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January 20, 2000

PG&E Letter DCL-00-008

U.S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington, DC 20555-0001

Docket No. 50-323, OL-DPR-82
Diablo Canyon Unit 2
Special Report 00-01 - 90 Day Report, Results of Steam Generator Alternate Repair
Criteria for Diablo Canyon Power Plant Unit 2 Ninth Refueling Outage

Dear Commissioners and Staff:

During the Unit 2 ninth refueling (2R9) outage, completed on October 23, 1999, PG&E implemented two steam generator tube alternate repair criteria (ARC): (1) WStar (W*) ARC; and (2) voltage-based ARC, in accordance with Generic Letter (GL) 95-05.

In accordance with Technical Specifications 4.4.5.5e, 4.4.5.5f, and 6.9.2, Enclosure 1 provides the 90 day report for W* ARC, including inspection results of W* tubes and the aggregate calculated steam line break leak rate from application of both ARCs in 2R9. In accordance with GL 95-05, Enclosure 2 provides the 90 day report for voltage-based ARC, and includes voltage distributions of indications and results of the tube integrity evaluation (calculated steam line break leak rate and conditional burst probability).

Sincerely,

Lawrence F. Womack

cc: Steven D. Bloom

Ellis W. Merschoff David L. Proulx

State of California
Diablo Distribution

Enclosures

DDM/469

A001 1/1

SPECIAL REPORT 00-01

90 DAY REPORT W* ALTERNATE REPAIR CRITERIA DIABLO CANYON POWER PLANT UNIT 2 NINTH REFUELING OUTAGE

NRC Reporting Requirements

Diablo Canyon Power Plant (DCPP) Technical Specification (TS) 4.4.5.5.e requires that the results of the inspection of W* tubes be reported to the Commission pursuant to TS 6.9.2 (i.e., as a Special Report) within 90 days following return to service of the steam generators (SGs). The report shall include:

- 1. Identification of W* tubes.
- 2. W* inspection distance measured with respect to the bottom of the W* transition (BWT) or the top of tubesheet, whichever is lower.
- 3. Elevation and length of axial indications within the flexible W* distance and the angle of inclination of clearly skewed axial cracks (if applicable).
- 4. The total steam line break leakage for the limiting steam generator per WCAP-14797.

DCPP TS 4.4.5.5.f requires that the aggregate calculated steam line break leakage from application of all alternate repair criteria (ARC) be reported to the Commission pursuant to TS 6.9.2 (i.e., Special Report) within 90 days following return to service of the SGs.

W* Inspections and Results

This report implements the DCPP TS reporting criteria. W* ARC was implemented for the first time in DCPP Unit 2 during the ninth refueling outage (2R9). Following inspections and maintenance, the SGs were returned to service on October 23, 1999, upon entry into Mode 4.

100 percent of the SG tubes were inspected by bobbin from tube end to tube end.
100 percent of the hot leg top of tube sheet (TTS) region was inspected by Plus Point.
Cold leg TTS inspections by Plus Point were not required.

Table 1 provides a comprehensive list of axial primary water stress corrosion cracking (PWSCC) indications detected in the WEXTEX region during 2R9 Plus Point inspections. The following TS-required reporting information is extracted from the table:

- 1. Identification of W* tubes. See "W* Tube" column in Table 1. Fifty seven tubes are categorized as W* tubes: 10 in SG 21, 6 in SG 22, 20 in SG 23, and 21 in SG 24. An additional 5 tubes with axial PWSCC were plugged because they did not meet W* ARC (upper crack tip was located above BWT, including uncertainty). One circumferential PWSCC indication (not listed) was also detected and plugged because circumferential indications in the W* region are excluded from W* ARC.
- 2. W* inspection distance measured with respect to BWT or TTS, whichever is lower. For the 100 percent Plus Point hot leg TTS exam, the inspection extent relative to the TTS was specified as +2/-8 in. Assuming no degradation in the W* length, 8 in. below the TTS constitutes the W* inspection distance. This distance bounds W* lengths for Zone A and Zone B (5.2 in. and 7.0 in., respectively, relative to BWT), and includes margin for a nominal distance from BWT to TTS plus non-destructive examination (NDE) uncertainty in measuring W* length. If degradation is detected in the W* region, the inspection extent must bound the calculated flexible W* length. The "W* Insp Dist" column in Table 1 lists the W* inspection distances measured with respect to BWT for tubes in which axial PWSCC was detected (in all cases, BWT was lower than the TTS).
- 3. Elevation and length of axial indications within the flexible W* distance. See "From-To" and "L" columns in Table 1 for elevation and length of axial indications.
- 4. Angle of inclination of clearly skewed axial cracks (if applicable). None of the axial indications were skewed, so the angle of inclination was reported as 0 degrees for all axial indications.
- 5. The total steam line break leakage for the limiting steam generator per WCAP-14797. Steam Line Break (SLB) leakage attributed to each W* indication at end of cycle (EOC) 9 (condition monitoring) and EOC 10 (operational assessment) are listed in "CM LR" and "OA LR" columns in Table 1. The limiting W* SLB leak rates for condition monitoring and operational assessment are 0.1468 gpm and 0.6330 gpm, respectively (see Table 2).

