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W3F1-2000-0023 A4.05 PR

February 28, 2000

U.S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington, D.C. 20555

Subject: Waterford 3 SES Docket No. 50-382 License No. NPF-38 Change to the Technical Specifications Bases

Gentlemen:

Entergy is hereby requesting the attached change to the Waterford 3 Technical Specifications Bases be issued. This change has been evaluated pursuant to 10CFR50.59 and has been determined to not involve an unreviewed safety question. This change has been reviewed and approved by the Plant Operations Review Committee. The proposed change affects the following TS Bases:

Bases 2.2.1 Page B 2-6

This Bases change provides the value for Integrated Radial Peaking Factor -High currently installed in the plant for Cycle 10.

Please issue the attached Bases page. Should you have any questions or comments concerning this request, please contact Edward Lemke at (504) 739-6349. This letter does not contain commitments.

Very truly yours,

Evenin P. Rucins &

E.P. Perkins Director. Nuclear Safety Assurance

EPP/ELL/rtk Attachment:

TS Bases Before and After Pages

Change to the Technical Specifications Bases W3F1-2000-0023 Page 2 February 28, 2000

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cc: E.W. Merschoff, NRC Region IV N. Kalyanam, NRC-NRR J. Smith N.S. Reynolds NRC Resident Inspectors Office

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ATTACHMENT

TS Bases Before and After Pages

EXISTING

DNBR - Low (Continued)

in actual core DNBR after the trip will not result in a violation of the DNBR Safety Limit of 1.26. CPC uncertainties related to DNBR cover CPC input measurement uncertainties, algorithm modelling uncertainties, and computer equipment processing uncertainties. Dynamic compensation is provided in the CPC calculations for the effects of coolant transport delays, core heat flux delays (relative to changes in core power), sensor time delays, and protection system equipment time delays.

The DNBR algorithm used in the CPC is valid only within the limits indicated below and operation outside of these limits will result in a CPC initiated trip.

a.	RCS Cold Leg Temperature-Low	> 495°F
b.	RCS Cold Leg Temperature-High	₹ 580°F
c.	Axial Shape Index-Positive	Not more positive than +0.5
d.	Axial Shape Index-Negative	Not more negative than -0.5
e.	Pressurizer Pressure-Low	> 1860 psia
f.	Pressurizer Pressure-High	< 2375 psia
g.	Integrated Radial Peaking	
-	Factor-Low	> 1.28
h.	Integrated Radial Peaking	
	Factor-High	< 4.28
i .	Quality Margin-Low	≥ 0

Steam Generator Level - High

The Steam Generator Level - High trip is provided to protect the turbine from excessive moisture carry over. Since the turbine is automatically tripped when the reactor is tripped, this trip provides a reliable means for providing protection to the turbine from excessive moisture carry over. This trip's setpoint does not correspond to a Safety Limit and no credit was taken in the safety analyses for operation of this trip. Its functional capability at the specified trip setting is required to enhance the overall reliability of the Reactor Protection System.

Reactor Coolant Flow - Low

The Reactor Coolant Flow - Low trip provides protection against a reactor coolant pump sheared shaft event and a steam line break event with a loss-ofoffsite power. A trip is initiated when the pressure differential across the primary side of either steam generator decreases below a nominal setpoint of 23.8 psid. The specified setpoint ensures that a reactor trip occurs to prevent violation of local power density or DNBR safety limits under the stated conditions.



BASES

PROPOSED

BASES

DNBR - Low (Continued)

in actual core DNBR after the trip will not result in a violation of the DNBR Safety Limit of 1.26. CPC uncertainties related to DNBR cover CPC input measurement uncertainties, algorithm modelling uncertainties, and computer equipment processing uncertainties. Dynamic compensation is provided in the CPC calculations for the effects of coolant transport delays, core heat flux delays (relative to changes in core power), sensor time delays, and protection system equipment time delays.

The DNBR algorithm used in the CPC is valid only within the limits indicated below and operation outside of these limits will result in a CPC initiated trip.

RCS Cold Leg Temperature-Low RCS Cold Leg Temperature-High Axial Shape Index-Positive Axial Shape Index-Negative Pressurizer Pressure-Low	> 495°F < 580°F Not more positive than Not more negative than > 1860 psia
Pressurizer Pressure-High	₹ 2375 psia
Integrated Radial Peaking Factor-Low	> 1.28
Integrated Radial Peaking	— 1 — 1
Factor-High Quality Margin-Low	< 4.28 7,00 > 0
	RCS Cold Leg Temperature-High Axial Shape Index-Positive Axial Shape Index-Negative Pressurizer Pressure-Low Pressurizer Pressure-High Integrated Radial Peaking Factor-Low Integrated Radial Peaking Factor-High

Steam Generator Level - High

The Steam Generator Level - High trip is provided to protect the turbine from excessive moisture carry over. Since the turbine is automatically tripped when the reactor is tripped, this trip provides a reliable means for providing protection to the turbine from excessive moisture carry over. This trip's setpoint does not correspond to a Safety Limit and no credit was taken in the safety analyses for operation of this trip. Its functional capability at the specified trip setting is required to enhance the overall reliability of the Reactor Protection System.

Reactor Coolant Flow - Low

The Reactor Coolant Flow - Low trip provides protection against a reactor coolant pump sheared shaft event and a steam line break event with a loss-ofoffsite power. A trip is initiated when the pressure differential across the primary side of either steam generator decreases below a nominal setpoint of 23.8 psid. The specified setpoint ensures that a reactor trip occurs to prevent violation of local power density or DNBR safety limits under the stated conditions.

PROPOSED

+0.5