



Northern States Power Company

Monticello Nuclear Generating Plant
2807 West County Road 75
Monticello, MN 55362

January 31, 2000

Technical Specifications
6.7.A.7

U S Nuclear Regulatory Commission
Attn: Document Control Desk
Washington, DC 20555

MONTICELLO NUCLEAR GENERATING PLANT
Docket No. 50-263 License No. DPR-22

Submittal of the Core Operating Limits Report for Cycle 20

The Core Operating Limits Report (COLR) for Cycle 20, Rev 0, is enclosed. This report provides the values of the limits for Cycle 20 as required by Technical Specification Section 6.7.A.7. These values have been established using NRC approved methodology such that all applicable limits of the plant safety analysis are met.

It is noted that this COLR incorporates changes given in a September 22, 1999 notification letter from General Electric (Reference 1) with regard to the Safety Limit Minimum Critical Power Ratio (SLMCPR), and as communicated to the NRC in our SLMCPR License Amendment Request of December 16, 1999 (Reference 2).

The COLR reflects a SLMCPR of 1.11 for two-loop operation, and 1.12 for single-loop operation for all fuel in Cycle 20.

The appropriate OLMCPR values in our core monitoring system will be changed prior to plant startup.

Please contact Sam Shirey at 612-295-1449 if you have any questions related to this submittal.

Byron D. Day
Plant Manager
Monticello Nuclear Generating Plant

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c: Regional Administrator-III, NRC
NRR Project Mgr., NRC
NRC Resident Inspector
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Attn: Steve Minn
J Silberg

Enclosure: Core Operating Limits Report for Cycle 20 (Rev 0)

References

1. Letter from T. G. Reason (GE Nuclear Energy) to T. J. Asmus (NSP), "Additional Information Regarding the Cycle Specific SLMCPR for Monticello Cycle 20," September 22, 1999.
2. Letter from Byron D. Day (NSP) to US Nuclear Regulatory Commission, "License Amendment Request for Monticello Cycle 20 Safety Limit Minimum Critical Power Ratio," December 16, 1999.

MONTICELLO NUCLEAR GENERATING PLANT

Core Operating Limit Report

Record of Revision

<u>Cycle</u>	<u>Revision Number</u>	<u>Approval Date</u>	<u>Remarks</u>
14	0	09/28/89	Core Operating Limit Report distributed with Technical Specification Revision 120
15	0	05/23/91	
16	0	03/25/93	
16	1	05/17/94	
16	2	06/27/94	
17	0	09/22/94	
18	0	05/14/96	
18	1	05/18/96	
18	2	07/12/96	
18	3	11/12/96	
19	0	04/13/98	
19	1	09/08/98	
19	2	09/21/98	
19	3	01/03/00	
20	0	01/31/00	



MONTICELLO NUCLEAR GENERATING PLANT

Core Operating Limits Report

Cycle 20

Revision 0

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Introduction

This report provides the values of the limits for Cycle 20 as required by Technical Specification Section 6.7.A.7. These values have been established using NRC approved methodology and are established such that all applicable limits of the plant safety analysis are met.

A SLCPR of 1.11 was used for two-loop operation for all fuel types in Cycle 20 (GE10, GE11, and GE12). The SLCPR for single-loop operation is 1.12. These values are consistent with the values specified by GE in Reference 2.

This report includes stability exclusion region definition, buffer region definition, and power distribution limits as required by amendment 97 to Monticello's operating license approved by the NRC in Reference 4.

- Reference 1: NSPNAD-99007 Revision 0, "Monticello Cycle 20 Final Reload Design Report (Reload Safety Evaluation)", November 1999.
- Reference 2: Letter TGR:99-063 from T.G. Reason (GE Nuclear) to T.J. Asmus (NSP), "Additional Information Regarding the Cycle Specific SLMCPR for Monticello Cycle 20", September, 1999.
- Reference 3: Letter from M. F. Hammer (NSP) to USNRC dated July 30, 1998, "Supplementary Information Regarding the Monticello Power Rerate (TAC No. 96238)," including attachments.
- Reference 4: Letter from Tae Kim (USNRC) to Roger O. Anderson (NSP), "Monticello Nuclear Generating Plant - Issuance of Amendment Re: Implementation of Boiling Water Reactor Owners Group Option I-D Core Stability Solution (TAC No. M92947)", including enclosures, September 17, 1996.
- Reference 5: Letter from M. F. Hammer (NSP) to USNRC dated December 4, 1997, "Revision 1 to License Amendment Request Dated July 26, 1996 Supporting the Monticello Nuclear Generating Plant Power Rerate Program," including attached exhibits.
- Reference 6: Letter from Tae Kim (USNRC) to Roger O. Anderson (NSP), "Monticello Nuclear Generating Plant - Issuance of Amendment Re: Power Uprate Program (Tac No. M96238)", including enclosures, September 16, 1998.

Rod Block Monitor Operability Requirements

The MCPR limit associated with the Rod Block Monitor operability is:

$$\text{MCPR} < 1.68$$

Whenever the monitored core MCPR is less than 1.68, a limiting control rod pattern exists and the RBM system is required to be operable.

Reference Technical Specification Section 3.2.C.2.a

Rod Block Monitor Upscale Trip Setpoints

Low Trip Setpoint (LTSP)	≤	120/125 of full scale
Intermediate Trip Setpoint (ITSP)	≤	115/125 of full scale
High Trip Setpoint (HTSP)	≤	110/125 of full scale

Reference Technical Specification Sections: Table 3.2.3 Item 4.a, Table 3.2.3 Note 8.

