})
  4. Instrument controls not set in operate mode. (Applicable to 1-R16 only {Unit 1})
- (3) The initial CHANNEL CALIBRATION was performed using appropriate liquid or gaseous calibration sources obtained from reputable suppliers. The activity of the calibration sources were reconfirmed using a multi-channel analyzer which was calibrated using one or more NBS (now NIST) standards.

\* At all times

\*\*\* During containment purge or containment pressure - vacuum relief.

### 3/4.11 RADIOACTIVE EFFLUENTS

#### 3/4.11.1 LIQUID EFFLUENTS

##### 3/4.11.1.1 CONCENTRATION

##### CONTROLS

---

3.11.1.1 In accordance with the Salem Units 1 and 2 Technical Specifications 6.8.4.g. 2 and 3, the concentration of radioactive material released in liquid effluents to UNRESTRICTED AREAS (See Figure 5.1-3) shall be limited to the concentrations specified in 10 CFR Part 20, Appendix B, Table II, Column 2 for radionuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to  $2 \times 10^{-4}$  microcuries/ml.

APPLICABILITY: At all times.

##### ACTION:

With the concentration of radioactive material released in liquid effluents to UNRESTRICTED AREAS exceeding the above limits, without delay restore the concentration to within the above limits.

##### SURVEILLANCE REQUIREMENTS

---

4.11.1.1.1 Radioactive liquid wastes shall be sampled and analyzed according to the sampling and analyses program in Table 4.11-1.

4.11.1.1.2 The results of the radioactivity analyses shall be used in accordance with the ODCM to assure that the concentrations at the point of release are maintained within the limits of CONTROL 3.11.1.1.

TABLE 4.11-1

RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM

Liquid Release Type	Sampling Frequency	Minimum Analysis Frequency	Type of Activity Analysis	Lower Limit of Detection (LLD) <sup>a</sup> ( $\mu\text{Ci/ml}$ )
A. Batch Waste Release Tanks <sup>b</sup>	P Each Batch	P Each Batch	Principal Gamma Emitters <sup>c</sup>	$5 \times 10^{-7}$
			I-131	$1 \times 10^{-6}$
	P One Batch/M	M	Dissolve and Entrained Gases (Gamma Emitters)	$1 \times 10^{-5}$
	P Each Batch	M Composite <sup>d</sup>	H-3	$1 \times 10^{-5}$
			Gross Alpha	$1 \times 10^{-7}$
	P Each Batch	Q Composite <sup>d</sup>	Sr-89, Sr-90	$5 \times 10^{-8}$
			Fe-55	$1 \times 10^{-6}$
B. Continuous Releases <sup>e</sup> 1. Steam Generator Blowdown	Weekly	W Composite	Principal Gamma Emitters <sup>c</sup>	$5 \times 10^{-7}$
			I-131	$1 \times 10^{-6}$
	M Grab Sample	M	Dissolved and Entrained Gases	$1 \times 10^{-5}$
	Weekly	M Composite	H-3	$1 \times 10^{-5}$
			Gross Alpha	$1 \times 10^{-7}$
	Weekly <sup>d</sup>	Q Composite	Sr-89, Sr-90	$5 \times 10^{-8}$
			Fe-55	$1 \times 10^{-6}$

TABLE 4.11-1 (Continued)TABLE NOTATION

- a. The LLD is defined, for purposes of these CONTROLS as the smallest concentration of radioactive material in a sample that will yield a net count (above system background) that will be detected with 95% probability with only 5% probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system (which may include radiochemical separation):

$$LLD = \frac{4.66 \cdot s_b}{E \cdot V \cdot 2.22E6 \cdot \xi \cdot \exp(-\lambda \Delta t)}$$

Where:

LLD is the "a priori" lower limit of detection as defined above (as microcuries per unit mass or volume),

$s_b$  is the standard deviation of the background counting rate or of the counting rate of a blank sample as appropriate (as counts per minute),

E is the counting efficiency (as counts per disintegration),

V is the sample size (in units of mass or volume),

2.22E6 is the number of disintegrations per minute per microcurie,

$\xi$  is the fractional radiochemical yield (when applicable),

$\lambda$  is the radioactive decay constant for the particular radionuclide, and

$\Delta t$  for environmental samples is the elapsed time between sample collection (or end of the sample collection period) and time of counting.

Typical values of E, V,  $\xi$ , and  $\Delta t$  should be used in the calculation.

It should be recognized that the LLD is defined as an a priori (before the fact) limit representing the capability of a measurement system and not as an a posteriori (after the fact) limit for a particular measurement.

TABLE 4.11-1 (Continued)TABLE NOTATION

- b. A batch release is the discharge of liquid wastes of a discrete volume. Prior to sampling for analyses, each batch shall be isolated, and then thoroughly mixed to assure representative sampling.
- c. The principal gamma emitters for which the LLD CONTROL applies exclusively are the following radionuclides: Mn-54, Fe-59, Co-58, Co-60, Zn-65, Mo-99, Cs-134, Cs-137, Ce-141, and Ce-144\*. This list does not mean that only these nuclides are to be detected and reported. Other peaks that are measurable and identifiable, together with the above nuclides, shall also be identified and reported.
- d. A composite sample is one in which the quantity of liquid sampled is proportional to the quantity of liquid waste discharged and in which the method of sampling employed results in a specimen that is representative of the liquids released.
- e. A continuous release is the discharge of liquid wastes of a nondiscrete volume, e.g., from a volume of a system that has an input flow during the continuous release.

\* The LLD for Ce-144 shall be  $2 \times 10^{-6}$   $\mu\text{Ci/ml}$ .

3/ 4.11 RADIOACTIVE EFFLUENTS

3/ 4.11.1.2 DOSE

CONTROLS

---

3.11.1.2 In accordance with Salem Units 1 and 2 Technical Specifications 6.8.4.g.4 and 5, the dose or dose commitment to a MEMBER OF THE PUBLIC from radioactive materials in liquid effluents released, from each reactor unit, to UNRESTRICTED AREAS (see Figure 5.1-3) shall be limited:

- a. During any calendar quarter to less than or equal to 1.5 mrem to the total body and to less than or equal to 5 mrem to any organ, and
- b. During any calendar year to less than or equal to 3 mrem to the total body and to less than or equal to 10 mrem to any organ.

APPLICABILITY: At all times.

ACTION:

- a. With the calculated dose from the release of radioactive materials in liquid effluents exceeding any of the above limits, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that identifies the cause(s) for exceeding the limit(s) and defines the corrective actions that have been taken to reduce the releases and the proposed corrective actions to be taken to assure that subsequent releases will be in compliance with the above limits.
- b. The provisions of CONTROL 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

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4.11.1.2 Cumulative dose contributions from liquid effluents shall be determined in accordance with the ODCM at least once per 31 days.

### 3/4.11 RADIOACTIVE EFFLUENTS

#### 3/4.11.1.3 LIQUID RADWASTE TREATMENT

##### CONTROLS

---

3.11.1.3 In accordance with the Salem Units 1 and 2 Technical Specifications 6.8.4.g.6, the liquid radwaste treatment system shall be used to reduce the radioactive materials liquid wastes prior to their discharge when the projected cumulative doses due to the liquid effluent from each reactor to UNRESTRICTED AREAS (see Figure 5.1-3) exceed 0.375 mrem to the total body or 1.25 mrem to any organ during any calendar quarter.

APPLICABILITY: At all times.

##### ACTION:

- a. With the radioactive liquid waste being discharged without treatment and in excess of the above limits, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that includes the following information:
  1. Explanation of why liquid radwaste was being discharged without treatment, identification of any inoperable equipment or subsystems, and the reason for the inoperability.
  2. Action(s) taken to restore the inoperable equipment to OPERABLE status, and
  3. Summary description of action(s) taken to prevent a recurrence.
- b. The provisions of CONTROL 3.0.3 and 3.0.4 are not applicable.

##### SURVEILLANCE REQUIREMENTS

---

4.11.1.3 Doses due to liquid releases shall be projected at least once per 31 days in accordance with the ODCM.

### 3/4.11 RADIOACTIVE EFFLUENTS

#### 3/4.11.2 GASEOUS EFFLUENTS

##### 3/4.11.2.1 DOSE RATE

#### CONTROLS

---

3.11.2.1 In accordance with the Salem Units 1 and 2 Technical Specifications 6.8.4.g.3 and 7, the dose rate due to radioactive materials released in gaseous effluents from the site to areas at and beyond the SITE BOUNDARY (see Figure 5.1-3) shall be limited to the following:

- a. For noble gases: Less than or equal to 500 mrem/yr to the total body and less than or equal to 3000 mrem/yr to the skin, and
- b. For iodine-131, for tritium, and for all radionuclides in particulate form with half lives greater than 8 days: Less than or equal to 1500 mrem/yr to any organ.

APPLICABILITY: At all times.

#### ACTION:

With the dose rate(s) exceeding the above limits, without delay restore the release rate to within the above limit(s).

#### SURVEILLANCE REQUIREMENTS

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4.11.2.1.1 The dose rate due to noble gases in gaseous effluents shall be determined continuously to be within the above limits in accordance with the ODCM.

4.11.2.1.2 The dose rate due to iodine-131, tritium, and all radionuclides in particulate form with half lives greater than 8 days in gaseous effluents shall be determined to be within the above limits in accordance with the ODCM by obtaining representative samples and performing analyses in accordance with the sampling and analysis program specified in Table 4.11-2.

TABLE 4.11-2

RADIOACTIVE GASEOUS WASTE SAMPLING AND ANALYSIS PROGRAM

Gaseous Release Type	Sampling Frequency	Minimum Analysis Frequency	Type of Activity Analysis	Lower Limit of Detection (LLD) ( $\mu\text{Ci/ml}$ )
A. Waste Gas Storage Tank	P Each Tank Grab Sample	P Each Tank	Principal Gamma Emitters <sup>b</sup>	$1 \times 10^{-4}$
B. Containment PURGE	P Each PURGE Grab Sample	P Each PURGE	Principal Gamma Emitters <sup>b</sup>	$1 \times 10^{-4}$
		M	H-3	$1 \times 10^{-6}$
C. Plant Vent	M <sup>c,d,e</sup> Grab Sample	M <sup>c</sup>	Principal Gamma Emitters <sup>b</sup>	$1 \times 10^{-4}$
			H-3	$1 \times 10^{-6}$
D. All Release Types as Listed in A, B. and C Above	Continuous <sup>f</sup>	W <sup>g</sup> Charcoal Sample	I-131	$1 \times 10^{-12}$
	Continuous <sup>f</sup>	W <sup>g</sup> Particulate Sample	Principal Gamma Emitters <sup>b</sup> (I-131, Others)	$1 \times 10^{-11}$
	Continuous <sup>f</sup>	M Composite Particulate Sample	Gross Alpha	$1 \times 10^{-11}$
	Continuous <sup>f</sup>	Q Composite Particulate Sample	Sr-89, Sr-90	$1 \times 10^{-11}$
	Continuous <sup>f</sup>	Noble Gas Monitor	Noble Gasses Gross Beta or Gamma	$1 \times 10^{-6}$

TABLE 4.11-2 (Continued)TABLE NOTATION

- a. The LLD is defined in Table 4.11.1
- b. The principal gamma emitters for which the LLD CONTROL applies exclusively are the following radionuclides: Kr-87, Kr-88, Xe-133, Xe-133m, Xe-135, Xe-138 for gaseous emissions and Mn-54, Fe-59, Co-58, Co-60, Zn-65, Mo-99, Cs-134, Cs-137, Ce-141 and Ce-144 for particulate emissions. This list does not mean that only these nuclides are to be detected and reported. Other peaks that are measurable and identifiable, together with the above nuclides, shall also be identified and reported.
- c. Sampling and analysis shall also be performed following shutdown, startup or a THERMAL POWER change that, within one hour, exceeds 15 percent of RATED THERMAL POWER unless:
  1. Analysis shows that the DOSE EQUIVALENT I-131 concentration in the primary coolant has not increased more than a factor of three; and
  2. The noble gas activity monitor shows that effluent activity has not increased by more than a factor of three.
- d. Tritium grab samples shall be taken at least once per 24 hours when the refueling canal is flooded.
- e. Tritium grab samples shall be taken at least once per 7 days from the ventilation exhaust from the spent fuel pool area whenever spent fuel is in the spent fuel pool.
- f. The ratio of the sample flow rate to the sampled stream flow rate shall be known for the time period covered by each dose or dose rate calculation made in accordance with CONTROLS 3.11.2.1, 3.11.2.2 and 3.11.2.3.
- g. Samples shall be changed at least once per 7 days and analyses shall be completed within 48 hours after changing (or after removal from sampler). Sampling shall also be performed at least once per 24 hours for at least 7 days following each shutdown, startup or THERMAL POWER change that, within one hour, exceeds 15 percent of RATED THERMAL POWER and analyses shall be completed within 48 hours of changing. When samples collected for 24 hours are analyzed, the corresponding LLDs may be increased by a factor of 10. This requirement does not apply if (1) analysis shows that the DOSE EQUIVALENT I-131 concentration in the primary coolant has not increased more than a factor of 3; and (2) the noble gas monitor shows that effluent activity has not increased by more than a factor of three.

3/4.11 RADIOACTIVE EFFLUENTS

3/4.11.2.2 DOSE - NOBLE GASES

CONTROLS

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3.11.2.2 In accordance with the Salem Units 1 and 2 Technical Specification 6.8.4.g.5 and 8, the air dose due to noble gases released in gaseous effluents, from each reactor unit, from the site areas and beyond the SITE BOUNDARY (see Figure 5.1-3) shall be limited to the following:

- a. During any calendar quarter: Less than or equal to 5 mrad for gamma radiation and less than or equal to 10 mrad for beta radiation and,
- b. During any calendar year: Less than or equal to 10 mrad for gamma radiation and less than or equal to 20 mrad for beta radiation.

APPLICABILITY: At all times.

ACTION:

- a. With the calculated air dose from radioactive noble gases in gaseous effluents exceeding any of the above limits, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that identifies the cause(s) for exceeding the limit(s) and defines the corrective actions that have been taken to reduce the release and the proposed corrective actions to be taken to assure that subsequent releases will be in compliance with the above limits.
- b. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

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4.11.2.2 Cumulative dose contributions for the current calendar quarter and current calendar year shall be determined in accordance with the ODCM at least once per 31 days.

### 3/4.11 RADIOACTIVE EFFLUENTS

#### 3/4.11.2.3 DOSE - IODINE-131, TRITIUM, AND RADIONUCLIDES IN PARTICULATE FORM

##### CONTROLS

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3.11.2.3 In accordance with the Salem Units 1 and 2 Technical Specification 6.8.4.g.5 and 9, the dose to a MEMBER OF THE PUBLIC from iodine-131, from tritium, and from all radionuclides in particulate form with half-lives greater than 8 days in gaseous effluents released, from each reactor unit, from the site to areas at and beyond the SITE BOUNDARY (see Figure 5.1-3) shall be limited to the following:

- a. During any calendar quarter: Less than or equal to 7.5 mrem to any organ and,
- b. During any calendar year: Less than or equal to 15 mrem to any organ.

APPLICABILITY: At all times.

##### ACTION:

- a. With the calculated air dose from the release of iodine-131, tritium, and radionuclides in particulate form with half-lives greater than 8 days, in gaseous effluents exceeding any of the above limits, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that identifies the cause(s) for exceeding the limit and defines the corrective actions that have been taken to reduce the release and the proposed corrective actions to be taken to assure that subsequent releases will be in compliance with the above limits.
- b. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

##### SURVEILLANCE REQUIREMENTS

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4.11.2.3 Cumulative dose contributions for the current calendar quarter and current calendar year for iodine-131, tritium, and radionuclides in particulate form with half-lives greater than 8 days shall be determined in accordance with the ODCM at least once per 31 days.

3/4.11 RADIOACTIVE EFFLUENTS

3/4.11.2.4 GASEOUS RADWASTE TREATMENT

CONTROLS

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3.11.2.4 In accordance with the Salem Units 1 and 2 Technical Specifications 6.8.4.g.6, the GASEOUS RADWASTE TREATMENT SYSTEM and the VENTILATION EXHAUST TREATMENT SYSTEM shall be used to reduce radioactive materials in gaseous waste prior to their discharge when the projected gaseous effluent air doses due to gaseous effluent releases, from the site to areas at and beyond the SITE BOUNDARY (see Figure 5.1-3), exceed 0.625 mrad for gamma radiation and 1.25 mrad for beta radiation in any calendar quarter. The VENTILATION EXHAUST TREATMENT SYSTEM shall be used to reduce radioactive materials in gaseous waste prior to their discharge when the projected doses due to gaseous effluent releases, from each reactor unit, from the site to areas at and beyond the SITE BOUNDARY (see Figure 5.1-3) would exceed 1.875 mrem to any organ in any calendar quarter.

APPLICABILITY: At all times.

ACTION:

- a. With gaseous waste being discharged without treatment and in excess of the above limits, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that includes the following information:
  1. Explanation of why gaseous radwaste was being discharged without treatment, identification of any inoperable equipment or subsystems, and the reason for the inoperability.
  2. Action(s) taken to restore the inoperable equipment to OPERABLE status, and
  3. Summary description of action(s) taken to prevent a recurrence.
- b. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

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4.11.2.4 Doses due to gaseous releases from the site shall be projected at least once per 31 days in accordance with the ODCM.

### 3/4.11 RADIOACTIVE EFFLUENTS

#### 3/4.11.4 TOTAL DOSE

#### CONTROLS

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3.11.4. In accordance with Salem Units 1 and 2 Technical Specifications 6.8.4.g.11, the annual (calendar year) dose or dose commitment to any MEMBER OF THE PUBLIC, due to releases of radioactivity and radiation, from uranium fuel cycle sources shall be limited to less than or equal to 25 mrem to the total body or any organ (except the thyroid, which shall be limited to less than or equal to 75 mrem).

APPLICABILITY: At all times

#### ACTION:

- a. With the calculated doses from the release of radioactive materials in liquid or gaseous effluents exceeding twice the limits of CONTROL 3.11.1.2a, 3.11.1.2b, 3.11.2.2a, 3.11.2.2b, 3.11.2.3a, or 3.11.2.3b, calculations should be made including direct radiation contributions from the reactor units and from outside storage tanks to determine whether the limits of this CONTROL have been exceeded. If such is the case, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that defines the corrective action to be taken to reduce subsequent releases to prevent recurrence of exceeding the above limits and includes the schedule for achieving conformance with the above limits. This Special Report, as defined in 10 CFR Part 20.405c, shall include an analysis that estimates the radiation exposure (dose) to a MEMBER OF THE PUBLIC from uranium fuel cycle sources, including all effluent pathways and direct radiation, for the calendar year that includes the release(s) covered by this report. It shall also describe levels of radiation and concentrations of radioactive material involved, and the cause of the exposure levels or concentrations. If the estimated dose(s) exceeds the above limits, and if the release condition resulting in violation of 40 CFR Part 190 has not already been corrected, the Special Report shall include a request for a variance in accordance with the provisions of 40 CFR Part 190. Submittal of the report is considered a timely request, and a variance is granted until staff action on the request is complete.
- b. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

#### SURVEILLANCE REQUIREMENTS

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4.11.4.1 Cumulative dose contributions from liquid and gaseous effluents shall be determined in accordance with CONTROLS 4.11.1.2, 4.11.2.2, 4.11.2.3, and in accordance with the ODCM.

4.11.4.2 Cumulative dose contributions from direct radiation from the reactor units and from radwaste storage shall be determined in accordance with the ODCM.

### 3/4.12 RADIOLOGICAL ENVIRONMENTAL MONITORING

#### 3/4.12.1 MONITORING PROGRAM

##### CONTROLS

3.12.1. In accordance with Salem Units 1 and 2 Technical Specifications 6.8.4.g.h.1, the radiological environmental monitoring program shall be conducted as specified in Table 3.12-1.

APPLICABILITY: At all times.

##### ACTION:

- a. With the radiological environmental monitoring program not being conducted as specified in Table 3.12-1, prepare and submit to the Commission, in the Annual Radiological Environmental Operating Report required by Specification 6.9.1.7, a description of the reasons for not conducting the program as required and the plans for preventing a recurrence.
- b. With the level of radioactivity as the result of plant effluents in an environmental sampling medium at a specified location exceeding the reporting levels of Table 3.12-2 when averaged over any calendar quarter, prepare and submit to the Commission within 30 days, pursuant to Specification 6.9.2, a Special Report that identifies the cause(s) for exceeding the limit(s) and defines the corrective actions to be taken to reduce radioactive effluents so that the potential annual dose\* to a MEMBER OF THE PUBLIC is less than the calendar year limits of CONTROLS 3.11.1.2, 3.11.2.2, and 3.11.2.3. When more than one of the radionuclides in Table 3.12-2 are detected in the sampling medium, this report shall be submitted if:

$$\frac{\text{concentration (1)}}{\text{reporting level (1)}} + \frac{\text{concentration (2)}}{\text{reporting level (2)}} + \dots > 1.0$$

When radionuclides other than those in Table 3.12-2 are detected and are the result of plant effluents, this report shall be submitted if the potential annual dose\* to a MEMBER OF THE PUBLIC from all radionuclides is equal to or greater than the calendar year limits of CONTROLS 3.11.1.2, 3.11.2.2, and 3.11.2.3. This report is not required if the measured level of radioactivity was not the result of plant effluents; however, in such an event, the condition shall be reported and described in the Annual Radiological Environmental Operating Report pursuant to CONTROL 6.9.1.7.

\*The methodology used to estimate the potential annual dose to a MEMBER OF THE PUBLIC shall be indicated in this report.

3/4.12 RADIOLOGICAL ENVIRONMENTAL MONITORING

3/4.12.1 MONITORING PROGRAM

CONTROLS

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ACTION: (Cont'd)

- c. With milk or fresh leafy vegetable samples unavailable from one or more of the sample locations required by Table 3.12-1, identify specific locations for obtaining replacement samples and add them to the radiological environmental monitoring program within 30 days. The specific locations from which samples were unavailable may then be deleted from the monitoring program.

Pursuant to Specification 6.9.1.8, identify the cause of the unavailability of samples and the new location(s) for obtaining replacement samples in the next Radioactive Effluent Release Report. Include in the report a revised figure(s) and table for the ODCM reflecting the new location(s).

- d. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

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4.12.1 The radiological environmental monitoring samples shall be collected pursuant to Table 3.12-1 from the specific locations given in the table and figure(s) in the ODCM, and shall be analyzed pursuant to the requirements of Table 3.12-1, and the detection capabilities required by Table 4.12-1.

TABLE 3.12-1

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM \*

<u>EXPOSURE PATHWAY AND/OR SAMPLE</u>	<u>NUMBER OF REPRESENTAIVE SAMPLES AND SAMPLE LOCATIONS<sup>(1)</sup></u>	<u>SAMPLING AND COLLECTION FREQUENCY</u>	<u>TYPE AND FREQUENCY OF ANALYSIS</u>
1. DIRECT RADIATION <sup>(2)</sup>	<p>Forty-three routine monitoring stations with two or more dosimeters be placed as follows:</p> <p>An inner ring of stations one in each meteorological sector in the general area of the SITE BOUNDARY;</p> <p>An outer ring of stations, one in each land-based meteorological sector in the 6- to 8-km range from the site; and</p> <p>The balance of the stations to be placed in special interest areas such as population centers, nearby residences, schools, and in one or two areas to serve as control stations.</p>	Quarterly	Gamma dose quarterly,

\*The number, media, frequency, and location of samples may vary from site to site. This table presents an acceptable minimum program for a site at which each entry is applicable. Local site characteristics must be examined to determine if pathways not covered by this table may significantly contribute to an individual's dose and should be included in the sample program.

TABLE 3.12-1(Cont'd)

<u>EXPOSURE PATHWAY AND/OR SAMPLE</u>	<u>NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS<sup>(1)</sup></u>	<u>SAMPLING AND COLLECTION FREQUENCY</u>	<u>TYPE AND FREQUENCY OF ANALYSIS</u>
2. AIRBORNE  Radioiodine and Particulates	<p>Samples from 5 locations:</p> <p>Three samples from close to the SITE BOUNDARY locations, in different sectors, of a high calculated annual average ground-level D/Q.</p> <p>One sample from the vicinity of a community having a high calculated annual average ground-level D/Q; and</p> <p>One sample from a control location, as for example 15-30 km distant and in the least prevalent wind direction.</p>	Continuous sampler operation with sample collection weekly or more frequently if required by dust loading.	<p><u>Radioiodine Canister:</u> I-131 analysis weekly.</p> <p><u>Particulate Sampler</u> Gross beta radioactivity analysis following filter change<sup>(3)</sup>;</p> <p>Gamma isotopic analysis<sup>(4)</sup> of composites (by location) quarterly.</p>
3. WATERBORNE a. Surface <sup>(5)</sup>	<p>One sample upstream.</p> <p>One sample downstream.</p> <p>One sample outfall</p> <p>One sample cross-stream</p>	Grab sample monthly.	Gamma isotopic analysis <sup>(4)</sup> monthly. Composite for tritium analysis quarterly.

TABLE 3.12-1(Cont'd)

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

<u>EXPOSURE PATHWAY AND/OR SAMPLE</u>	<u>NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS<sup>(1)</sup></u>	<u>SAMPLING AND COLLECTION FREQUENCY</u>	<u>TYPE AND FREQUENCY OF ANALYSIS</u>
3. WATERBORNE (Continued)			
b. Ground	Samples from one or two sources only if likely to be affected <sup>(7)</sup> .	Monthly	Gamma isotopic analysis <sup>(4)</sup> and tritium analysis quarterly.
c. Drinking	One sample of each of one to three of the nearest water supplies that could be affected by its discharge.	Composite sample over two-week period <sup>(6)</sup> when I-131 analysis is performed; monthly composite otherwise.	I-131 analysis on each composite when the dose calculated for the consumption of the water is greater than 1 mrem per year <sup>(8)</sup> . Composite for gross beta and gamma isotopic analysis <sup>(4)</sup> monthly. Composite for tritium analysis quarterly.
	One sample from a control location.		
d. Sediment	One sample from downstream area One sample from cross-stream area One sample from outfall area One sample from upstream area	Semiannually	Gamma isotopic analysis <sup>(4)</sup> semiannually.

TABLE 3.12-1(Cont'd)

<u>EXPOSURE PATHWAY AND/OR SAMPLE</u>	<u>NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS<sup>(1)</sup></u>	<u>SAMPLING AND COLLECTION FREQUENCY</u>	<u>TYPE AND FREQUENCY OF ANALYSIS</u>
4. INGESTION			
a. Milk	Samples from milking animals in three locations within 5 km distance having the highest dose potential. If there are none, then, one sample from milking animals in each of three areas between 5 to 8 km distant where doses are calculated to be greater than 1 mrem per yr <sup>(8)</sup> .	Semimonthly when animals are on pasture, monthly at other time.	Gamma isotopic <sup>(4)</sup> and I-131 analysis semi-monthly when animals are on pasture; monthly at other times
	One sample from milking animals at a control location 15 to 30 km distant.		
b. Fish and Invertebrates	One sample of each commercially and recreationally important species in vicinity of plant discharge area.	Sample in season, or semiannual if they are not seasonal	Gamma isotopic analysis <sup>(4)</sup> on edible portions.
	One sample of same species in area not influenced by plant discharge.		

TABLE 3.12-1(Cont'd)

<u>EXPOSURE PATHWAY AND/OR SAMPLE</u>	<u>NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS<sup>(1)</sup></u>	<u>SAMPLING AND COLLECTION FREQUENCY</u>	<u>TYPE AND FREQUENCY OF ANALYSIS</u>
c. Food Products	One sample of each principal class of food products from any area that is irrigated by water in which liquid plant wastes have been discharged.	At time of harvest <sup>(9)</sup>	Gamma isotopic analysis <sup>(4)</sup> on edible portion.

TABLE 3.12.1 (Continued)TABLE NOTATION

- (1) Specific parameters of distance and direction sector from the centerline of one reactor, and additional description where pertinent, shall be provided for each and every sample location in Table 3.12-1 in a table and figure(s) in the ODCM. Refer to NUREG-0133, "Preparation of Radiological Effluent Technical Specifications for Nuclear Power Plants," October 1978, and to Radiological Assessment Branch Technical Position, Revision 1, November 1979. Deviations are permitted from the required sampling schedule if specimens are unobtainable due to circumstances such as hazardous conditions, seasonal unavailability, malfunction of automatic sampling equipment, and other legitimate reasons. If specimens are unobtainable due to sampling equipment malfunction, effort shall be made to complete corrective action prior to the end of the next sampling period. All deviations from the sampling schedule shall be documented in the Annual Radiological Environmental Operating Report pursuant to CONTROL 6.9.1.7. It is recognized that, at times, it may not be possible or practicable to continue to obtain samples of the media of choice at the most desired location or time. In these instances suitable specific alternative media and locations may be chosen for the particular pathway in question and appropriate substitutions made within 30 days in the Radiological Environmental Monitoring Program given in the ODCM. Pursuant to CONTROL 6.9.1.8, submit in the next Radioactive Effluent Release Report documentation for a change in the ODCM including revised figure(s) and table for the ODCM reflecting the new location(s) with supporting information identifying the cause of the unavailability of samples for the pathway and justifying the selection of the new location(s) for obtaining samples.
- (2) One or more instruments, such as pressurized ion chamber, for measuring and recording dose rate continuously may be used in place of, or in addition to, integrating dosimeters. For the purposes of this table, a thermoluminescent dosimeter (TLD) is considered to be one phosphor; two or more phosphors in a packet are considered as two or more dosimeters. Film badges shall not be used for measuring direct radiation. The frequency of analysis or readout will depend upon the characteristics of the specific TLD system used and should be selected to obtain optimum dose information with minimal fading.
- (3) Airborne particulate sample filters shall be analyzed for gross beta radioactivity 24 hours or more after sampling to allow for radon and thoron daughter decay. If gross beta activity in air particulate is greater than ten times the yearly mean of control samples, gamma isotopic analysis shall be performed on the individual samples.
- (4) Gamma isotopic analysis means the identification and quantification of gamma-emitting radionuclides that may be attributable to the effluents from the facility.

TABLE 3.12-1 (Continued)

TABLE NOTATION

- (5) The "upstream sample" shall be taken at a distance beyond significant influence of the discharge. The "downstream" sample shall be taken in an area beyond but near the mixing zone. "Upstream" samples in an estuary must be taken far enough upstream to be beyond the plant influence. Saltwater shall be sampled only when the receiving water is utilized for recreational activities.
- (6) A composite sample is one which the quantity (aliquot) of liquid sampled is proportional to the quantity of flowing liquid and in which the method of sampling employed results in a specimen that is representative of the liquid flow. In this program composite sample aliquots shall be collected at time intervals that are very short relative to the compositing period in order to assure obtaining a representative sample.
- (7) Groundwater samples shall be taken when this source is tapped for drinking or irrigation purposes in areas where the hydraulic gradient or recharge properties are suitable for contamination.
- (8) The dose shall be calculated for the maximum organ and age group, using the methodology and parameters in the ODCM.
- (9) If harvest occurs more than once a year, sampling shall be performed during each discrete harvest. If harvest occurs continuously, sampling shall be monthly. Attention shall be paid to including samples of tuberous and root food products.

TABLE 3.12-2

## REPORTING LEVELS FOR RADIOACTIVITY CONCENTRATIONS IN ENVIRONMENTAL SAMPLES

## Reporting Levels

Analysis	Water (pCi/l)	Airborne Particulate or Gases (pCi/m <sup>3</sup> )	Fish (pCi/Kg, wet)	Milk (pCi/l)	Food Products (pCi/Kg, wet)
H-3	2 x 10 <sup>4(a)</sup>				
Mn-54	1 x 10 <sup>3</sup>		3 x 10 <sup>4</sup>		
Fe-59	4 x 10 <sup>2</sup>		1 x 10 <sup>4</sup>		
Co-58	1 x 10 <sup>3</sup>		3 x 10 <sup>4</sup>		
Co-60	3 x 10 <sup>2</sup>		1 x 10 <sup>4</sup>		
Zn-65	3 x 10 <sup>2</sup>		2 x 10 <sup>4</sup>		
Zr-Nb-95	4 x 10 <sup>2</sup>				
I-131	2 <sup>(b)</sup>	0.9		3	1 x 10 <sup>2</sup>
Cs-134	30	10	1 x 10 <sup>3</sup>	60	1 x 10 <sup>3</sup>
Cs-137	50	20	2 x 10 <sup>3</sup>	70	2 x 10 <sup>3</sup>
Ba-La-140	2 x 10 <sup>2</sup>			3 x 10 <sup>2</sup>	

(a) For drinking water samples. This is a 40 CFR Part 141 value. If no drinking water pathway exists, a value of 3 x 10<sup>4</sup> pCi/l may be used.