Table 2 reports the following SLB leak rates, pursuant to TS 4.4.5.5.e.4 and 4.4.5.5.f:

- 1. Total W* ARC SLB leakage for each SG at EOC 9.
- 2. Total W* ARC SLB leakage for each SG at EOC 10.
- 3. Total Generic Letter (GL) 95-05 voltage based ARC SLB leakage for each SG at EOC 9 and EOC 10.
- 4. The aggregate calculated SLB leakage from application of both ARC at EOC 9.
- 5. The aggregate calculated SLB leakage from application of both ARC at EOC 10.

Table 3 provides the updated cumulative probability distribution for growth of W* region axial PWSCC indications. The updated 95 percent cumulative probability DCPP Units 1 and 2 growth rate is 0.18 in./effective full power year (EFPY), and the distribution includes 28 data points (19 of which are Plus Point to Plus Point). The updated 95% cumulative probability combined industry data growth rate is 0.24 in./EFPY (which is lower than the prior 0.25 in./EFPY growth rate documented in WCAP-14797, Rev 1), and the distribution includes the 28 DCPP data points plus 31 data points from plants W1 and W2 documented in WCAP-14797, Rev 1. The W* operational assessment documented herein applies the 0.24 in./EFPY growth rate.

In-situ Leak Testing

In an effort to validate the leak rate model in WCAP-14797, Rev 1, three W* indications were in-situ leak tested in 2R9: SG 21 R3C59, SG 21 R7C62, and SG 22 R31C25. All three indications were in deplugged tubes. The in-situ guidelines for selecting indications for leak testing were established in PG&E letter DCL-98-148, "Response To NRC Request For Additional Information, Dated August 6, 1998, Regarding Proposed W* Steam Generator Tube Repair Criteria," dated October 22, 1998. The peak voltage for R3C59 and R31C25 exceeded the 4.0 volt critical voltage and the peak voltage for R31C35 was 3.99 volts (approximately 4 volts), requiring that all three indications be leak tested. The indications were locally tested to normal operating pressure differential. Because they did not leak, the test was terminated at that pressure. Plus Point inspections were performed again and verified that the indications satisfy the W* repair criteria. The indications were returned to service.

Tube Integrity Performance Monitoring

Performance Criteria to Limit Free Span Cracking: The upper crack tip of W* indications returned to service under W* ARC shall remain below the TTS by at least the NDE uncertainty on locating the crack tip relative to the TTS. The "UCT to TSH" column in Table 1 provides the elevation of the upper crack tip relative to the top of tubesheet, accounting for NDE uncertainty in locating the crack relative to the top of tubesheet. In all cases, the crack tip is below the top of tubesheet. Therefore, the performance criteria has been satisfied for condition monitoring at EOC 9.

Accident-Induced Leakage Performance Criteria: Calculated W* leak rates under postulated SLB conditions, when combined with calculated leak rates from application of GL 95-05 voltage-based ARC, shall not exceed 12.8 gpm (at room temperature) in the faulted SG for condition monitoring and operational assessment. Based on Table 2, the aggregate calculated SLB leakage from application of both ARC at EOC 9 is 0.4683 gpm for limiting SG 24, and 1.7247 gpm at EOC 10 for limiting SG 24. In both assessments, SLB leakage is less than the allowable limit of 12.8 gpm for a faulted SG. Therefore, the performance criteria has been satisfied for condition monitoring at EOC 9 and operational assessment at EOC 10.

