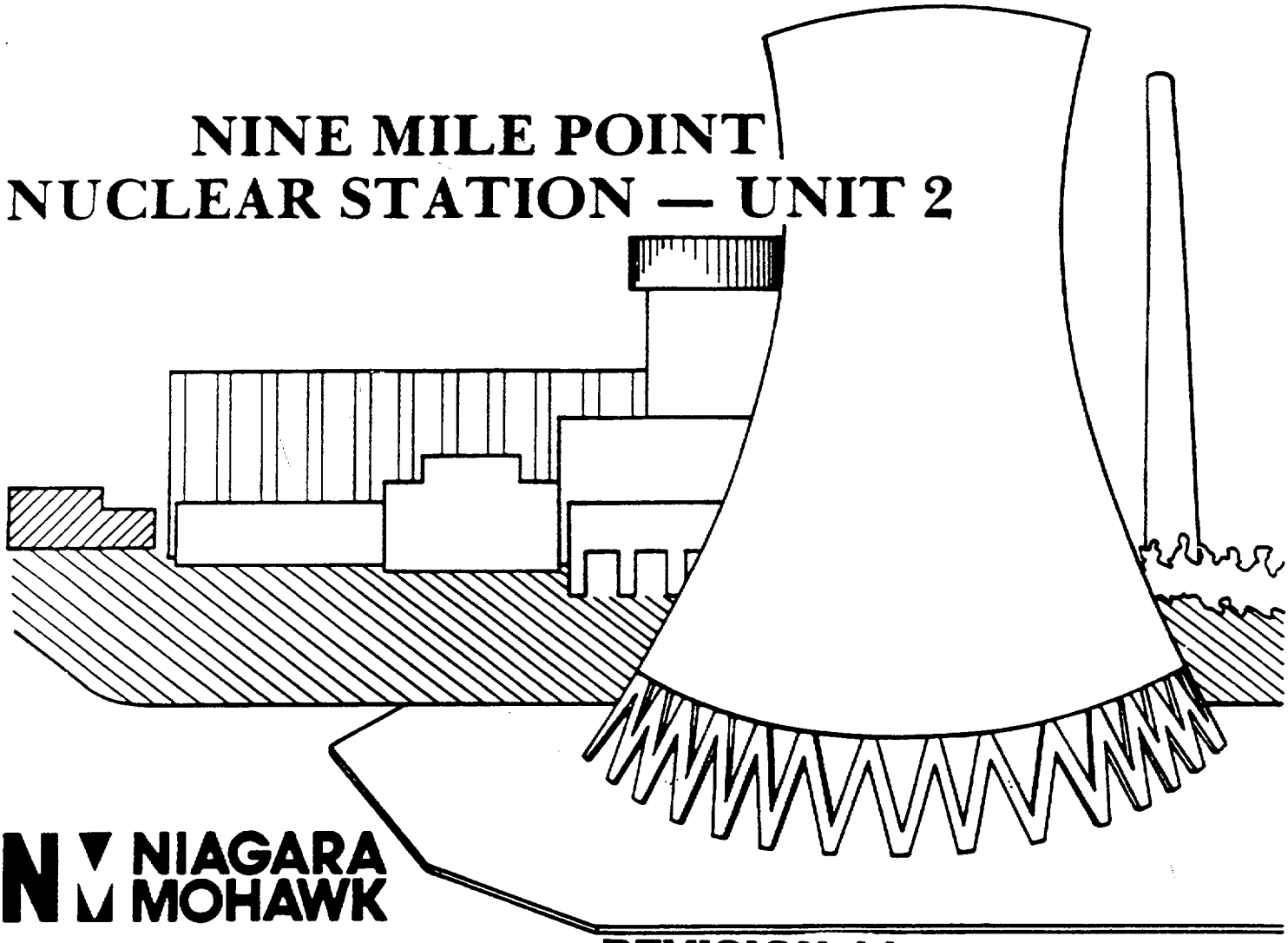
UPDATED SAFETY ANALYSIS REPORT

NINE MILE POINT NUCLEAR STATION — UNIT 2



NIAGARA MOHAWK

REVISION 11

A053 0/11

INSERTION INSTRUCTIONS

The following instructions are for the insertion of the current revision into the Nine Mile Point Unit 2 USAR.