(b) For drinking water samples. This is a 40 CFR Part 141 value. If no drinking water pathway exists, a value of 2 pCi/l may be used.

TABLE 4.12-1

DETECTION CAPABILITIES FOR ENVIRONMENTAL SAMPLE ANALYSIS<sup>(1), (2)</sup>LOWER LIMITS OF DETECTION (LLD)<sup>(3)</sup>

Analysis	Water (pCi/l)	Airborne Particulate or Gases (pCi/m <sup>3</sup> )	Fish (pCi/Kg, wet)	Milk (pCi/l)	Food Products (pCi/Kg, wet)	Sediment (pCi/Kg, dry)
gross beta	4	$1 \times 10^{-2}$				
H-3	2000*					
Mn-54	15		130			
Fe-59	30		260			
Co-58,60	15		130			
Zn-65	30		260			
Zr-Nb-95	15					
I-131	1**	$7 \times 10^{-2}$		1	60	
Cs-134	15	$5 \times 10^{-2}$	130	15	60	150
Cs-137	18	$6 \times 10^{-2}$	150	18	80	180
Ba-La-140	15			15		

\* LLD for drinking water samples. If no drinking water pathway exists, a value of 3000 pCi/l may be used.

\*\* LLD for drinking water samples. If no drinking water pathway exists, a value of 10 pCi/l may be used.

TABLE 4.12-1 (Continued)TABLE NOTATION

- (1) This list does not mean that only these nuclides are to be considered. Other peaks that are identifiable, together with those of the above nuclides, shall also be analyzed and reported in the Annual Radiological Environmental Operating Report pursuant to CONTROL 6.9.1.7.
- (2) Required detection capabilities for thermoluminescent dosimeters used for environmental measurements shall be in accordance with the recommendations of Regulatory Guide 4.13.
- (3) The LLD is defined, for purposes of these CONTROLS as the smallest concentration of radioactive material in a sample that will yield a net count, above system background, that will be detected with 95% probability with only 5% probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system, which may include radiochemical separation:

$$LLD = \frac{4.66 \cdot s_b}{E \cdot V \cdot 2.22E6 \cdot \xi \cdot \exp(-\lambda \Delta t)}$$

Where:

LLD is the "a priori" lower limit of detection as defined above (as microcuries per unit mass or volume).

$s_b$  is the standard deviation of the background counting rate or of the counting rate of a blank sample as appropriate (as counts per minute),

E is the counting efficiency (as counts per disintegration),

V is the sample size (in units of mass or volume),

2.22E6 is the number of disintegrations per minute per microcurie,

$\xi$  is the fractional radiochemical yield (when applicable),

$\lambda$  is the radioactive decay constant for the particular radionuclide, and

$\Delta t$  for environmental samples is the elapsed time between sample collection (or end of the sample collection period) and time of counting.

Typical values of E, V,  $\xi$ , and  $\Delta t$  should be used in the calculation.

TABLE 4.12-1 (Continued)TABLE NOTATION

It should be recognized that the LLD is defined as an a priori (before the fact) limit representing the capability of a measurement system and not as an a posteriori (after the fact) limit for a particular measurement. Analyses shall be performed in such a manner that the stated LLDs will be achieved under routine conditions. Occasionally background fluctuations, unavoidable small sample sizes the presence of interfering nuclides, or other uncontrollable circumstances may render these LLDs unachievable. In such cases, the contributing factors shall be identified and described in the Annual Radiological Environmental Operating Report pursuant to CONTROL 6.9.1.7.

RADIOLOGICAL ENVIRONMENTAL MONITORING3/4.12.2 LAND USE CENSUSCONTROLS

3.12.2. In accordance with the Salem Units 1 and 2 Technical Specifications 6.8.4.h.2, a land use census shall be conducted and shall identify within a distance of 8 km (5 miles) the location in each of the 16 meteorological sectors of the nearest milk animal, the nearest residence and the nearest garden\* of greater than 50 m<sup>2</sup> (500 ft<sup>2</sup>) producing broad leaf vegetation. (For elevated releases as defined in Regulatory Guide 1.111, Revision 1, July 1977, the land use census shall also identify within a distance of 5 km (3 miles) the locations in each of the 16 meteorological sectors of all milk animals and all gardens of greater than 50 m<sup>2</sup> producing broad leaf vegetation.

APPLICABILITY: At all times.

ACTION:

- a. With a land use census identifying a location(s) that yields a calculated dose or dose commitment greater than the values currently being calculated in CONTROL 4.11.2.3, identify the new location(s) in the next Radioactive Effluent Release Report, pursuant to CONTROL 6.9.1.8.
- b. With a land use census identifying a location(s) that yields a calculated dose or dose commitment (via the same exposure pathway) 20 percent greater than at a location from which samples are currently being obtained in accordance with CONTROL 3.12.1, add the new location(s) to the radiological environmental monitoring program within 30 days. The sampling location(s), excluding the control station location, having the lowest calculated dose or dose commitment(s), via the same exposure pathway, may be deleted from this monitoring program after October 31 of the year in which this land use census was conducted. Pursuant to CONTROL 6.9.1.8, identify the new location(s) in the next Radioactive Effluent Release Report and also include in the report a revised figure(s) and table for the ODCM reflecting the new location(s).
- c. The provisions of CONTROLS 3.0.3 and 3.0.4 are not applicable.

\*Broad leaf vegetation sampling of at least three different kinds of vegetation may be performed at the SITE BOUNDARY in each of two different direction sectors with the highest predicted D/Q in lieu of the garden census. CONTROLS for broadleaf vegetation sampling in Table 3.12-1.4c shall be followed, including analysis of control samples.

3/ 4.12 RADIOLOGICAL ENVIRONMENTAL MONITORING

3/4.12.2 LAND USE CENSUS (Cont'd)

SURVEILLANCE REQUIREMENTS

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4.12.2 The land use census shall be conducted during the growing season at least once per 12 months using that information that will provide the best results, such as by a door-to-door survey, visual survey, aerial survey, or by consulting local agriculture authorities. The results of the land use census shall be included in the Annual Radiological Environmental Operating Report pursuant to CONTROL 6.9.1.7.

RADIOLOGICAL ENVIRONMENTAL MONITORING

3/4.12.3 INTERLABORATORY COMPARISON PROGRAM

CONTROLS

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3.12.3 In accordance with Salem Units 1 and 2 Technical Specifications 6.8.4.h.3, analyses shall be performed on radioactive materials supplied as part of an Interlaboratory Comparison Program which has been approved by the Commission.

APPLICABILITY: At all times.

ACTION:

- a. With analyses not being performed as required above, report the corrective actions taken to prevent a recurrence to the Commission in the Annual Radiological Environmental Operating Report pursuant to Specification 6.9.1.7.
- b. The provisions of CONTROLS 3.0.3 and 3.0.4. are not applicable.

SURVEILLANCE REQUIREMENTS

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4.12.3 The Interlaboratory Comparison Program shall be described in the ODCM. A summary of the results obtained as part of the above required Interlaboratory Comparison Program shall be included in the Annual Radiological Environmental Operating Report pursuant to CONTROL 6.9.1.7.

BASES  
FOR  
SECTIONS 3.0 AND 4.0  
CONTROLS  
AND  
SURVEILLANCE REQUIREMENTS

NOTE

The BASES contained in the succeeding pages summarize the reasons for the CONTROLS of Sections 3.0 and 4.0, but are not considered a part of these CONTROLS.

## 3/4.3 INSTRUMENTATION

## BASES

3/4.3.3.8 RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

The radioactive liquid effluent instrumentation is provided to monitor and control, as applicable, the releases of radioactive materials in liquid effluents during actual or potential releases of liquid effluents. The alarm/trip setpoints for these instruments shall be calculated and adjusted in accordance with the procedures in the ODCM to ensure that the alarm/trip will occur prior to exceeding the limits of 10 CFR Part 20. The OPERABILITY and use of this instrumentation is consistent with the requirements of General Design Criteria 60, 63, and 64 of Appendix A to 10 CFR Part 50.

CROSS REFERENCE - TABLES 3.3-12 and 4.3-12

Unit 1:

T/S Table Item No.	Instrument Description	Acceptable RMS Channels
1a	Liquid Radwaste Effluent Line Gross Activity	1R18
1b	Steam Generator Blowdown Line Gross Activity	1R19A, B, C, and D
2a	Containment Fan Coolers Service Water Line Discharge Gross Activity	1R13 A, B, C, D and E

Unit 2:

T/S Table Item No.	Instrument Description	Acceptable RMS Channels
1a	Liquid Radwaste Effluent Line Gross Activity	2R18
1b	Steam Generator Blowdown Line Gross Activity	2R19A,B,C, and D <sup>(1)</sup>
2a	Containment Fan Coolers - Service Water Line Discharge Gross Activity	2R13A, B and C <sup>(1)</sup>
2b	Chemical Waste Basin Line Gross Activity	R37

- (1) The channels listed are required to be operable to meet a single operable channel for the Technical Specification's "Minimum Channels Operable" requirement.

## 3/ 4.3 INSTRUMENTATION

## BASES

3/4.3.3.9 RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION

The radioactive gaseous effluent instrumentation is provided to monitor and control, as applicable, the releases of radioactive materials in gaseous effluents during actual or potential releases of gaseous effluents. The alarm/trip setpoints for these instruments shall be calculated and adjusted in accordance with the procedures in the ODCM to ensure that the alarm/trip will occur prior to exceeding the limits of 10 CFR Part 20. The OPERABILITY and use of this instrumentation is consistent with the requirements of General Design Criteria 60, 63, and 64 of Appendix A to 10 CFR Part 50.

CROSS REFERENCE - TABLES 3.3-13 and 4.3-13

Unit 1:

T/S Table Item No.	Instrument Description	Acceptable RMS Channels
1a	Waste Gas Holdup System Noble Gas Activity	1R41A and D <sup>(1)(2)</sup>
2a	Containment Purge and Pressure - Vacuum Relief Noble Gas Activity	1R12A or 1R41A and D <sup>(1)(2)</sup>
3a	Plant Vent Header System Noble Gas Activity	1R16 or 1R41A and D <sup>(1)(2)</sup>
3b	Plant Vent Header System Iodine Sampler <sup>(3)</sup>	1RME 4, 5 (1R41) or 1XT8911 (1R45)
3c	Plant Vent Header System Particular Sampler <sup>(3)</sup>	1RME 4, 5 (1R41) or 1XT8911 (1R45)

- (1) The channels listed are required to be operable to meet a single operable channel for the Technical Specification's "Minimum Channels Operable" requirement.
- (2) 1R41D is the setpoint channel. 1R41A is the measurement channel.
- (3) Laboratory analysis of the sampler filters ensures that the limits of Specification 3.11.2.1 are not exceeded. Alarm/trip setpoints do not apply to these passive components.

## 3/ 4.3 INSTRUMENTATION

## BASES

## Unit 2:

T/S Table Item No.	Instrument Description	Acceptable RMS Channels
1a	Waste Gas Holdup System Noble Gas Activity	2R41A, B and D <sup>(1)(2)</sup>
2a	Containment Purge and Pressure - Vacuum Relief Noble Gas Activity	2R12A or 2R41A, B and D <sup>(1)(2)</sup>
3a	Plant Vent Header System Noble Gas Activity	2R16 or 2R41A, B and D <sup>(1)(2)</sup>

- (1) The channels listed are required to be operable to meet a single operable channel for the Technical Specification's "Minimum Channels Operable" requirement.
- (2) 2R41D is the setpoint channel. 2R41A and 2R41B are the measurement channels.

## 3/4.11 RADIOACTIVE EFFLUENTS

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#### 3/4.11.1 LIQUID EFFLUENTS

##### 3/4.11.1.1 CONCENTRATION

The CONTROL is provided to ensure that the concentration of radioactive materials released in liquid waste effluents will be less than the concentration levels specified in 10 CFR Part 20, Appendix B Table II, Column 2. This limitation provides additional assurance that the levels of radioactive materials in bodies of water in UNRESTRICTED AREAS will result in exposures within (1) the Section II.A design objectives of Appendix I, 10 CFR Part 50, to a MEMBER OF THE PUBLIC and (2) the limits of 10 CFR Part 20.106(a) to the population. The concentration limit for dissolved or entrained noble gases is based upon the assumption that Xe-135 is the controlling radioisotope and its MPC in air (submersion) was converted to an equivalent concentration in water using the methods described in International Commission on Radiological Protection (ICRP) Publication 2.

The required detection capabilities for radioactive materials in liquid waste samples are tabulated in terms of the lower limits of detection (LLDs).

##### 3/4.11.1.2 DOSE

This CONTROL is provided to implement the requirements of Sections II.A, III.A, and IV.A of Appendix I, 10 CFR Part 50. The CONTROL implements the guides set forth in Section II.A of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A of Appendix I to assure that the releases of radioactive material in liquid effluents will be kept "as low as is reasonably achievable." Also, for freshwater sites with drinking water supplies that can be potentially affected by plant operations, there is reasonable assurance that the operation of the facility will not result in radionuclide concentrations in the finished drinking water that are in excess of the requirements of 40 CFR Part 141. The dose calculations in the ODCM implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data, such that the actual exposure of a MEMBER OF THE PUBLIC through appropriate pathways is unlikely to be substantially underestimated. The equations specified in the ODCM for calculating the doses due to the actual release rates of radioactive materials in liquid effluents are consistent with the methodology provided in Regulatory Guide 1.109, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I," Revision 1, October 1977 and Regulatory Guide 1.113, "Estimating Aquatic Dispersion of Effluents from Accidental and Routine Reactor Releases for the Purposes of Implementing Appendix I," April 1977.

The CONTROL applies to the release of liquid effluents from each reactor at the site. For units with shared radwaste treatment systems, the liquid effluents from the shared system are proportioned among the units sharing that system.

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#### 3/4.11.1.3 LIQUID RADWASTE TREATMENT

The requirement that the appropriate portions of this system be used, when specified, provides assurance that the releases of radioactive materials in liquid effluents will be kept "as low as is reasonably achievable". This CONTROL implements the requirements of 10 CFR Part 50.36a, General Design Criterion 60 of Appendix A to 10 CFR Part 50 and the design objective given in Section II.0 of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the liquid radwaste treatment system were specified as a suitable fraction of the dose design objectives set forth the Section II.A of Appendix I, 10 CFR Part 50, for liquid effluents.

#### 3/4.11.2 GASEOUS EFFLUENTS

##### 3/4.11.2.1 DOSE RATE

This CONTROL is provided to ensure that the dose at any time at and beyond the SITE BOUNDARY from gaseous effluents from all units on the site will be within the annual dose limits of 10 CFR Part 20. The annual dose limits are the doses associated with the concentrations of 10 CFR Part 20, Appendix B, Table II, Column I. These limits provide reasonable assurance that radioactive material discharged in gaseous effluents will not result in the exposure of a MEMBER OF THE PUBLIC either within or outside the SITE BOUNDARY, to annual average concentrations exceeding the limits specified in Appendix B, Table II of 10 CFR Part 20 [10 CFR Part 20.106(b)]. For MEMBERS OF THE PUBLIC who may at times be within the SITE BOUNDARY, the occupancy of the individual will usually be sufficiently low to compensate for any increase in the atmospheric diffusion factor above that for the SITE BOUNDARY. Examples of calculations for such MEMBERS OF THE PUBLIC with the appropriate occupancy factors shall be given in the ODCM. The specified release rate limits restrict, at all times, the corresponding gamma and beta dose rates above background to a MEMBER OF THE PUBLIC at or beyond the SITE BOUNDARY to less than or equal to 500 mrem/year to the whole body and 3000 mrem/yr to the skin. These release rate limits also restrict, at all times, the corresponding thyroid dose rate above background to a child via the inhalation pathway to less than or equal to 1500 mrem/year.

This CONTROL applies to the release of gaseous effluents from all reactors at the site.

##### 3/4.11.2.2 DOSE - NOBLE GASES

This CONTROL is provided to implement the requirements of Section II.B, III.A and IV.A of Appendix I, 10 CFR Part 50. The CONTROL implements the guides set forth in Section II.B of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A of Appendix I to assure that the releases of radioactive material in gaseous effluents will be kept "as low as is reasonably achievable." The Surveillance Requirements implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data such that the actual exposure of a MEMBER OF THE PUBLIC through appropriate pathways is unlikely to be

## RADIOACTIVE EFFLUENTS

### BASES

substantially underestimated. The dose calculations established in the ODCM for calculating the doses due to the actual release rates of radioactive noble gases in gaseous effluents are consistent with the methodology provided in Regulatory Guide 1.109, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR 50, Appendix I," Revision I, October 1977 and Regulatory Guide 1.111, "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water Cooled Reactors," Revision 1, July 1977. The ODCM equations provided for determining the air doses at and beyond the SITE BOUNDARY are based upon the historical average atmospheric conditions.

### 3/4.11.2.3 DOSE - IODINE-131, TRITIUM, AND RADIONUCLIDES IN PARTICULATE FORM

This CONTROL is provided to implement the requirements of Section II.C, III.A and IV.A of Appendix I, 10 CFR Part 50. The CONTROL are the guides set forth in Section II.C of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A of Appendix I to assure that the releases of radioactive material in gaseous effluents will be kept "as low as is reasonably achievable." The ODCM calculational methods specified in Surveillance Requirements implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data such that the actual exposure of a MEMBER OF THE PUBLIC through appropriate pathways is unlikely to be substantially underestimated. The ODCM calculational methods for calculating the doses due to the actual release rates of the subject materials are consistent with the methodology provided in Regulatory Guide 1.109, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR 50, Appendix I," Revision 1, October 1977 and Regulatory Guide 1.111, "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water Cooled Reactors," Revision 1, July 1977. These equations also provide for determining the actual dose based upon the historical average atmospheric conditions. The release rate controls for iodine-131, tritium, and radionuclides in particulate form with half-life greater than 8 days are dependent on the existing radionuclide pathways to man in the areas at and beyond the SITE BOUNDARY. The pathways that were examined in the development of these calculations were: 1) individual inhalation of airborne radionuclides, 2) deposition of radionuclides onto green leafy vegetation with subsequent consumption by man, 3) deposition onto grassy areas where milk animals and meat producing animals graze with consumption of the milk and meat by man, and 4) deposition on the ground with subsequent exposure of man.

### 3/4.11.2.4 GASEOUS RADWASTE TREATMENT SYSTEM

The requirement that the appropriate portions of this system be used, when specified, provides reasonable assurance that the releases of radioactive materials in gaseous effluents will be kept "as low as is reasonably achievable." This CONTROL implements the requirements of 10 CFR Part 50.36a, General Design Criterion 60 of Appendix A to 10 CFR Part 50 and the design objectives given in Section II.0 of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the systems were specified as a suitable fraction of the dose design objectives set forth in Section II.B and II.C of Appendix I, 10 CFR Part 50, for gaseous effluents.

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This CONTROL is provided to meet the dose limitations of 40 CFR Part 190 that have now been incorporated into 10 CFR Part 20 to 46 Fr 18525. The CONTROL requires the preparation and submittal of a Special Report whenever the calculated doses from plant radioactive effluents exceed twice the design objective doses of Appendix I. For sites containing up to 4 reactors, it is highly unlikely that the resultant dose to a MEMBER OF THE PUBLIC will exceed the dose limits of 40 CFR Part 190 if the individual reactors remain within the reporting requirement level. The Special Report will describe a course of action that should result in the limitation of the annual dose to a MEMBER OF THE PUBLIC to within the 40 CFR Part 190 limits. For purposes of the Special Report, it may be assumed that the dose commitment to the MEMBER OF THE PUBLIC from other uranium fuel cycle sources is negligible, with the exception that dose contributions from other nuclear fuel cycle facilities at the same site or within a radius of 8 km must be considered. If the dose to any MEMBER OF THE PUBLIC is estimated to exceed the requirements of 40 CFR Part 190, the Special Report with a request for a variance (provided the release conditions resulting in violation of 40 CFR Part 190 have not already been corrected), in accordance with the provisions of 40 CFR Part 190 and 10 CFR Part 20.405c, is considered to be a timely request and fulfills the requirements of 40 CFR Part 190 until NRC staff action is completed. The variance only relates to the limits of 40 CFR Part 190, and does not apply in any way to the other requirements for dose limitation of 10 CFR Part 20, as addressed in CONTROLS 3.11.1 and 3.11.2. An individual is not considered a MEMBER OF THE PUBLIC during any period in which he/she is engaged in carrying out any operation that is part of the nuclear fuel cycle.

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#### 3/4.12 RADIOLOGICAL ENVIRONMENTAL MONITORING

##### 3/4.12.1 MONITORING PROGRAM

The radiological environmental monitoring program required by this CONTROL provides measurements of radiation and of radioactive materials in those exposure pathways and for those radionuclides that lead to the highest potential radiation exposures of MEMBERS OF THE PUBLIC resulting from the station operation. This monitoring program implements Section IV.B.2 of Appendix I to 10 CFR Part 50 and thereby supplements the radiological effluent monitoring program by verifying that the measurable concentrations of radioactive materials and levels of radiation are not higher than expected on the basis of the effluent measurements and the modeling of the environmental exposure pathways. The initial specified monitoring program will be effective for at least the first three years of commercial operation. Following this period, program changes may be initiated based on operational experience.

The LLDs required by Table 4.12-1 are considered optimum for routine environmental measurements in industrial laboratories. It should be recognized that the LLD is defined as an a priori (before the fact) limit representing the capability of a measurement system and not as an a posteriori (after the fact) limit for a particular measurement.

##### 3/4.12.2 LAND USE CENSUS

This CONTROL is provided to ensure that changes in the use of areas at and beyond the SITE BOUNDARY are identified and that modifications to the radiological environmental monitoring program are made if required by the results of this census. The best information from the door-to-door survey, aerial survey or consulting with local agricultural authorities shall be used. This census satisfies the requirements of Section IV.B.3 of Appendix I to 10 CFR Part 50. Restricting the census to gardens of greater than 50m<sup>2</sup> provides assurance that significant exposure pathways via leafy vegetables will be identified and monitored since a garden of this size is the minimum required to produce the quantity (26 kg/year) of leafy vegetables assumed in Regulatory Guide 1.109 for consumption by a child. To determine this minimum garden size, the following assumptions were made: 1) 20% of the garden was used for growing broad leaf vegetation (i.e., similar to lettuce and cabbage), and 2) yield of 2 kg/m<sup>2</sup>.

##### 3/4.12.3 INTERLABORATORY COMPARISON PROGRAM

This requirement for participation in an Interlaboratory Comparison Program is provided to ensure that independent checks on the precision and accuracy of the measurements of radioactive material in environmental sample matrices are performed as part of the quality assurance program for environmental monitoring in order to demonstrate that the results are reasonably valid for the purposes of Section IV.B.2 of Appendix I to 10 CFR Part 50.

SECTION 5.0  
DESIGN FEATURES

5.0 DESIGN FEATURES

5.1 SITE

UNRESTRICTED AREAS FOR RADIOACTIVE GASEOUS AND LIQUID EFFLUENTS

5.1.3 UNRESTRICTED AREAS within the SITE BOUNDARY that are accessible to MEMBERS OF THE PUBLIC, shall be as shown in Figure 5.1-3. (Provided FOR INFORMATION ONLY. Technical Specifications Section 5.0 is controlling.)



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### 6.9.1.7 ANNUAL RADIOLOGICAL ENVIRONMENTAL OPERATING REPORT

6.9.1.7 In accordance with Salem Units 1 and 2 Technical Specifications 6.9.1.7, Routine Radiological Environmental Operating Reports\* covering the operation of the unit during the previous calendar year shall be submitted prior to May 1 of each year.

The Annual Radiological Environmental Operating Reports shall include summaries, interpretations, and an analysis of trends of the results of the radiological environmental surveillance activities for the report period, including a comparison with preoperational studies with operational controls (as appropriate), and with previous environmental surveillance reports, and an assessment of the observed impacts of the plant operation on the environment. The reports shall also include the results of land use censuses required by CONTROL 3.12.2. The Annual Radiological Environmental Operating Reports shall include the results of analysis of all radiological environmental samples and of all measurements taken during the period pursuant to the Table and Figures in the environmental radiation section of the ODCM; as well as summarized and tabulated results of locations specified in these analyses and measurements in the format of the table in the Radiological Assessment Branch Technical Position, Revision 1, November 1979. In the event that some individual results are not available for inclusion with the report, the report shall be submitted noting and explaining the reasons for the missing results. The missing data shall be submitted as soon as possible in a supplementary report.

The reports shall also include the following: a summary description of the radiological environmental monitoring program; at least two legible maps, one covering sampling locations near the SITE BOUNDARY and a second covering the more distant locations, all keyed to a table giving distances and directions from the centerline of one reactor; the results of licensee participation in the Interlaboratory Comparison Program, required by CONTROL 3.12.1; and discussion of all analyses in which the LLD required by Table 4.12-1 was not achievable.

### 6.9.1.8 RADIOACTIVE EFFLUENT RELEASE REPORT

6.9.1.8 In accordance with Salem Units 1 and 2 Technical Specifications 6.9.1.8, Routine Radioactive Effluent Release Reports\* covering the operation of the units during the previous calendar year of operation shall be submitted by May 1 of each year and in accordance with the requirements of 10CFR50.36a.

The Radioactive Effluent Release Reports shall include a summary of the quantities of radioactive liquid and gaseous effluents and solid waste released from the unit as outlined in Regulatory Guide 1.21. "Measuring,

\* A single submittal may be made for a multiple unit station. The submittal should combine those sections that are common to all units at the station; however, for units with separate radwaste systems, the submittal shall specify the releases of radioactive material from each unit.

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Evaluating, and Reporting Radioactivity in Solid Wastes and Releases of Radioactive Materials in Liquid and Gaseous Effluents from Light-Water-Cooled Nuclear Power Plants." Revision 1, June 1974, with data summarized on a quarterly basis following the format of Appendix B thereof.

The Radioactive Effluent Release Report shall include an annual summary of hourly meteorological data collected over the previous year. This annual summary may be either in the form of an hour-by-hour listing of magnetic tape of wind speed, wind direction, atmospheric stability, and precipitation (if measured), or in the form of joint frequency distributions of wind speed, wind direction, and atmospheric stability. The report shall include an assessment of the radiation doses due to the radioactive liquid and gaseous effluents released from the unit or station during the previous calendar year. The report shall also include an assessment of the radiation doses from radioactive liquid and gaseous effluents to MEMBERS OF THE PUBLIC due to their activities inside the SITE BOUNDARY (Figure 5.1-3) during the report period. All assumptions used in making these assessments (i.e., specific activity, exposure time and location) shall be included in these reports. The historical annual average meteorology or the meteorological conditions concurrent with the time of release of radioactive materials in gaseous effluents (as determined by sampling frequency and measurement) shall be used for determining the gaseous pathway doses. The assessment of radiation doses shall be performed in accordance with the OFFSITE DOSE CALCULATION MANUAL.

The Radioactive Effluent Release Report shall also include an assessment of radiation doses to the likely most exposed MEMBER OF THE PUBLIC from reactor releases and other nearby uranium fuel cycle sources (including doses from primary effluent pathways and direct radiation) for the previous calendar year to show conformance with 40 CFR Part 190, Environmental Radiation Protection Standards for Nuclear Power Operation. Acceptable methods for calculating the dose contribution from liquid and gaseous effluents are given in Regulatory Guide 1.109, Rev. 1, October 1977.

The Radioactive Effluent Release Reports shall include the following information for each class of solid waste (as defined by 10 CFR Part 61) shipped offsite during the report period:

- a. Container volume.
- b. Total curie quantity (specify whether determined by measurement or estimate),
- c. Principal radionuclides (specify whether determined by measurement or estimate),
- d. Source of waste and processing employed (e.g., dewatered spent resin, compacted dry waste, evaporator bottoms),
- e. Type of container (e.g., LSA, Type A, Type B, Large Quantity), and
- f. Solidification agent or absorbent (e.g., cement, urea formaldehyde).

The Radioactive Effluent Release Report shall include a list of descriptions of unplanned releases from the site to UNRESTRICTED AREAS of radioactive materials in gaseous and liquid effluents made during the reporting period.

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The Radioactive Effluent Release Report shall include any changes made during the reporting period to the PROCESS CONTROL PROGRAM (PCP) and to the OFFSITE DOSE CALCULATION MANUAL (ODCM), as well as a listing of new locations for dose calculations and/or environmental monitoring identified by the land use census pursuant to CONTROL 3.12.2.

6.15 MAJOR CHANGES TO RADIOACTIVE LIQUID, GASEOUS AND SOLID WASTE TREATMENT SYSTEMS

6.15.1 Licensee initiated major changes to the radioactive waste system (liquid, gaseous and solid):

1. Shall be reported to the Commission in the UFSAR for the period in which the evaluation was reviewed by (SORC). The discussion of each change shall contain:
  - a. A summary of the evaluation that led to the determination that the change could be made in accordance with 10CFR50.59;
  - b. Sufficient detailed information to totally support the reason for the change without benefit of additional or supplemental information;
  - c. A detailed description of the equipment, components and processes involved and the interfaces with other plant systems;
  - d. An evaluation of the change, which shows the predicted releases of radioactive materials in liquid and gaseous effluents and/or quantity of solid waste that differ from those previously predicted in the license application and amendments thereto;
  - e. An evaluation of the change, which shows the expected maximum exposures to individual in the unrestricted area and to the general population that differ from those previously estimated in the license application and amendments thereto;
  - f. A comparison of the predicted releases of radioactive materials, in liquid and gaseous effluents and in solid waste, to the actual releases for the period prior to when the changes are to be made;
  - g. An estimate of the exposure to plant operating personnel as a result of the change; and
  - h. Documentation of the fact that the change was reviewed and found acceptable by the (SORC).
2. Shall become effective upon review and acceptance by the SORC.

## **PART II – CALCULATIONAL METHODOLOGIES**

## 1.0 LIQUID EFFLUENTS

### 1.1 Radiation Monitoring Instrumentation and Controls

The liquid effluent monitoring instrumentation and controls at Salem for controlling and monitoring normal radioactive material releases in accordance with the Salem Radiological Effluent Technical Specifications (CONTROLS) are summarized as follows:

- 1) Alarm (and Automatic Termination) - 1-R18 (Unit 1) and 2-R18 (Unit 2) provide the alarm and automatic termination of liquid radioactive material releases as required by Technical Specification (CONTROL) 3.3.3.8.

1-R19 A, B, C, and D provide the alarm and isolation function for the Unit 1 steam generator blowdown lines. 2-R19 A, B, C, and D provide this function for Unit 2.

- 2) Alarm (only) - The alarm functions for the Service Water System are provided by the radiation monitors on the Containment Fan Cooler discharges (1R 13 A,B,C,D and E for Unit 1 and 2R 13 A, B, and C for Unit 2).

Releases from the secondary system are routed through the Chemical Waste Basin where the effluent is monitored (with an alarm function) by 2R37 prior to release to the environment.

Liquid radioactive release flow diagrams with the applicable, associated radiation monitoring instrumentation and controls are presented as Figures 1-1 and 1-2 for Units 1 and 2, respectively. The Liquid Radioactive Waste System is presented in Figure 1-3.

### 1.2 Liquid Effluent Monitor Setpoint Determination

Per the requirements of Technical Specification (CONTROL) 3.3.3.8, alarm setpoints shall be established for the liquid effluent monitoring instrumentation to ensure that the release concentration limits of Specification 3.11.1.1 are met (i.e., the concentration of radioactive material released in liquid effluents to UNRESTRICTED AREAS shall be limited to the concentrations specified in 10 CFR 20, Appendix B, Table II, Column 2, (Appendix F) for radionuclides and 2.0E-04  $\mu\text{Ci/ml}$  for dissolved or entrained noble gases).