Minimum Critical Power Ratio

The Minimum Critical Power Ratio (MCPR) limit shall be determined for two Recirculation Loop Operation as follows:

If thermal power > 45%, then the MCPR for GE10 is the greater of:

$$1.51 * K_p \text{ (} K_p \text{ from Figure 3) or TICPR}_f \text{ from Figure 5.}$$

If thermal power > 45%, then the MCPR for GE11 fuel is the greater of:

$$1.49 * K_p \text{ (} K_p \text{ from Figure 4) or TICPR}_f \text{ from Figure 5.}$$

If thermal power > 45%, then the MCPR for GE12 Fuel is the greater of:

$$1.51 * K_p \text{ (} K_p \text{ from Figure 4) or TICPR}_f \text{ from Figure 5.}$$

If thermal power \leq 45%, then the MCPR limit for GE10 is obtained in Figure 3.

If thermal power \leq 45%, then the MCPR limit for GE11 and GE12 fuel is obtained in Figure 4.

For single recirculation loop operation the MCPR limit as defined previously by two recirculation loop operation is increased by the following adders:

0.01 Δ MCPR to account for core flow measuring and TIP reading uncertainties.

Reference Technical Specification Section: 3.11.C.

When both recirculation loops are in operation, the MCPRs calculated above may be replaced by values calculated in Table 3 if taking credit for scram speeds.

Power-Flow Operating Map

The Power-Flow Operating Map based on analysis to support Cycle 20 is shown in Figures 6 & 7. This Power-Flow Operating Map is consistent with the rated power of 1775 as described in References 3, 5, and 6.

Approved Analytical Methods

NEDE-24011-P-A	Rev 13	"General Electric Standard Application for Reactor Fuel"
NSPNAD-8608-A	Rev 4	"Reload Safety Evaluation Methods for Application to the Monticello Nuclear Generating Plant"
NSPNAD-8609-A	Rev 3	"Qualification of Reactor Physics Methods for Application to Monticello"
NEDO-31960-A		"BWR Owners Group Long-Term Stability Solutions Licensing Methodology," Licensing Topical Report, November 1995.
NEDO-31960-A	Sup 1	"BWR Owners Group Long-Term Stability Solutions Licensing Methodology," Licensing Topical Report, Supplement 1, March 1992.

Maximum Average Linear Heat Generation Rate as a Function of Exposure

When hand calculations are required, the Maximum Average Linear Heat Generation Rate (MAPLHGR) for each fuel bundle design as a function of average planar exposure shall not exceed the limiting lattice (excluding natural Uranium) provided in Table 1 (based on straight line interpolation between data points) multiplied by the smaller of the two MAPFAC factors determined from Figures 1 and 2.

The MAPLHGR limits in Table 1 are conservative values bounding all fuel lattice types (excluding natural Uranium) in a given fuel bundle design and are intended only for use in hand calculations as described in Technical Specification 3.11.A. No channel bow effects are included in the bounding MAPLHGR values below because there are no reused channels. MAPLHGR limits for each individual fuel lattice design in a bundle design as a function of axial location and average planar exposure are determined based on the approved methodology referenced in Monticello Technical Specification 6.7.A.7.b and loaded in the process computer for use in core monitoring calculations.

Reference Technical Specification Section 3.11.A.

TABLE 1
MAPLHGR Limit for each fuel type [kW/ft]

Exposure [MWD/STU]	GE10- DXB333- 10GZ	GE10- DXB324- 11GZ					
200	11.64	10.71					
1000	11.70	10.82					
5000	12.30	11.78					
10000	12.88	13.17					
15000	12.65	12.88					
20000	11.97	12.25					
25000	11.31	11.60					
30000	10.67	10.95					
35000	10.02	10.30					
40000	9.21	9.61					
45000	8.40	8.92					
50000	5.93	6.43					
Exposure [MWD/STU]	GE11- DUB348- 10GZ	GE11- DUB347- 10GZ	GE12- DSB330- 12GZ	GE11- DUB366- 16GZ	GE11- DUB366- 17GZ	GE11- DUB380- 16GZ	GE11- DUB380- 17GZ
200	10.32	9.96	8.54	9.96	9.45	9.47	9.32
1000	10.47	10.02	8.57	10.17	9.64	9.63	9.48
5000	11.21	11.04	9.31	11.21	10.73	10.51	10.40
10000	12.21	12.32	10.25	12.21	12.05	11.60	11.70
15000	12.06	11.93	10.13	12.03	11.92	11.52	11.52
20000	11.40	11.32	9.78	11.58	11.50	10.95	10.96
25000	10.71	10.73	9.45	10.90	10.75	10.39	10.39
30000	10.03	10.15	9.08	10.20	10.00	9.82	9.83
35000	9.37	9.56	8.66	9.54	9.28	9.24	9.25
40000	8.71	8.91	8.19	8.88	8.54	8.57	8.57
45000	8.05	8.27	7.46	8.22	7.85	7.88	7.87
50000	7.38	7.59	6.70	7.56	7.19	7.22	7.21
55000	6.70	6.62	5.99	6.90	6.55	6.58	6.57
55920	-	-	-	-	-	6.46	-
55980	-	-	-	-	-	-	6.44
57680	6.28	-	-	6.29	-	-	-
57900	-	-	-	-	6.18	-	-
58050	-	6.06	-	-	-	-	-
58220	-	-	-	-	6.14	-	-
60060	-	-	5.31	-	-	-	-

Note: Table 1 is for two recirculation loop operation. For single loop operation, multiply the GE10 values by 0.78 and the GE11 and GE12 values by 0.80.