Remove pages, tables, and/or figures listed in the REMOVE column and replace them with the pages, tables, and/or figures listed in the INSERT column. Dashes (---) in either column indicate no action required.

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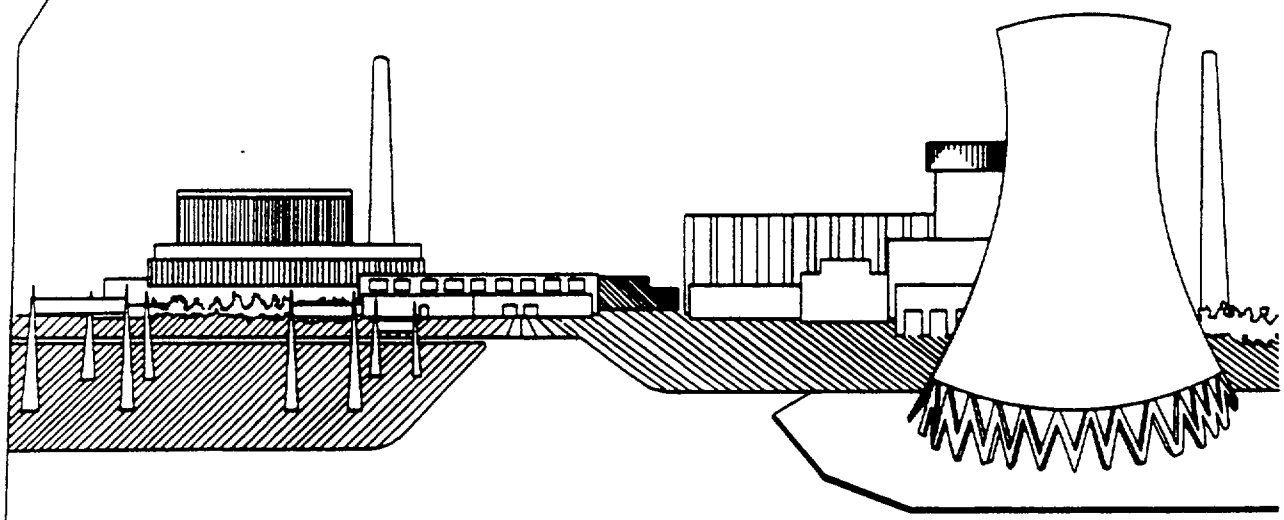

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UPDATED SAFETY ANALYSIS REPORT