The following equation\* must be satisfied to meet the liquid effluent restrictions:

$$c \leq \frac{C(F + f)}{f} \quad (1.1)$$

Where:

- C = the effluent concentration limit of Technical Specification (CONTROL) 3.11.1.1 implementing the 10 CFR 20 MPC (Appendix F) for the site, in  $\mu\text{Ci/ml}$
- c = the setpoint, in  $\mu\text{Ci/ml}$ , of the radioactivity monitor measuring the radioactivity concentration in the effluent line prior to dilution and subsequent release; the setpoint,

- represents a value which, if exceeded, would result in concentrations exceeding the limits of 10 CFR 20 (Appendix F) in the UNRESTRICTED AREA
- f = the flow rate at the radiation monitor location, in volume per unit time, but in the same units as F, below
- F = the dilution water flow rate as measured prior to the release point, in volume per unit time

[Note that if no dilution is provided,  $c \leq C$ . Also, note that when (F) is large compared to (f), then  $(F + f) = F$ .]

\* Adapted from NUREG-0133

### 1.2.1 Liquid Effluent Monitors (Radwaste, Steam Generator Blowdown, Chemical Waste Basin and Service Water.

The setpoints for the liquid effluent monitors at the Salem Nuclear Generating Station are determined by the following equations:

$$SP \leq \frac{MPCe * SEN * CW * CF * AF}{RR} + bkg \quad (1.2)$$

with:

$$MPCe = \frac{\sum_i C_i \text{ (gamma only)}}{\sum_i \frac{C_i}{MPC_i} \text{ (gamma only)}} \quad (1.3)$$

Where:

- SP = alarm setpoint corresponding to the maximum allowable release rate (cpm)
- MPCe = an effective MPC value for the mixture of gamma emitting radionuclides in the effluent stream ( $\mu\text{Ci/ml}$ )
- $C_i$  = the concentration of radionuclide i in the undiluted liquid effluents ( $\mu\text{Ci/ml}$ )
- $MPC_i$  = the MPC value corresponding to radionuclide i from 10 CFR 20, Appendix B, Table II, Column 2 (Appendix F) ( $\mu\text{Ci/ml}$ )
- SEN = the sensitivity value to which the monitor is calibrated (cpm per  $\mu\text{Ci/ml}$ )
- CW = the circulating water flow rate (dilution water flow) at the time of release (gal/min)
- RR = the liquid effluent release rate (gal/min)
- bkg = the background of the monitor (cpm)
- CF = Correction factor to account for non-gamma emitting nuclides in setpoint calculations.
- AF = an allocation factor applicable for steam generator blowdown

The radioactivity monitor setpoint equation (1.2) remains valid during outages when the circulating water dilution is potentially at its lowest value. Reduction of the waste stream flow (RR) may be necessary during these periods to meet the discharge criteria. However, in order to maximize the available plant discharge dilution and thereby minimize the potential offsite doses, releases from either Unit-1 or Unit-2 may be routed to either the Unit-1 or Unit-2 Circulating Water System discharge.

This routing is possible via interconnections between the Service Water Systems. Procedural restrictions prevent simultaneous batch releases from either a single unit or both units into a single Circulating Water System discharge.

### 1.2.2 Conservative Default Values

Conservative alarm setpoints may be determined through the use of default parameters. Tables 1-1 and 1-2 summarize all current default values in use for Salem Unit-1 and Unit-2, respectively. They are based upon the following:

- a) substitution of the effective MPC value with a default value of  $6.05E-06$   $\mu\text{Ci/ml}$  (Unit 1) and  $4.81E-06$   $\mu\text{Ci/ml}$  (Unit 2). (refer to Appendix A for justification);
- b) for additional conservatism\*, substitution of the I-131 MPC value of  $3E-07$   $\mu\text{Ci/ml}$  for the R19 Steam Generator Blowdown monitors, the R-37 Chemical Waste Basin monitor and the R-13 Service Water monitors;
- c) for conservatism, use of an allocation factor of 0.5 for the Steam Generator Blowdown monitors to limit consequences of potential simultaneous primary-to-secondary leaks in two steam generators.\*\* The allocation factor equals 1.0 for all other liquid effluent setpoints;
- d) substitutions of the operational circulating water flow with the lowest flow, in gal/min;
- e) substitutions of the effluent release rate with the highest allowed rate, in gal/min; and,
- f) substitution of a Correction factor of 0.75 to account for non-gamma emitting nuclides.

For batch liquid releases a fixed alarm setpoint is established for the 1, 2 R18 monitors and the release rate is controlled to ensure the inequality of equation 1.1 is maintained. With this approach, values selected for the parameters in the setpoint calculation (e.g., Table 1-1 and Table 1-2) should be any set of reasonable values that provide a setpoint value reasonably above anticipated monitor response, plus background, so as not to yield spurious alarms. The release rate is controlled to ensure compliance with the requirements of Technical Specification (CONTROL) 3.3.3.8.

Calculations, as performed by Engineering, to establish the actual fixed setpoints for use in the plant, incorporate uncertainties and instrument drift. These factors will cause the actual installed instrument setpoint to be at a lower (conservative) value. However, for batch releases, when the rate is controlled, these uncertainties and drift should not be included in the evaluation of acceptable release rate, since this could cause a non-conservative correction, i.e., a higher allowable release rate. Therefore, for 1, 2 R18 monitors, the setpoint value used for calculating the allowable release rate should be that value prior to correction for uncertainty and drift.

\* Based upon the potential for I-131 to be present in the secondary and service water systems, the use of the default effective MPC ( $\text{MPC}_e$ ) value as derived in Appendix A may be non-conservative for the 1, 2 R-19 SGBD monitors, the R-37 Chemical Waste Basin monitor and the R-13 Service Water monitors.

\*\*Setpoints using the Allocation Factor of 0.5 become invalid if primary-to-secondary leaks are identified in more than two steam generators simultaneously.

### 1.3 Liquid Effluent Concentration Limits - 10 CFR 20

Technical Specification (CONTROL) 3.11.1.1 limits the concentration of radioactive material in liquid effluents (after dilution in the Circulating Water System) to less than the concentrations as specified in 10 CFR 20, Appendix B, Table II, Column 2 (Appendix F) for radionuclides other than noble gases. Noble gases are limited to a diluted concentration of  $2.0E-04 \mu\text{Ci/ml}$ .

Release rates are controlled and radiation monitor alarm setpoints are established as addressed above to ensure that these concentration limits are not exceeded. However, in the event any liquid release results in an alarm setpoint being exceeded, an evaluation of compliance with the concentration limits of Technical Specification (CONTROL) 3.11.1.1 may be performed using the following equation:

$$\sum_i \left( \frac{C_i}{MPC} * \frac{RR}{CW + RR} \right) \leq 1 \quad (1.4)$$

Where:

- $C_i$  = actual concentration of radionuclide  $i$  as measured in the undiluted liquid effluent ( $\mu\text{Ci/ml}$ )
- $MPC$  = the MPC value corresponding to radionuclide  $i$  from 10 CFR 20, Appendix B, Table II, Column 2 ( $\mu\text{Ci/ml}$ ) [ODCM Appendix F]  
=  $2E-04 \mu\text{Ci/ml}$  for dissolved or entrained noble gases
- $RR$  = the actual liquid effluent release rate (gal/min)
- $CW$  = the actual circulating water flow rate (dilution water flow) at the time of the release (gal/min)

### 1.4 Liquid Effluent Dose Calculation - 10 CFR 50

#### 1.4.1 MEMBER OF THE PUBLIC Dose - Liquid Effluents.

Technical Specification (CONTROL) 3.11.1.2 limits the dose or dose commitment to MEMBERS OF THE PUBLIC from radioactive materials in liquid effluents from each unit of the Salem Nuclear Generating Station to:

- during any calendar quarter;
  - $\leq 1.5$  mrem to total body per unit
  - $\leq 5.0$  mrem to any organ per unit
- during any calendar year;
  - $\leq 3.0$  mrem to total body per unit
  - $\leq 10.0$  mrem to any organ per unit.

Per the surveillance requirements of Technical Specification (CONTROL) 4.11.1.2, the following calculational methods shall be used for determining the dose or dose commitment due to the liquid radioactive effluents from Salem:

$$D_o = \frac{1.67E-02 * VOL}{CW} * \sum_i (C_i * A_{io}) \quad (1.5)$$

Where:

- $D_o$  = dose or dose commitment to organ o (mrem). Total body dose can also be calculated using site-related total body dose commitment factor.
- $A_{io}$  = site-related ingestion dose commitment factor to the total body or any organ o for radionuclide i (mrem/hr per  $\mu\text{Ci/ml}$ )
- $C_i$  = average concentration of radionuclide i, in undiluted liquid effluent representative of the volume VOL ( $\mu\text{Ci/ml}$ )
- VOL = volume of liquid effluent released (gal)
- CW = average circulating water discharge rate during release period (gal/min)
- 1.67E-02 = conversion factor (hr/min)

The site-related ingestion dose/dose commitment factors ( $A_{io}$ ) are presented in Table 1-3 and have been derived in accordance with the requirements of NUREG-0133 by the equation:

$$A_{io} = 1.14E + 05 * [(UI * BI_i) + (UF * BF_i)] * DF_{io} \quad (1.6)$$

Where:

- $A_{io}$  = composite dose parameter for the total body or critical organ o of an adult for radionuclide i, for the fish and invertebrate ingestion pathways (mrem/hr per  $\mu\text{Ci/ml}$ )
- UI = adult invertebrate consumption (5 kg/yr)
- $BI_i$  = bioaccumulation factor for radionuclide i in invertebrates from Table 1-4 (pCi/kg per pCi/l)
- UF = adult fish consumption (21 kg/yr)
- $BF_i$  = bioaccumulation factor for radionuclide i in fish from Table 1-4 (pCi/kg per pCi/l)
- $DF_{io}$  = dose conversion factor for nuclide i for adults in pre-selected organ, o, from Table E-11 of Regulatory Guide 1.109 (mrem/pCi)
- 1.14E+05 = conversion factor (pCi/ $\mu\text{Ci}$  \* ml/kg per hr/yr)

The radionuclides included in the periodic dose assessment per the requirements of Technical Specification (CONTROL) 3/4.11.1.2 are those as identified by gamma spectral analysis of the liquid waste samples collected and analyzed per the requirements of Technical Specification (CONTROL) 3/4.11.1.1, Table 4.11-1.

Radionuclides requiring radiochemical analysis (e.g., Sr-89 and Sr-90) will be added to the dose analysis at a frequency consistent with the required minimum analysis frequency of Technical Specification (CONTROL) Table 4.11-1.

### 1.4.2 Simplified Liquid Effluent Dose Calculation.

In lieu of the individual radionuclide dose assessment as presented in Section 1.4.1, the following simplified dose calculation equation may be used for demonstrating compliance with the dose limits of Technical Specification (CONTROL) 3.11.1.2. (Refer to Appendix B for the derivation and justification for this simplified method.)

#### Total Body

$$D_{tb} = \frac{1.21E + 03 * VOL}{CW} * \sum_i C_i \quad (1.7)$$

#### Maximum Organ

$$D_{max} = \frac{2.52E + 04 * VOL}{CW} * \sum_i C_i \quad (1.8)$$

Where:

- $C_i$  = average concentration of radionuclide  $i$ , in undiluted liquid effluent representative of the volume  $VOL$  ( $\mu\text{Ci/ml}$ )
- $VOL$  = volume of liquid effluent released (gal)
- $CW$  = average circulating water discharge rate during release period (gal/min)
- $D_{tb}$  = conservatively evaluated total body dose (mrem)
- $D_{max}$  = conservatively evaluated maximum organ dose (mrem)
- $1.21E+03$  = conversion factor (hr/min) and the total body dose conversion factor (Fe-59, total body --  $7.27E+04$  mrem/hr per  $\mu\text{Ci/ml}$ )
- $2.52E+04$  = conversion factor (hr/min) and the conservative maximum organ dose conversion factor (Nb-95, GI-LLI --  $1.51E+06$  mrem/hr per  $\mu\text{Ci/ml}$ )

### 1.5 Secondary Side Radioactive Liquid Effluents and Dose Calculations During Primary to Secondary Leakage

During periods of primary to secondary leakage (i.e., steam generator tube leaks), radioactive material will be transmitted from the primary system to the secondary system. The potential exists for the release of radioactive material to the off-site environment (Delaware River) via secondary system discharges. Potential releases are controlled/monitored by the Steam Generator Blowdown monitors (R19) and the Chemical Waste Basin monitor (2R37).

However to ensure compliance with the regulatory limits on radioactive material releases, it may be desirable to account for potential releases from the secondary system during periods of primary to secondary leakage. Any potentially significant releases will be via the Chemical Waste Basin with the major source of activity being the Steam Generator Blowdown.

With identified radioactive material levels in the secondary system, appropriate samples should be collected and analyzed for the principal gamma emitting radionuclides. Based on the identified

radioactive material levels and the volume of water discharged, the resulting environmental doses may be calculated based on equation (1.5).

Because the release rate from the secondary system is indirect (e.g., SG blowdown is normally routed to condenser where the condensate clean-up system will remove much of the radioactive material), samples should be collected from the final release point (i.e., Chemical Waste Basin) for quantifying the radioactive material releases. However, for conservatism and ease of controlling and quantifying all potential release paths, it is prudent to sample the SG blowdown and to assume all radioactive material is released directly to the environment via the Chemical Waste Basin. This approach while not exact, is conservative and ensures timely analysis for regulatory compliance. Accounting for radioactive material retention of the condensate clean-up system ion exchange resins may be needed to more accurately account for actual releases.

### 1.6 Liquid Effluent Dose Projections

Technical Specification (CONTROL) 3.11.1.3 requires that the liquid radioactive waste processing system be used to reduce the radioactive material levels in the liquid waste prior to release when the quarterly projected doses exceed:

- 0.375 mrem to the total body, or
- 1.25 mrem to any organ.

The applicable liquid waste processing system for maintaining radioactive material releases ALARA is the ion exchange system as delineated in Figure 1-3. Alternately, the waste evaporator as presented in the Salem FSAR has processing capabilities meeting the NRC ALARA design requirements and may be used in conjunction or in lieu of the ion exchange system for waste processing requirements in accordance with Technical Specification (CONTROL) 3.11.1.3. These processing requirements are applicable to each unit individually. Exceeding the projected dose requiring processing prior to release for one unit does not in itself dictate processing requirements for the other unit.

Dose projections are made at least once per 31 days by the following equations:

$$D_{ibp} = D_{ib} \left( \frac{91}{d} \right) \quad (1.9)$$

$$D_{maxp} = D_{max} \left( \frac{91}{d} \right) \quad (1.10)$$

Where:

- $D_{ibp}$  = the total body dose projection for current calendar quarter (mrem)
- $D_{ib}$  = the total body dose to date for current calendar quarter as determined by Equation 1.5 or 1.7 (mrem)
- $D_{maxp}$  = the maximum organ dose projection for current calendar quarter (mrem)
- $D_{max}$  = the maximum organ dose to date for current calendar quarter as determined by Equation 1.5 or 1.7 (mrem)
- $d$  = the number of days to date for current calendar quarter
- 91 = the number of days in a calendar quarter

## 2.0 GASEOUS EFFLUENTS

### 2.1 Radiation Monitoring Instrumentation and Controls

The gaseous effluent monitoring instrumentation and controls at Salem for controlling and monitoring normal radioactive material releases in accordance with the Radiological Effluent Technical Specifications (CONTROLS) are summarized as follows:

- 1) Waste Gas Holdup System - The vent header gases are collected by the waste gas holdup system. Gases may be recycled to provide cover gas for the CVCS hold-up tank or held in the waste gas tanks for decay prior to release. Waste gas decay tanks are batch released after sampling and analysis. The tanks are discharged via the Plant Vent. 1-R41D provides noble gas monitoring and automatic isolation of waste gas decay tank releases for Unit-1. This function is provided by 2-R41D for Unit-2.
- 2) Containment Purge and Pressure/Vacuum Relief - containment purges and pressure/vacuum reliefs are released to the atmosphere via the respective unit Plant Vent. Noble gas monitoring and auto isolation function are provided by 1-R41D for Unit-1 and 2-R41D for Unit-2. Additionally, in accordance with Technical Specification (CONTROL) 3.3.3.9, Table 3.3-13, 1-R12A and 2-R12A may be used to provide the containment monitoring and automatic isolation function during purge and pressure/vacuum reliefs (\*).
- 3) Plant Vent - The Plant Vent for each respective unit receives discharges from the waste gas hold-up system, condenser evacuation system, containment purge and pressure/vacuum reliefs, and the Auxiliary Building ventilation. Effluents are monitored by R41D, a flow through gross activity monitor (for noble gas monitoring). Additionally, in-line gross activity monitors (1-R16 and 2-R16) provide redundant back-up monitoring capabilities to the R41D monitors. Radioiodine and particulate sampling capabilities are provided by charcoal cartridge and filter medium samplers. Additionally, back-up sampling capability for radioiodine and particulates is provided at the 1-R45 and 2-R45 sampling skids. Plant Vent flow rate is measured and as a back-up may be determined empirically as a function of fan operation (fan curves). Sampler flow rates are determined by flow rate instrumentation (e.g., venturi rotameter).

Gaseous radioactive effluent flow diagrams with the applicable, associated radiation monitoring instrumentation and controls are presented in Figures 2-1. A simplified diagram of the Gaseous radioactive waste disposal system is provided in Figure 2-2.

**\* The R12A monitors also provide the safety function of containment isolation in the event of a fuel handling accident during refueling. During MODE 6 in accordance with Technical Specification (CONTROL) 3/4.3.3, Table 3.3-6, the R12A alarm/trip setpoint shall be established at twice background. This will provide containment isolation and indication of unexpected increases in containment airborne radioactive material levels which can be indicative of fuel degradation. The R41D monitor may also provide this function if the R12A monitor is inoperable during MODE 6.**

## 2.2 Gaseous Effluent Monitor Setpoint Determination

### 2.2.1 Containment and Plant Vent Monitor

Per the requirements of Technical Specification (CONTROL) 3.3.3.9, alarm setpoints shall be established for the gaseous effluent monitoring instrumentation to ensure that the release rate of noble gases does not exceed the limits of Specification 3.11.2.1, which corresponds to a dose rate at the SITE BOUNDARY of 500 mrem/year to the total body or 3000 mrem/year to the skin.

Based on a grab sample analysis of the applicable release (i.e., grab sample of the Containment atmosphere, waste gas decay tank, or Plant Vent), the radiation monitoring alarm setpoints may be established by the following calculation method. The measured radionuclide concentrations and release rate are used to calculate the fraction of the allowable release rate, as limited by Specification 3.11.2.1, by the equation:

$$FRAC = \left[ 4.72E + 02 * \chi/Q * VF * \sum_i (C_i * K_i) \right] / 500 \quad (2.1)$$

$$FRAC = \left[ 4.72E + 02 * \chi/Q * VF * \sum_i (C_i * (L_i + 1.1M_i)) \right] / 3000 \quad (2.2)$$

Where:

- FRAC = fraction of the allowable release rate based on the identified radionuclide concentrations and the release flow rate
- $\chi/Q$  = annual average meteorological dispersion to the controlling site boundary location (sec/m<sup>3</sup>)
- VF = ventilation system flow rate for the applicable release point and monitor (ft<sup>3</sup>/min)
- C<sub>i</sub> = concentration of noble gas radionuclide i as determined by radioanalysis of grab sample (μCi/cm<sup>3</sup>)
- K<sub>i</sub> = total body dose conversion factor for noble gas radionuclide i (mrem/yr per μCi/m<sup>3</sup> from Table 2-1)
- L<sub>i</sub> = beta skin dose conversion factor for noble gas radionuclide i (mrem/yr per μCi/m<sup>3</sup> from Table 2-1)
- M<sub>i</sub> = gamma air dose conversion factor for noble gas radionuclide i (mrem/yr per μCi/m<sup>3</sup> from Table 2-1)
- 1.1 = mrem skin dose per mrad gamma air dose (mrem/mrad)
- 500 = total body dose rate limit (mrem/yr)
- 3000 = skin dose rate limit (mrem/yr)
- 4.72 E+02 = conversion factor (cm<sup>3</sup>/ft<sup>3</sup> \* min/sec)

Based on the more limiting FRAC (i.e., higher value) as determined above, the alarm setpoints for the applicable monitors (R16, R41D, and/or R12A) may be calculated by the equation:

$$SP = \left[ AF * \frac{\sum C_i * SEN}{FRAC} \right] + bkg \quad (2.3)$$

Where:

- SP = alarm setpoint corresponding to the maximum allowable release rate (cpm)  
 SEN = monitor sensitivity (cpm per  $\mu\text{Ci}/\text{cm}^3$ )  
 bkg = background of the monitor (cpm)  
 AF = administrative allocation factor for the specific monitor and type release, which corresponds to the fraction of the total allowable release rate that is administratively allocated to the release.

The allocation factor (AF) is an administrative control imposed to ensure that combined releases from Salem Units 1 and 2 and Hope Creek will not exceed the regulatory limits on release rate from the site (i.e., the release rate limits of Technical Specification (CONTROL) 3.11.2.1). Normally, the combined AF value for Salem Units 1 and 2 is equal to 0.5 (0.25 per unit), with the remainder 0.5 allocated to Hope Creek. Any increase in AF above 0.5 for the Salem Nuclear Generating Station will be coordinated with the Hope Creek Generating Station to ensure that the combined allocation factors for all units do not exceed 1.0.

### 2.2.2 Conservative Default Values

A conservative alarm setpoint can be established, in lieu of the individual radionuclide evaluation based on the grab sample analysis, to eliminate the potential of periodically having to adjust the setpoint to reflect minor changes in radionuclide distribution and variations in release flow rate. The alarm setpoint may be conservatively determined by the default values presented in Table 2-2 and 2-3 for Units 1 and 2, respectively. These values are based upon:

- the maximum ventilation (or purge) flow rate;
- a radionuclide distribution<sup>a</sup> comprised of 95% Xe-133, 2% Xe-135, 1% Xe-133m, 1% Kr-88 and 1% Kr-85; and
- an administrative allocation factor of 0.25 to conservatively ensure that any simultaneous releases from Salem Units 1 and 2 do not exceed the maximum allowable release rate. For this radionuclide distribution, the alarm setpoint based on the total body dose rate is more restrictive than the corresponding setpoint based on the skin dose rate.

a) Adopted from ANSI N237-1976/ANS-18.1, Source Term Specifications, Table 6

## 2.3 Gaseous Effluent Instantaneous Dose Rate Calculations -10 CFR 20

### 2.3.1 Site Boundary Dose Rate - Noble Gases

Technical Specification (CONTROL) 3.11.2.1a limits the dose rate at the SITE BOUNDARY due to noble gas releases to  $\leq 500$  mrem/yr, total body and  $\leq 3000$  mrem/yr, skin. Radiation monitor alarm setpoints are established to ensure that these release limits are not exceeded. In the event any gaseous releases from the station results in an alarm setpoint being exceeded, an evaluation of the SITE BOUNDARY dose rate resulting from the release shall be performed using the following equations:

$$D_{tb} = \chi/Q * \sum_i (K_i * Q_i) \quad (2.4)$$

and

$$D_s = \chi/Q * \sum_i ((L_i + 1.1M_i) * Q_i) \quad (2.5)$$

Where:

- $D_{tb}$  = total body dose rate (mrem/yr)  
 $D_s$  = skin dose rate (mrem/yr)  
 $\chi/Q$  = atmospheric dispersion to the controlling SITE BOUNDARY location (sec/m<sup>3</sup>)  
 $Q_i$  = average release rate of radionuclide i over the release period under evaluation ( $\mu\text{Ci}/\text{sec}$ )  
 $K_i$  = total body dose conversion factor for noble gas radionuclide i (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ , from Table 2-1)  
 $L_i$  = beta skin dose conversion factor for noble gas radionuclide i (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ , from Table 2-1)  
 $M_i$  = gamma air dose conversion factor for noble gas radionuclide i (mrad/yr per  $\mu\text{Ci}/\text{m}^3$ , from Table 2-1)  
 1.1 = mrem skin dose per mrad gamma air dose (mrem/mrad)

As appropriate, simultaneous releases from Salem Units 1 and 2 and Hope Creek will be considered in evaluating compliance with the release rate limits of Specification 3.11.2.1a, following any release exceeding the above prescribed alarm setpoints.

Monitor indications (readings) may be averaged over a time period not to exceed 15 minutes when determining noble gas release rate based on correlation of the monitor reading and monitor sensitivity. The 15 minute averaging is needed to allow for reasonable monitor response to potentially changing radioactive material concentrations and to exclude potential electronic spikes in monitor readings that may be unrelated to radioactive material releases. As identified, any electronic spiking monitor responses may be excluded from the analysis.

**NOTE: For administrative purposes, more conservative alarm setpoints than those as prescribed above may be imposed. However, conditions exceeding these more limiting alarm setpoints do not necessarily indicate radioactive material release rates exceeding the limits of Technical Specification (CONTROL) 3.11.2.1a. Provided actual releases do not result in radiation monitor indications exceeding alarm setpoint values based on the above criteria, no further analyses are required for demonstrating compliance with the limits of Specification 3.11.2.1a.**

Actual meteorological conditions concurrent with the release period or the default, annual average dispersion parameters as presented in Table 2-4 may be used for evaluating the gaseous effluent dose rate.

### 2.3.2 Site Boundary Dose Rate - Radioiodine and Particulates

Technical Specification (CONTROL) 3.11.2.1.b limits the dose rate to  $\leq 1500$  mrem/yr to any organ for I-131, tritium, and particulates with half-lives greater than 8 days. To demonstrate compliance with this limit, an evaluation is performed at a frequency no greater than that corresponding to the sampling and analysis time period (e.g., nominally once per 7 days). The following equation shall be used for the dose rate evaluation:

$$D_o = \chi/Q * \sum_i (R_{io} * Q_i) \quad (2.6)$$

Where:

- $D_o$  = average organ dose rate over the sampling time period (mrem/yr)
- $\chi/Q$  = atmospheric dispersion to the controlling SITE BOUNDARY location for the inhalation pathway ( $\text{sec}/\text{m}^3$ )
- $R_{io}$  = dose parameter for radionuclide  $i$  (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) and organ  $o$  for the child inhalation pathway from Table 2-5
- $Q_i$  = average release rate over the appropriate sampling period and analysis frequency for radionuclide  $i$  -- I-131, tritium or other radionuclide in particulate form with half-life greater than 8 days ( $\mu\text{Ci}/\text{sec}$ )

By substituting 1500 mrem/yr for  $D_o$  and solving for  $Q$ , an allowable release rate for I-131 can be determined. Based on the annual average meteorological dispersion (see Table 2-4) and the most limiting potential pathway, age group and organ (inhalation, child, thyroid --  $R_{io} = 1.62\text{E}+07$  mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ), the allowable release rate for I-131 is 42  $\mu\text{Ci}/\text{sec}$ . Reducing this release rate by a factor of 4 to account for potential dose contributions from other radioactive particulate material and other release points (e.g., Hope Creek), the corresponding release rate allocated to each of the Salem units is 10.5  $\mu\text{Ci}/\text{sec}$ .

For a 7 day period, which is the nominal sampling and analysis frequency for I-131, the cumulative release is 6.3 Ci. Therefore, as long as the I-131 releases in any 7 day period do not exceed 6.3 Ci, no additional analyses are needed for verifying compliance with the Technical Specification (CONTROL) 3.11.2.1.b limits on allowable release rate.

## 2.4 Noble Gas Effluent Dose Calculations - 10 CFR 50

### 2.4.1 UNRESTRICTED AREA Dose - Noble Gases

Technical Specification (CONTROL) 3.11.2.2 requires a periodic assessment of releases of noble gases to evaluate compliance with the quarterly dose limits of  $\leq 5$  mrad, gamma-air and  $\leq 10$  mrad, beta-air and the calendar year limits  $\leq 10$  mrad, gamma-air and  $\leq 20$  mrad, beta-air. The limits are applicable separately to each unit and are not combined site limits. The following equations shall be used to calculate the gamma-air and beta-air doses:

$$D_\gamma = 3.17\text{E} - 08 * \chi/Q * \sum_i (M_i * Q_i) \quad (2.7)$$

and

$$D_{\beta} = 3.17E - 08 * \chi/Q * \sum_i (N_i * Q_i) \quad (2.8)$$

Where:

- $D_{\gamma}$  = air dose due to gamma emissions for noble gas radionuclides (mrad)  
 $D_{\beta}$  = air dose due to beta emissions for noble gas radionuclides (mrad)  
 $\chi/Q$  = atmospheric dispersion to the controlling SITE BOUNDARY location (sec/m<sup>3</sup>)  
 $Q_i$  = cumulative release of noble gas radionuclide i over the period of interest ( $\mu\text{Ci}$ )  
 where  $\mu\text{Ci} = (\mu\text{Ci/cc}) * (\text{cc released})$  or  $(\mu\text{Ci/sec}) * (\text{sec released})$   
 $M_i$  = air dose factor due to gamma emissions from noble gas radionuclide i  
 (mrad/yr per  $\mu\text{Ci/m}^3$ , from Table 2-1)  
 $N_i$  = air dose factor due to beta emissions from noble gas radionuclide i  
 (mrad/yr per  $\mu\text{Ci/m}^3$ , Table 2-1)  
 3.17E-08 = conversion factor (yr/sec)

#### 2.4.2 Simplified Dose Calculation for Noble Gases

In lieu of the individual noble gas radionuclide dose assessment as presented above, the following simplified dose calculation equations may be used for verifying compliance with the dose limits of Technical Specification (CONTROL) 3.11.2.2. (Refer to Appendix C for the derivation and justification for this simplified method and for values of  $M_{\text{eff}}$ , and  $N_{\text{eff}}$ .)

$$D_{\gamma} = \frac{3.17E-08}{0.50} * \chi/Q * M_{\text{eff}} * \sum_i Q_i \quad (2.9)$$

and

$$D_{\beta} = \frac{3.17E-08}{0.50} * \chi/Q * N_{\text{eff}} * \sum_i Q_i \quad (2.10)$$

Where:

- $M_{\text{eff}}$  = 5.3E+02, effective gamma-air dose factor (mrad/yr per  $\mu\text{Ci/m}^3$ )  
 $N_{\text{eff}}$  = 1.1E+03, effective beta-air dose factor (mrad/yr per  $\mu\text{Ci/m}^3$ )  
 $Q_i$  = cumulative release for all noble gas radionuclides ( $\mu\text{Ci}$ ), where  $\mu\text{Ci} = (\mu\text{Ci/cc}) * (\text{cc released})$  or  $(\mu\text{Ci/sec}) * (\text{sec released})$   
 0.50 = conservatism factor to account for potential variability in the radionuclide distribution

Actual meteorological conditions concurrent with the release period or the default, annual average dispersion parameters as presented in Table 2-4, may be used for the evaluation of the gamma-air and beta-air doses.