Linear Heat Generation Rate

TABLE 2 LHGR Limit for Each Fuel Type (kW/ft)								
GE10- DXB333- 10GZ	GE10- DXB324- 11GZ	GE11- DUB347- 10GZ	GE11- DUB348- 10GZ	GE12- DSB330- 12GZ	GE11- DUB366- 16GZ	GE11- DUB366- 17GZ	GE11- DUB380- 16GZ	GE11- DUB380- 17GZ
14.4	14.4	14.4	14.4	11.8	14.4	14.4	14.4	14.4

Reference Technical Specification Section: 3.11.B.

Core Stability Requirements

Stability Exclusion Region

The stability exclusion region is shown in Figure 6 and is given in greater detail in Figure 7.

Stability Buffer Region

The stability buffer region is shown in Figure 6 and is given in greater detail in Figure 7.

Power Distribution Controls

Prior to intentionally entering the stability buffer region, the hot channel and core wide decay ratios will be shown to be within the stable portion of Figure 8. While operating in the stability buffer region, the hot channel and core wide decay ratios will be maintained within the stable portion of Figure 8.

Reference Technical Specification Section 3.5.F.

Scram Time Dependence

Technical Specification 3.3.C provides the scram insertion time versus position requirements for continued operations. Technical Specification 4.3.C provides the surveillance requirements for the CRDs. Data from testing of the CRDs, or from an unplanned scram, is summarized in Surveillance Test 0081. Using this cycle specific information, values of τ_{20} can be calculated in accordance with the equation at the 20% insertion position, which is:

$$\tau_{20} = \frac{\sum_{i=1}^n N_i t_i}{\sum_{i=1}^n N_i} + 0.0875 \left[\frac{N_1}{\sum_{i=1}^n N_i} \right]^{\frac{1}{2}}$$

- where: τ_{20} = the weighted cycle average scram time at a 95% confidence level at the 20% insertion position.
 n = the number of surveillance tests performed following core alterations.
 N_i = the number of control rods measured in the i^{th} test.
 N_1 = the total number of active rods measured in the first test following core alterations.
 t_i = average scram time at the 20% insertion position of all rods measured in the i^{th} test.

$\tau_{20} = 0.900$ seconds shall be assumed until cycle specific scram data following a core alteration becomes available. When scram insertion time data is available, credit may be taken for faster insertion times, if desired. It should also be noted that when data does become available, the average scram time values must be calculated with either CRD insertion time data at reactor pressures above 965 psia, or with data that is corrected for low reactor pressures in accordance with Surveillance Test 0081 Appendix A.

After obtaining the cycle specific values of τ_{20} for the 20% insertion positions, a comparison can be made to Table 3 in order to get the scram time adjusted OLCPR. The value of the scram time adjusted OLCPR is obtained from Table 3 by linearly interpolating the value of τ at the 20% insertion position. Note that extrapolation is not permitted in Table 3.

The adjustment to the OLCPR limit can only be performed if the plant is operating with both recirculation loops. Credit for scram insertion times may not be taken if the plant is operating with a single recirculation loop.

TABLE 3
Full Power/Flow OLCPR as a Function of Scram Time

τ_{20}	0.773	0.900
OLCPR GE10	1.45	1.51
OLCPR GE11	1.45	1.49
OLCPR GE12	1.45	1.51

NOTES

1. Credit for scram insertion times may not be taken if the plant is operating with a single recirculation loop.

Sample Interpolation

After a Surveillance Test 0081 has been completed for Cycle 20 the results can be used to calculate a new average scram insertion time at the 20% insertion position. This time can then be linearly interpolated to change the OLCPR values found in Table 3. If the scram insertion time changed from 0.900 seconds to 0.800 seconds then the OLCPR values would change as follows:

Table 4
Sample Interpolation for Full Power/Flow OLCPR as a Function of Scram Time

τ_{20}	0.773	0.800	0.900
OLCPR GE10	1.45	1.47	1.51
OLCPR GE11	1.45	1.46	1.49
OLCPR GE12	1.45	1.47	1.51

For example, from Table 4 the OLCPR for GE10 would be 1.47 instead of 1.51 at the technical specification scram insertion time thus increasing operating margin.