Table 1
DCPP Unit 2 - 2R9 Axial PWSCC Indications in Hot Leg WEXTEX Region

| SG | R | С | IND | +Pt volt | From | То | L | UCT to TSH | W* Zone | W* L | BWT | UCT to BWT | UCT Below W* | UCT Below BWT | EOC 10 UCT | UCT Below TSH at EOC10 | W* Tube | Insp Ext | W* Insp Dist | Flex W* L | CM LR | EOC10 UCT- BWT | OA LR | Deplug | Plug |
|----|----|----|-----|-------------|-------|-------|------|------------------|------------|------|--------------|------------------|--------------------|---------------------|------------------|---------------------------------|------------|-------------|--------------------|--------------|--------|----------------------|--------|--------|------|
| 21 | 7 | 24 | SAI | | -1.92 | -1.78 | 0.14 | -1.56 | B3 | 7.12 | -0.26 | 1.24 | No | Yes | -1.20 | Yes | Yes | -21.4 | 21.05 | 7.48 | | -0.95 | 0.019 | Yes | |
| 21 | 8 | 32 | SAI | 0.48 | -1.88 | -1.79 | 0.09 | -1.57 | B2_ | 7.12 | -0.24 | 1,27 | No | Yes | -1.21 | Yes | Yes | -9.2 | 8.87 | 7.43 | 0.015 | -Q.98 | 0.019 | | |
| 21 | 11 | 37 | SAI | 0.5 | -7.49 | -7,4 | 0.09 | -7.18 | B2_ | 7.12 | -0.32 | 6.8 | No | Yes | -6.82 | Yes | Yes | -9.31 | 8.9 | 7.63 | 0.0005 | -6.51 | 0.0005 | | |
| 21 | | | SAI | 0.68 | -6.61 | -6.48 | 0.13 | -6.26 | B2 | 7.12 | -0.32 | 5.88 | No | Yes | -5.90 | Yes | Yes | -9.31 | 8.9 | 7.63 | 0.0005 | -5.59 | 0.0008 | | |
| 21 | | | SAI | 0.28 | -2.02 | -1.95 | 0.07 | -1.73 | B2 | 7,12 | -0.32 | 1.35 | No | Yes | -1.37 | Yes | Yes | -9.31 | 8.9 | 7.63 | 0.015 | -1.06 | 0.019 | | |
| 21 | 11 | 39 | SAL | 1.27 | -1.7 | -1.58 | 0.14 | -1.34 | B1 | 7,12 | -0.33 | 0.95 | No | Yes | -0.98 | Yes | Yes | -21.08 | 20.66 | 7,48 | | -0.66 | 0.023 | Yes | ł |
| 21 | 11 | 40 | SAI | 0.45 | -0.98 | -0.81 | 0,17 | -0.59 | B1 | 7.12 | -0.34 | 0.19 | No | Yes | -0.23 | Yes | Yes | -9.46 | 9.03 | 7.51 | 0.038 | 0.10 | 0.045 | | |
| 21 | 11 | 48 | SAI | 1.21 | -4.86 | -4.47 | 0.39 | <u>-4.25</u> | B1 | 7.12 | -0.31 | 3.88 | No | Yes | -3.89 | Yes | Yes | -9.36 | 8.96 | 7.73 | 0.005 | -3.59 | 0.0055 | | |
| 21 | 3 | 8 | SAI | 5.58 | -1.39 | -0,9 | 0.49 | -0.68 | B1 | 7.12 | -0.39 | 0.23 | No | Yes | -0.32 | Yes | Yes | -21.4 | 20.92 | 7.83 | | 0.06 | 0.045 | Yes | |