## 2.5 Radioiodine and Particulate Dose Calculations - 10 CFR 50

### 2.5.1 UNRESTRICTED AREA Dose - Radioiodine and Particulates

In accordance with requirements of Technical Specification (CONTROL) 3.11.2.3, a periodic assessment shall be performed to evaluate compliance with the quarterly dose limit of  $\leq 7.5$  mrem and calendar year limit  $\leq 15$  mrem to any organ. The following equation shall be used to evaluate the maximum organ dose due to releases of I-131, tritium and particulates with half-lives greater than 8 days:

$$D_{aop} = 3.17E-08 * W * SF_p * \sum_i (R_{iop} * Q_i) \quad (2.11)$$

Where:

- $D_{aop}$  = dose or dose commitment via all pathways p and controlling age group a (as identified in Table 2-4) to organ o, including the total body (mrem)
- $W$  = atmospheric dispersion parameter to the controlling location(s) as identified in Table 2-4
- $\chi/Q$  = atmospheric dispersion for inhalation pathway and H-3 dose contribution via other pathways ( $\text{sec}/\text{m}^3$ )
- $D/Q$  = atmospheric deposition for vegetation, milk and ground plane exposure pathways ( $\text{m}^{-2}$ )
- $R_{iop}$  = dose factor for radionuclide i ( $\text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{m}^3$ ) or ( $\text{m}^2 - \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) and organ o from Table 2-5 for each age group and the applicable pathway p as identified in Table 2-4. Values for  $R_{iop}$  were derived in accordance with the methods described in NUREG-0133.
- $Q_i$  = cumulative release over the period of interest for radionuclide i -- I-131, tritium, or radioactive material in particulate form with half-life greater than 8 days ( $\mu\text{Ci}$ ).
- $SF_p$  = annual seasonal correction factor to account for the fraction of the year that the applicable exposure pathway does not exist.
- 1) For milk and vegetation exposure pathways:  
A six month fresh vegetation and grazing season (May through October) = 0.5
  - 2) For inhalation and ground plane exposure pathways: = 1.0

**For evaluating the maximum exposed individual, only the controlling pathways and age group as identified in Table 2-4 need be evaluated for compliance with Technical Specification (CONTROL) 3.11.2.3.**

### 2.5.2 Simplified Dose Calculation for Radioiodines and Particulates.

In lieu of the individual radionuclide (I-131, tritium, and particulates) dose assessment as presented above, the following simplified dose calculation equation may be used for verifying compliance with the dose limits of Technical Specification (CONTROL) 3.11.2.3 (refer to Appendix D for the derivation and justification of this simplified method).

$$D_{\max} = 3.17E-08 * W * SF_p * R_{I-131} * \sum_i Q_i \quad (2.12)$$

Where:

- $D_{\max}$  = maximum organ dose (mrem)  
 $R_{I-131}$  = I-131 dose parameter for the thyroid for the identified controlling pathway  
 = 1.05E+12, infant thyroid dose parameter with the grass-cow-milk pathway controlling ( $m^2$  - mrem/yr per  $\mu\text{Ci}/\text{sec}$ )  
 $W$  =  $D/Q$  for radioiodine,  $2.1\text{E}-10$   $1/m^2$   
 $Q_i$  = cumulative release over the period of interest for radionuclide  $i$  - I-131, tritium, or radioactive material in particulate from with half life greater than 8 days ( $\mu\text{Ci}$ )

The dose should be evaluated based on the predetermined controlling pathways as identified in Table 2-4. If more limiting exposure pathways are determined to exist in the surrounding environment of Salem by the annual land-use census, Table 2-4 will be revised as specified in Technical Specification (CONTROL) 3.12.2.

## 2.6 Secondary Side Radioactive Gaseous Effluents and Dose Calculations

During periods of primary to secondary leakage, minor levels of radioactive material may be released via the secondary system to the atmosphere. Non-condensables (e.g., noble gases) will be predominately released via the condenser evacuation system and will be monitored and quantified by the routine plant vent monitoring and sampling system and procedures (e.g., R15 on condenser evacuation, R41D on plant vent, and the plant vent particulate and charcoal samplers).

However, if the Steam Generator blowdown is routed directly to the Chemical Waste Basin (via the SG blowdown flash tank) instead of being recycled through the condenser, it may be desirable to account for the potential atmospheric releases of radioiodines and particulates from the flash tank vent (i.e., releases due to moisture carry over). Since this pathway is not sampled or monitored, it is necessary to calculate potential releases.

Based on the guidance in NRC NUREG-0133, the releases of the radioiodines and particulates shall be calculated by the equation:

$$Q_i = C_i * R_{sgb} * F_{ft} * (1 - SQ_{ftv}) \quad (2.13)$$

Where:

- $Q_i$  = the release rate of radionuclide,  $i$ , from the steam generator flash tank vent ( $\mu\text{Ci}/\text{sec}$ )  
 $C_i$  = the concentration of radionuclide,  $i$ , in the secondary coolant water averaged over not more than one week ( $\mu\text{Ci}/\text{ml}$ )  
 $R_{sgb}$  = the steam generator blowdown rate to the flash tank (ml/sec)  
 $F_{ft}$  = the fraction of blowdown flashed in the tank determined from a heat balance taken around the flash tank at the applicable reactor power level  
 $SQ_{ftv}$  = the measured steam quality in the flash tank vent; or an assumed value of 0.85, based on NUREG-0017.

Tritium releases via the steam flashing may also be quantified using the above equation with the assumption of a steam quality ( $SQ_{ftv}$ ) equal to 0. Since the H-3 will be associated with the water

molecules, it is not necessary to account for the moisture carry-over which is the transport media for the radioiodines and particulates.

Based on the design and operating conditions at Salem, the fraction of blowdown converted to steam ( $F_R$ ) is approximately 0.48. The equation simplifies to the following:

$$Q_i = 0.072 * C_i * R_{sgb} \quad (2.14)$$

For H-3, the simplified equation is:

$$Q_i = 0.48 * C_i * R_{sgb} \quad (2.15)$$

Also during reactor shutdown operations with a radioactively contaminated secondary system, radioactive material may be released to the atmosphere via the atmospheric reliefs (PORV) and the safety reliefs on the main steam lines and via the steam driven auxiliary feed pump exhaust. The evaluation of the radioactive material concentration in the steam relative to that in the steam generator water is based on the guidance of NUREG-0017, Revision 1. The partitioning factors for the radioiodines is 0.01 and is 0.001 for all other particulate radioactive material. The resulting equation for quantifying releases via the atmospheric steam releases is:

$$Q_{ij} = 0.13 * (C_{ij} * SF_{ij}) * PF_i \quad (2.16)$$

Where:

- $Q_{ij}$  = release rate of radionuclide i via pathway j, ( $\mu\text{Ci}/\text{sec}$ )
- $C_{ij}$  = concentration of radionuclide i, in pathway j, ( $\mu\text{Ci}/\text{ml}$ )
- $SF_j$  = steam flow for release pathway j
  - = 450,000 lb/hr per PORV
  - = 800,000 lb/hr per safety relief valve
  - = 50,000 lb/hr for auxiliary feed pump exhaust
- $PF_i$  = partitioning factor, ratio of concentration in steam to that in the water in the steam generator
  - = 0.01 for radioiodines
  - = 0.001 for all other particulates
  - = 1.0 for H-3
- 0.13 = conversion factor - [(hr\*ml) / (sec\*lb)]

Any significant releases of noble gases via the atmospheric steam releases can be quantified in accordance with the calculation methods of the Salem Emergency Plan Implementation Procedure.

Alternately, the quantification of the release rate and cumulative releases may be based on actual samples of main steam collected at the R46 sample locations. The measured radionuclide concentration in the steam may be used for quantifying the noble gases, radioiodine and particulate releases.

**Note: The expected mode of operation would be to isolate the effected steam generator, thereby reducing the potential releases during the shutdown/cool-down process. Use of the above calculation methods should consider actual operating conditions and release mechanisms.**

The calculated quantities of radioactive materials may be used as inputs to the equation (2.11) or (2.12) to calculate offsite doses for demonstrating compliance with the Radiological Effluent Technical Specifications (CONTROLS).

## 2.7 Gaseous Effluent Dose Projection

Technical Specification (CONTROL) 3.11.2.4 requires that the GASEOUS RADWASTE TREATMENT SYSTEM and VENTILATION EXHAUST TREATMENT SYSTEM be used to reduce radioactive material levels prior to discharge when projected doses exceed one-half the annual design objective rate in any calendar quarter, i.e., exceeding:

- 0.625 mrad/quarter, gamma air;
- 1.25 mrad/quarter, beta air; or
- 1.875 mrem/quarter, maximum organ.

The applicable gaseous processing systems for maintaining radioactive material releases ALARA are the Auxiliary Building normal ventilation system (filtration systems # 1, 2 and 3) and the Waste Gas Decay Tanks as delineated in Figures 2-1 and 2-2. Dose projections are performed at least once per 31 days by the following equations:

$$D_{\gamma p} = D_{\gamma} * \left( \frac{91}{d} \right) \quad (2.17)$$

$$D_{\beta p} = D_{\beta} * \left( \frac{91}{d} \right) \quad (2.18)$$

$$D_{\max p} = D_{\max} * \left( \frac{91}{d} \right) \quad (2.19)$$

Where:

- $D_{\gamma p}$  = gamma air dose projection for current calendar quarter(mrad)
- $D_{\gamma}$  = gamma air dose to date for current calendar quarter as determined by Equation 2.7 or 2.9 (mrem)
- $D_{\beta p}$  = beta air dose projection for current calendar quarter (mrad)
- $D_{\beta}$  = beta air dose to date for current calendar quarter as determined by Equation 2.8 or 2.10 (mrem)
- $D_{\max p}$  = maximum organ dose projection for current calendar quarter (mrem)
- $D_{\max}$  = maximum organ dose to date for current calendar quarter as determined by Equation 2.11 or 2.12 (mrem)
- $d$  = number of days to date in current calendar quarter
- 91 = number of days in a calendar quarter

### 3.0 SPECIAL DOSE ANALYSES

#### 3.1 Doses Due To Activities Inside the SITE BOUNDARY

In accordance with Technical Specification (CONTROL) 6.9.1.8, the Radioactive Effluent Release Report (RERR) shall include an assessment of radiation doses from radioactive liquid and gaseous effluents to MEMBERS OF THE PUBLIC due to their activities inside the SITE BOUNDARY.

In accordance with Salem Technical Specification (CONTROL) BASES Section 3/4.11.2.1, an example calculation for assessing dose to members of the public follows:

Typically, the members of the public that spend the most time at PSEG Nuclear are various food vendors, who spend a few hours in front of the Security Center during lunch hours. In accordance with the requirements of Technical Specification (CONTROL) 6.9.1.8, the dose to members of the public inside the site boundary can be calculated based on the following assumptions:

- a. The food vendors deliver Monday through Friday.
- b. They arrive at approximately 10:00 A.M. at the Security Center.
- c. The food vendors leave the site at 1:00 P.M.
- d. No deliveries are made on major holidays, making the total weeks equal 50 for the year.
- e. The dose data is based on the TLD located outside the Security Center in the vicinity of the food vendors and the calculated dose due to gaseous effluents at that location.

The occupancy factor for these food vendors would be:

$$\frac{3hr / day * 5day / wk * 50wk / yr}{8760hr / yr} = 0.086$$

The dose to these food vendors would be determined from the annual TLD dose at location CA16 plus the annual gaseous effluents dose (inhalation and ground plane pathways) from both Salem and Hope Creek stations, multiplied by the occupancy factor.

The GASPAR computer program could be used to determine the gaseous effluent dose to the food vendors. The calculation methods as presented in Sections 2.4 and 2.5 may be used for determining the maximum potential dose to a MEMBER OF THE PUBLIC based on the parameters from Table 2-4. The default value for the meteorological dispersion data as presented in Table 2-3 may be used if current year meteorology is unavailable at the time of NRC reporting. However, a follow-up evaluation shall be performed when the data becomes available.

#### 3.2 Total dose to MEMBERS OF THE PUBLIC - 40 CFR 190

The Radioactive Effluent Release Report (RERR) shall also include an assessment of the radiation dose to the likely most exposed MEMBER OF THE PUBLIC for reactor releases and other nearby uranium fuel cycle sources (including dose contributions from effluents and direct radiation from on-site sources). For the likely most exposed MEMBER OF THE PUBLIC in the vicinity of Artificial

Island, the sources of exposure need only consider the Salem Nuclear Generating Station and the Hope Creek Nuclear Generating Station: No other fuel cycle facilities contribute to the MEMBER OF THE PUBLIC dose for the Artificial Island vicinity.

The dose contribution from the operation of Hope Creek Nuclear Generating Station will be estimated based on the methods as presented in the Hope Creek Offsite Dose Calculation Manual (HCGS ODCM).

As appropriate for demonstrating/evaluating compliance with the limits of Technical Specification (CONTROL) 3.11.4 (40 CFR 190), the results of the environmental monitoring program may be used for providing data on actual measured levels of radioactive material in the actual pathways of exposure.

### **3.2.1 Effluent Dose Calculations**

For purposes of implementing the surveillance requirements of Technical Specification (CONTROL) 3/4.11.4 and the reporting requirements of 6.9.1.8 (RERR), dose calculations for the Salem Nuclear Generating Station should be performed using the controlling pathways and locations of Table 2-4 and the calculation methods contained within this ODCM. If more limiting exposure pathways are determined to exist in the surrounding environment of Salem by the annual land-use census, Table 2-4 will be revised as specified in Technical Specification (CONTROL) 3.12.2.

Average annual meteorological dispersion parameters or meteorological conditions concurrent with the release period under evaluation may be used.

### **3.2.2 Direct Exposure Dose Determination.**

Any potentially significant direct exposure contribution to off-site individual doses may be evaluated based on the results of the environmental measurements (e.g., TLD, ion chamber measurements) and/or by the use of a radiation transport and shielding calculation method.

Only during a non-typical condition will there exist any potential for significant on-site sources at Salem that would yield potentially significant off-site doses (i.e., in excess of 1 mrem per year to a MEMBER OF THE PUBLIC), that would require detailed evaluation for demonstrating compliance with 40 CFR 190.

However, should a situation exist where the direct exposure contribution is potentially significant, on-site measurements, off-site measurements and/or calculation techniques will be used for determination of dose for assessing 40 CFR 190 compliance.

## 4.0 RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

### 4.1 Sampling Program

The operational phase of the Radiological Environmental Monitoring Program (REMP) is conducted in accordance with the requirements of Technical Specification (CONTROL) 3.12. The objectives of the program are:

- To determine whether any significant increases occur in the concentration of radionuclides in the critical pathways of exposure in the vicinity of Artificial Island;
- To determine if the operation of the Salem Nuclear Generating Stations has resulted in any increase in the inventory of long lived radionuclides in the environment;
- To detect any changes in the ambient gamma radiation levels; and
- To verify that SNGS operations have no detrimental effects on the health and safety of the public or on the environment.

The sampling requirements (type of samples\*, collection frequency and analysis) and sample locations are presented in Appendix E.

**\*NOTE: No public drinking water samples or irrigation water samples are taken as these pathways are not directly effected by liquid effluents discharged from Salem Generating Station.**

### 4.2 Interlaboratory Comparison Program

Technical Specification (CONTROL) 3.12.3 requires analyses be performed on radioactive material supplied as part of an Interlaboratory Comparison Program. Participation in an approved Interlaboratory Comparison Program provides a check on the precision and accuracy of measurements of radioactive materials in environmental samples.

A summary of the Interlaboratory Comparison Program results will be provided in the Annual Radiological Environmental Operating Report pursuant to Technical Specification (CONTROL) 6.9.1.7.

Figure 1-1: Liquid Release Flowpath Unit 1

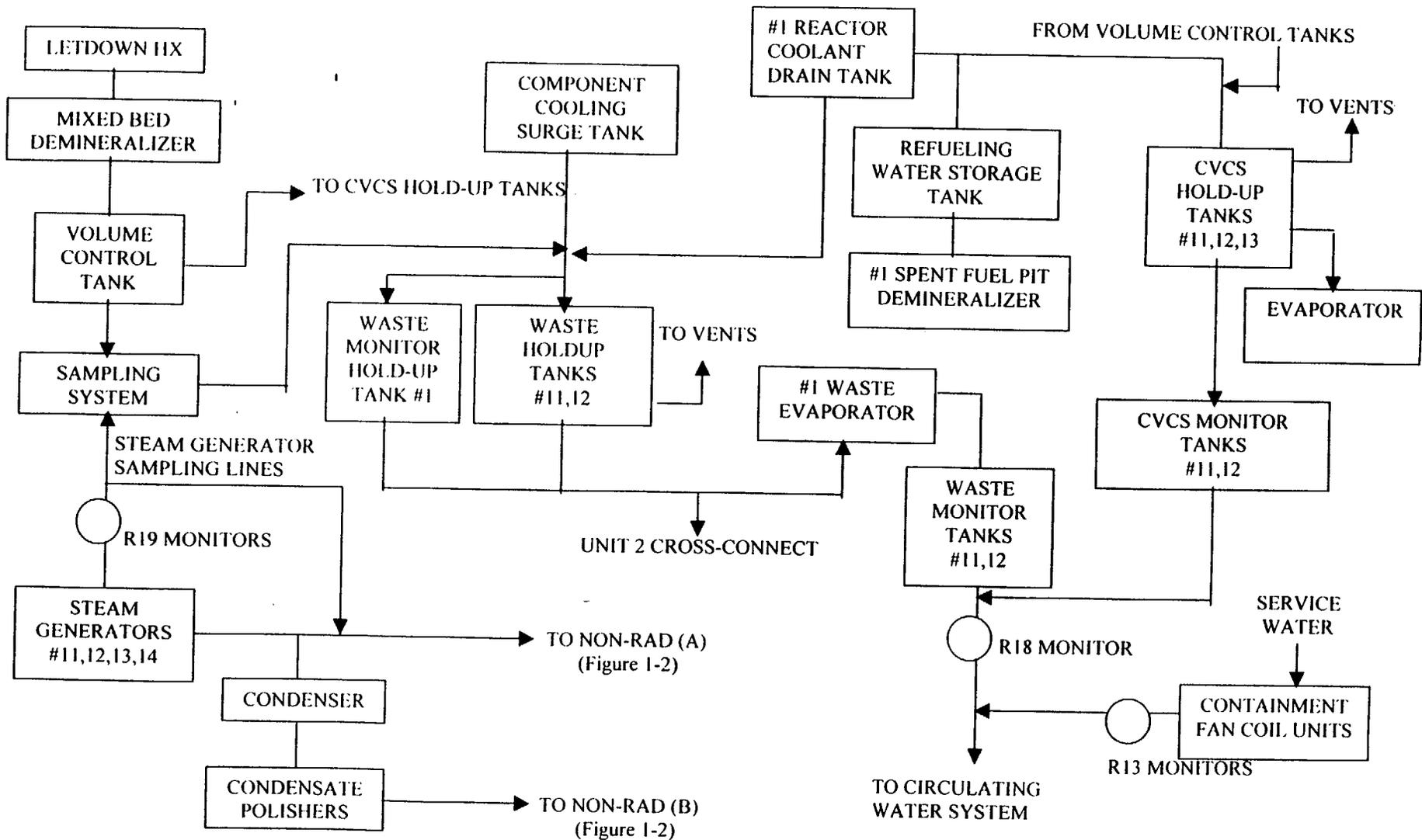


Figure 1-2: Liquid Release Flowpath Unit 2

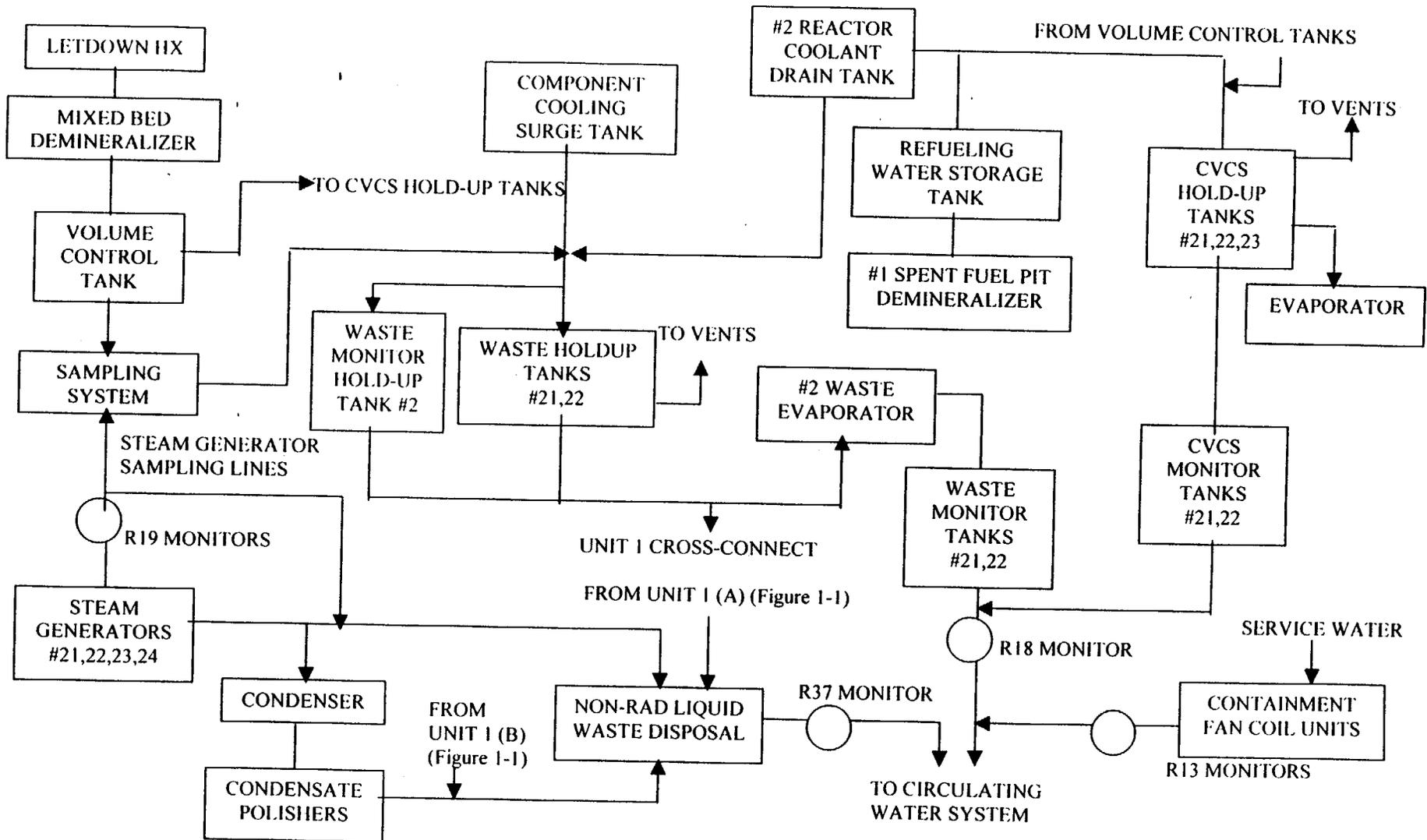


Figure 1-3: Liquid Radioactive Waste System

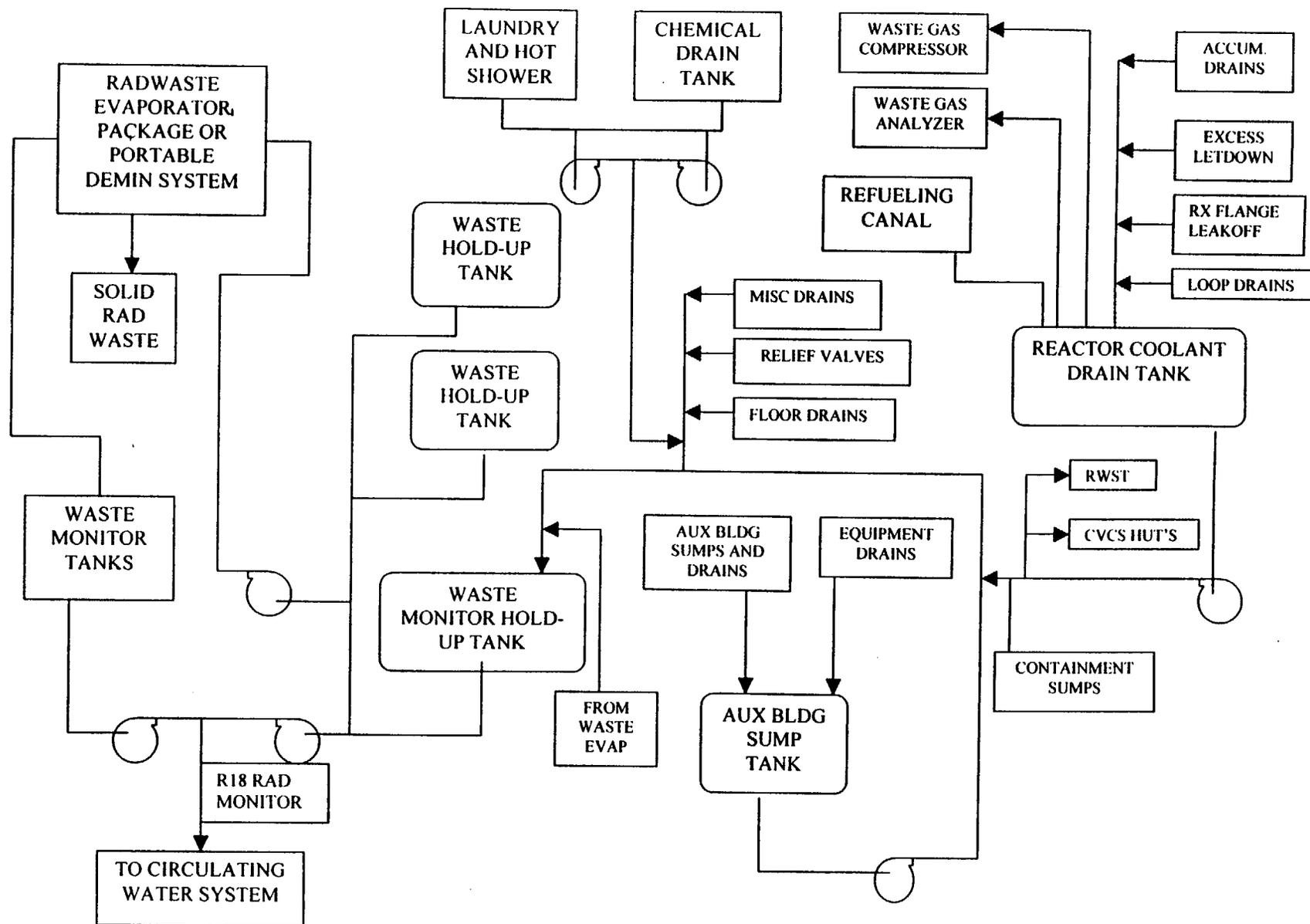


Table 1-1: Parameters for Liquid Alarm Setpoint Determinations Unit 1

Parameter	Actual Value	Default Value	Units	Comments
MPC <sub>c</sub>	Calculated	6.05E-06 *	µCi/ml	Calculated for each batch to be released.
MPC I-131	3.0E-07	N/A	µCi/ml	I-131 MPC conservatively used for SG blowdown and Service Water monitor setpoints.
C <sub>i</sub>	Measured	N/A	µCi/ml	Taken from gamma spectral analysis of liquid effluent.
MPC <sub>i</sub>	as determined	N/A	µCi/ml	Taken from 10 CFR 20, Appendix B, Table II, Col 2 (Appendix F).
Sensitivity 1-R18 1-R19 (A,B,C,D) 1-R13 (A,B,C,D,E)	as determined	N/A	cpm per µCi/ml	Monitor sensitivities are controlled under Public Service Blueprint Document (PSBP) 315733
CW	as determined	1.00E+05	gpm	Circulating water system – single CW pump
RR 1-R18	as determined	120	gpm	Determined prior to release; release rate can be adjusted for Technical Specification (CONTROL) compliance
1-R19		250		Steam Generator blowdown rate per Generator
1-R13		2500		Service Water flow rate for Containment fan coolers
Setpoint 1-R18 1-R19 (A,B,C,D)** 1-R13 (A,B,C,D,E)**	Calculated	N/A	cpm	Monitor setpoints are controlled under Public Service Blueprint Document (PSBP) 315733
Correction Factor (Non-Gamma)	as determined	0.75	Unitless	Default parameter to account for non-gamma emitting nuclides.
Allocation Factor	0.5	0.5	Unitless	Conservatism factor to preclude exceeding MPC limit in the case of simultaneous primary-to-secondary leaks at both Salem Units

\* Refer to Appendix A for derivation

\*\* The MPC value of I-131 (3E-07 µCi/ml) has been used for derivation of R19 Steam Generator Blowdown and R13 Service Water monitor setpoints as discussed in Section 1.2.2

Table 1-2: Parameters for Liquid Alarm Setpoint Determinations – Unit 2

Parameter	Actual Value	Default Value	Units	Comments
MPC <sub>c</sub>	Calculated	4.81E-06 *	μCi/ml	Calculated for each batch to be released.
MPC I-131	3.0E-07	N/A	μCi/ml	I-131 MPC conservatively used for SG blowdown, Service Water and Chemical Waste Basin monitor setpoints.
C <sub>i</sub>	Measured	N/A	μCi/ml	Taken from gamma spectral analysis of liquid effluent.
MPC <sub>i</sub>	as determined	N/A	μCi/ml	Taken from 10 CFR 20, Appendix B, Table II, Col. 2 (Appendix F)
Sensitivity 2-R18 2R19(A,B,C,D) 2-R13(A,B,C) 2R37	as determined	N/A	cpm per μCi/ml	Monitor sensitivities are controlled under Public Service Blueprint Document 315734
CW	as determined	1.0E+05	gpm	Circulating Water System, single CW pump (Note: no CW pump in service for 2R13 monitor – see section 1.2.2)
RR 2-R18  2-R19  2-R13  2R37	as determined	120  250  2500  1200	gpm	Determined prior to release; release rate can be adjusted for Technical Specification (CONTROL) Compliance  Steam Generator Blowdown rate per Generator  Service Water flow rate for Containment fan coolers  Chemical Waste Basin discharge
Setpoint 2-R18 2-R19(A,B,C,D)** 2-R13(A,B,C)** 2R37 **	Calculated	N/A	cpm	Monitor setpoints are controlled under Public Service Blueprint Document (PSBP) 315734
Correction Factor (Non-Gamma)	as determined	0.75	Unitless	Default parameter to account for non-gamma emitting nuclides.
Allocation Factor	0.5	0.5	Unitless	Conservatism factor to preclude exceeding MPC limit in the case of simultaneous primary-to-secondary leaks at both Salem Units

\* Refer to Appendix A for derivation

\*\* The MPC value of I-131 (3.0E-7 μCi/ml) has been used for derivation of the R13, R19 and R37 monitor setpoints as discussed in Section 1.2.2

TABLE 1-3: Site Related Ingestion Dose Commitment Factor,  $A_{io}$   
 (Fish And Invertebrate Consumption)  
 (mrem/hr per  $\mu\text{Ci/ml}$ )

Nuclide	Bone	Liver	T.Body	Thyroid	Kidney	Lung	G.I.LI
H-3	-	2.82E-1	2.82E-1	2.82E-1	2.82E-1	2.82E-1	2.82E-1
C-14	1.45E+4	2.90E+3	2.90E+3	2.90E+3	2.90E+3	2.90E+3	2.90E+3
Na-24	4.57E-1						
P-32	4.69E+6	2.91E+5	1.81E+5	-	-	-	5.27E+5
Cr-51	-	-	5.58E+0	3.34E+0	1.23E+0	7.40E+0	1.40E+3
Mn-54	-	7.06E+3	1.35E+3	-	2.10E+3	-	2.16E+4
Mn-56	-	1.78E+2	3.15E+1	-	2.26E+2	-	5.67E+3
Fe-55	5.11E+4	3.53E+4	8.23E+3	-	-	1.97E+4	2.03E+4
Fe-59	8.06E+4	1.90E+5	7.27E+4	-	-	5.30E+4	6.32E+5
Co-57	-	1.42E+2	2.36E+2	-	-	-	3.59E+3
Co-58	-	6.03E+2	1.35E+3	-	-	-	1.22E+4
Co-60	-	1.73E+3	3.82E+3	-	-	-	3.25E+4
Ni-63	4.96E+4	3.44E+3	1.67E+3	-	-	-	7.18E+2
Ni-65	2.02E+2	2.62E+1	1.20E+1	-	-	-	6.65E+2
Cu-64	-	2.14E+2	1.01E+2	-	5.40E+2	-	1.83E+4
Zn-65	1.61E+5	5.13E+5	2.32E+5	-	3.43E+5	-	3.23E+5
Zn-69	3.43E+2	6.56E+2	4.56E+1	-	4.26E+2	-	9.85E+1
As-76	4.38E+2	1.16E+3	5.14E+3	3.42E+2	1.39E+3	3.58E+2	4.30E+4
Br-82	-	-	4.07E+0	-	-	-	4.67E+0
Br-83	-	-	7.25E-2	-	-	-	1.04E-1
Br-84	-	-	9.39E-2	-	-	-	7.37E-7
Br-85	-	-	3.86E-3	-	-	-	-
Rb-86	-	6.24E+2	2.91E+2	-	-	-	1.23E+2
Rb-88	-	1.79E+0	9.49E-1	-	-	-	2.47E-11
Rb-89	-	1.19E+0	8.34E-1	-	-	-	6.89E-14
Sr-89	4.99E+3	-	1.43E+2	-	-	-	8.00E+2
Sr-90	1.23E+5	-	3.01E+4	-	-	-	3.55E+3
Sr-91	9.18E+1	-	3.71E+0	-	-	-	4.37E+2
Sr-92	3.48E+1	-	1.51E+0	-	-	-	6.90E+2
Y-90	6.06E+0	-	1.63E-1	-	-	-	6.42E+4
Y-91m	5.73E-2	-	2.22E-3	-	-	-	1.68E-1
Y-91	8.88E+1	-	2.37E+0	-	-	-	4.89E+4
Y-92	5.32E-1	-	1.56E-2	-	-	-	9.32E+3
Y-93	1.69E+0	-	4.66E-2	-	-	-	5.35E+4
Zr-95	1.59E+1	5.11E+0	3.46E+0	-	8.02E+0	-	1.62E+4
Zr-97	8.81E-1	1.78E-1	8.13E-2	-	2.68E-1	-	5.51E+4
Nb-95	4.47E+2	2.49E+2	1.34E+2	-	2.46E+2	-	1.51E+6
Nb-97	3.75E+0	9.49E-1	3.46E-1	-	1.11E+0	-	3.50E+3
Mo-99	-	1.28E+2	2.43E+1	-	2.89E+2	-	2.96E+2
Tc-99m	1.30E-2	3.66E-2	4.66E-1	-	5.56E-1	1.79E-2	2.17E+1
Tc-101	1.33E-2	1.92E-2	1.88E-1	-	3.46E-1	9.81E-3	5.77E-14