FIGURE 1

Monticello Cycle 20

Power Dependent MAPLHGR Limits

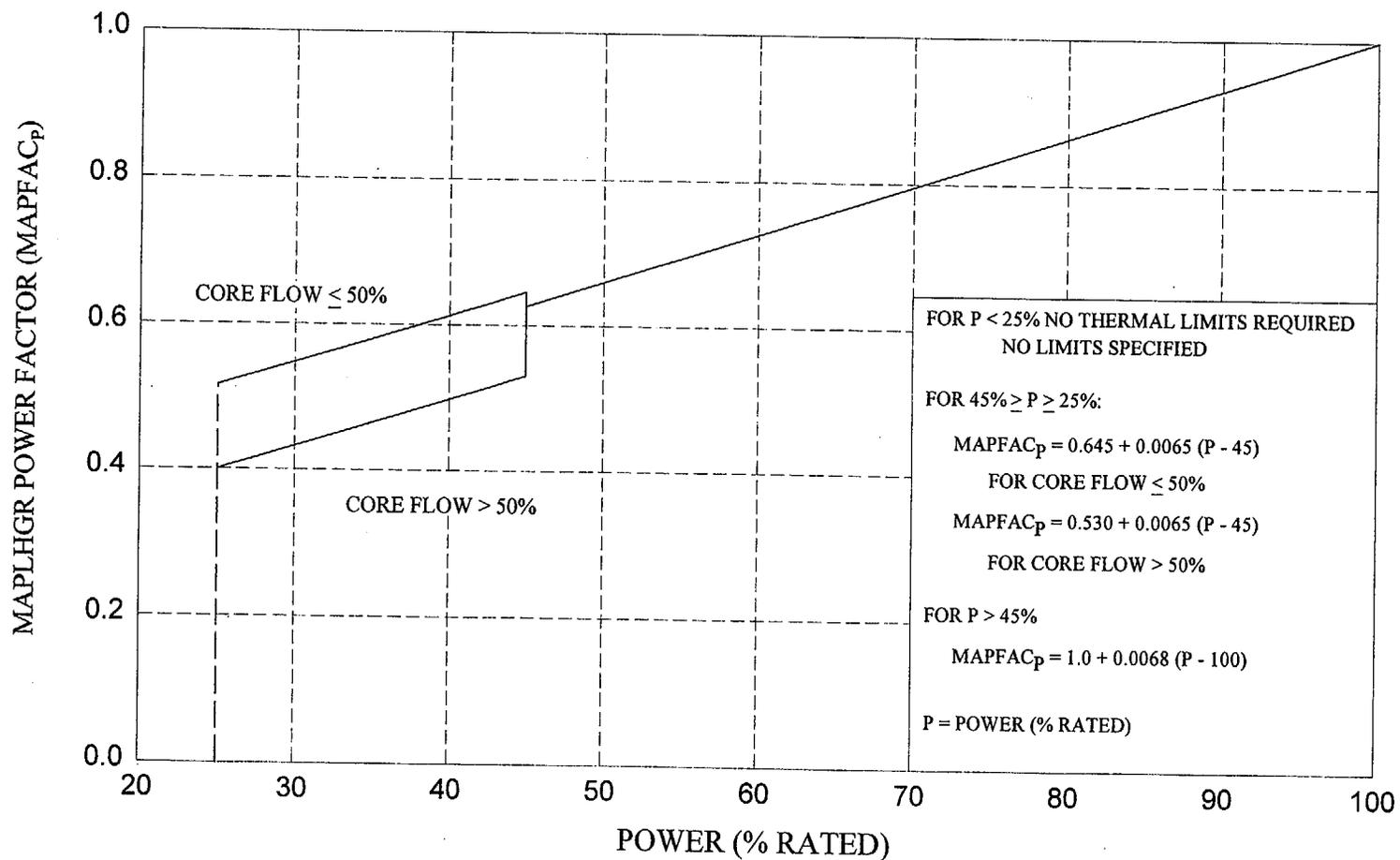


FIGURE 2

Monticello Cycle 20 Flow Dependent MAPLHGR Limits

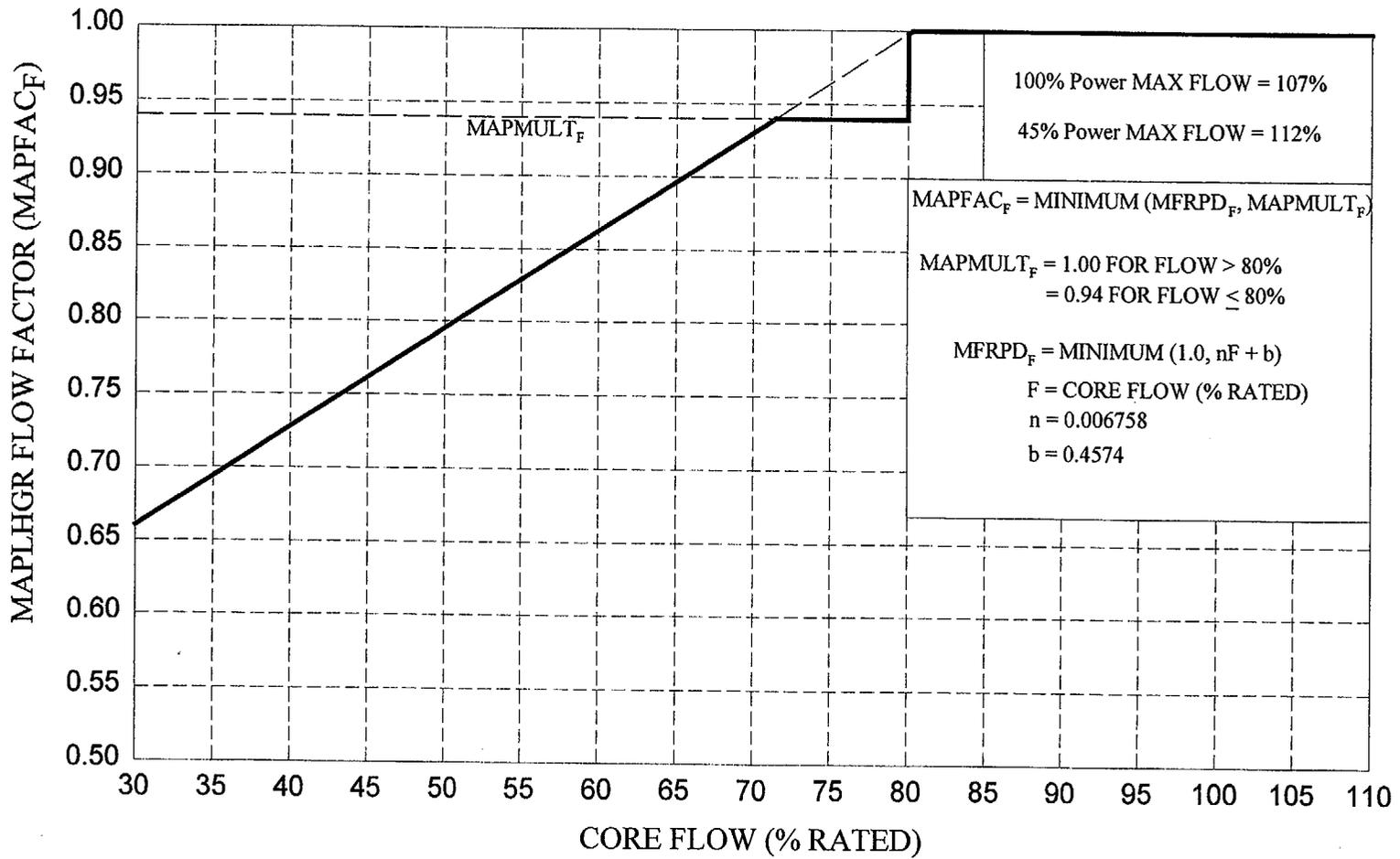