| 21 | 7 | 62 | SAI | 4.17 | -2.13 | -1.66 | 0.47 | -1,44 | 82 | 7.12 | -1.07 | 0.31 | No | Yes | -1.08 | Yes | Yes | -21.4 | 20.24 | 7.81 | | -0.02 | 0.045 | Yes | |
| 21 | 28 | 62 | SAL | 0.31 | -0.55 | -0.46 | 0.09 | -0.24 | Α | 5.32 | -0.27 | -0.09 | No | No | 0.12 | No | No | -9.96 | 9.6 | 5.63 | 0.043 | | | | Yes |
| 21 | 23 | 70 | SAI | 0,9 | -1.57 | -1.24 | 0.33 | -1.02 | Α | 5.32 | -0.12 | 0.84 | No | Yes | -0.68 | Yes | Yes | -21.4 | 21.19 | 5.87 | | -0.55 | 0.025 | Yes | |
| 21 | 6 | 77 | SAL | 1.31 | -1.33 | -1.2 | | -0.98 | B4 | 7.12 | -0.5 | 0.42 | No | Yes | -0.62 | Yes | Yes | -21.4 | 20.81 | 7.47 | | -0.13 | 0.041 | Yes | |
| 22 | 28 | 15 | SAI | 0.76 | 11.48 | 11.35 | 0.13 | 11.13 | Α | 5.32 | -0.49 | 10.58 | Yes | Yes | 10.77 | Yes | Yes | -21.4 | 20.82 | N/A | | -10.29 | | Yes | |
| 22 | | | SAI | 0.68 | -2.53 | -2.4 | 0.13 | -2.18 | Α | 5.32 | -0.49 | 1.63 | No | Yes | -1.82 | Yes | Yes | -21.4 | 20.82 | 5.98 | | -1.34 | 0.007 | Yes | |
| 22 | | | ŞAI | 0.66 | -2.04 | -1.86 | 0.18 | -1.64 | Α | 5.32 | -0.49 | 1.09 | No | Yes | -1.28 | Yes | Yes | -21.4 | 20.82 | 5.98 | | -0.80 | 0.013 | Yes | |
| 22 | 5 | 18 | SAI | 0.46 | -1.14 | -0.97 | 0.17 | -0.75 | B4 | 7.12 | -0.3 | 0.39 | No | Yes | -0.39 | Yes | Yes | -11.04 | 10.65 | 7.51 | 0.03 | -0.10 | 0.043 | | |
| 22 | 31 | 25 | SAI | 3.99 | -2.06 | -1.59 | 0.47 | -1.37 | A | 5.32 | -0.61 | 0.70 | No | Yes | -1.01 | Yes | Yes | -21.4 | 20.7 | 6.01 | | -0.41 | 0.03 | Yes | |
| 22 | 13 | 43 | SAI | 1.03 | -1.57 | -1.36 | 0.21 | -1.14 | B1 | 7.12 | -0.45 | 0.63 | No | Yes | -0.78 | Yes | Yes | -21.4 | 20.86 | 7.55 | | -0.34 | 0.031 | Yes | |
| 22 | 10 | 48 | SAI | 0.51 | -3.17 | -3.05 | 0.12 | -2.83 | B1 | 7.12 | -0.31 | 2.46 | No | Yes | -2.47 | Yes | Yes | -9.04 | 8.64 | 7.46 | 0.0083 | -2.17 | 0.0095 | | |
| 22 | 10 | 56 | SAI | 0.96 | -1.05 | -0.90 | 0.15 | -0.68 | B1 | 7.12 | -0.35 | 0.27 | No | Yes | -0.32 | Yes | Yes | -21.4 | 20.96 | 7,49 | | 0.02 | 0.045 | Yes | |
| 23 | 28 | 12 | SAI | 0.72 | -1.86 | -1.7 | 0.16 | -1.48 | A | 5.32 | -0.59 | 0.83 | No | Yes | -1.12 | Yes | Yes | -8.88 | 8.2 | 5.70 | 0.012 | -0.54 | 0.028 | | |
| 23 | 9 | 22 | SAI | 0.26 | -0.15 | -0.01 | 0.14 | 0.21 | B4 | 7.12 | -0.45 | -0.72 | No | No | 0.57 | No | No | -8.19 | 7.65 | 7,48 | 0.043 | | | | Yes |