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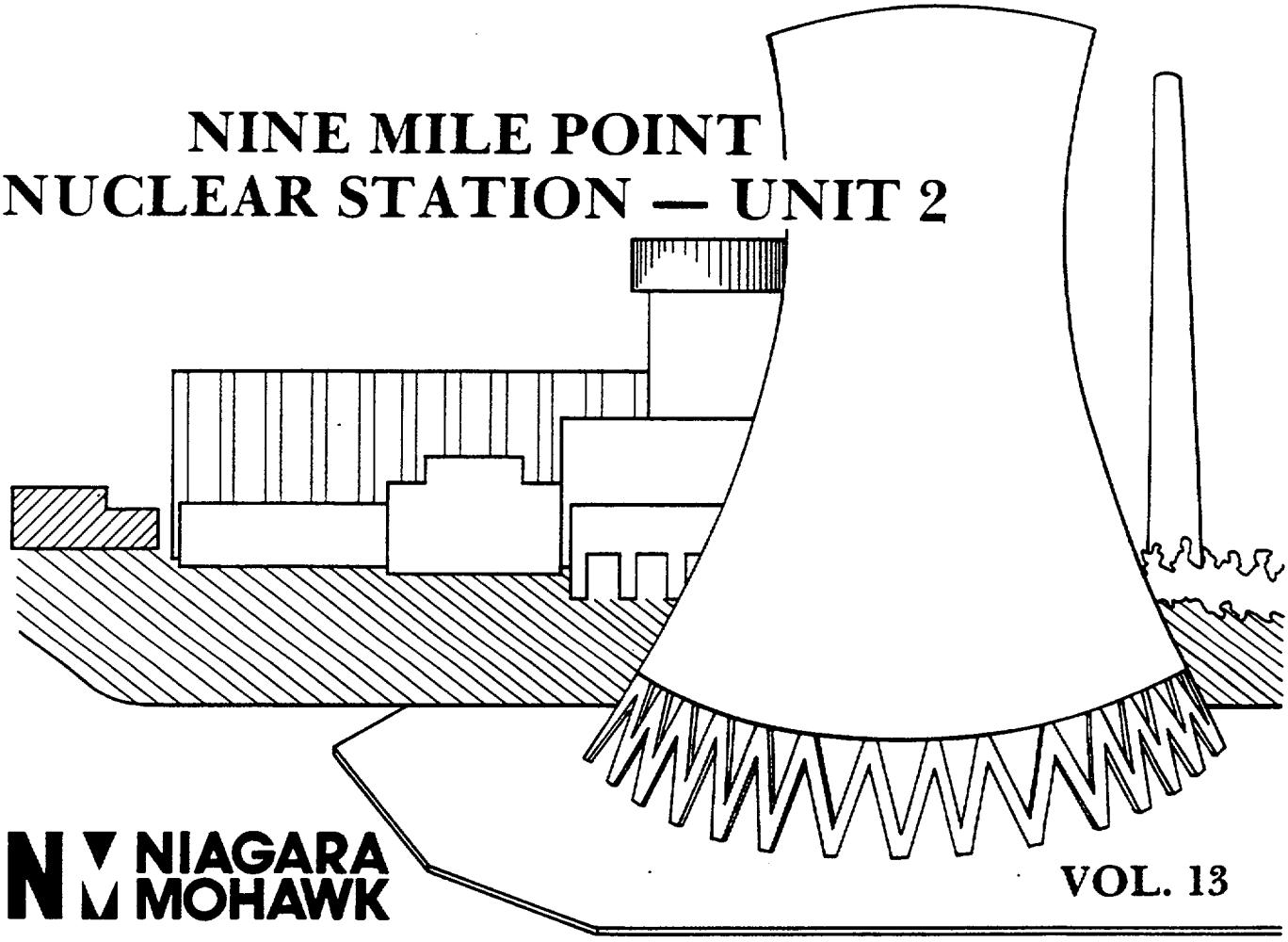

NIAGARA MOHAWK

VOL. 13

CHAPTER 5

REACTOR COOLANT SYSTEM AND CONNECTED SYSTEMS

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oxygen generation. Up to this point, the oxygen is degassed from the water and is displaced to the steam dome above the water surface.

Further increase in power increases the oxygen generation as well as the temperature. The solubility of oxygen in the reactor water at the prevailing temperature controls the oxygen level in the coolant until rated temperature (540°F) is reached. Thus, a gradual increase from the minimum level of 20 ppb to a maximum value of about 200 ppb oxygen takes place. At and after this point (540°F), steaming and the radiolytic process control the coolant oxygen concentration to a level of around 200 ppb.

2. Plant Shutdown Upon plant shutdown following power operation, the radiolytic oxygen generation essentially ceases as the fission process is terminated. Because oxygen is no longer generated, while some steaming still takes place due to residual energy, the oxygen concentration in the coolant decreases to a minimum value determined by steaming rate temperature. If venting is performed, a gradual increase to essentially oxygen saturation at the coolant temperature takes place, but does not exceed a maximum value of <8 ppm oxygen.