FIGURE 3

Monticello Cycle 20 Power Dependent CPR Limits (GE10)

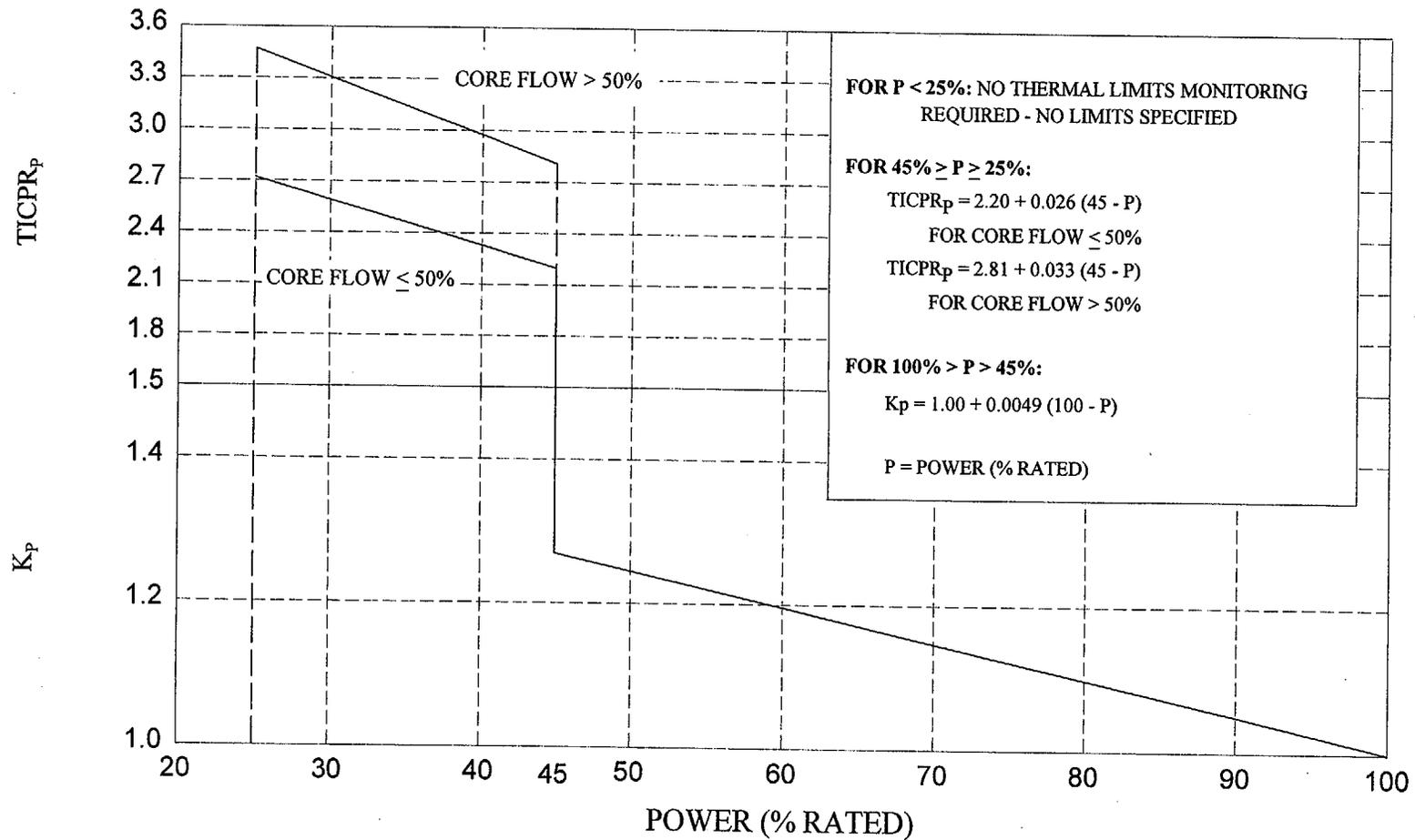


FIGURE 4

Monticello Cycle 20 Power Dependent CPR Limits (GE11, GE12)