| 23 | 14 | 24 | SAI | 0.59 | -1.87 | -1.64 | 0.23 | -1.42 | B4 | 7.12 | -0.14 | 1.22 | No | Yes | -1.06 | Yes | Yes | -21.4 | 21.17 | 7.57 | | -0.93 | 0.015 | Yes | |
| 23 | 16 | 24 | SAI | 0.35 | -1.39 | -1.28 | 0.11 | -1.08 | B4 | 7.12 | -0.24 | 0.76 | No | Yes | -0.70 | Yes | Yes | -21.4 | 21.07 | 7.45 | | -0.47 | 0.028 | Yes | |
| 23 | 25 | 37 | SAI | 2.41 | -1.44 | -0.96 | 0.48 | -0.74 | B4 | 7.12 | -0.59 | 0.09 | No | Yes | -0.38 | Yes | Yes | -21.4 | 20.72 | 7.82 | | 0.20 | 0.043 | Yes | |
| 23 | 45 | 37 | SAI | 1.65 | -1.76 | -1.27 | 0.49 | -1.05 | Α | 5.32 | -0.36 | 0.63 | No | Yes | -0.69 | Yes | Yes | -21.4 | 20.95 | 6.03 | | -0.34 | 0.028 | Yes | |
| 23 | 21 | 38 | SAI | 1.17 | -1.68 | -1.09 | 0.59 | -0.87 | B3 | 7.12 | -0.43 | 0.38 | No | Yes | -0.51 | Yes | Yes | -21.4 | 20.88 | 7.93 | | -0.09 | 0.04 | Yes | |
| 23 | 12 | 48 | IAS | 0.35 | -2.09 | -1.97 | 0.12 | -1.75 | B1 | 7.12 | -0.35 | 1.34 | No | Yes | -1.39 | Yes | Yes | -21.4 | 20.96 | 7,46 | | -1.05 | 0.018 | Yes | |
| 23 | 5 | 51 | SAI | 0.3 | -2.04 | -1.94 | 0.1 | -1.72 | B 1 | 7.12 | -0.32 | 1.34 | No | Yes | -1.36 | Yes | Yes | -21.4 | 20.99 | 7,44 | | -1.05 | 0.018 | Yes | |
| 23 | 7 | 52 | SAI | 3,44 | -1.61 | -1.11 | 0.5 | -0.89 | B1 | 7.12 | -0.15 | 0.68 | No | Yes | -0.53 | Yes | Yes | -21.4 | 21.16 | 7.84 | | -0.39 | 0.03 | Yes | |
| 23 | 5 | 55 | SAI | 0.51 | -1.82 | -1.72 | 0.1 | -1.5 | B1 | 7.12 | -0.22 | 1.22 | No | Yes | -1.14 | Yes | Yes | -9,66 | 9.35 | 7.44 | 0.015 | -0.93 | 0.015 | | |
| 23 | 32 | 55 | SAI | 0.94 | -1.22 | -1.02 | 0.2 | -0.8 | Α | 5.32 | -0.46 | 0.28 | No | Yes | -0.44 | Yes | Yes | -21.4 | 20.85 | 5.74 | | 0.01 | 0.043 | Yes | |
| 23 | 7 | 59 | 8AI | 0.98 | -1.49 | -1.17 | 0.32 | -0.95 | B1 | 7.12 | -0.24 | 0.65 | No | Yes | -0.59 | Yes | Yes | -21.4 | 21.07 | 7.66 | | -0.36 | 0.031 | Yes | |
| 23 | 3 | 69 | 8AI | 0.31 | -1.16 | -0.98 | 0.18 | -0.76 | B2 | 7.12 | -0.29 | 0.41 | No | Yes | -0.40 | Yes | Yes | -9.71 | 9.33 | 7.52 | 0.03 | -0.12 | 0.04 | | |
| 23 | 19 | 71 | 8AI | 1.22 | -1,99 | -1.59 | 0.4 | -1.37 | Α | 5.32 | -0.32 | 0.89 | No | Yes | -1.01 | Yes | Yes | -21.4 | 20.99 | 5.94 | | -0.70 | 0.02 | Yes | |
| 23 | 17 | 72 | 8AI | 1.75 | -1.01 | -0.60 | 0.41 | -0.38 | Α | 5.32 | -0.25 | 0.07 | No | Yes | -0.02 | Yes | Yes | -21.4 | 21.06 | 5.95 | | 0.22 | 0.043 | Yes | |