3. Oxygen in Piping and Parts Other Than the Reactor Vessel Proper As can be concluded from the preceding descriptions, the maximum possible oxygen concentration in the reactor coolant and any other directly related or associated parts is that of air saturation at ambient temperature. At no time or location in the water phase do oxygen levels exceed the nominal value of 8 ppm. As temperature is increased and, hence, oxygen solubility decreased accordingly, the oxygen concentration is maintained at this maximum value or reduced below it depending on available removal mechanisms, i.e., diffusion, steam stripping, flow transfer, or degassing.

   Depending on the location or configuration, such as dead legs or stagnant water, inventories may contain approximately 8 ppm dissolved oxygen or some other value below this maximum limitation.

Conductivity of the reactor coolant is continuously monitored. These measurements provide reasonable assurance for adequate surveillance of the reactor coolant.

Grab samples are provided, for the locations shown in Table 9.3-1, for special and noncontinuous measurements such as pH, oxygen, chloride, and radiochemical measurements. The relationship of chloride concentration to specific conductance

measured at 25°C for chloride compounds such as sodium chloride and hydrochloric acid can be calculated, as shown on Figure 5.2-7. Conductance values for these compounds essentially bracket those for other common chloride salts or mixtures at the same chloride concentration. Surveillance requirements are based on these relationships.

In addition to this program, limits, monitoring, and sampling requirements are imposed on the condensate, condensate treatment system, and feedwater by warranty requirements and specifications. Thus, a total plant water quality surveillance program is established providing assurance that off-specification conditions are quickly detected and corrected.

The sampling frequency when reactor water has a low specific conductance is adequate for calibration and routine audit purposes. When specific conductance increases and higher chloride concentrations are possible, or when continuous conductivity monitoring is unavailable, increased sampling is provided as described below. For the higher than normal limits of <1 umho/cm, more frequent sampling and analyses are invoked by the coolant chemistry surveillance program.

The chemistry of the RCS system shall be maintained within the limits specified in Table 5.2-11 at all times.

Failure to satisfy the limits of Table 5.2-11 in Operational Condition 1 does not need to be reported to the Nuclear Regulatory Commission (NRC) provided the conductivity, chloride concentration, or pH exceeding the limit is for less than 72 hr during one continuous time interval, and for conductivity and chloride concentration for less than 336 hr per yr, but with the conductivity less than 10 micromho/cm at 25°C and with the chloride concentration less than 0.5 ppm. With the conductivity, chloride concentration, or pH exceeding the limit specified in Table 5.2-11 in Operational Condition 1 for more than 72 hr during one continuous time interval, or with the conductivity and chloride concentration exceeding the limit specified in Table 5.2-11 for more than 336 hr per yr, be in at least startup within the next 6 hr. With the conductivity exceeding 10 micromho/cm at 25°C, or chloride concentration exceeding 0.5 ppm in Operational Condition 1, be in at least hot shutdown within 12 hr and in cold shutdown within the following 24 hr.

With the conductivity, chloride concentration, or pH exceeding the limit specified in Table 5.2-11 in Operational Condition 2 and 3 for more than 48 hr during one continuous time interval, be in at least hot shutdown within the next 12 hr and in cold shutdown within the following 24 hr.

At all other times (i.e., when not in Operational Conditions 1, 2 and 3):

1. with the conductivity or pH exceeding the limit specified in Table 5.2-11, restore the conductivity and pH to within the limit within 72 hr; or

2. with the chloride concentration exceeding the limit specified in Table 5.2-11, restore the chloride concentration to within the limit within 24 hr, or perform an engineering evaluation to determine the effects of the out-of-limit condition on the structural integrity of the RCS system, and determine that the structural integrity of the RCS system remains acceptable for continued operation before proceeding to Operational Condition 3.