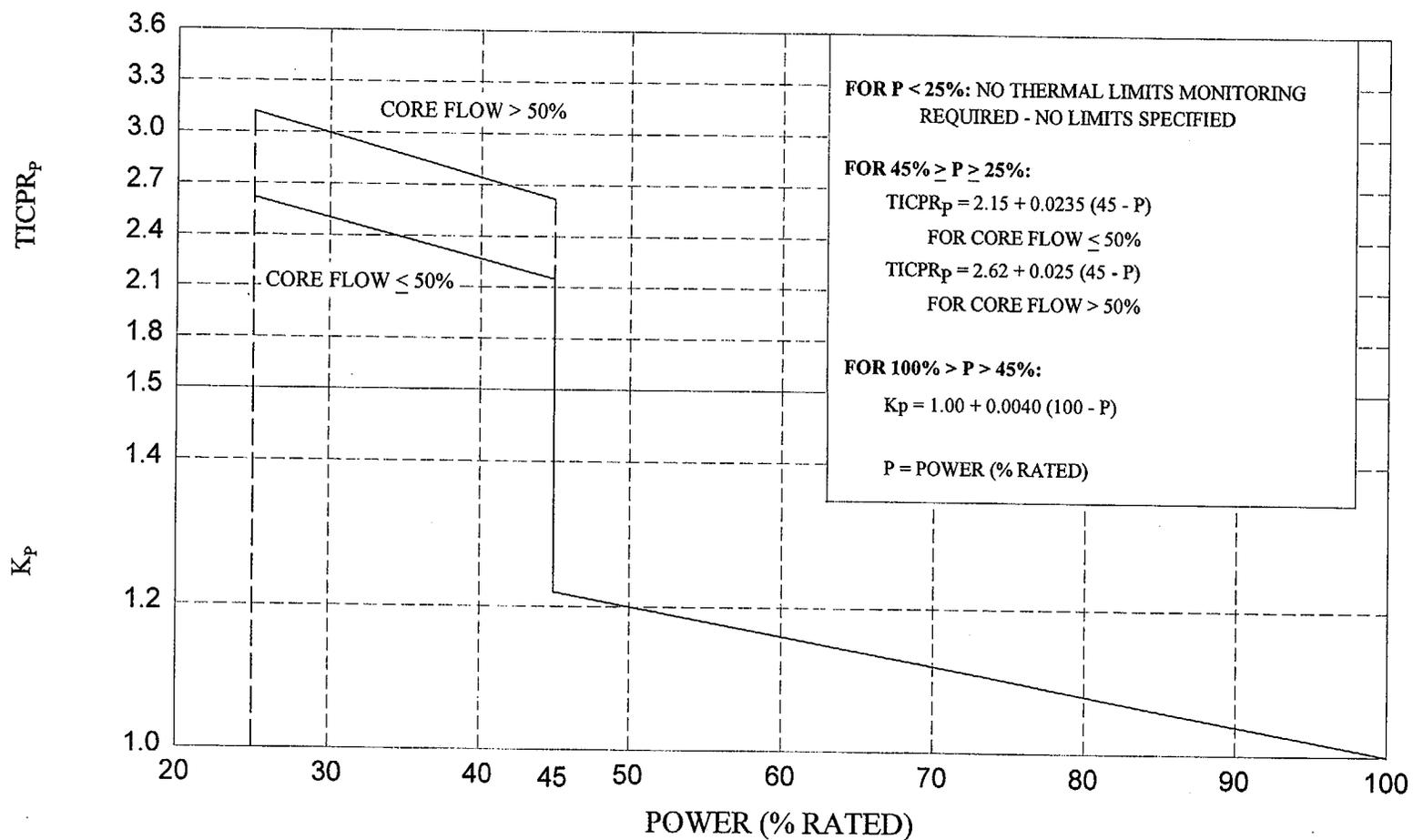


FIGURE 5

Monticello Cycle 20 Flow Dependent CPR Limits