Enclosure 1 PG&E Letter DCL-00-008

| SG | R | С | IND | +Pt volt | From | То | L | UCT to TSH | W* Zone | W * L | BWT | UCT to BWT | UCT Below W* | UCT Below BWT | EOC 10 UCT | UCT Below TSH at EOC10 | W* Tube | inep Ext | W* Insp Dist | Flex W* L | CM LR | EOC10 UCT- BWT | OA LR | Deplug | Plug |
|----|----|----|-----|-------------|-------|-------|------|------------------|------------|--------------|-------|------------------|--------------------|---------------------|------------------|---------------------------------|------------|-------------------|--------------------|--------------|----------|----------------------|--------|--------|------|
| 23 | 6 | 77 | SAI | 0,39 | -1.6 | -1.50 | 0.1 | -1.28 | B4 | 7.12 | -0.34 | 0.88 | No | Yes | -0.92 | Yes | Yes | -21.4 | 20.97 | 7.44 | | -0.59 | 0.021 | Yes | |
| 23 | 21 | 83 | SAI | 1.39 | -1.23 | -0.90 | 0.33 | -0.68 | Α | 5.32 | -0.31 | 0.31 | No | Yes | -0.32 | Yes | Yes | -21.4 | 21 | 5.87 | | -0.02 | 0.043 | Yes | |
| 23 | 2 | 91 | 8AI | 0.61 | -0.94 | -0.59 | 0.35 | -0.37 | Α | 5.32 | -0.12 | 0.19 | No | Yes | -0.01 | Yes | Yes | -21.4 | 21.19 | 5.89 | | 0.10 | 0.043 | Yes | |
| 23 | 7 | 92 | SAI | 0,68 | -1.22 | -1.00 | 0.22 | -0.78 | Α | 5.32 | -0.38 | 0.34 | No | Yes | -0.42 | Yes | Yes | -21.4 | 20.93 | 5.76 | | -0.05 | 0.043 | Yes | |
| 23 | 8_ | 93 | SAI | 1.54 | -0.95 | -0.59 | 0.36 | -0.37 | Α | 5.32 | -0.12 | 0.19 | No | Yes | -0.01 | Yes | Yes | -21,4 | 21.19 | 5.90 | | 0.10 | 0.043 | Yes | |
| 24 | 7 | 4 | SAI | 1.02 | -1.36 | -1.15 | 0.21 | -0.93 | Α | 5.32 | -0.26 | 0.61 | No | Yes | -0.57 | Yes | Yes | -21.4 | 21.05 | 5.75 | | -0.32 | 0.031 | Yes | |
| 24 | 13 | 4 | SAI | 0.44 | -1.4 | -1.27 | 0.13 | -1.05 | Α | 5.32 | -0.41 | 0.58 | No | Yes | -0.69 | Yes | Yes | -9 .21 | 8.71 | 5.67 | 0.023 | -0.29 | 0.031 | | |
| 24 | 3 | 5 | SAI | 1.1 | -2 | -0.97 | 1.03 | -0.75 | Α | 5.32 | -0.34 | 0.35 | No | Yes | -0.39 | Yes | Yes | -21.4 | 20.97 | 6.57 | | -0.06 | 0.043 | Yes | |
| 24 | 2 | 10 | SAI | 0.61 | -1.61 | -1.5 | 0.11 | -1.28 | A | 5.32 | -0.1 | 1.12 | No | Yes | -0.92 | Yes | Yes | -21.4 | 21.21 | 5.65 | | -0.83 | 0.013 | Yes | |
| 24 | 15 | 10 | SAI | 0.47 | -1.07 | -0.8 | 0.27 | -0.58 | Α | 5.32 | -0.36 | 0.16 | No | Yes | -0.22 | Yes | Yes | -21.4 | 20.95 | 5.81 | | 0.13 | 0.043 | Yes | |
| 24 | 16 | 10 | SAL | 1.17 | -2.57 | -2.15 | 0.42 | -1.93 | Α | 5.32 | -0.48 | 1,39 | No | Yes | -1.57 | Yes | Yes | -21.4 | 20.83 | 5.96 | | -1.10 | 0.009 | Yes | |