The surveillance requirements described below provide adequate assurance that concentrations in excess of the limits will be detected in sufficient time to take corrective action. The reactor coolant shall be determined to be within the limits specified in Table 5.2-11 at all times.

Before pressurizing the reactor during each startup, the limits shall be determined to be satisfied by measurement if not performed within the previous 72 hr.

A sample of the reactor coolant shall be analyzed for chlorides, conductivity and pH at least once per 72 hr. Also, the sample shall be analyzed for chlorides at least once per 8 hr whenever conductivity is greater than the limit in Table 5.2-11. In addition, the sample shall be analyzed for pH at least once per 8 hr whenever conductivity is greater than the limit in Table 5.2-11.

The conductivity of the reactor coolant shall be continuously recorded. When the continuous recording conductivity monitor is inoperable, for up to 31 days, an in-line conductivity measurement shall be obtained at least once per 4 hr in Operational Conditions 1, 2 and 3 and at least once per 24 hr at all other times.

A channel check of the continuous conductivity monitor with an in-line flow cell shall be performed at least once per 7 days. Also, a channel check shall be performed with an in-line flow cell at least once per 24 hr whenever conductivity is greater than the limit in Table 5.2-11.

For the above surveillance intervals of 4, 8, 24 and 72 hr and 7 days, a maximum allowable extension not to exceed 25 percent of the surveillance interval is allowed for each of these surveillance intervals.

The primary coolant conductivity monitoring instrumentation is listed in Table 9.3-1 and is further described in Section 9.3.2.5.

Water Purity During Condenser Leakage The design of the Unit 2 condensate demineralizer (CND) system is in conformance with RG 1.56. The operational aspects of the CND system are in accordance with the operational guidance of RG 1.56.

5.2.3.2.3 Compatibility of Construction Materials with Reactor Coolant

Construction materials exposed to the reactor coolant consist of the following:

1. Solution-annealed austenitic stainless steels (both wrought and cast); Types 304, 304L, 316, 316K, and 316L.

2. Nickel-base alloys - Inconel 600 and Inconel 750X.

3. Carbon steel and low-alloy steel.

4. Some 400 series martensitic stainless steel (all tempered at a minimum of 1,100°F).

5. Colmonoy and Stellite hardfacing material.

All of these construction materials are highly resistant to stress corrosion in the BWR coolant. General corrosion on all materials, except carbon and low-alloy steel, is negligible.

Conservative corrosion allowances are provided for all exposed surfaces of carbon and low-alloy steels.

Contaminants in the reactor coolant are controlled to very low limits by the reactor water quality specifications. No detrimental effects will occur to any of the materials from allowable contaminant levels in the high-purity reactor coolant. Expected radiolytic products in the BWR coolant have no adverse effects on the construction materials.

5.2.3.2.4 Compatibility of Construction Materials with External Insulation and Reactor Coolant

Construction materials exposed to external insulation are:

1. Solution-annealed austenitic stainless steels. Types 304, 304L with 0.035-percent maximum of carbon content, 316 and 316K with 0.02-percent weight maximum of carbon content.

2. Carbon and low-alloy steel.

Two types of external insulation are employed on BWRs. Stainless steel reflective metal insulation used does not contribute to any surface contamination and has no effect on construction materials. Similarly, the fibrous (nonmetallic) insulation is

encapsulated in metal sheeting which prevents direct contact with the RCS materials. In addition, the fibrous insulation used is assessed to meet the requirements of RG 1.36, and has the proper ratios of leachable sodium and silicate ions to chloride and fluoride ions.

Since there are no additives in the BWR coolant, leakage would expose materials to high-purity, demineralized water. Exposure to demineralized water would cause no detrimental effects.