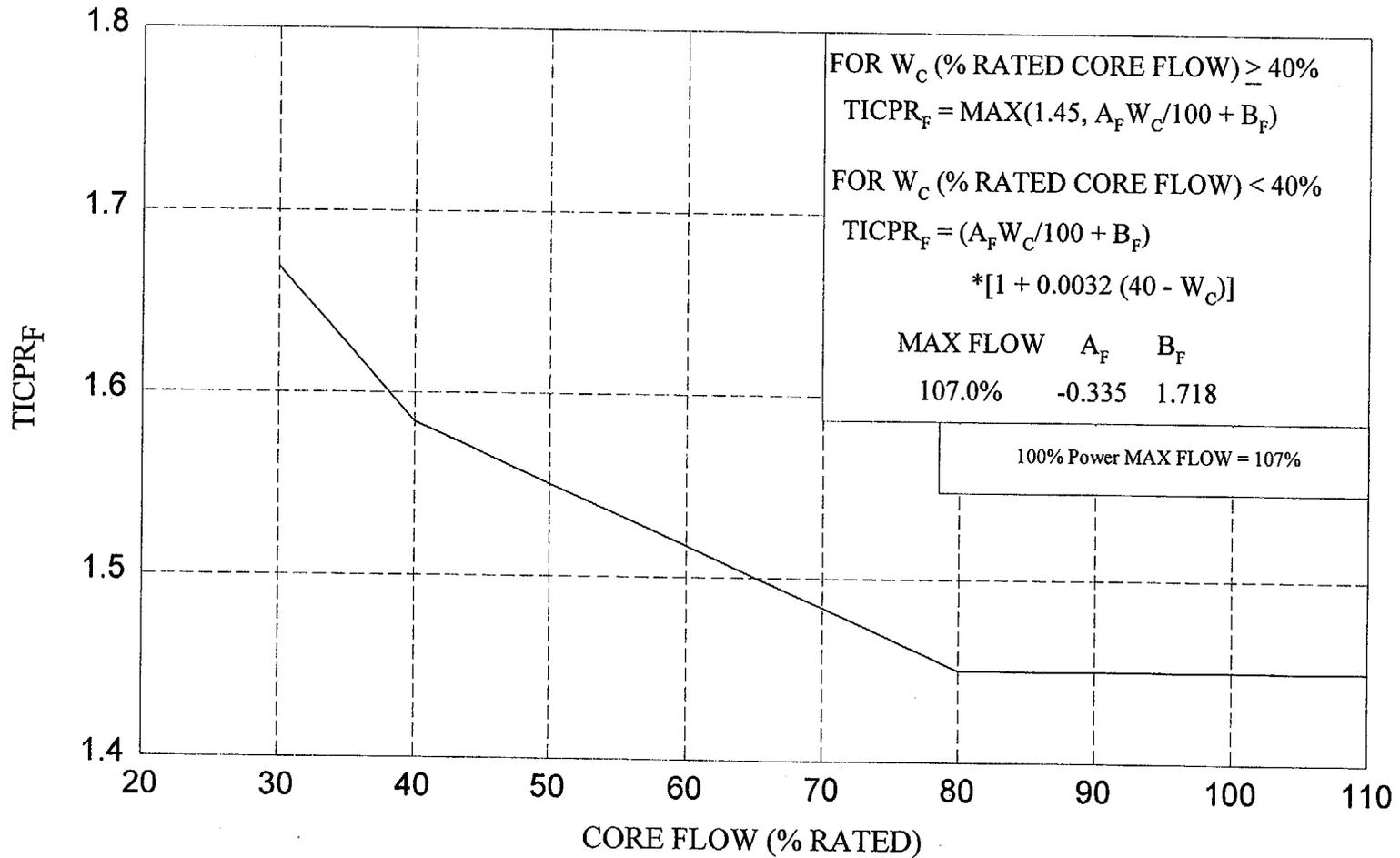


FIGURE 6

Power-Flow Operating Map

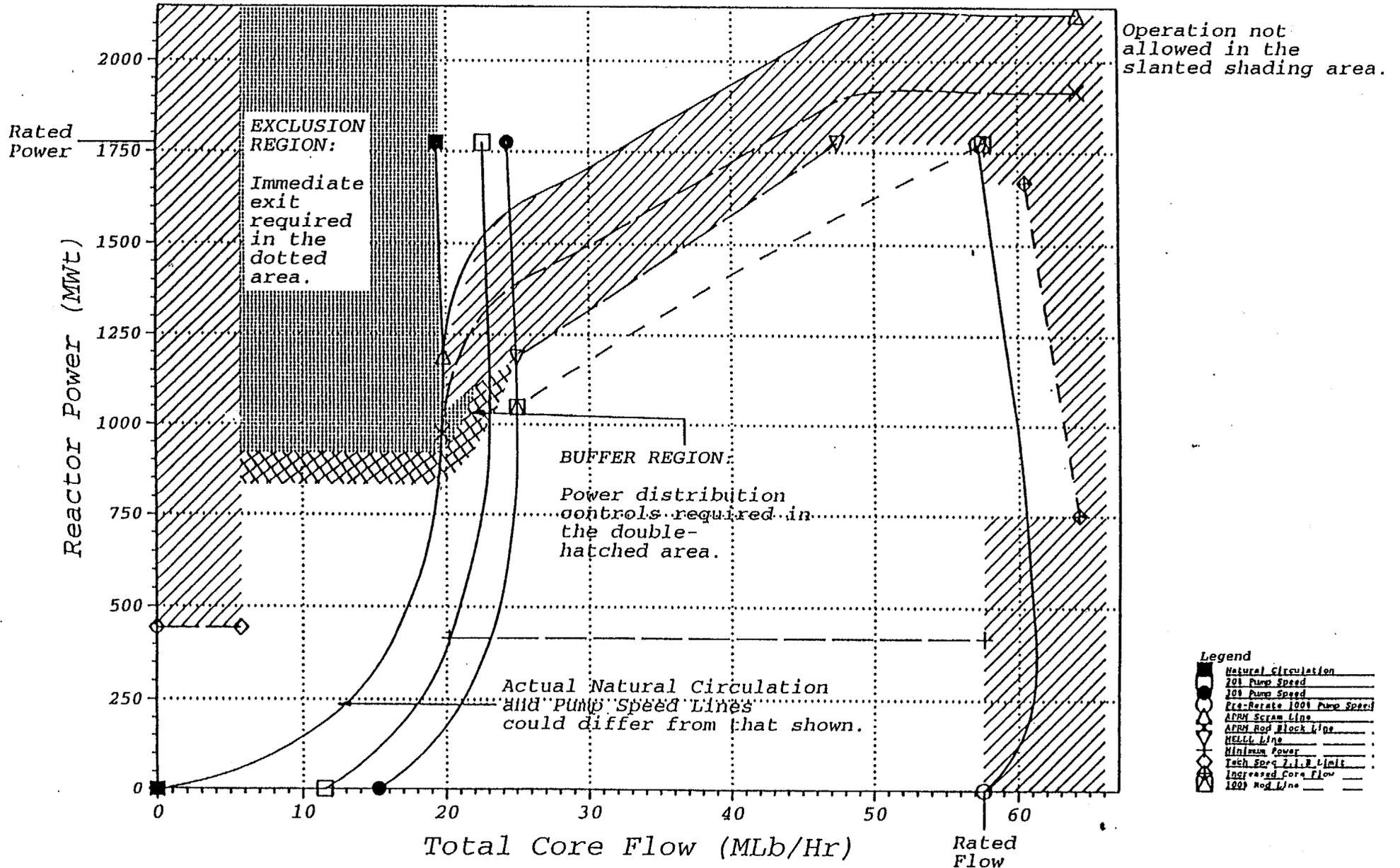