| 24 | ω | 12 | SAI | 0.57 | -2.98 | -2.85 | 0.13 | -2.63 | Α | 5.32 | -0.3 | 2.27 | No | Yes | -2.27 | Yes | Yes | -21.4 | 21.01 | 5.86 | | -1.98 | 0,004 | Yes | |
| 24 | | | SAI | 1.2 | -2.61 | -2.42 | 0.19 | -2.2 | A | 5.32 | -0.3 | 1.84 | No | Yes | -1.84 | Yes | Yes | -21.4 | 21.01 | 5.86 | | -1.55 | 0.006 | Yes | |
| 24 | 26 | 24 | SAI | 3.94 | -2.42 | -1.77 | 0,65 | -1.55 | Α | 5.32 | -0.39 | 1.1 | No | Yes | -1.19 | Ю | No | -21.4 | 20.92 | 6.3 | | | | Yes | Yes |
| 24 | | | SAI | 0.57 | -0.49 | -0.38 | 0.11 | -0.16 | Α | 5.32 | -0.39 | -0.29 | No | No | 0.20 | No | No | -21.4 | 20.92 | 6.3 | | | | Yes | Yes |
| 24 | 24 | 26 | SAI | 0.55 | -1.93 | -1.77 | 0.16 | -1.55 | A | 5.32 | -0.43 | 1.06 | No | Yes | -1.19 | Yes | Yes | -9.69 | 9.17 | 5.7 | 0.0083 | -0.77 | 0.022 | | |
| 24 | 2 | 29 | SAI | 1.7 | -4.77 | -3.85 | 0.92 | -3.63 | B2 | 7.12 | -0.58 | 2.99 | No | Yes | -3.27 | Yes | Yes | -21.4 | 20.73 | 8.94 | | -2.70 | 0.007 | Yes | |
| 24 | | | SAI | 0.39 | -3.56 | -3.38 | 0.18 | -3.16 | B2 | 7.12 | -0.58 | 2.52 | No | Yes | -2.80 | Yes | Yes | -21.4 | 20.73 | 8.94 | | -2.23 | 0.0082 | Yes | |
| 24 | | | SAI | 0.49 | -2.48 | -2.14 | 0.32 | -1.92 | B2 | 7.12 | -0.58 | 1.28 | No | Yes | -1.56 | Yes | Yes | -21.4 | 20.73 | 8.94 | | -0.99 | 0.019 | Yes | |
| 24 | | | SAI | 0.23 | -2.08 | -2.03 | 0.05 | -1.81 | B2 | 7.12 | -0.58 | 1.17 | No | Yes | -1.45 | Yes | Yes | -21.4 | 20.73 | 8.94 | | -0.88 | 0.02 | Yes | |
| 24 | | | SAI | 0.32 | -2 | -1.87 | 0.13 | -1.65 | B2 | 7.12 | -0.58 | 1.01 | No | Yes | -1.29 | Yes | Yes | -21.4 | 20.73 | 8.94 | | -0.72 | 0.022 | Yes | |
| 24 | 6 | 33 | SAI | 0.4 | -2.87 | -2.75 | 0.12 | -2.53 | B2 | 7.12 | -0.14 | 2.33 | No | Yes | -2.17 | Yes | Yes | -10.82 | 10.59 | 7,46 | 0.008 | -2.04 | 0.009 | | |
| 24 | 13 | 34 | SAI | 0.4 | -0.14 | -0.01 | 0.13 | 0.21 | B2 | 7.12 | -0.34 | -0.61 | No | No | 0.57 | No | No | -9.42 | 8,99 | 7.47 | 0.043 | | | | Yes |
| 24 | 4 | 35 | SAI | 1.15 | -1.79 | -1.34 | 0.45 | -1.12 | 81 | 7.12 | -0.24 | 0.82 | No | Yes | -0.76 | Yes | Yes | -21.4 | 21.07 | 7.79 | | -0.53 | 0.025 | Yes | |
| 24 | 6 | 35 | SAI | 0.91 | -2.3 | -2.14 | 0.16 | -1.92 | B1 | 7.12 | -0.31 | 1.55 | No | Yes | -1.56 | Yes | Yes | -21.4 | 21 | 7.5 | | -1.26 | 0.015 | Yes | |
| 24 | 5 | 36 | SAI | 0.22 | -1.53 | -1.44 | 0.09 | -1.22 | B1 | 7.12 | -0.17 | 0.99 | No | Yes | -0.86 | Yes | Yes | -8.45 | 8.19 | 7.43 | 0.019 | -0.70 | 0.022 | | |
| 24 | 5 | 37 | SAI | 0.36 | -4.58 | -4.43 | 0.15 | -4.21 | B1 | 7.12 | -0.43 | 3.72 | No | Yes | -3.85 | Yes | Yes | -21.4 | 20.88 | 8.02 | | -3.43 | 0.008 | Yes | |