TABLE 1-3 (cont'd)  
 Site Related Ingestion Dose Commitment Factor,  $A_{i0}$   
 (Fish And Invertebrate Consumption)  
 (mrem/hr per  $\mu\text{Ci/ml}$ )

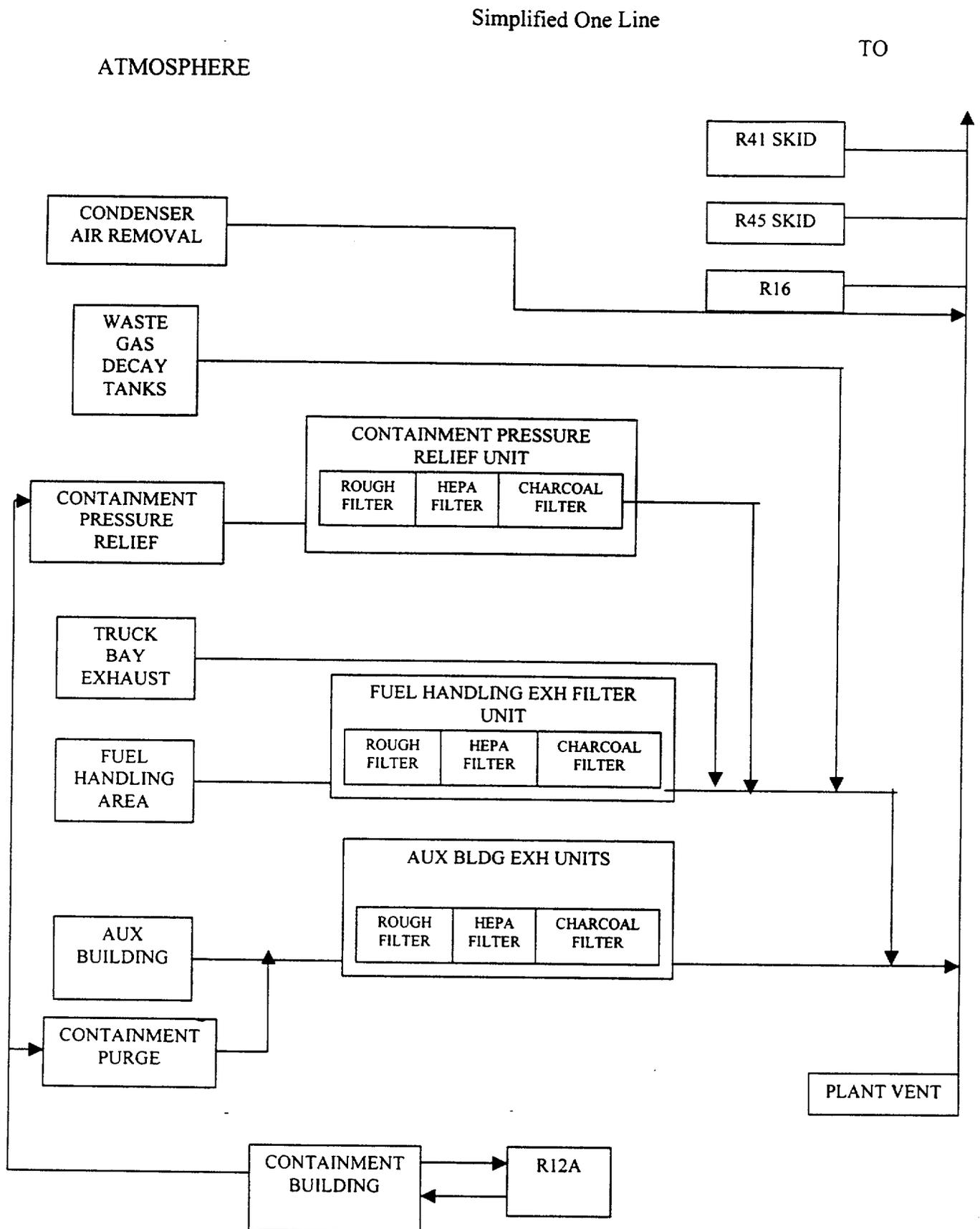
Nuclide	Bone	Liver	T.Body	Thyroid	Kidney	Lung	GI-LI
Ru-103	1.07E+2	-	4.60E+1	-	4.07E+2	-	1.25E+4
Ru-105	8.89E+0	-	3.51E+0	-	1.15E+2	-	5.44E+3
Ru-106	1.59E+3	-	2.01E+2	-	3.06E+3	-	1.03E+5
Rh-103m	-	-	-	-	-	-	-
Rh-106	-	-	-	-	-	-	-
Ag-110m	1.56E+3	1.45E+3	8.60E+2	-	2.85E+3	-	5.91E+5
Sb-124	2.77E+2	5.23E+0	1.10E+2	6.71E-1	-	2.15E+2	7.86E+3
Sb-125	1.77E+2	1.98E+0	4.21E+1	1.80E-1	-	1.36E+2	1.95E+3
Te-125m	2.17E+2	7.86E+1	2.91E+1	6.52E+1	8.82E+2	-	8.66E+2
Te-127m	5.48E+2	1.96E+2	6.68E+1	1.40E+2	2.23E+3	-	1.84E+3
Te-127	8.90E+0	3.20E+0	1.93E+0	6.60E+0	3.63E+1	-	7.03E+2
Te-129m	9.31E+2	3.47E+2	1.47E+2	3.20E+2	3.89E+3	-	4.69E+3
Te-129	2.54E+0	9.55E-1	6.19E-1	1.95E+0	1.07E+1	-	1.92E+0
Te-131m	1.40E+2	6.85E+1	5.71E+1	1.08E+2	6.94E+2	-	6.80E+3
Te-131	1.59E+0	6.66E-1	5.03E-1	1.31E+0	6.99E+0	-	2.26E-1
Te-132	2.04E+2	1.32E+2	1.24E+2	1.46E+2	1.27E+3	-	6.24E+3
I-130	3.96E+1	1.17E+2	4.61E+1	9.91E+3	1.82E+2	-	1.01E+2
I-131	2.18E+2	3.12E+2	1.79E+2	1.02E+5	5.35E+2	-	8.23E+1
I-132	1.06E+1	2.85E+1	9.96E+0	9.96E+2	4.54E+1	-	5.35E+0
I-133	7.45E+1	1.30E+2	3.95E+1	1.90E+4	2.26E+2	-	1.16E+2
I-134	5.56E+0	1.51E+1	5.40E+0	2.62E+2	2.40E+1	-	1.32E-2
I-135	2.32E+1	6.08E+1	2.24E+1	4.01E+3	9.75E+1	-	6.87E+1
Cs-134	6.84E+3	1.63E+4	1.33E+4	-	5.27E+3	1.75E+3	2.85E+2
Cs-136	7.16E+2	2.83E+3	2.04E+3	-	1.57E+3	2.16E+2	3.21E+2
Cs-137	8.77E+3	1.20E+4	7.85E+3	-	4.07E+3	1.35E+3	2.32E+2
Cs-138	6.07E+0	1.20E+1	5.94E+0	-	8.81E+0	8.70E-1	5.12E-5
Ba-139	7.85E+0	5.59E-3	2.30E-1	-	5.23E-3	3.17E-3	1.39E+1
Ba-140	1.64E+3	2.06E+0	1.08E+2	-	7.02E-1	1.18E+0	3.38E+3
Ba-141	3.81E+0	2.88E-3	1.29E-1	-	2.68E-3	1.63E-3	1.80E-9
Ba-142	1.72E+0	1.77E-3	1.08E-1	-	1.50E-3	1.00E-3	2.43E-18
La-140	1.57E+0	7.94E-1	2.10E-1	-	-	-	5.83E+4
La-142	8.06E-2	3.67E-2	9.13E-3	-	-	-	2.68E+2
Ce-141	3.43E+0	2.32E+0	2.63E-1	-	1.08E+0	-	8.86E+3
Ce-143	6.04E-1	4.46E+2	4.94E-2	-	1.97E-1	-	1.67E+4
Ce-144	1.79E+2	7.47E+1	9.59E+0	-	4.43E+1	-	6.04E+4
Pr-143	5.79E+0	2.32E+0	2.87E-1	-	1.34E+0	-	2.54E+4
Pr-144	1.90E-2	7.87E-3	9.64E-4	-	4.44E-3	-	2.73E-9
Nd-147	3.96E+0	4.58E+0	2.74E-1	-	2.68E+0	-	2.20E+4
W-187	9.16E+0	7.66E+0	2.68E+0	-	-	-	2.51E+3
Np-239	3.53E-2	3.47E-3	1.91E-3	-	1.08E-2	-	7.11E+2

TABLE 1-4: Bioaccumulation Factors  
(pCi/kg per pCi/liter)\*

ELEMENT	SALTWATER FISH	SALTWATER INVERTEBRATES
H	9.0E-01	9.3E-01
C	1.8E+03	1.4E+03
Na	6.7E-02	1.9E-01
P	3.0E+03	3.0E+04
Cr	4.0E+02	2.0E+03
Mn	5.5E+02	4.0E+02
Fe	3.0E+03	2.0E+04
Co	1.0E+02	1.0E+03
Ni	1.0E+02	2.5E+02
Cu	6.7E+02	1.7E+03
Zn	2.0E+03	5.0E+04
As	3.3E+02	3.3E+02
Br	1.5E-02	3.1E+00
Rb	8.3E+00	1.7E+01
Sr	2.0E+00	2.0E+01
Y	2.5E+01	1.0E+03
Zr	2.0E+02	8.0E+01
Nb	3.0E+04	1.0E+02
Mo	1.0E+01	1.0E+01
Tc	1.0E+01	5.0E+01
Ru	3.0E+00	1.0E+03
Rh	1.0E+01	2.0E+03
Ag	3.3E+03	3.3E+03
Sb	4.0E+01	5.4E+00
Te	1.0E+01	1.0E+02
I	1.0E+01	5.0E+01
Cs	4.0E+01	2.5E+01
Ba	1.0E+01	1.0E+02
La	2.5E+01	1.0E+03
Ce	1.0E+01	6.0E+02
Pr	2.5E+01	1.0E+03
Nd	2.5E+01	1.0E+03
W	3.0E+01	3.0E+01
Np	1.0E+01	1.0E+01

\* Values in this table are taken from Regulatory Guide 1.109 except for phosphorus (fish) which is adapted from NUREG/CR-1336 and silver, arsenic and antimony which are taken from UCRL 50564, Rev. 1, October 1972.

Figure 2-1: Salem Ventilation Exhaust Systems and Effluent Monitor Interfaces



**Figure 2-2: Gaseous Radioactive Waste Disposal System**

Simplified One Line

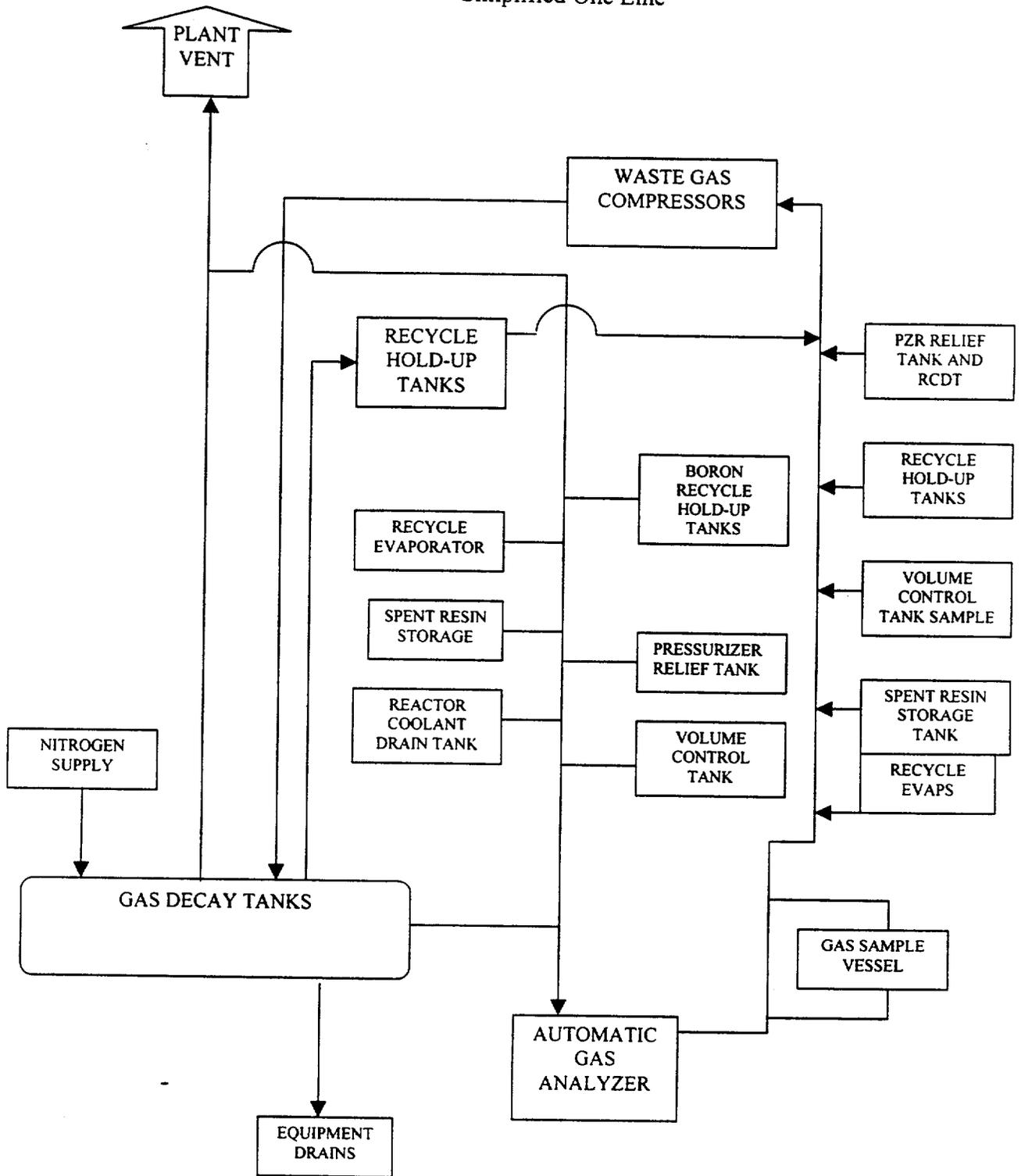


TABLE 2-1: Dose Factors For Noble Gases

Radionuclide	Total Body Dose Factor Ki (mrem/yr per $\mu\text{Ci}/\text{m}^3$ )	Skin Dose Factor Li (mrem/yr per $\mu\text{Ci}/\text{m}^3$ )	Gamma Air Dose Factor Mi (mrad/yr per $\mu\text{Ci}/\text{m}^3$ )	Beta Air Dose Factor Ni (mrad/yr per $\mu\text{Ci}/\text{m}^3$ )
Kr-83m	7.56E-02	-	1.93E+01	2.88E+02
Kr-85m	1.17E+03	1.46E+03	1.23E+03	1.97E+03
Kr-85	1.61E+01	1.34E+03	1.72E+01	1.95E+03
Kr-87	5.92E+03	9.73E+03	6.17E+03	1.03E+04
Kr-88	1.47E+04	2.37E+03	1.52E+04	2.93E+03
Kr-89	1.66E+04	1.01E+04	1.73E+04	1.06E+04
Kr-90	1.56E+04	7.29E+03	1.63E+04	7.83E+03
Xe-131m	9.15E+01	4.76E+02	1.56E+02	1.11E+03
Xe-133m	2.51E+02	9.94E+02	3.27E+02	1.48E+03
Xe-133	2.94E+02	3.06E+02	3.53E+02	1.05E+03
Xe-135m	3.12E+03	7.11E+02	3.36E+03	7.39E+02
Xe-135	1.81E+03	1.86E+03	1.92E+03	2.46E+03
Xe-137	1.42E+03	1.22E+04	1.51E+03	1.27E+04
Xe-138	8.83E+03	4.13E+03	9.21E+03	4.75E+03
Ar-41	8.84E+03	2.69E+03	9.30E+03	3.28E+03

Table 2-2: Parameters for Gaseous Alarm Setpoint Determinations - Unit 1

Parameter	Actual Value	Default Value	Units	Comments
X/Q	calculated	2.2E-06	sec/m <sup>3</sup>	USNRC Salem Safety Evaluation, Sup 3
VF (Plant Vent)  (Cont Purge)	as measured or fan curves	1.30E+05  3.50E+04	ft <sup>3</sup> /min	Plant Vent - normal operation  Containment Purge
AF	coordinated	0.25	N/A	Administrative allocation factor with HCGS to ensure combined releases do not exceed release rate limit for site.
C <sub>i</sub>	measured	N/A	μCi/cm <sup>3</sup>	Taken from gamma spectral analysis of gaseous effluent
K <sub>i</sub>	nuclide specific	N/A	mrem/yr per μCi/m <sup>3</sup>	Values from Table 2-1
L <sub>i</sub>	nuclide specific	N/A	mrem/yr per μCi/m <sup>3</sup>	Values from Table 2-1
M <sub>i</sub>	nuclide specific	N/A	mrem/yr per μCi/m <sup>3</sup>	Values from Table 2-1
Sensitivities 1-R41D 1-R16 1-R12A	as determined	N/A	cpm per μCi/m <sup>3</sup>	Monitor sensitivities are controlled under Public Service Blueprint Document (PSBP) 315733
Setpoint 1-R41D 1-R16 1-R12A **	calculated	N/A	cpm	Monitor setpoints are controlled under Public Service Blueprint Document (PSBP 315733)

\*\* Applicable during Modes 1 through 5. During Mode 6 (refueling), monitor setpoint shall be reduced to 2x background in accordance with Technical Specification (CONTROL) Table 3.3-6

Table 2-3: Parameters for Gaseous Alarm Setpoint Determinations - Unit 2

Parameter	Actual Value	Default Value	Units	Comments
X/Q	Calculated	2.2E-6	sec/m <sup>3</sup>	Licensing Technical Specification value
VF Plant Vent	as measured or fan curves	1.30E+05	ft <sup>3</sup> /min	Plant Vent – normal operation
Cont. Purge		3.50E+04		Containment Purge
AF	Coordinated with HCGS	0.25	N/A	Administrative allocation factor to ensure combined releases do not exceed release rate for site.
C <sub>1</sub>	Measured	N/A	μCi/cm <sup>3</sup>	Taken from gamma spectral analysis of gaseous effluent
K <sub>1</sub>	Nuclide specific	N/A	mrem/yr per μCi/m <sup>3</sup>	Values from Table 2-1
L <sub>1</sub>	Nuclide specific	N/A	mrem/yr per μCi/m <sup>3</sup>	Values from Table 2-1
M <sub>1</sub>	Nuclide specific	N/A	mrem/yr per μCi/m <sup>3</sup>	Values from Table 2-1
Sensitivities 2-R41D 2-R16 2-R12A	as determined	N/A	cpm per μCi/m <sup>3</sup>	Monitor sensitivities are controlled under Public Service Blueprint Document (PSBP) 315734
Setpoint 2-R41D 2-R16 2-R12A **	Calculated	N/A	cpm	Monitor setpoints are controlled under Public Service Blueprint Document (PSBP) 315734

\*\* Applicable during MODES 1 through 5. During MODE 6 (refueling), monitor setpoints shall be reduced to 2x background in accordance with Technical Specification (CONTROL) 3.3-6.

Table 2-4: Controlling Locations, Pathways  
and  
Atmospheric Dispersion for Dose Calculations \*

Technical Specification	Location	Pathway(s)	Controlling Age Group	Atmospheric Dispersion	
				X/Q (sec/m <sup>3</sup> )	D/Q (1/m <sup>2</sup> )
3.11.2.1a	site boundary (0.83 mile, N)	noble gases direct exposure	N/A	2.2E-06	N/A
3.11.2.1b	site boundary (0.83 mile, N)	inhalation	child	2.2E-06	N/A
3.11.2.2	site boundary (0.83 mile, N)	gamma-air beta-air	N/A	2.2E-06	N/A
3.11.2.3	residence/dairy** (4.9 miles, W)	milk, ground plane and inhalation	infant	5.4E-08	2.1E-10

\* The identified controlling locations, pathways and atmospheric dispersion are from the Safety Evaluation Report, Supplement No. 3 for the Salem Nuclear Generating Station, Unit 2 (NUREG-0517, December 1978).

\*\* Location and distance are determined from the performance of the annual land use census as required by Technical Specification (CONTROL) 3.12.2.

Table 2-5: Pathway Dose Factors - Atmospheric Releases  
 R(io), Inhalation Pathway Dose Factors - ADULT  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ )

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	1.26E+3	1.26E+3	1.26E+3	1.26E+3	1.26E+3	1.26E+3
C-14	1.82E+4	3.41E+3	3.41E+3	3.41E+3	3.41E+3	3.41E+3	3.41E+3
P-32	1.32E+6	7.71E+4	-	-	-	8.64E+4	5.01E+4
Cr-51	-	-	5.95E+1	2.28E+1	1.44E+4	3.32E+3	1.00E+2
Mn-54	-	3.96E+4	-	9.84E+3	1.40E+6	7.74E+4	6.30E+3
Fe-55	2.46E+4	1.70E+4	-	-	7.21E+4	6.03E+3	3.94E+3
Fe-59	1.18E+4	2.78E+4	-	-	1.02E+6	1.88E+5	1.06E+4
Co-57	-	6.92E+2	-	-	3.70E+5	3.14E+4	6.71E+2
Co-58	-	1.58E+3	-	-	9.28E+5	1.06E+5	2.07E+3
Co-60	-	1.15E+4	-	-	5.97E+6	2.85E+5	1.48E+4
Ni-63	4.32E+5	3.14E+4	-	-	1.78E+5	1.34E+4	1.45E+4
Zn-65	3.24E+4	1.03E+5	-	6.90E+4	8.64E+5	5.34E+4	4.66E+4
Rb-86	-	1.35E+5	-	-	-	1.66E+4	5.90E+4
Sr-89	3.04E+5	-	-	-	1.40E+6	3.50E+5	8.72E+3
Sr-90	9.92E+7	-	-	-	9.60E+6	7.22E+5	6.10E+6
Y-91	4.62E+5	-	-	-	1.70E+6	3.85E+5	1.24E+4
Zr-95	1.07E+5	3.44E+4	-	5.42E+4	1.77E+6	1.50E+5	2.33E+4
Nb-95	1.41E+4	7.82E+3	-	7.74E+3	5.05E+5	1.04E+5	4.21E+3
Ru-103	1.53E+3	-	-	5.83E+3	5.05E+5	1.10E+5	6.58E+2
Ru-106	6.91E+4	-	-	1.34E+5	9.36E+6	9.12E+5	8.72E+3
Ag-110m	1.08E+4	1.00E+4	-	1.97E+4	4.63E+6	3.02E+5	5.94E+3
Sb-124	3.12E+4	5.89E+2	7.55E+1	-	2.48E+6	4.06E+5	1.24E+4
Sb-125	5.34E+4	5.95E+2	5.40E+1	-	1.74E+6	1.01E+5	1.26E+4
Te-125m	3.42E+3	1.58E+3	1.05E+3	1.24E+4	3.14E+5	7.06E+4	4.67E+2
Te-127m	1.26E+4	5.77E+3	3.29E+3	4.58E+4	9.60E+5	1.50E+5	1.57E+3
Te-129m	9.76E+3	4.67E+3	3.44E+3	3.66E+4	1.16E+6	3.83E+5	1.58E+3
I-131	2.52E+4	3.58E+4	1.19E+7	6.13E+4	-	6.28E+3	2.05E+4
I-132	1.16E+3	3.26E+3	1.14E+5	5.18E+3	-	4.06E+2	1.16E+3
I-133	8.64E+3	1.48E+4	2.15E+6	2.58E+4	-	8.88E+3	4.52E+3
I-134	6.44E+2	1.73E+3	2.98E+4	2.75E+3	-	1.01E+0	6.15E+2
I-135	2.68E+3	6.98E+3	4.48E+5	1.11E+4	-	5.25E+3	2.57E+3
Cs-134	3.73E+5	8.48E+5	-	2.87E+5	9.76E+4	1.04E+4	7.28E+5
Cs-136	3.90E+4	1.46E+5	-	8.56E+4	1.20E+4	1.17E+4	1.10E+5
Cs-137	4.78E+5	6.21E+5	-	2.22E+5	7.52E+4	8.40E+3	4.28E+5
Ba-140	3.90E+4	4.90E+1	-	1.67E+1	1.27E+6	2.18E+5	2.57E+3
Ce-141	1.99E+4	1.35E+4	-	6.26E+3	3.62E+5	1.20E+5	1.53E+3
Ce-144	3.43E+6	1.43E+6	-	8.48E+5	7.78E+6	8.16E+5	1.84E+5
Pr-143	9.36E+3	3.75E+3	-	2.16E+3	2.81E+5	2.00E+5	4.64E+2
Nd-147	5.27E+3	6.10E+3	-	3.56E+3	2.21E+5	1.73E+5	3.65E+2

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Inhalation Pathway Dose Factors - TEENAGER  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ )

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	1.27E+3	1.27E+3	1.27E+3	1.27E+3	1.27E+3	1.27E+3
C-14	2.60E+4	4.87E+3	4.87E+3	4.87E+3	4.87E+3	4.87E+3	4.87E+3
P-32	1.89E+6	1.10E+5	-	-	-	9.28E+4	7.16E+4
Cr-51	-	-	7.50E+1	3.07E+1	2.10E+4	3.00E+3	1.35E+2
Mn-54	-	5.11E+4	-	1.27E+4	1.98E+6	6.68E+4	8.40E+3
Fe-55	3.34E+4	2.38E+4	-	-	1.24E+5	6.39E+3	5.54E+3
Fe-59	1.59E+4	3.70E+4	-	-	1.53E+6	1.78E+5	1.43E+4
Co-57	-	6.92E+2	-	-	5.86E+5	3.14E+4	9.20E+2
Co-58	-	2.07E+3	-	-	1.34E+6	9.52E+4	2.78E+3
Co-60	-	1.51E+4	-	-	8.72E+6	2.59E+5	1.98E+4
Ni-63	5.80E+5	4.34E+4	-	-	3.07E+5	1.42E+4	1.98E+4
Zn-65	3.86E+4	1.34E+5	-	8.64E+4	1.24E+6	4.66E+4	6.24E+4
Rb-86	-	1.90E+5	-	-	-	1.77E+4	8.40E+4
Sr-89	4.34E+5	-	-	-	2.42E+6	3.71E+5	1.25E+4
Sr-90	1.08E+8	-	-	-	1.65E+7	7.65E+5	6.68E+6
Y-91	6.61E+5	-	-	-	2.94E+6	4.09E+5	1.77E+4
Zr-95	1.46E+5	4.58E+4	-	6.74E+4	2.69E+6	1.49E+5	3.15E+4
Nb-95	1.86E+4	1.03E+4	-	1.00E+4	7.51E+5	9.68E+4	5.66E+3
Ru-103	2.10E+3	-	-	7.43E+3	7.83E+5	1.09E+5	8.96E+2
Ru-106	9.84E+4	-	-	1.90E+5	1.61E+7	9.60E+5	1.24E+4
Ag-110m	1.38E+4	1.31E+4	-	2.50E+4	6.75E+6	2.73E+5	7.99E+3
Sb-124	4.30E+4	7.94E+2	9.76E+1	-	3.85E+6	3.98E+5	1.68E+4
Sb-125	7.38E+4	8.08E+2	7.04E+1	-	2.74E+6	9.92E+4	1.72E+4
Te-125m	4.88E+3	2.24E+3	1.40E+3	-	5.36E+5	7.50E+4	6.67E+2
Te-127m	1.80E+4	8.16E+3	4.38E+3	6.54E+4	1.66E+6	1.59E+5	2.18E+3
Te-129m	1.39E+4	6.58E+3	4.58E+3	5.19E+4	1.98E+6	4.05E+5	2.25E+3
I-131	3.54E+4	4.91E+4	1.46E+7	8.40E+4	-	6.49E+3	2.64E+4
I-132	1.59E+3	4.38E+3	1.51E+5	6.92E+3	-	1.27E+3	1.58E+3
I-133	1.22E+4	2.05E+4	2.92E+6	3.59E+4	-	1.03E+4	6.22E+3
I-134	8.88E+2	2.32E+3	3.95E+4	3.66E+3	-	2.04E+1	8.40E+2
I-135	3.70E+3	9.44E+3	6.21E+5	1.49E+4	-	6.95E+3	3.49E+3
Cs-134	5.02E+5	1.13E+6	-	3.75E+5	1.46E+5	9.76E+3	5.49E+5
Cs-136	5.15E+4	1.94E+5	-	1.10E+5	1.78E+4	1.09E+4	1.37E+5
Cs-137	6.70E+5	8.48E+5	-	3.04E+5	1.21E+5	8.48E+3	3.11E+5
Ba-140	5.47E+4	6.70E+1	-	2.28E+1	2.03E+6	2.29E+5	3.52E+3
Ce-141	2.84E+4	1.90E+4	-	8.88E+3	6.14E+5	1.26E+5	2.17E+3
Ce-144	4.89E+6	2.02E+6	-	1.21E+6	1.34E+7	8.64E+5	2.62E+5
Pr-143	1.34E+4	5.31E+3	-	3.09E+3	4.83E+5	2.14E+5	6.62E+2
Nd-147	7.86E+3	8.56E+3	-	5.02E+3	3.72E+5	1.82E+5	5.13E+2

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Inhalation Pathway Dose Factors - CHILD  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ )

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	1.12E+3	1.12E+3	1.12E+3	1.12E+3	1.12E+3	1.12E+3
C-14	3.59E+4	6.73E+3	6.73E+3	6.73E+3	6.73E+3	6.73E+3	6.73E+3
P-32	2.60E+6	1.14E+5	-	-	-	4.22E+4	9.88E+4
Cr-51	-	-	8.55E+1	2.43E+1	1.70E+4	1.08E+3	1.54E+2
Mn-54	-	4.29E+4	-	1.00E+4	1.58E+6	2.29E+4	9.51E+3
Fe-55	4.74E+4	2.52E+4	-	-	1.11E+5	2.87E+3	7.77E+3
Fe-59	2.07E+4	3.34E+4	-	-	1.27E+6	7.07E+4	1.67E+4
Co-57	-	9.03E+2	-	-	5.07E+5	1.32E+4	1.07E+3
Co-58	-	1.77E+3	-	-	1.11E+6	3.44E+4	3.16E+3
Co-60	-	1.31E+4	-	-	7.07E+6	9.62E+4	2.26E+4
Ni-63	8.21E+5	4.63E+4	-	-	2.75E+5	6.33E+3	2.80E+4
Zn-65	4.26E+4	1.13E+5	-	7.14E+4	9.95E+5	1.63E+4	7.03E+4
Rb-86	-	1.98E+5	-	-	-	7.99E+3	1.14E+5
Sr-89	5.99E+5	-	-	-	2.16E+6	1.67E+5	1.72E+4
Sr-90	1.01E+8	-	-	-	1.48E+7	3.43E+5	6.44E+6
Y-91	9.14E+5	-	-	-	2.63E+6	1.84E+5	2.44E+4
Zr-95	1.90E+5	4.18E+4	-	5.96E+4	2.23E+6	6.11E+4	3.70E+4
Nb-95	2.35E+4	9.18E+3	-	8.62E+3	6.14E+5	3.70E+4	6.55E+3
Ru-103	2.79E+3	-	-	7.03E+3	6.62E+5	4.48E+4	1.07E+3
Ru-106	1.36E+5	-	-	1.84E+5	1.43E+7	4.29E+5	1.69E+4
Ag-110m	1.69E+4	1.14E+4	-	2.12E+4	5.48E+6	1.00E+5	9.14E+3
Sb-124	5.74E+4	7.40E+2	1.26E+2	-	3.24E+6	1.64E+5	2.00E+4
Sb-125	9.84E+4	7.59E+2	9.10E+1	-	2.32E+6	4.03E+4	2.07E+4
Te-125m	6.73E+3	2.33E+3	1.92E+3	-	4.77E+5	3.38E+4	9.14E+2
Te-127m	2.49E+4	8.55E+3	6.07E+3	6.36E+4	1.48E+6	7.14E+4	3.02E+3
Te-129m	1.92E+4	6.85E+3	6.33E+3	5.03E+4	1.76E+6	1.82E+5	3.04E+3
I-131	4.81E+4	4.81E+4	1.62E+7	7.88E+4	-	2.84E+3	2.73E+4
I-132	2.12E+3	4.07E+3	1.94E+5	6.25E+3	-	3.22E+3	1.88E+3
I-133	1.66E+4	2.03E+4	3.85E+6	3.38E+4	-	5.48E+3	7.70E+3
I-134	1.17E+3	2.16E+3	5.07E+4	3.30E+3	-	9.55E+2	9.95E+2
I-135	4.92E+3	8.73E+3	7.92E+5	1.34E+4	-	4.44E+3	4.14E+3
Cs-134	6.51E+5	1.01E+6	-	3.30E+5	1.21E+5	3.85E+3	2.25E+5
Cs-136	6.51E+4	1.71E+5	-	9.55E+4	1.45E+4	4.18E+3	1.16E+5
Cs-137	9.07E+5	8.25E+5	-	2.82E+5	1.04E+5	3.62E+3	1.28E+5
Ba-140	7.40E+4	6.48E+1	-	2.11E+1	1.74E+6	1.02E+5	4.33E+3
Ce-141	3.92E+4	1.95E+4	-	8.55E+3	5.44E+5	5.66E+4	2.90E+3
Ce-144	6.77E+6	2.12E+6	-	1.17E+6	1.20E+7	3.89E+5	3.61E+5
Pr-143	1.85E+4	5.55E+3	-	3.00E+3	4.33E+5	9.73E+4	9.14E+2
Nd-147	1.08E+4	8.73E+3	-	4.81E+3	3.28E+5	8.21E+4	6.81E+2

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Inhalation Pathway Dose Factors - INFANT  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ )

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	6.47E+2	6.47E+2	6.47E+2	6.47E+2	6.47E+2	6.47E+2
C-14	2.65E+4	5.31E+3	5.31E+3	5.31E+3	5.31E+3	5.31E+3	5.31E+3
P-32	2.03E+6	1.12E+5	-	-	-	1.61E+4	7.74E+4
Cr-51	-	-	5.75E+1	1.32E+1	1.28E+4	3.57E+2	8.95E+1
Mn-54	-	2.53E+4	-	4.98E+3	1.00E+6	7.06E+3	4.98E+3
Fe-55	1.97E+4	1.17E+4	-	-	8.69E+4	1.09E+3	3.33E+3
Fe-59	1.36E+4	2.35E+4	-	-	1.02E+6	2.48E+4	9.48E+3
Co-57	-	6.51E+2	-	-	3.79E+5	4.86E+3	6.41E+2
Co-58	-	1.22E+3	-	-	7.77E+5	1.11E+4	1.82E+3
Co-60	-	8.02E+3	-	-	4.51E+6	3.19E+4	1.18E+4
Ni-63	3.39E+5	2.04E+4	-	-	2.09E+5	2.42E+3	1.16E+4
Zn-65	1.93E+4	6.26E+4	-	3.25E+4	6.47E+5	5.14E+4	3.11E+4
Rb-86	-	1.90E+5	-	-	-	3.04E+3	8.82E+4
Sr-89	3.98E+5	-	-	-	2.03E+6	6.40E+4	1.14E+4
Sr-90	4.09E+7	-	-	-	1.12E+7	1.31E+5	2.59E+6
Y-91	5.88E+5	-	-	-	2.45E+6	7.03E+4	1.57E+4
Zr-95	1.15E+5	2.79E+4	-	3.11E+4	1.75E+6	2.17E+4	2.03E+4
Nb-95	1.57E+4	6.43E+3	-	4.72E+3	4.79E+5	1.27E+4	3.78E+3
Ru-103	2.02E+3	-	-	4.24E+3	5.52E+5	1.61E+4	6.79E+2
Ru-106	8.68E+4	-	-	1.07E+5	1.16E+7	1.64E+5	1.09E+4
Ag-110m	9.98E+3	7.22E+3	-	1.09E+4	3.67E+6	3.30E+4	5.00E+3
Sb-124	3.79E+4	5.56E+2	1.01E+2	-	2.65E+6	5.91E+4	1.20E+4
Sb-125	5.17E+4	4.77E+2	6.23E+1	-	1.64E+6	1.47E+4	1.09E+4
Te-125m	4.76E+3	1.99E+3	1.62E+3	-	4.47E+5	1.29E+4	6.58E+2
Te-127m	1.67E+4	6.90E+3	4.87E+3	3.75E+4	1.31E+6	2.73E+4	2.07E+3
Te-129m	1.41E+4	6.09E+3	5.47E+3	3.18E+4	1.68E+6	6.90E+4	2.23E+3
I-131	3.79E+4	4.44E+4	1.48E+7	5.18E+4	-	1.06E+3	1.96E+4
I-132	1.69E+3	3.54E+3	1.69E+5	3.95E+5	-	1.90E+3	1.26E+3
I-133	1.32E+4	1.92E+4	3.56E+6	2.24E+4	-	2.61E+3	5.60E+3
I-134	9.21E+2	1.88E+3	4.45E+4	2.09E+3	-	1.29E+3	6.65E+2
I-135	3.86E+3	7.60E+3	6.96E+5	8.47E+3	-	1.83E+3	2.77E+3
Cs-134	3.96E+5	7.03E+5	-	1.90E+5	7.97E+4	1.33E+3	7.45E+4
Cs-136	4.83E+4	1.35E+5	-	5.64E+4	1.18E+4	1.43E+3	5.29E+4
Cs-137	5.49E+5	6.12E+5	-	1.72E+5	7.13E+4	1.33E+3	4.55E+4
Ba-140	5.60E+4	5.60E+1	-	1.34E+1	1.60E+6	3.84E+4	2.90E+3
Ce-141	2.77E+4	1.67E+4	-	5.25E+3	5.17E+5	2.16E+4	1.99E+3
Ce-144	3.19E+6	1.21E+6	-	5.38E+5	9.84E+6	1.48E+5	1.76E+5
Pr-143	1.40E+4	5.24E+3	-	1.97E+3	4.33E+5	3.72E+4	6.99E+2
Nd-147	7.94E+3	8.13E+3	-	3.15E+3	3.22E+5	3.12E+4	5.00E+2

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Grass-Cow-Milk Pathway Dose Factors - ADULT  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	7.63E+2	7.63E+2	7.63E+2	7.63E+2	7.63E+2	7.63E+2
C-14	3.63E+5	7.26E+4	7.26E+4	7.26E+4	7.26E+4	7.26E+4	7.26E+4
P-32	1.71E+10	1.06E+9	-	-	-	1.92E+9	6.60E+8
Cr-51	-	-	1.71E+4	6.30E+3	3.80E+4	7.20E+6	2.86E+4
Mn-54	-	8.40E+6	-	2.50E+6	-	2.57E+7	1.60E+6
Fe-55	2.51E+7	1.73E+7	-	-	9.67E+6	9.95E+6	4.04E+6
Fe-59	2.98E+7	7.00E+7	-	-	1.95E+7	2.33E+8	2.68E+7
Co-57	-	1.28E+6	-	-	-	3.25E+7	2.13E+6
Co-58	-	4.72E+6	-	-	-	9.57E+7	1.06E+7
Co-60	-	1.64E+7	-	-	-	3.08E+8	3.62E+7
Ni-63	6.73E+9	4.66E+8	-	-	-	9.73E+7	2.26E+8
Zn-65	1.37E+9	4.36E+9	-	2.92E+9	-	2.75E+9	1.97E+9
Rb-86	-	2.59E+9	-	-	-	5.11E+8	1.21E+9
Sr-89	1.45E+9	-	-	-	-	2.33E+8	4.16E+7
Sr-90	4.68E+10	-	-	-	-	1.35E+9	1.15E+10
Y-91	8.60E+3	-	-	-	-	4.73E+6	2.30E+2
Zr-95	9.46E+2	3.03E+2	-	4.76E+2	-	9.62E+5	2.05E+2
Nb-95	8.25E+4	4.59E+4	-	4.54E+4	-	2.79E+8	2.47E+4
Ru-103	1.02E+3	-	-	3.89E+3	-	1.19E+5	4.39E+2
Ru-106	2.04E+4	-	-	3.94E+4	-	1.32E+6	2.58E+3
Ag-110m	5.83E+7	5.39E+7	-	1.06E+8	-	2.20E+10	3.20E+7
Sb-124	2.57E+7	4.86E+5	6.24E+4	-	2.00E+7	7.31E+8	1.02E+7
Sb-125	2.04E+7	2.28E+5	2.08E+4	-	1.58E+7	2.25E+8	4.86E+6
Te-125m	1.63E+7	5.90E+6	4.90E+6	6.63E+7	-	6.50E+7	2.18E+6
Te-127m	4.58E+7	1.64E+7	1.17E+7	1.86E+8	-	1.54E+8	5.58E+6
Te-129m	6.04E+7	2.25E+7	2.08E+7	2.52E+8	-	3.04E+8	9.57E+6
I-131	2.96E+8	4.24E+8	1.39E+11	7.27E+8	-	1.12E+8	2.43E+8
I-132	1.64E-1	4.37E-1	1.53E+1	6.97E-1	-	8.22E-2	1.53E-1
I-133	3.97E+6	6.90E+6	1.01E+9	1.20E+7	-	6.20E+6	2.10E+6
I-134	-	-	-	-	-	-	-
I-135	1.39E+4	3.63E+4	2.40E+6	5.83E+4	-	4.10E+4	1.34E+4
Cs-134	5.65E+9	1.34E+10	-	4.35E+9	1.44E+9	2.35E+8	1.10E+10
Cs-136	2.61E+8	1.03E+9	-	5.74E+8	7.87E+7	1.17E+8	7.42E+8
Cs-137	7.38E+9	1.01E+10	-	3.43E+9	1.14E+9	1.95E+8	6.61E+9
Ba-140	2.69E+7	3.38E+4	-	1.15E+4	1.93E+4	5.54E+7	1.76E+6
Ce-141	4.84E+3	3.27E+3	-	1.52E+3	-	1.25E+7	3.71E+2
Ce-144	3.58E+5	1.50E+5	-	8.87E+4	-	1.21E+8	1.92E+4
Pr-143	1.59E+2	6.37E+1	-	3.68E+1	-	6.96E+5	7.88E+0
Nd-147	9.42E+1	1.09E+2	-	6.37E+1	-	5.23E+5	6.52E+0

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Grass-Cow-Milk Pathway Dose Factors - TEENAGER  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	9.94E+2	9.94E+2	9.94E+2	9.94E+2	9.94E+2	9.94E+2
C-14	6.70E+5	1.34E+5	1.34E+5	1.34E+5	1.34E+5	1.34E+5	1.34E+5
P-32	3.15E+10	1.95E+9	-	-	-	2.65E+9	1.22E+9
Cr-51	-	-	2.78E+4	1.10E+4	7.13E+4	8.40E+6	5.00E+4
Mn-54	-	1.40E+7	-	4.17E+6	-	2.87E+7	2.78E+6
Fe-55	4.45E+7	3.16E+7	-	-	2.00E+7	1.37E+7	7.36E+6
Fe-59	5.20E+7	1.21E+8	-	-	3.82E+7	2.87E+8	4.68E+7
Co-57	-	2.25E+6	-	-	-	4.19E+7	3.76E+6
Co-58	-	7.95E+6	-	-	-	1.10E+8	1.83E+7
Co-60	-	2.78E+7	-	-	-	3.62E+8	6.26E+7
Ni-63	1.18E+10	8.35E+8	-	-	-	1.33E+8	4.01E+8
Zn-65	2.11E+9	7.31E+9	-	4.68E+9	-	3.10E+9	3.41E+9
Rb-86	-	4.73E+9	-	-	-	7.00E+8	2.22E+9
Sr-89	2.67E+9	-	-	-	-	3.18E+8	7.66E+7
Sr-90	9.92E+7	-	-	-	9.60E+6	7.22E+5	6.10E+6
Y-91	1.58E+4	-	-	-	-	6.48E+6	4.24E+2
Zr-95	1.65E+3	5.22E+2	-	7.67E+2	-	1.20E+6	3.59E+2
Nb-95	1.41E+5	7.80E+4	-	7.57E+4	-	3.34E+8	4.30E+4
Ru-103	1.81E+3	-	-	6.40E+3	-	1.52E+5	7.75E+2
Ru-106	3.75E+4	-	-	7.23E+4	-	1.80E+6	4.73E+3
Ag-110m	9.63E+7	9.11E+7	-	1.74E+8	-	2.56E+10	5.54E+7
Sb-124	4.59E+7	8.46E+5	1.04E+5	-	4.01E+7	9.25E+8	1.79E+7
Sb-125	3.65E+7	3.99E+5	3.49E+4	-	3.21E+7	2.84E+8	8.54E+6
Te-125m	3.00E+7	1.08E+7	8.39E+6	-	-	8.86E+7	4.02E+6
Te-127m	8.44E+7	2.99E+7	2.01E+7	3.42E+8	-	2.10E+8	1.00E+7
Te-129m	1.11E+8	4.10E+7	3.57E+7	4.62E+8	-	4.15E+8	1.75E+7
I-131	5.38E+8	7.53E+8	2.20E+11	1.30E+9	-	1.49E+8	4.04E+8
I-132	2.90E-1	7.59E-1	2.56E+1	1.20E+0	-	3.31E-1	2.72E-1
I-133	7.24E+6	1.23E+7	1.72E+9	2.15E+7	-	9.30E+6	3.75E+6
I-134	-	-	-	-	-	-	-
I-135	2.47E+4	6.35E+4	4.08E+6	1.00E+5	-	7.03E+4	2.35E+4
Cs-134	9.81E+9	2.31E+10	-	7.34E+9	2.80E+9	2.87E+8	1.07E+10
Cs-136	4.45E+8	1.75E+9	-	9.53E+8	1.50E+8	1.41E+8	1.18E+9
Cs-137	1.34E+10	1.78E+10	-	6.06E+9	2.35E+9	2.53E+8	6.20E+9
Ba-140	4.85E+7	5.95E+4	-	2.02E+4	4.00E+4	7.49E+7	3.13E+6
Ce-141	8.87E+3	1.35E+4	-	2.79E+3	-	1.69E+7	6.81E+2
Ce-144	6.58E+5	2.72E+5	-	1.63E+5	-	1.66E+8	3.54E+4
Pr-143	2.92E+2	1.17E+2	-	6.77E+1	-	9.61E+5	1.45E+1
Nd-147	1.81E+2	1.97E+2	-	1.16E+2	-	7.11E+5	1.18E+1

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Grass-Cow-Milk Pathway Dose Factors - CHILD  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

H-3	-	1.57E+3	1.57E+3	1.57E+3	1.57E+3	1.57E+3	1.57E+3
C-14	1.65E+6	3.29E+5	3.29E+5	3.29E+5	3.29E+5	3.29E+5	3.29E+5
P-32	7.77E+10	3.64E+9	-	-	-	2.15E+9	3.00E+9
Cr-51	-	-	5.66E+4	1.55E+4	1.03E+5	5.41E+6	1.02E+5
Mn-54	-	2.09E+7	-	5.87E+6	-	1.76E+7	5.58E+6
Fe-55	1.12E+8	5.93E+7	-	-	3.35E+7	1.10E+7	1.84E+7
Fe-59	1.20E+8	1.95E+8	-	-	5.65E+7	2.03E+8	9.71E+7
Co-57	-	3.84E+6	-	-	-	3.14E+7	7.77E+6
Co-58	-	1.21E+7	-	-	-	7.08E+7	3.72E+7
Co-60	-	4.32E+7	-	-	-	2.39E+8	1.27E+8
Ni-63	2.96E+10	1.59E+9	-	-	-	1.07E+8	1.01E+9
Zn-65	4.13E+9	1.10E+10	-	6.94E+9	-	1.93E+9	6.85E+9
Rb-86	-	8.77E+9	-	-	-	5.64E+8	5.39E+9
Sr-89	6.62E+9	-	-	-	-	2.56E+8	1.89E+8
Sr-90	1.12E+11	-	-	-	-	1.51E+9	2.83E+10
Y-91	3.91E+4	-	-	-	-	5.21E+6	1.04E+3
Zr-95	3.84E+3	8.45E+2	-	1.21E+3	-	8.81E+5	7.52E+2
Nb-95	3.18E+5	1.24E+5	-	1.16E+5	-	2.29E+8	8.84E+4
Ru-103	4.29E+3	-	-	1.08E+4	-	1.11E+5	1.65E+3
Ru-106	9.24E+4	-	-	1.25E+5	-	1.44E+6	1.15E+4
Ag-110m	2.09E+8	1.41E+8	-	2.63E+8	-	1.68E+10	1.13E+8
Sb-124	1.09E+8	1.41E+8	2.40E+5	-	6.03E+7	6.79E+8	3.81E+7
Sb-125	8.70E+7	1.41E+6	8.06E+4	-	4.85E+7	2.08E+8	1.82E+7
Te-125m	7.38E+7	2.00E+7	2.07E+7	-	-	7.12E+7	9.84E+6
Te-127m	2.08E+8	5.60E+7	4.97E+7	5.93E+8	-	1.68E+8	2.47E+7
Te-129m	2.72E+8	7.61E+7	8.78E+7	8.00E+8	-	3.32E+8	4.23E+7
I-131	1.30E+9	1.31E+9	4.34E+11	2.15E+9	-	1.17E+8	7.46E+8
I-132	6.86E-1	1.26E+0	5.85E+1	1.93E+0	-	1.48E+0	5.80E-1
I-133	1.76E+7	2.18E+7	4.04E+9	3.63E+7	-	8.77E+6	8.23E+6
I-134	-	-	-	-	-	-	-
I-135	5.84E+4	1.05E+5	9.30E+6	1.61E+5	-	8.00E+4	4.97E+4
Cs-134	2.26E+10	3.71E+10	-	1.15E+10	4.13E+9	2.00E+8	7.83E+9
Cs-136	1.00E+9	2.76E+9	-	1.47E+9	2.19E+8	9.70E+7	1.79E+9
Cs-137	3.22E+10	3.09E+10	-	1.01E+10	3.62E+9	1.93E+8	4.55E+9
Ba-140	1.17E+8	1.03E+5	-	3.34E+4	6.12E+4	5.94E+7	6.84E+6
Ce-141	2.19E+4	1.09E+4	-	4.78E+3	-	1.36E+7	1.62E+3
Ce-144	1.62E+6	5.09E+5	-	2.82E+5	-	1.33E+8	8.66E+4
Pr-143	7.23E+2	2.17E+2	-	1.17E+2	-	7.80E+5	3.59E+1
Nd-147	4.45E+2	3.60E+2	-	1.98E+2	-	5.71E+5	2.79E+1

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Grass-Cow-Milk Pathway Dose Factors - INFANT  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	2.38E+3	2.38E+3	2.38E+3	2.38E+3	2.38E+3	2.38E+3
C-14	3.23E+6	6.89E+5	6.89E+5	6.89E+5	6.89E+5	6.89E+5	6.89E+5
P-32	1.60E+11	9.42E+9	-	-	-	2.17E+9	6.21E+9
Cr-51	-	-	1.05E+5	2.30E+4	2.05E+5	4.71E+6	1.61E+5
Mn-54	-	3.89E+7	-	8.63E+6	-	1.43E+7	8.83E+6
Fe-55	1.35E+8	8.72E+7	-	-	4.27E+7	1.11E+7	2.33E+7
Fe-59	2.25E+8	3.93E+8	-	-	1.16E+8	1.88E+8	1.55E+8
Co-57	-	8.95E+6	-	-	-	3.05E+7	1.46E+7
Co-58	-	2.43E+7	-	-	-	6.05E+7	6.06E+7
Co-60	-	8.81E+7	-	-	-	2.10E+8	2.08E+8
Ni-63	3.49E+10	2.16E+9	-	-	-	1.07E+8	1.21E+9
Zn-65	5.55E+9	1.90E+10	-	9.23E+9	-	1.61E+10	8.78E+9
Rb-86	-	2.22E+10	-	-	-	5.69E+8	1.10E+10
Sr-89	1.26E+10	-	-	-	-	2.59E+8	3.61E+8
Sr-90	1.22E+11	-	-	-	-	1.52E+9	3.10E+10
Y-91	7.33E+4	-	-	-	-	5.26E+6	1.95E+3
Zr-95	6.83E+3	1.66E+3	-	1.79E+3	-	8.28E+5	1.18E+3
Nb-95	5.93E+5	2.44E+5	-	1.75E+5	-	2.06E+8	1.41E+5
Ru-103	8.69E+3	-	-	1.81E+4	-	1.06E+5	2.91E+3
Ru-106	1.90E+5	-	-	2.25E+5	-	1.44E+6	2.38E+4
Ag-110m	3.86E+8	2.82E+8	-	4.03E+8	-	1.46E+10	1.86E+8
Sb-124	2.09E+8	3.08E+6	5.56E+5	-	1.31E+8	6.46E+8	6.49E+7
Sb-125	1.49E+8	1.45E+6	1.87E+5	-	9.38E+7	1.99E+8	3.07E+7
Te-125m	1.51E+8	5.04E+7	5.07E+7	-	-	7.18E+7	2.04E+7
Te-127m	4.21E+8	1.40E+8	1.22E+8	1.04E+9	-	1.70E+8	5.10E+7
Te-129m	5.59E+8	1.92E+8	2.15E+8	1.40E+9	-	3.34E+8	8.62E+7
I-131	2.72E+9	3.21E+9	1.05E+12	3.75E+9	-	1.15E+8	1.41E+9
I-132	1.42E+0	2.89E+0	1.35E+2	3.22E+0	-	2.34E+0	1.03E+0
I-133	3.72E+7	5.41E+7	9.84E+9	6.36E+7	-	9.16E+6	1.58E+7
I-134	-	-	1.01E-9	-	-	-	-
I-135	1.21E+5	2.41E+5	2.16E+7	2.69E+5	-	8.74E+4	8.80E+4
Cs-134	3.65E+10	6.80E+10	-	1.75E+10	7.18E+9	1.85E+8	6.87E+9
Cs-136	1.96E+9	5.77E+9	-	2.30E+9	4.70E+8	8.76E+7	2.15E+9
Cs-137	5.15E+10	6.02E+10	-	1.62E+10	6.55E+9	1.88E+8	4.27E+9
Ba-140	2.41E+8	2.41E+5	-	5.73E+4	1.48E+5	5.92E+7	1.24E+7
Ce-141	4.33E+4	2.64E+4	-	8.15E+3	-	1.37E+7	3.11E+3
Ce-144	2.33E+6	9.52E+5	-	3.85E+5	-	1.33E+8	1.30E+5
Pr-143	1.49E+3	5.59E+2	-	2.08E+2	-	7.89E+5	7.41E+1
Nd-147	8.82E+2	9.06E+2	-	3.49E+2	-	5.74E+5	5.55E+1

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Vegetation Pathway Dose Factors - ADULT  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	2.26E+3	2.26E+3	2.26E+3	2.26E+3	2.26E+3	2.26E+3
C-14	8.97E+5	1.79E+5	1.79E+5	1.79E+5	1.79E+5	1.79E+5	1.79E+5
P-32	1.40E+9	8.73E+7	-	-	-	1.58E+8	5.42E+7
Cr-51	-	-	2.79E+4	1.03E+4	6.19E+4	1.17E+7	4.66E+4
Mn-54	-	3.11E+8	-	9.27E+7	-	9.54E+8	5.94E+7
Fe-55	2.09E+8	1.45E+8	-	-	8.06E+7	8.29E+7	3.37E+7
Fe-59	1.27E+8	2.99E+8	-	-	8.35E+7	9.96E+8	1.14E+8
Co-57	-	1.17E+7	-	-	-	2.97E+8	1.95E+7
Co-58	-	3.09E+7	-	-	-	6.26E+8	6.92E+7
Co-60	-	1.67E+8	-	-	-	3.14E+9	3.69E+8
Ni-63	1.04E+10	7.21E+8	-	-	-	1.50E+8	3.49E+8
Zn-65	3.17E+8	1.01E+9	-	6.75E+8	-	6.36E+8	4.56E+8
Rb-86	-	2.19E+8	-	-	-	4.32E+7	1.02E+8
Sr-89	9.96E+9	-	-	-	-	1.60E+9	2.86E+8
Sr-90	6.05E+11	-	-	-	-	1.75E+10	1.48E+10
Y-91	5.13E+6	-	-	-	-	2.82E+9	1.37E+5
Zr-95	1.19E+6	3.81E+5	-	5.97E+5	-	1.21E+9	2.58E+5
Nb-95	1.42E+5	7.91E+4	-	7.81E+4	-	4.80E+8	4.25E+4
Ru-103	4.80E+6	-	-	1.83E+7	-	5.61E+8	2.07E+6
Ru-106	1.93E+8	-	-	3.72E+8	-	1.25E+10	2.44E+7
Ag-110m	1.06E+7	9.76E+6	-	1.92E+7	-	3.98E+9	5.80E+6
Sb-124	1.04E+8	1.96E+6	2.52E+5	-	8.08E+7	2.95E+9	4.11E+7
Sb-125	1.36E+8	1.52E+6	1.39E+5	-	1.05E+8	1.50E+9	3.25E+7
Te-125m	9.66E+7	3.50E+7	2.90E+7	3.93E+8	-	3.86E+8	1.29E+7
Te-127m	3.49E+8	1.25E+8	8.92E+7	1.42E+9	-	1.17E+9	4.26E+7
Te-129m	2.55E+8	9.50E+7	8.75E+7	1.06E+9	-	1.28E+9	4.03E+7
I-131	8.09E+7	1.16E+8	3.79E+10	1.98E+8	-	3.05E+7	6.63E+7
I-132	5.74E+1	1.54E+2	5.38E+3	2.45E+2	-	2.89E+1	5.38E+1
I-133	2.12E+6	3.69E+6	5.42E+8	6.44E+6	-	3.31E+6	1.12E+6
I-134	1.06E-4	2.88E-4	5.00E-3	4.59E-4	-	2.51E-7	1.03E-4
I-135	4.08E+4	1.07E+5	7.04E+6	1.71E+5	-	1.21E+5	3.94E+4
Cs-134	4.66E+9	1.11E+10	-	3.59E+9	1.19E+9	1.94E+8	9.07E+9
Cs-136	4.20E+7	1.66E+8	-	9.24E+7	1.27E+7	1.89E+7	1.19E+8
Cs-137	6.36E+9	8.70E+9	-	2.95E+9	9.81E+8	1.68E+8	5.70E+9
Ba-140	1.29E+8	1.62E+5	-	5.49E+4	9.25E+4	2.65E+8	8.43E+6
Ce-141	1.96E+5	1.33E+5	-	6.17E+4	-	5.08E+8	1.51E+4
Ce-144	3.29E+7	1.38E+7	-	8.16E+6	-	1.11E+10	1.77E+6
Pr-143	6.34E+4	2.54E+4	-	1.47E+4	-	2.78E+8	3.14E+3
Nd-147	3.34E+4	3.86E+4	-	2.25E+4	-	1.85E+8	2.31E+3

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Vegetation Pathway Dose Factors - TEENAGER  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	2.59E+3	2.59E+3	2.59E+3	2.59E+3	2.59E+3	2.59E+3
C-14	1.45E+6	2.91E+5	2.91E+5	2.91E+5	2.91E+5	2.91E+5	2.91E+5
P-32	1.61E+9	9.96E+7	-	-	-	1.35E+8	6.23E+7
Cr-51	-	-	3.44E+4	1.36E+4	8.85E+4	1.04E+7	6.20E+4
Mn-54	-	4.52E+8	-	1.35E+8	-	9.27E+8	8.97E+7
Fe-55	3.25E+8	2.31E+8	-	-	1.46E+8	9.98E+7	5.38E+7
Fe-59	1.81E+8	4.22E+8	-	-	1.33E+8	9.98E+8	1.63E+8
Co-57	-	1.79E+7	-	-	-	3.34E+8	3.00E+7
Co-58	-	4.38E+7	-	-	-	6.04E+8	1.01E+8
Co-60	-	2.49E+8	-	-	-	3.24E+9	5.60E+8
Ni-63	1.61E+10	1.13E+9	-	-	-	1.81E+8	5.45E+8
Zn-65	4.24E+8	1.47E+9	-	9.41E+8	-	6.23E+8	6.86E+8
Rb-86	-	2.73E+8	-	-	-	4.05E+7	1.28E+8
Sr-89	1.51E+10	-	-	-	-	1.80E+9	4.33E+8
Sr-90	7.51E+11	-	-	-	-	2.11E+10	1.85E+11
Y-91	7.87E+6	-	-	-	-	3.23E+9	2.11E+5
Zr-95	1.74E+6	5.49E+5	-	8.07E+5	-	1.27E+9	3.78E+5
Nb-95	1.92E+5	1.06E+5	-	1.03E+5	-	4.55E+8	5.86E+4
Ru-103	6.87E+6	-	-	2.42E+7	-	5.74E+8	2.94E+6
Ru-106	3.09E+8	-	-	5.97E+8	-	1.48E+10	3.90E+7
Ag-110m	1.52E+7	1.44E+7	-	2.74E+7	-	4.04E+9	8.74E+6
Sb-124	1.55E+8	2.85E+6	3.51E+5	-	1.35E+8	3.11E+9	6.03E+7
Sb-125	2.14E+8	2.34E+6	2.04E+5	-	1.88E+8	1.66E+9	5.00E+7
Te-125m	1.48E+8	5.34E+7	4.14E+7	-	-	4.37E+8	1.98E+7
Te-127m	5.51E+8	1.96E+8	1.31E+8	2.24E+9	-	1.37E+9	6.56E+7
Te-129m	3.67E+8	1.36E+8	1.18E+8	1.54E+9	-	1.38E+9	5.81E+7
I-131	7.70E+7	1.08E+8	3.14E+10	1.85E+8	-	2.13E+7	5.79E+7
I-132	5.18E+1	1.36E+2	4.57E+3	2.14E+2	-	5.91E+1	4.87E+1
I-133	1.97E+6	3.34E+6	4.66E+8	5.86E+6	-	2.53E+6	1.02E+6
I-134	9.59E-5	2.54E-4	4.24E-3	4.01E-4	-	3.35E-6	9.13E-5
I-135	3.68E+4	9.48E+4	6.10E+6	1.50E+5	-	1.05E+5	3.52E+4
Cs-134	7.09E+9	1.67E+10	-	5.30E+9	2.02E+9	2.08E+8	7.74E+9
Cs-136	4.29E+7	1.69E+8	-	9.19E+7	1.45E+7	1.36E+7	1.13E+8
Cs-137	1.01E+10	1.35E+10	-	4.59E+9	1.78E+9	1.92E+8	4.69E+9
Ba-140	1.38E+8	1.69E+5	-	5.75E+4	1.14E+5	2.13E+8	8.91E+6
Ce-141	2.82E+5	1.88E+5	-	8.86E+4	-	5.38E+8	2.16E+4
Ce-144	5.27E+7	2.18E+7	-	1.30E+7	-	1.33E+10	2.83E+6
Pr-143	7.12E+4	2.84E+4	-	1.65E+4	-	2.34E+8	3.55E+3
Nd-147	3.63E+4	3.94E+4	-	2.32E+4	-	1.42E+8	2.36E+3