FIGURE 7

Power-Flow Operating Map

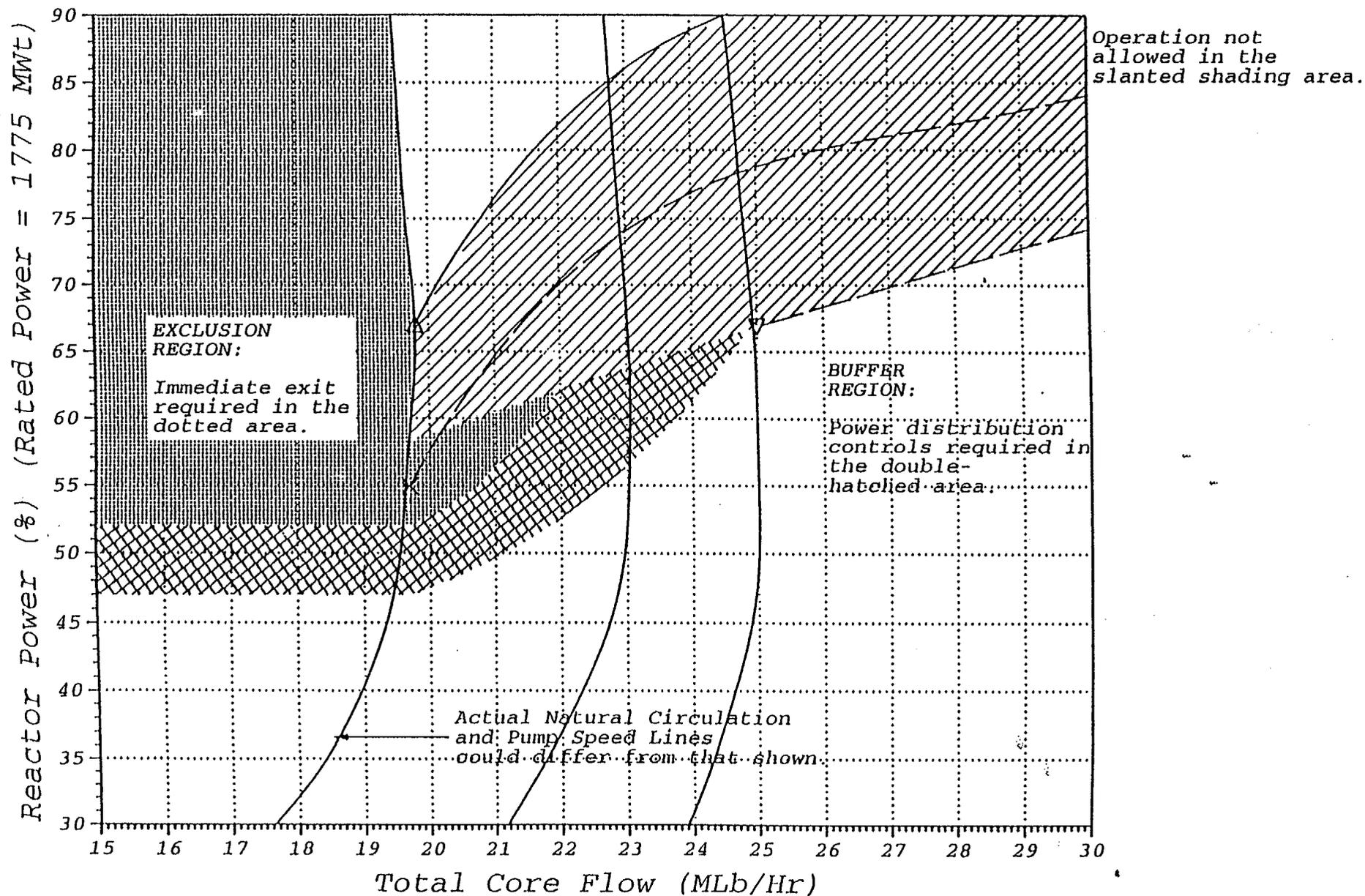


FIGURE 8

Stability Criterion Map