5.2.3.2.5 Monitoring BWR Structural Components Exposed to Reactor Coolant

A crack arrest verification (CAV) system is installed in Unit 2 to provide indication and to record the performance of plant materials in the primary coolant environment. The CAV is an in-line system which exposes precracked fracture mechanics test specimens made from BWR structural materials such as Inconel 182, Inconel 600, and Type 304 stainless steel. At Unit 2, the CAV system consists of three specimens installed in a test vessel and load frame, a water chemistry monitoring station, and electrochemical potential (ECP) monitor. Changes in crack length are detected by measuring variations in voltage drop across each crack. In addition to providing information related to crack growth, the CAV records key water chemistry parameters such as levels of dissolved oxygen, primary coolant conductivity and water temperature.

The CAV system is located in the secondary containment of the reactor building and is nonsafety related. Suction flow is taken from the recirculation (2RCS) sample line (Figure 5.4-2b), and discharge flow is connected to the RWCU (2WCS, Figure 5.4-16a). The crack extension rate test (CERT) pressure vessel for the test specimens is designed and fabricated per ASME Section VIII, Division 1, 1986 Edition. Valves, fitting, tubing, seals and other pressure-retaining components meet ANSI B31.1 standards.

5.2.3.3 Fabrication and Processing of Ferritic Materials

5.2.3.3.1 Fracture Toughness

Materials in the RCPB, other than the RPV, are required by 10CFR50.55a and Appendix G to meet the fracture toughness requirements of ASME Section III, NB-2300. These fracture toughness requirements for ferritic piping, valve, bolting, and pump materials are met as follows:

1. Piping and weld filler materials are in accordance with ASME Section III, NB-2300, 1974 Edition; field weld filler materials are to 1974 Edition.

2. Valves are in accordance with ASME III, NB-2300, as follows:

a. Motor-operated valves (MOVs), Winter 1975, except as noted in Appendix 5A, 1971 Edition and Winter 1973 Addenda.

b. MSIVs, Summer 1977.

c. Carbon Steel Manual Valves, Winter 1973.

3. Materials for bolts with diameters exceeding 1 in meet the 25-mil lateral expansion requirement of ASME Section III, NB-2300, of the same code date as the associated equipment. In addition, bolting greater than 1 in is required to meet a minimum of 45 ft-lb absorbed energy.

4. There are no ferritic pumps in the RCPB.

The fracture toughness properties of the RPV are discussed in Section 5.3.1 and Appendix 5A.

5.2.3.3.2 Control of Welding

Control of Preheat Temperature Employed for Welding of Low-Alloy Steel (Regulatory Guide 1.50)

RG 1.50 delineates preheat temperature control requirements and welding procedure qualifications supplementing those in ASME Sections III and IX.

The use of low-alloy steel is restricted to the RPV. Other ferritic components in the RCPB are fabricated from carbon steel materials. Preheat temperatures employed for welding of low-alloy steel meet or exceed the recommendations of ASME Section III, Appendix D. Components were either held for an extended time at preheat temperature to assure removal of hydrogen, or preheat was maintained until postweld heat treatment. The minimum preheat and maximum interpass temperatures were specified and monitored.

Control of Electroslag Weld Properties (Regulatory Guide 1.34)

No electroslag welding was performed on RCPB components.

Welder Qualification for Areas of Limited Accessibility (Regulatory Guide 1.71)

Qualification for areas of limited accessibility is discussed in Section 5.2.3.4.2.

TABLE 5.2-11

REACTOR COOLANT SYSTEM CHEMISTRY LIMITS

Operational Condition	Chlorides	Conductivity (micromho/cm @ 25°C)	pH
1	≤ 0.2 ppm	≤ 1.0	5.6 ≤ pH ≤ 8.6
2 and 3	≤ 0.1 ppm	≤ 2.0	5.6 ≤ pH ≤ 8.6
At all other times	≤ 0.5 ppm	≤ 10.0	5.3 ≤ pH ≤ 8.6