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Vegetation Pathway Dose Factors - CHILD  
 (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) for H-3 and C-14  
 ( $\text{m}^2 * \text{mrem}/\text{yr}$  per  $\mu\text{Ci}/\text{sec}$ ) for others

Nuclide	Bone	Liver	Thyroid	Kidney	Lung	GI-LLI	T.Body
H-3	-	4.01E+3	4.01E+3	4.01E+3	4.01E+3	4.01E+3	4.01E+3
C-14	3.50E+6	7.01E+5	7.01E+5	7.01E+5	7.01E+5	7.01E+5	7.01E+5
P-32	3.37E+9	1.58E+8	-	-	-	9.30E+7	1.30E+8
Cr-51	-	-	6.54E+4	1.79E+4	1.19E+5	6.25E+6	1.18E+5
Mn-54	-	6.61E+8	-	1.85E+8	-	5.55E+8	1.76E+8
Fe-55	8.00E+8	4.24E+8	-	-	2.40E+8	7.86E+7	1.31E+8
Fe-59	4.01E+8	6.49E+8	-	-	1.88E+8	6.76E+8	3.23E+8
Co-57	-	2.99E+7	-	-	-	2.45E+8	6.04E+7
Co-58	-	6.47E+7	-	-	-	3.77E+8	1.98E+8
Co-60	-	3.78E+8	-	-	-	2.10E+9	1.12E+9
Ni-63	3.95E+10	2.11E+9	-	-	-	1.42E+8	1.34E+9
Zn-65	8.12E+8	2.16E+9	-	1.36E+9	-	3.80E+8	1.35E+9
Rb-86	-	4.52E+8	-	-	-	2.91E+7	2.78E+8
Sr-89	3.59E+10	-	-	-	-	1.39E+9	1.03E+9
Sr-90	1.24E+12	-	-	-	-	1.67E+10	3.15E+11
Y-91	1.87E+7	-	-	-	-	2.49E+9	5.01E+5
Zr-95	3.90E+6	8.58E+5	-	1.23E+6	-	8.95E+8	7.64E+5
Nb-95	4.10E+5	1.59E+5	-	1.50E+5	-	2.95E+8	1.14E+5
Ru-103	1.55E+7	-	-	3.89E+7	-	3.99E+8	5.94E+6
Ru-106	7.45E+8	-	-	1.01E+9	-	1.16E+10	9.30E+7
Ag-110m	3.22E+7	2.17E+7	-	4.05E+7	-	2.58E+9	1.74E+7
Sb-124	3.52E+8	4.57E+6	7.78E+5	-	1.96E+8	2.20E+9	1.23E+8
Sb-125	4.99E+8	3.85E+6	4.62E+5	-	2.78E+8	1.19E+9	1.05E+8
Te-125m	3.51E+8	9.50E+7	9.84E+7	-	-	3.38E+8	4.67E+7
Te-127m	1.32E+9	3.56E+8	3.16E+8	3.77E+9	-	1.07E+9	1.57E+8
Te-129m	8.54E+8	2.39E+8	2.75E+8	2.51E+9	-	1.04E+9	1.33E+8
I-131	1.43E+8	1.44E+8	4.76E+10	2.36E+8	-	1.28E+7	8.18E+7
I-132	9.20E+1	1.69E+2	7.84E+3	2.59E+2	-	1.99E+2	7.77E+1
I-133	3.59E+6	4.44E+6	8.25E+8	7.40E+6	-	1.79E+6	1.68E+6
I-134	1.70E-4	3.16E-4	7.28E-3	4.84E-4	-	2.10E-4	1.46E-4
I-135	6.54E+4	1.18E+5	1.04E+7	1.81E+5	-	8.98E+4	5.57E+4
Cs-134	1.60E+10	2.63E+10	-	8.14E+9	2.92E+9	1.42E+8	5.54E+9
Cs-136	8.06E+7	2.22E+8	-	1.18E+8	1.76E+7	7.79E+6	1.43E+8
Cs-137	2.39E+10	2.29E+10	-	7.46E+9	2.68E+9	1.43E+8	3.38E+9
Ba-140	2.77E+8	2.43E+5	-	7.90E+4	1.45E+5	1.40E+8	1.62E+7
Ce-141	6.35E+5	3.26E+5	-	1.43E+5	-	4.07E+8	4.84E+4
Ce-144	1.27E+8	3.98E+7	-	2.21E+7	-	1.04E+10	6.78E+6
Pr-143	1.48E+5	4.46E+4	-	2.41E+4	-	1.60E+8	7.37E+3
Nd-147	7.16E+4	5.80E+4	-	3.18E+4	-	9.18E+7	4.49E+3

Table 2-5 (cont'd)  
 Pathway Dose Factors - Atmospheric Releases  
 R(io), Ground Plane Pathway Dose Factors  
 (m2 \* mrem/yr per  $\mu$ Ci/sec)

<u>Nuclide</u>	<u>Any Organ</u>
H-3	-
C-14	-
P-32	-
Cr-51	4.68E+6
Mn-54	1.34E+9
Fe-55	-
Fe-59	2.75E+8
Co-58	3.82E+8
Co-60	2.16E+10
Ni-63	-
Zn-65	7.45E+8
Rb-86	8.98E+6
Sr-89	2.16E+4
Sr-90	-
Y-91	1.08E+6
Zr-95	2.48E+8
Nb-95	1.36E+8
Ru-103	1.09E+8
Ru-106	4.21E+8
Ag-110m	3.47E+9
Te-125m	1.55E+6
Te-127m	9.17E+4
Te-129m	2.00E+7
I-131	1.72E+7
I-132	1.24E+6
I-133	2.47E+6
I-134	4.49E+5
I-135	2.56E+6
Cs-134	6.75E+9
Cs-136	1.49E+8
Cs-137	1.04E+10
Ba-140	2.05E+7
Ce-141	1.36E+7
Ce-144	6.95E+7
Pr-143	-
Nd-147	8.40E+6

**APPENDIX A**  
**Evaluation of Default Parameters**  
**for Liquid Effluents**

## APPENDIX A

Evaluation of Default Parameters  
for Liquid Effluents**A. Effective Maximum Permissible Concentration (MPC<sub>e</sub>)**

In accordance with the requirements of Technical Specification (CONTROL) 3.3.3.8 the radioactive liquid effluent monitors shall be operable with alarm setpoints established to ensure that the concentration of radioactive material at the discharge point does not exceed the MPC value of 10 CFR 20, Appendix B, Table II, Column 2 (Appendix F). The determination of allowable radionuclide concentration and corresponding alarm setpoint is a function of the individual radionuclide distribution and corresponding MPC values.

In order to limit the need for routinely having to reestablish the alarm setpoints as a function of changing radionuclide distributions, a default alarm setpoint can be established. This default setpoint can be based on an evaluation of the radionuclide distribution of the liquid effluents from Salem and the effective MPC value for this distribution.

The effective MPC value for a radionuclide distribution is calculated by the equation:

$$MPC_e = \frac{\sum_i C_i \text{ (gamma)}}{\sum_i \frac{C_i}{MPC_i} \text{ (gamma)}}$$

where:

- MPC<sub>e</sub> = an effective MPC value for a mixture of gamma emitting radionuclides (μCi/ml)
- C<sub>i</sub> = concentration of radionuclide i in the mixture
- MPC<sub>i</sub> = the 10 CFR 20, Appendix B, Table II, Column 2 MPC value for radionuclide i (Appendix F) (μCi/ml)

The equation for determining the liquid effluent setpoints (Section 1.2.1, equation 1.2) is based on a multiplication of the effective MPC times the monitor sensitivity. Considering the average effective MPC value for the years 1993, 1994, and 1998, it is reasonable to select an MPC<sub>e</sub> value of 6.05E-06 μCi/ml for Unit 1 and 4.81E-06 μCi/ml for Unit 2 as typical of liquid radwaste discharges.

## B. Correction Factor

The type of radiation detector used to monitor radioactive releases is not capable of detecting non-gamma emitting radionuclides such as H-3, Fe-55, and Sr-89,90, as required by Technical Specification (CONTROL) 3.11.1.1. A conservative default safety factor can be determined to account for non-gamma emitting radionuclides. Non-gamma emitting radionuclides are analyzed at Salem station on a monthly basis from a composite sample of liquid releases.

Nuclide	MPC ( $\mu\text{Ci/ml}$ )	Activity ( $\mu\text{Ci/ml}$ )	Activity / MPC
H-3	3E-3	5.2E-1	173.3
Fe-55	8E-4	2.5E-3	3.1
Sr-89	3E-6	2.0E-5	6.7
Sr-90	3E-7	7.2E-7	2.4
<b>Total</b>			<b>185.5</b>

The values in the table above represent the maximum reactor coolant values for non-gamma emitting nuclides in 1994 for Unit 1 and 2. Reactor coolant values were chosen to represent the maximum concentration of non-gamma emitting nuclides that could be released from Salem Station. The activity values in the table will be diluted by a minimum factor of 800 prior to release. The minimum dilution factor is obtained by using the minimum circulating water flowrate of 100,000 gpm and the maximum release rate of 120 gpm.

A conservative non-gamma factor for non-gamma emitting nuclides can be obtained using the highest Activity/MPC fraction and the minimum dilution factor as follows:

$$\begin{aligned} \text{Non-Gamma Factor} &= 185.5 / 800 = 0.23 \text{ (Rounded up to 0.25)} \\ \text{Correction Factor} &= 1 - 0.25 = 0.75 \end{aligned}$$

## C. Default setpoint determination:

Using the information and parameters described above a default setpoint can be calculated for Unit 1 and 2 liquid radwaste disposal process radiation monitors (R18).

Using these values to calculate the default R18 alarm setpoint value, results in a setpoint that:

- 1) Will not require frequent re-adjustment due to minor variations in the nuclide distribution which are typical of routine plant operations, and
- 2) Will provide for a liquid radwaste discharge rate (as evaluated for each batch release) that is compatible with plant operations (refer to Tables 1-1 and 1-2).

Table A-1: Calculation of Effective MPC - Unit 1

Nuclide	MPC* ( $\mu\text{Ci/ml}$ )	Activity Released (Ci)		
		1993 CURIES	1994 CURIES	1998 CURIES
BE-7	2.00E-03	8.88E-04	ND	ND
NA-24	3.00E-05	6.68E-04	1.62E-04	1.00E-04
CR-51	2.00E-03	5.38E-03	2.02E-03	ND
MN-54	1.00E-04	3.52E-02	1.37E-02	7.16E-04
MN-56	1.00E-04	ND	ND	0.00E+00
FE-59	5.00E-05	4.76E-04	4.84E-03	ND
CO-57	4.00E-04	1.03E-02	3.10E-03	1.78E-05
CO-58	9.00E-05	1.71E+00	6.47E-01	3.39E-02
CO-60	3.00E-05	3.04E-01	1.10E-01	2.42E-02
ZR-95	6.00E-05	3.29E-03	7.13E-04	ND
NB-95	1.00E-04	5.78E-03	1.28E-03	ND
NB-97	9.00E-04	1.27E-03	1.07E-03	4.90E-05
TC-99M	3.00E-03	2.66E-04	ND	ND
SR-89	3.00E-06	ND	ND	2.18E-04
SR-92	6.00E-05	ND	7.32E-06	ND
MO-99	4.00E-05	1.76E-04	1.76E-04	ND
AG-110m	3.00E-05	1.19E-02	1.10E-02	6.58E-05
SN-113	8.00E-05	7.88E-05	4.91E-05	ND
SB-122	3.00E-05	1.21E-03	5.35E-04	1.12E-03
SB-124	2.00E-05	2.08E-02	1.75E-02	1.73E-02
SB-125	1.00E-04	9.04E-02	8.23E-02	3.56E-02
SB-126	3.00E-06	ND	6.18E-05	2.23E-04
I-131	3.00E-07	1.27E-01	1.82E-02	2.32E-03
I-133	1.00E-06	2.16E-03	1.88E-04	8.32E-06
I-134	2.00E-05	ND	3.63E-04	ND
CE-141	9.00E-05	ND	4.24E-05	ND
CE-143	4.00E-05	5.42E-05	ND	ND
CS-134	9.00E-06	3.54E-01	6.46E-01	2.49E-02
CS-136	6.00E-05	3.61E-03	1.59E-03	ND
CS-137	2.00E-05	4.53E-01	8.54E-01	7.51E-02
CS-138	3.00E-06	4.15E-06	1.35E-04	ND
BA-140	2.00E-05	ND	8.62E-05	ND
LA-140	2.00E-05	2.12E-04	1.86E-04	ND
RU-105	1.00E-04	2.21E-04	1.35E-04	ND
RU-106	1.00E-05	ND	1.03E-03	ND
ZN-65	1.00E-04	6.72E-04	ND	ND
Total Ci	Gamma	<b>3.14E+00</b>	<b>2.42E+00</b>	<b>2.16E-01</b>
MPCe	( $\mu\text{Ci/ml}$ )	<b>6.05E-06</b>	<b>1.28E-05</b>	<b>1.28E-05</b>

\* MPC value for unrestricted area from 10 CFR 20, Appendix B, Table II, Column 2.

\*\* ND - not detected

Table A-2: Calculation of Effective MPC - Unit 2

Nuclide	MPC* ( $\mu\text{Ci/ml}$ )	Activity Released (Ci)		
		1993 CURIES	1994 CURIES	1998 CURIES
BE-7	2.00E-03	1.59E-03	2.88E-04	ND
NA-24	3.00E-05	1.05E-03	5.77E-05	7.39E-05
CR-51	2.00E-03	4.39E-03	1.55E-03	1.14E-04
MN-54	1.00E-04	3.73E-02	1.37E-02	7.54E-04
MN-56	1.00E-04	ND	ND	4.66E-05
FE-59	5.00E-05	4.83E-04	3.25E-03	ND
CO-57	4.00E-04	1.17E-02	3.24E-03	ND
CO-58	9.00E-05	1.75E+00	6.60E-01	4.52E-02
CO-60	3.00E-05	3.47E-01	1.03E-01	2.12E-02
ZR-95	6.00E-05	2.34E-03	3.22E-04	ND
NB-95	1.00E-04	3.97E-03	1.11E-03	ND
NB-97	9.00E-04	1.46E-03	1.10E-03	4.22E-05
TC-99M	3.00E-03	3.77E-04	ND	2.35E-06
SR-89	3.00E-06	ND	ND	2.71E-04
SR-92	6.00E-05	ND	1.43E-05	ND
MO-99	4.00E-05	ND	ND	ND
AG-110m	3.00E-05	1.03E-02	1.34E-02	ND
SN-113	8.00E-05	7.45E-05	ND	ND
SB-122	3.00E-05	1.20E-03	ND	6.37E-04
SB-124	2.00E-05	3.77E-02	9.82E-03	1.44E-02
SB-125	1.00E-04	1.35E-01	6.03E-02	1.88E-02
SB-126	3.00E-06	3.51E-04	ND	1.97E-04
I-131	3.00E-07	1.87E-01	7.98E-03	3.14E-03
I-132	8.00E-06	8.72E-05	ND	1.68E-04
I-134	2.00E-05	2.39E-04	1.85E-04	ND
CE-141	9.00E-05	ND	2.87E-05	ND
CE-143	4.00E-05	ND	ND	ND
CS-134	9.00E-06	4.57E-01	6.44E-01	2.64E-02
CS-136	6.00E-05	4.82E-03	1.51E-03	ND
CS-137	2.00E-05	5.70E-01	8.54E-01	7.97E-02
CS-138	3.00E-06	ND	ND	4.90E-05
BA-140	2.00E-05	ND	ND	ND
LA-140	2.00E-05	2.03E-03	1.11E-04	ND
RU-105	1.00E-04	4.07E-05	ND	ND
RU-106	1.00E-05	ND	4.38E-04	ND
ZN-65	1.00E-04	1.59E-04	ND	ND
W-187	6.00E-05	ND	7.98E-05	ND
Total Ci	Gamma	3.57E+00	2.38E+00	2.31E-01
MPCe	( $\mu\text{Ci/ml}$ )	4.81E-06	1.55E-05	1.12E-05

\* MPC value for unrestricted area from 10 CFR 20, Appendix B, Table II, Column 2.

\*\* ND = not detected

**APPENDIX B**

**Technical Basis for Simplified Dose Calculations**

**Liquid Radioactive Effluent**

## APPENDIX B

Technical Basis for Simplified Dose Calculations -  
Liquid Effluent Releases

The radioactive liquid effluents for the years 1993, 1994, and 1998 were evaluated to determine the dose contribution of the radionuclide distribution. These were the most recent years of full power operation for both Units. This analysis was performed to evaluate the use of a limited dose analysis for determining environmental doses, providing a simplified method of determining compliance with the dose limits of Technical Specification (CONTROL) 3.11.1.2.

For the radionuclide distribution of effluents from Salem, the controlling organ is typically the GI-LLI. The calculated GI-LLI dose is predominately a function of the Fe-55, Co-58, Co-60, Fe-59 and Ag-110m releases. The radionuclides, Cs-134 and Cs-137 contribute the large majority of the calculated total body dose. The results of the evaluation for 1993, 1994, and 1998 are presented in Table B-1 and Table B-2.

For purposes of simplifying the details of the dose calculational process, it is conservative to identify a controlling, dose significant radionuclide and limit the calculation process to the use of the dose conversion factor for this nuclide. Multiplication of the total release (i.e., cumulative activity for all radionuclides) by this dose conversion factor provides for a dose calculation method that is simplified while also being conservative.

For the evaluation of the maximum organ dose, it is conservative to use the Nb-95 dose conversion factor (1.51 E+06 mrem/hr per  $\mu\text{Ci/ml}$ , GI-LLI). By this approach, the maximum organ dose will be overestimated since this nuclide has the highest organ dose factor of all the radionuclides evaluated.

For the total body calculation, the Fe-59 dose factor (2.32 E+05 mrem/hr per  $\mu\text{Ci/ml}$ , total body) is the highest among the identified dominant nuclides. For evaluating compliance with the dose limits of Technical Specification (CONTROL) 3.11.1.2, the following simplified equations may be used:

**Total Body**

$$D_{tb} = \frac{1.67E-02 * VOL}{CW} * A_{Fe-59.TB} * \sum_i C_i \quad (\text{B.1})$$

Where:

- $D_{tb}$  = dose to the total body (mrem)
- $A_{Fe-59.TB}$  = 7.27E+04, total body ingestion dose conversion factor for Fe-59 (mrem/hr per  $\mu\text{Ci/ml}$ )
- $VOL$  = volume of liquid effluent released (gal)
- $C_i$  = total concentration of all radionuclides ( $\mu\text{Ci/ml}$ )
- $CW$  = average circulating water discharge rate during release period (gal/min)
- 1.67E-02 = conversion factor (hr/min)

Substituting the value for the Fe-59 total body dose conversion factor, the equation simplifies to:

$$D_{tb} = \frac{1.21E+03 * VOL}{CW} * \sum_i C_i \quad (B.2)$$

**Maximum Organ**

$$D_{max} = \frac{1.67E-02 * VOL}{CW} * A_{Nb-95,GI-LLI} * \sum_i C_i \quad (B.3)$$

Where:

$$D_{max} = \text{maximum organ dose (mrem)}$$

$$A_{Nb-95,GI-LLI} = 1.51E+06, \text{ Gi-LLI ingestion dose conversion factor for Nb-95 (mrem/hr per } \mu\text{Ci/ml)}$$

Substituting the value for  $A_{Nb-95,GI-LLI}$  the equation simplifies to:

$$D_{max} = \frac{2.52E+04 * VOL}{CW} * \sum_i C_i \quad (B.4)$$

Tritium is not included in the limited analysis dose assessment for liquid releases, because the potential dose resulting from normal reactor releases is relatively negligible. The average annual tritium release from each Salem Unit is approximately 350 curies. The calculated total body dose from such a release is  $2.4E-03$  mrem/yr via the fish and invertebrate ingestion pathways. This amounts to 0.08% of the design limit dose of 3 mrem/yr. Furthermore, the release of tritium is a function of operating time and power level and is essentially unrelated to radwaste system operation.

Table B-1: Adult Dose Contributions - Fish and Invertebrate Pathways - Unit 1

Nuclide	Release (Ci)			T.Body Dose Fraction			GI-LLI Dose Fraction			Liver Dose Fraction		
	1994	1993	1998	1994	1993	1998	1994	1993	1998	1994	1993	1998
Mn-54	1.32E-2	3.51E-2	7.16E-4	*	*	*	0.03	0.02	*	*	0.02	*
Fe-55	1.49E-1	6.40E-2	8.39E-2	0.07	0.04	0.37	0.12	0.03	0.52	0.19	0.14	0.67
Fe-59	4.84E-3	4.77E-4	N/D	0.02	*	*	0.12	0.01	*	0.03	0.01	*
Co-58	6.47E-1	1.71E+0	3.39E-2	0.05	0.18	0.02	0.31	0.51	0.13	0.01	0.07	*
Co-60	1.10E-1	3.04E-1	2.42E-2	0.02	0.09	0.05	0.14	0.24	0.24	*	0.03	0.01
Zn-65	N/D	6.72E-4	N/D	*	0.01	*	*	0.01	*	*	0.02	*
Nb-95	1.28E-3	5.78E-3	N/D	*	*	*	*	0.01	*	*	*	*
Ag-110m	1.10E-2	1.19E-2	6.58E-5	*	*	*	0.26	0.17	0.01	*	*	*
Sb-124	1.75E-2	2.58E-2	1.73E-2	*	*	*	*	*	0.04	*	*	*
Sb-125	8.23E-2	9.04E-2	3.56E-2	*	*	*	*	*	0.02	*	*	*
Cs-134	6.46E-1	3.54E-1	2.49E-2	0.47	0.38	0.18	*	*	*	0.38	0.37	0.09
Cs-137	8.54E-1	4.53E-1	7.51E-2	0.37	0.28	0.32	*	*	*	0.37	0.35	0.20
Total	2.53E+0	3.21E+0	3.31E-1									

\* Less than 0.01

N/D = not detected

Table B-2: Adult Dose Contributions - Fish and Invertebrate Pathways - Unit 2

Nuclide	Release (Ci)			T.Body Dose Fraction			GI-LLI Dose Fraction			Liver Dose Fraction		
	1994	1993	1998	1994	1993	1998	1994	1993	1998	1994	1993	1998
Mn-54	1.37E-2	3.73E-2	7.54E-4	*	*	*	0.01	0.02	*	*	0.01	*
Fe-55	1.38E-1	6.61E-2	1.64E-2	0.06	0.04	0.10	0.10	0.03	0.18	0.18	0.12	0.27
Fe-59	3.25E-3	4.82E-4	N/D	0.01	*	*	0.08	0.01	*	0.02	*	*
Co-58	6.60E-1	1.75E+0	4.52E-2	0.05	0.16	0.04	0.29	0.51	0.29	0.01	0.06	0.01
Co-60	1.03E-1	3.47E-1	2.12E-2	0.02	0.09	0.06	0.12	0.27	0.37	0.01	0.03	0.02
Zn-65	N/D	1.59E-4	N/D	*	*	*	*	*	*	*	*	*
Nb-95	1.11E-3	3.97E-3	N/D	*	*	*	0.06	0.01	*	*	*	*
Ag-110m	1.34E-2	1.03E-2	N/D	*	*	*	0.31	0.14	*	*	*	*
Sb-124	9.82E-3	3.77E-2	1.44E-2	*	*	*	*	0.01	0.06	*	*	*
Sb-125	6.03E-2	1.35E-1	1.88E-2	*	*	*	*	0.01	0.02	*	*	*
Cs-134	6.44E-1	4.58E-1	2.64E-2	0.48	0.41	0.26	0.01	*	*	0.39	0.40	0.20
Cs-137	8.54E-1	5.70E-1	7.97E-2	0.37	0.30	0.46	*	*	*	0.38	0.36	0.45
Total	2.48E+0	3.65E+0	2.23E-1									

\* Less than 0.01

N/D = not detected

**APPENDIX C**

**Technical Bases for Effective Dose Factors**

**Gaseous Radioactive Effluent**

APPENDIX C  
 Technical Bases for Effective Dose Factors -  
 Gaseous Radioactive Effluents

**Overview**

The evaluation of doses due to releases of radioactive material to the atmosphere can be simplified by the use of effective dose transfer factors instead of using dose factors which are radionuclide specific.

These effective factors, which can be based on typical radionuclide distributions of releases, can be applied to the total radioactivity released to approximate the dose in the environment (i.e., instead of having to perform individual radionuclide dose analyses only a single multiplication ( $K_{eff}$ ,  $M_{eff}$  or  $N_{eff}$ ) times the total quantity of radioactive material released would be needed).

This approach provides a reasonable estimate of the actual dose while eliminating the need for a detailed calculational technique.

**Determination of Effective Dose Factors**

Effective dose transfer factors are calculated by the following equations:

$$K_{eff} = \sum_i (K_i * f_i) \quad (C.1)$$

Where:

- $K_{eff}$  = the effective total body dose factor due to gamma emissions from all noble gases released
- $K_i$  = the total body dose factor due to gamma emissions from each noble gas radionuclide  $i$  released
- $f_i$  = the fractional abundance of noble gas radionuclide  $i$  relative to the total noble gas activity

$$(L + 1.1 M)_{eff} = \sum_i [(L + 1.1 M)_i * f_i] \quad (C.2)$$

Where:

- $(L + 1.1 M)_{eff}$  = the effective skin dose factor due to beta and gamma emissions from all noble gases released
- $(L + 1.1 M)_i$  = the skin dose factor due to beta and gamma emissions from each noble gas radionuclide  $i$  released

$$M_{eff} = \sum_i (M_i * f_i) \quad (C.3)$$

Where:

- $M_{eff}$  = the effective air dose factor due to gamma emissions from all noble gases released  
 $M_i$  = the air dose factor due to gamma emissions from each noble gas radionuclide  $i$  released

$$N_{eff} = \sum_i (N_i * f_i) \quad (C.4)$$

Where:

- $N_{eff}$  = the effective air dose factor due to beta emissions from all noble gases released  
 $N_i$  = the air dose factor due to beta emissions from each noble gas radionuclide  $i$  released

Normally, it would be expected that past radioactive effluent data would be used for the determination of the effective dose factors. However, the noble gas releases from Salem have been maintained to such negligible quantities that the inherent variability in the data makes any meaningful evaluations difficult.

Therefore, in order to provide a reasonable basis for the derivation of the effective noble gas dose factors, the primary coolant source term from ANSI N237-1976/ANS-18.1, "Source Term Specifications," has been used as representing a typical distribution. The effective dose factors as derived are presented in Table C-1.

### Application

To provide an additional degree of conservatism, a factor of 0.50 is introduced into the dose calculational process when the effective dose transfer factor is used. This conservatism provides additional assurance that the evaluation of doses by the use of a single effective factor will not significantly underestimate any actual doses in the environment.

For evaluating compliance with the dose limits of Technical Specification (CONTROL) 3.11.2.2, the following simplified equations may be used:

$$\bar{D}_\gamma = \frac{3.17E-08}{0.50} * \chi / Q * M_{eff} * \sum_i Q_i \quad (C.5)$$

and

$$D_\beta = \frac{3.17E-08}{0.50} * \chi / Q * N_{eff} * \sum_i Q_i \quad (C.6)$$

Where:

- $D_\gamma$  = air dose due to gamma emissions for the cumulative release of all noble gases (mrad)  
 $D_\beta$  = air dose due to beta emissions for the cumulative release of all noble gases (mrad)  
 $X/Q$  = atmospheric dispersion to the controlling site boundary (sec/m<sup>3</sup>)  
 $M_{\text{eff}}$  = 5.3E+02, effective gamma-air dose factor (mrad/yr per  $\mu\text{Ci}/\text{m}^3$ )  
 $N_{\text{eff}}$  = 1.1E+03, effective beta-air dose factor (mrad/yr per  $\mu\text{Ci}/\text{m}^3$ )  
 $Q_i$  = cumulative release for all noble gas radionuclides ( $\mu\text{Ci}$ )  
 3.17E-08 = conversion factor (yr/sec)  
 0.50 = conservatism factor to account for the variability in the effluent data

Combining the constants, the dose calculational equations simplify to:

$$D_\gamma = 3.5\text{E-}05 * \frac{\lambda}{Q} * \sum_i Q_i \quad (\text{C.7})$$

and

$$D_\beta = 7.0\text{E-}05 * \frac{\lambda}{Q} * \sum_i Q_i \quad (\text{C.8})$$

The effective dose factors are used on a very limited basis for the purpose of facilitating the timely assessment of radioactive effluent releases, particularly during periods of computer malfunction where a detailed dose assessment may be unavailable.

Table C-1: Effective Dose Factors

## Noble Gases - Total Body and Skin

Radionuclide	$f_i^*$	Total Body Effective Dose Factor $K_{eff}$ (mrem/yr per $\mu\text{Ci}/\text{m}^3$ )	Skin Effective Dose Factor (L+ 1.1 M) $_{eff}$ (mrem/yr per $\mu\text{Ci}/\text{m}^3$ )
Kr-85	0.01	--	1.4E+01
Kr-88	0.01	1.5E+02	1.9E+02
Xe-133m	0.01	2.5E+00	1.4E+01
Xe-133	0.95	2.8E+02	6.6E+02
Xe-135	0.02	3.6E+01	7.9E+01
Total		4.7E+02	9.6E+02

## Noble Gases - Air

Radionuclide	$f_i^*$	Gamma Air Effective Dose Factor $M_{eff}$ (mrad/yr per $\mu\text{Ci}/\text{m}^3$ )	Beta Air Effective Dose Factor $N_{eff}$ (mrad/yr per $\mu\text{Ci}/\text{m}^3$ )
Kr-85	0.01	--	2.0E+01
Kr-88	0.01	1.5E+02	2.9E+01
Xe-133m	0.01	3.3E+00	1.5E+01
Xe-133	0.95	3.4E+02	1.0E+03
Xe-135	0.02	3.8E+01	4.9E+01
Total		5.3E+02	1.1E+03

\* Based on Noble gas distribution from ANSI N237-1976/ANSI-18.1, "Source Term Specifications."

**APPENDIX D**

**Technical Basis for Simplified Dose Calculation**

**Gaseous Radioactive Effluent**

## APPENDIX D

**Technical Basis for Simplified Dose Calculation  
Gaseous Radioactive Effluent Releases**

The pathway dose factors for the controlling infant age group were evaluated to determine the controlling pathway, organ and radionuclide. This analysis was performed to provide a simplified method for determining compliance with Technical Specification (CONTROL) 3.11.2.3

For the infant age group, the controlling pathway is the grass-cow-milk (g/c/m) pathway. An infant receives a greater radiation dose from the g/c/m pathway than any other pathway. Of this g/c/m pathway, the maximum exposed organ including the total body, is the thyroid, and the highest dose contributor is radionuclide I-131. The results for this evaluation are presented in Table D-1.

For purposes of simplifying the details of the dose calculation process, it is conservative to identify a controlling, dose significant organ and radionuclide and limit the calculation process to the use of the dose conversion factor for the organ and radionuclide. Multiplication of the total release (i.e. cumulative activity for all radionuclides) by this dose conversion factor provides for a dose calculation method that is simplified while also being conservative.

For the evaluation of the dose commitment via a controlling pathway and age group, it is conservative to use the infant, g/c/m, thyroid, I-131 pathway dose factor (1.05E12 m<sup>2</sup> mrem/yr per μCi/sec). By this approach, the maximum dose commitment will be overestimated since I-131 has the highest pathway dose factor of all radionuclides evaluated.

For evaluating compliance with the dose limits of Technical Specification (CONTROL) 3.11.2.3, the following simplified equation may be used:

$$D_{\max} = 3.17E-08 * W * R_{I-131} * \sum_i Q_i$$

Where:

- $D_{\max}$  = maximum organ dose (mrem)
- $W$  = atmospheric dispersion parameters to the controlling location(s) as identified in Table 3.2-4.
- $X/Q$  = atmospheric dispersion for inhalation pathway and H-3 dose contribution via other pathways (sec/m<sup>3</sup>)
- $D/Q$  = atmospheric deposition for vegetation, milk and ground plane exposure pathways (m<sup>-2</sup>)
- $Q_i$  = cumulative release over the period of interest for radioiodines and particulates
- 3.17E-8 = conversion factor (yr/sec)
- $R_{I-131}$  = I-131 dose parameter for the thyroid for the identified controlling pathway  
= 1.05E+12 (m<sup>2</sup> mrem/yr per μCi/sec), infant thyroid dose parameter with the grass-cow-milk pathway controlling

The ground plane exposure and inhalation pathways need not be considered when the above simplified calculation method is used because of the overall negligible contribution of these pathways to the total thyroid dose.

It is recognized that for some particulate radionuclides (e.g., Co-60 and Cs-137), the ground exposure pathway may represent a higher dose contribution than either the vegetation or milk pathway. However, use of the I-131 thyroid dose parameter for all radionuclides will maximize the organ dose calculation, especially considering that no other radionuclide has a higher dose parameter for any organ via any pathway than I-131 for the thyroid via the milk pathway (see Table D-1).

The dose should be evaluated based on the predetermined controlling pathways as identified in Table 2-4. If more limiting pathways in the surrounding environment of Salem are identified by the annual land use census, Table 2-4 will be revised as specified in Technical Specification (CONTROL) 3.12.2.

Table D-1: Infant Dose Contributions  
 Fraction of Total Organ and Body Dose

PATHWAYS

<u>Target Organs</u>	<u>Grass-Cow-Milk</u>	<u>Ground Plane</u>
Total Body	0.02	0.15
Liver	0.23	0.14
Thyroid	0.59	0.15
Kidney	0.02	0.15
Lung	0.01	0.02
GI-LLI	0.02	0.15

Fraction of Dose Contribution by Pathway

<u>Pathway</u>	<u>f</u>
Grass-Cow-Milk	0.92
Ground Plane	0.08
Inhalation	N/A

**APPENDIX E**

**Radiological Environmental Monitoring Program**

**Sample Type, Location and Analysis**

## APPENDIX E

## SAMPLE DESIGNATION

Samples are identified by a three part code. The first two letters are the power station identification code, in this case "SA". The next three letters are for the media sampled.

AIO = Air Iodine	IDM = Immersion Dose (TLD)
APT = Air Particulates	MLK = Milk
ECH = Hard Shell Blue Crab	PWR = Potable Water (Raw)
ESF = Edible Fish	PWT = Potable Water (Treated)
ESS = Sediment	
SWA = Surface Water	
WWA = Well Water	

The last four symbols are a location code based on direction and distance from the site. Of these, the first two represent each of the sixteen angular sectors of 22.5 degrees centered about the reactor site. Sector one is divided evenly by the north axis and other sectors are numbered in a clockwise direction; i.e., 2=NNE, 3=NE, 4=ENG, etc. The next digit is a letter which represents the radial distance from the plant:

S = On-site location	E = 4-5 miles off-site
A = 0-1 miles off-site	F = 5-10 miles off-site
B = 1-2 miles off-site	G = 10-20 miles off-site
C = 2-3 miles off-site	H = > 20 miles off-site
D = 3-4 miles off-site	

The last number is the station numerical designation within each sector and zone; e.g., 1,2,3,... For example; the designation SA-WWA-5D1 would indicate a sample in the SGS and HCGS program (SA), consisting of well water (WWA), which had been collected in sector number 5, centered at 90° (due east) with respect to the reactor site at a radial distance of 3 to 4 miles off-site, (therefore, radial distance D). The number 1 indicated that this is sampling station #1 in that particular sector.

## SAMPLING LOCATIONS

All sampling locations and specific information about the individual locations are given in Table E-1. Maps E-1 and E-2 show the locations of sampling stations with respect to the site.

**TABLE E-1**

**A. Direct Radiation Monitoring Locations (IDM)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
1S1	0.55 mi. N of vent
2S2	0.4 mi. NNE of vent
2S4	0.59 mi. NNE of vent
3S1	0.58 mi. NE of vent
4S1	0.60 mi ENE of vent
5S1	1.0 mi. E of vent; site access road
6S2	0.21 mi. ESE of vent; observation building
** 7S1	0.12 mi. SE of vent; station personnel gate
**10S1	0.14 mi. SSW of vent; circ water bldg.
**11S1	0.09 mi. SW of vent; service water bldg.
15S1	0.57 mi. NW of vent
16S1	0.54 mi. NNW of vent
4D2	3.7 mi. ENE of vent; Alloway Creek Neck Road
5D1	3.5 mi. E of vent; local farm
10D1	3.9 mi. SSW of vent; Taylor's Bridge Spur
14D1	3.4 mi. WNW of vent; Bay View, Delaware
15D1	3.8 mi. NW of vent; Rt 9, Augustine Beach, DE.
2E1	4.4 mi. NNE of vent; local farm
3E1	4.1 mi. NE of vent; local farm
9E1	4.2 mi. S of vent
11E2	5.0 mi. SW of vent
12E1	4.4 mi. WSW of vent; Thomas Landing
13E1	4.2 mi. W of vent; Diehl House Lab
16E1	4.1 mi. NNW of vent; Port Penn
1F1	5.8 mi. N of vent; Fort Elfsborg
2F2	8.7 mi. NNE of vent; Salem Substation
2F5	7.4 mi. NNE of vent; Salem High School
2F6	7.3 mi. NNE of vent; PSE&G Training Center
3F2	5.1 mi. NE of vent; Hancocks Bridge Munc Bldg
3F3	8.6 mi. NE of vent; Quinton Township School
4F2	6.0 mi. ENE of vent; Mays Lane, Harmersville
5F1	6.5 mi. E of vent; Canton

**TABLE E-1 (Cont'd)****A. Direct Radiation Monitoring Locations (IDM) (Cont'd)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
6F1	6.4 mi. ESE of vent; Stow Neck Road
7F2	9.1 mi. SE of vent; Bayside, NJ
10F2	5.8 mi. SSW of vent; Rt. 9
11F1	6.2 mi. SW of vent; Taylors Bridge, DE
12F1	9.4 mi. WSW of vent; Townsend Elementary School
13F2	6.5 mi. W of vent; Odessa, DE
13F3	9.3 mi. W of vent; Redding Middle School
13F4	9.8 mi. W of vent; Middletown, DE
14F2	6.6 mi. WNW of vent; Boyds Corner
15F3	5.4 mi. NW of vent
16F2	8.1 mi. NNW of vent; Delaware City Public School
1G3	19 mi. N of vent; N. Church St. Wilmington, DE
3G1	17 mi. NE of vent; local farm
10G1	12 mi. SSW of vent; Smyrna, Delaware
14G1	11.8 mi. WNW of Vent; Rte 286, Bethel Church Rd., DE
16G1	15 mi. NNW of vent; Wilmington Airport
3H1	32 mi. NE of vent; National Park, NJ

\*\* TLD locations will be maintained by site area monitoring program

**B. Air Sampling Locations (AIO,APT)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
5S1	1.0 mi. E of vent; site access road
5D1	3.5 mi. E of vent; local farm
16E1	4.1 mi. NNW of vent; Port Penn
1F1	5.8 mi. N of vent; Fort Elfsborg
2F6	7.3 mi. NNE of vent; PSE&G Training Center
14G1	11.8 mi. WNW of Vent; Rte 286, Bethel Church Rd., DE

**Table E-1 (Cont'd)****C. Surface Water Locations (SWA) - Delaware River**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
11A1	0.2 mi. SW of vent; Salem Outfall Area
12C1	2.5 mi. WSW of vent; West bank of Delaware River
7E1	4.5 mi. SE of vent; Delaware River
16F1	6.9 mi. NNW of vent; C&D Canal

**D. Ground Water Locations (WWA)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
---------------------	-------------------------

No groundwater samples are taken as this pathway is not directly affected by liquid effluents discharged from Salem Generating Station.

**E. Drinking Water Locations (PWR,PWT)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
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No public drinking water samples or irrigation water samples are taken as these pathways are not directly affected by liquid effluents discharged from Salem Generating Station.

**F. Water Sediment Locations (ESS)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
11A1	0.2 mi. SW of vent; Salem outfall area
15A1	0.3 mi. NW of vent; Hope Creek outfall area
16A1	0.7 mi. NNW of vent; South Storm Drain outfall
12C1	2.5 mi. WSW of vent; West bank of Delaware river
7E1	4.5 mi. SE of vent; 1 mi West of Mad Horse River
16F1	6.9 mi. NNW of vent; C&D Canal
6S2	0.2 mi. ESE of vent; observation building

**G. Milk Sampling Locations (MLK)**

<u>STATION CODE</u>	<u>STATION LOCATION</u>
2F9	7.5 mi. NNE of vent; local farm
11F3	5.3 mi. SW of vent; Townsend DE
14F4	7.6 mi. WNW of vent; local farm
3G1	17 mi. NE of vent; local farm

**Table E-1 (Cont'd)**

## H. Fish and Invertebrate Locations (ESF,ECH)

<u>STATION CODE</u>	<u>STATION LOCATION</u>
11A1	0.2 mi. SW of vent; Salem outfall area
12C1	2.5 mi. WSW of vent; West bank of Delaware River
7E1	4.5 mi. SE of vent; 1 mi West of Mad Horse Creek

## I. Food Product Locations

<u>STATION CODE</u>	<u>STATION LOCATION</u>
---------------------	-------------------------

The Delaware River at the location of Salem and Hope Creek Nuclear Power Plants is a brackish water source. No irrigation of food products is performed using water in the vicinity from which liquid plant wastes have been discharged.

## SAMPLES COLLECTION AND ANALYSIS

<u>Sample</u>	<u>Collection Method</u>	<u>Analysis</u>
Air Particulate	Continuous low volume air sampler. Sample collected every week along with the filter change.	Gross Beta analysis on each weekly sample. Gamma spectrometry shall be performed if gross beta exceeds 10 times the yearly mean of the control station value. Samples shall be analyzed 24 hrs or more after collection to allow for radon and thorium daughter decay. Gamma isotopic analysis on quarterly composites.
Air Iodine	A TEDA impregnated charcoal cartridge is connected to air particulate air sampler and is collected weekly at filter change.	Iodine 131 analysis are performed on each weekly sample.
Crab and Fish	Two batch samples are sealed in a plastic bag or jar and frozen semi-annually or when in season.	Gamma isotopic analysis of edible portion on collection.
Sediment	A sediment sample is taken semi-annually.	Gamma isotopic analysis semi-annually.
Direct	2 TLD's will be collected from each location quarterly.	Gamma dose quarterly.

## SAMPLE COLLECTION AND ANALYSIS (Cont'd)

<u>Sample</u>	<u>Collection Method</u>	<u>Analysis</u>
Milk	Sample of fresh milk is collected for each farm semi-monthly when cows are in pasture, monthly at other times.	Gamma isotopic analysis and I-131 analysis on each sample on collection.
Water (Potable, Surface)	Sample to be collected monthly providing winter icing conditions allow.	Gamma isotopic monthly H-3 on quarterly surface sample, monthly on ground water sample.

Figure E-1

ONSITE SAMPLING LOCATIONS

ON-SITE SAMPLING LOCATIONS

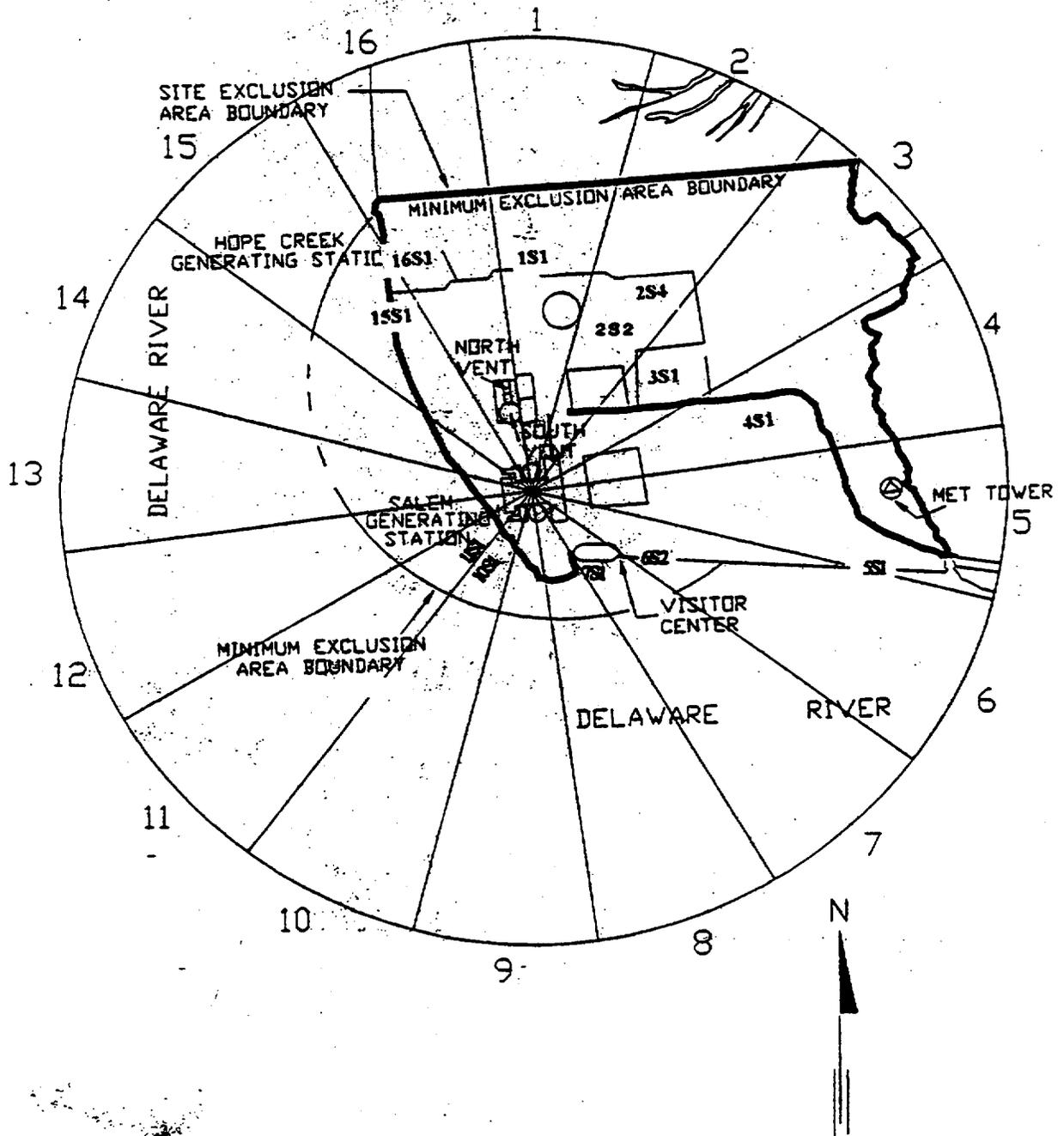
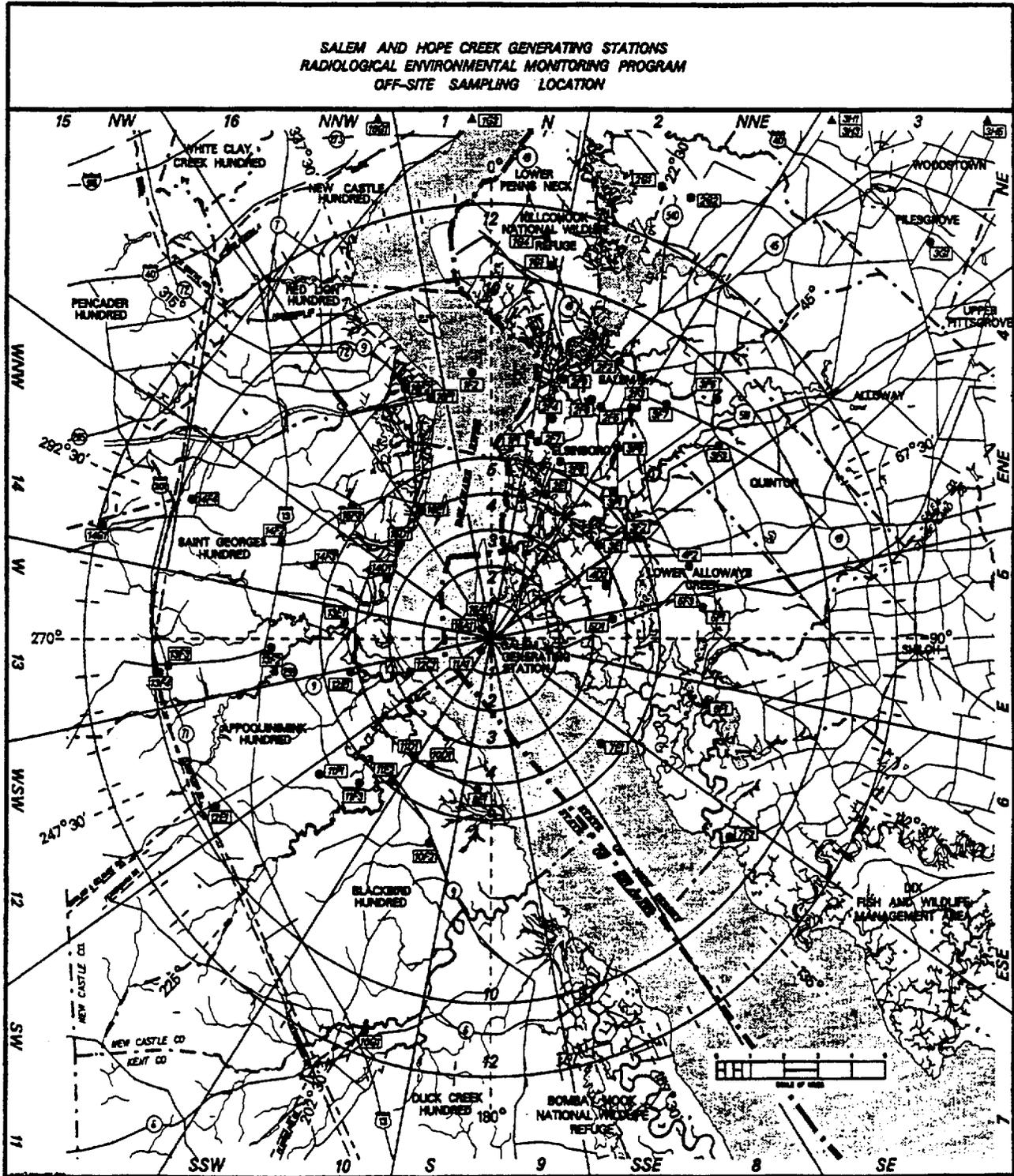


Figure E-2

OFF-SITE SAMPLING LOCATIONS



**APPENDIX F**  
**MAXIMUM PERMISSIBLE CONCENTRATIONS**  
**LIQUID EFFLUENTS**

The following radionuclide concentrations were obtained from 10 CFR 20 Appendix B, Table II, Column 2 as revised January 1, 1991.

### Maximum Permissible Concentrations

Element	Isotope	Soluble Conc ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Actinium (89)	Ac-227	2E-6	3E-4
	Ac-228	9E-5	9E-5
Americium (95)	Am-241	4E-6	3E-5
	Am-242m	4E-6	9E-5
	Am-242	1E-4	1E-4
	Am-243	4E-6	3E-5
	Am-244	5E-3	5E-3
Antimony (51)	Sb-122	3E-5	3E-5
	Sb-124	2E-5	2E-5
	Sb-125	1E-4	1E-4
Arsenic (33)	As-73	5E-4	5E-4
	As-74	5E-5	5E-5
	As-76	2E-5	2E-5
	As-77	8E-5	8E-5
Astatine (85)	At-211	2E-6	7E-5
Barium (56)	Ba-131	2E-4	2E-4
	Ba-140	3E-5	2E-5
Berkelium (97)	Bk-249	6E-4	6E-4
	Bk-250	2E-4	2E-4
Beryllium (4)	Be-7	2E-3	2E-3
Bismuth (83)	Bi-206	4E-5	4E-5
	Bi-207	6E-5	6E-5
	Bi-210	4E-5	4E-5
	Bi-212	4E-4	4E-4
Bromine (35)	Br-82	3E-4	4E-5
Cadmium (48)	Cd-109	2E-4	2E-4
	Cd-115m	3E-5	3E-5
	Cd-115	3E-5	4E-5
Calcium (20)	Ca-45	9E-6	2E-4
	Ca-47	5E-5	3E-5
Californium (98) -	Cf-249	4E-6	2E-5
	Cf-250	1E-5	3E-5
	Cf-251	4E-6	3E-5
	Cf-252	7E-6	7E-6
	Cf-253	1E-4	1E-4
	Cf-254	1E-7	1E-7

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Carbon (6)	C-14	8E-4	-----
Cerium (58)	Ce-141	9E-5	9E-5
	Ce-143	4E-5	4E-5
	Ce-144	1E-5	1E-5
Cesium (55)	Cs-131	2E-3	9E-4
	Cs-134m	6E-3	1E-3
	Cs-134	9E-6	4E-5
	Cs-135	1E-4	2E-4
	Cs-136	9E-5	6E-5
	Cs-137	2E-5	4E-5
Chlorine (17)	Cl-36	8E-5	6E-5
	Cl-38	4E-4	4E-4
Chromium (24)	Cr-51	2E-3	2E-3
Cobalt (27)	Co-57	5E-4	4E-4
	Co-58m	3E-3	2E-3
	Co-58	1E-4	9E-5
	Co-60	5E-5	3E-5
Copper (29)	Cu-64	3E-4	2E-4
Curium (96)	Cm-242	2E-5	2E-5
	Cm-243	5E-6	2E-5
	Cm-244	7E-6	3E-5
	Cm-245	4E-6	3E-5
	Cm-246	4E-6	3E-5
	Cm-247	4E-6	2E-5
	Cm-248	4E-7	1E-6
	Cm-249	2E-3	2E-3
Dysprosium (66)	Dy-165	4E-4	4E-4
	Dy-166	4E-5	4E-5
Einsteinium (99)	Es-253	2E-5	2E-5
	Es-254m	2E-5	2E-5
	Es-254	1E-5	1E-5
	Es-255	3E-5	3E-5
Erbium (68)	Er-169	9E-5	9E-5
	Er-171	1E-4	1E-4
Europium (63)	Eu-152 (9.2 hrs)	6E-5	6E-5
	Eu-152 (13 yrs)	8E-5	8E-5
	Eu-154	2E-5	2E-5
	Eu-155	2E-4	2E-4
Fermium (100)	Fm-254	1E-4	1E-4
	Fm-255	3E-5	3E-5
	Fm-256	9E-7	9E-7

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Fluorine (9)	F-18	8E-4	5E-4
Gadolinium (64)	Gd-153	2E-4	2E-4
	Gd-159	8E-5	8E-5
Gallium (31)	Ga-72	4E-5	4E-5
Germanium (32)	Ge-71	2E-3	2E-3
Gold (79)	Au-196	2E-4	1E-4
	Au-198	5E-5	5E-5
	Au-199	2E-4	2E-4
Hafnium (72)	Hf-181	7E-5	7E-5
Holmium (67)	Ho-166	3E-5	3E-5
Hydrogen (3)	H-3	3E-3	3E-3
Indium (49)	In-113m	1E-3	1E-3
	In-114m	2E-5	2E-5
	In-115m	4E-4	4E-4
	In-115	9E-5	9E-5
Iodine (53)	I-125	2E-7	2E-4
	I-126	3E-7	9E-5
	I-129	6E-8	2E-4
	I-131	3E-7	6E-5
	I-132	8E-6	2E-4
	I-133	1E-6	4E-5
	I-134	2E-5	6E-4
	I-135	4E-6	7E-5
Iridium (77)	Ir-190	2E-4	2E-4
	Ir-192	4E-5	4E-5
	Ir-194	3E-5	3E-5
Iron (26)	Fe-55	8E-4	2E-3
	Fe-59	6E-5	5E-5
Lanthanum (57)	La-140	2E-5	2E-5
Lead (82)	Pb-203	4E-4	4E-4
	Pb-210	1E-7	2E-4
	Pb-212	2E-5	2E-5
Lutetium (71)	Lu-177	1E-4	1E-4
Manganese (25)	Mn-52	3E-5	3E-5
	Mn-54	1E-4	1E-4
	Mn-56	1E-4	1E-4
Mercury (80)	Hg-197m	2E-4	2E-4
	Hg-197	3E-4	5E-4
	Hg-203	2E-5	1E-4
Molybdenum (42)	Mo-99	2E-4	4E-5

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Neodymium (60)	Nd-144	7E-5	8E-5
	Nd-147	6E-5	6E-5
	Nd-149	3E-4	3E-4
Neptunium (93)	Np-237	3E-6	3E-5
	Np-239	1E-4	1E-4
Nickel (28)	Ni-59	2E-4	2E-3
	Ni-63	3E-5	7E-4
	Ni-65	1E-4	1E-4
Niobium (41)	Nb-93m	4E-4	4E-4
	Nb-95	1E-4	1E-4
	Nb-97	9E-4	9E-4
Osmium (76)	Os-185	7E-5	7E-5
	Os-191m	3E-3	2E-3
	Os-191	2E-4	2E-4
	Os-193	6E-5	5E-5
Palladium (46)	Pd-103	3E-4	3E-4
	Pd-109	9E-5	7E-5
Phosphorus (15)	P-32	2E-5	2E-5
Platinum (78)	Pt-191	1E-4	1E-4
	Pt-193m	1E-3	1E-3
	Pt-193	9E-4	2E-3
	Pt-197m	1E-3	9E-4
	Pt-197	1E-4	1E-4
Plutonium (94)	Pu-238	5E-6	3E-5
	Pu-239	5E-6	3E-5
	Pu-240	5E-6	3E-5
	Pu-241	2E-4	1E-3
	Pu-242	5E-6	3E-5
	Pu-243	3E-4	3E-4
Polonium (84)	Po-210	7E-7	3E-5
Potassium (19)	K-42	3E-4	2E-5
Praseodymium(59)	Pr-142	3E-5	3E-5
	Pr-143	5E-5	5E-5
Promethium (61)	Pm-147	2E-4	2E-4
	Pm-149	4E-5	4E-5
Protactinium(91)	Pa-230	2E-4	2E-4
	Pa-231	9E-7	2E-5
	Pa-233	1E-4	1E-4
Radium (88)	Ra-223	7E-7	4E-6
	Ra-224	2E-6	5E-6
	Ra-226	3E-8	3E-5

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
	Ra-228	3E-8	3E-5
Rhenium (75)	Re-183	6E-4	3E-4
	Re-186	9E-5	5E-5
	Re-187	3E-3	2E-3
	Re-188	6E-5	3E-5
Rhodium (45)	Rh-103m	1E-2	1E-2
	Rh-105	1E-4	1E-4
Rubidium (37)	Rb-86	7E-5	2E-5
	Rb-87	1E-4	2E-4
Ruthenium (44)	Ru-97	4E-4	3E-4
	Ru-103	8E-5	8E-5
	Ru-105	1E-4	1E-4
	Ru-106	1E-5	1E-5
Samarium (62)	Sm-147	6E-5	7E-5
	Sm-151	4E-4	4E-4
	Sm-153	8E-5	8E-5
Scandium (21)	Sc-46	4E-5	4E-5
	Sc-47	9E-5	9E-5
	Sc-48	3E-5	3E-5
Selenium (34)	Se-75	3E-4	3E-4
Silicon (14)	Si-31	9E-4	2E-4
Silver (47)	Ag-105	1E-4	1E-4
	Ag-110m	3E-5	3E-5
	Ag-111	4E-5	4E-5
Sodium (11)	Na-22	4E-5	3E-5
	Na-24	2E-4	3E-5
Strontium (38)	Sr-85m	7E-3	7E-3
	Sr-85	1E-4	2E-4
	Sr-89	3E-6	3E-5
	Sr-90	3E-7	4E-5
	Sr-91	7E-5	5E-5
	Sr-92	7E-5	6E-5
Sulfur (16)	S-35	6E-5	3E-4
Tantalum (73)	Ta-182	4E-5	4E-5
Technetium (43)	Tc-96m	1E-2	1E-2
	Tc-96	1E-4	5E-5
	Tc-97m	4E-4	2E-4
	Tc-97	2E-3	8E-4
	Tc-99m	6E-3	3E-3
	Tc-99	3E-4	2E-4

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Tellurium (52)	Te-125m	2E-4	1E-4
	Te-127m	6E-5	5E-5
	Te-127	3E-4	2E-4
	Te-129m	3E-5	2E-5
	Te-129	8E-4	8E-4
	Te-131m	6E-5	4E-5
	Te-132	3E-5	2E-5
Terbium (65)	Tb-160	4E-5	4E-5
Thallium (81)	Tl-200	4E-4	2E-4
	Tl-201	3E-4	2E-4
	Tl-202	1E-4	7E-5
	Tl-204	1E-4	6E-5
Thorium (90)	Th-227	2E-5	2E-5
	Th-228	7E-6	1E-5
	Th-230	2E-6	3E-5
	Th-231	2E-4	2E-4
	Th-232	2E-6	4E-5
	Th-natural	2E-6	2E-5
	Th-234	2E-5	2E-5
Thulium (69)	Tm-170	5E-5	5E-5
	Tm-171	5E-4	5E-4
Tin (50)	Sn-113	9E-5	8E-5
	Sn-124	2E-5	2E-5
Tungsten (74)	W-181	4E-4	3E-4
	W-185	1E-4	1E-4
	W-187	7E-5	6E-5
Uranium (92)	U-230	5E-6	5E-6
	U-232	3E-5	3E-5
	U-233	3E-5	3E-5
	U-234	3E-5	3E-5
	U-235	3E-5	3E-5
	U-236	3E-5	3E-5
	U-238	4E-5	4E-5
	U-240	3E-5	3E-5
-	U-natural	3E-5	3E-5
Vanadium (23)	V-48	3E-5	3E-5
Ytterbium (70)	Yb-175	1E-4	1E-4

Element	Isotope	Soluble Conc. ( $\mu\text{Ci/ml}$ )	Insoluble Conc. ( $\mu\text{Ci/ml}$ )
Yttrium	Y-90	2E-5	2E-5
	Y-91m	3E-3	3E-3
	Y-91	3E-5	3E-5
	Y-92	6E-5	6E-5
	Y-93	3E-5	3E-5
Zinc (30)	Zn-65	1E-4	2E-4
	Zn-69m	7E-5	6E-5
	Zn-69	2E-3	2E-3
Zirconium (40)	Zr-93	8E-4	8E-4
	Zr-95	6E-5	6E-5
	Zr-97	2E-5	2E-5
Any single radionuclide not listed above with decay mode other than alpha emission or spontaneous fission and with radioactive half-life greater than 2 hours		3E-6	3E-6
Any single radionuclide not listed above, which decays by alpha emission or spontaneous fission.		3E-8	3E-8

## Notes:

1. If the identity of any radionuclide is not known, the limiting values for purposes of this table shall be: 3E-8  $\mu\text{Ci/ml}$ .
2. If the identity and concentration of each radionuclide are known, the limiting values should be derived as follows: Determine, for each radionuclide in the mixture, the ratio between the quantity present in the mixture and the limit otherwise established in Appendix B for the specific radionuclide not in a mixture. The sum of such ratios for all the radionuclides in the mixture may not exceed "1" (i.e. "unity").