| 24 | | | SAI | 1.06 | -4.4 | -3.87 | 0.53 | -3.65 | B1 | 7.12 | -0.43 | 3.16 | No | Yes | -3.29 | Yes | Yes | -21.4 | 20.88 | 8.02 | | -2.87 | 0.0075 | Yes | |
| 24 | 7 | 38 | SAI | 3.04 | -7.16 | -6.65 | 0.51 | -6.43 | | 7.12 | -0.35 | 6.02 | No | Yes | -6.07 | Yes | Yes | -21.4 | 20.96 | 8.58 | <u> </u> | -5.73 | 0.0009 | Yes | |
| 24 | | | SAI | 2.16 | -4.73 | 4 | 0.73 | -3.78 | B1 | 7.12 | -0.35 | | No | Yes | -3.42 | Yes | Yes | -21.4 | 20.96 | 8.58 | | -3.08 | 0.007 | Yes | |
| 24 | 13 | 8 | SAI | 1.35 | -1.91 | -1.48 | 0.43 | -1.26 | B2 | 7.12 | -0.28 | 0.92 | No | Yes | -0.90 | Yes | Yes | -21.4 | 21.03 | 7.77 | | -0.63 | 0.023 | Yes | |
| 24 | 29 | 42 | SAI | 0.52 | -0.23 | -0.11 | 0.12 | 0.11 | B4 | 7.12 | -0.38 | -0.55 | No | No | 0.47 | No | No | -10.56 | 10.09 | 7.46 | 0.043 | | | | Yes |
| 24 | 26 | 45 | SAI | 0.52 | -3.76 | -3.61 | 0.15 | -3.39 | B4 | 7.12 | -0.36 | 2.97 | No | Yes | -3.03 | Yes | Yes | -10.52 | 10.07 | 7.49 | 0.0025 | -2.68 | 0.0033 | | |
| 24 | 31 | 45 | SAI | 1.59 | -2.09 | -1.57 | 0.52 | -1.35 | A | 5.32 | -0.34 | 0.95 | No | Yes | -0.99 | Yes | Yes | -21.4 | 20.97 | 6.06 | | -0.66 | 0.021 | Yes | |
| 24 | 20 | 47 | SAI | 0.55 | -1.7 | -1.54 | 0.16 | -1.32 | B2 | 7.12 | -0.24 | 1.02 | No | Yes | -0.96 | Yes | Yes | -21.4 | 21.07 | 7.5 | <u> </u> | -0.73 | 0.021 | Yes | |
| 24 | 5 | 53 | SAI | 1.22 | -2.03 | -1.62 | 0.41 | -1.4 | B1 | 7.12 | -0.32 | 1.02 | No | Yes | -1.04 | Yes | Yes | -20.86 | 20.45 | 7.75 | | -0.73 | 0.021 | Yes | |
| 24 | 25 | 64 | SAI | 1.54 | -1.62 | -1.16 | 0.46 | -0.94 | B4 | 7.12 | -0.31 | 0.57 | No | Yes | -0.58 | Yes | Yes | -21.4 | 21 | 7.8 | | -0.28 | 0.02 | Yes | |

| Column - Table 1 | Legend and Notes for Table 1 |
|-------------------------|---|
| SG | Steam generator |
| R | Row |
| C | Column |
| IND | Plus point indication. SAI is single axial indication. Some tubes have multiple non-parallel SAI. |
| +P Volt | Peak voltage from Plus Point coil |
| From - To | Elevation (in.) of lower crack tip (from) to upper crack tip (to), relative to the hot leg top of tubesheet (TSH). |
| L | Length of crack (in.) |
| UCT to TSH | Elevation (in.) of the upper crack tip (UCT) relative to TSH, including ΔNDE _{CT-TTS} (Plus Point NDE uncertainty on locating the crack tip relative to the TTS). None of the indications extended above the top of tubesheet. |
| W* Zone | W⁺ tubesheet zone based on crack location. |
| W*L | W* length based on W* Zone, plus ∆NDE _W (NDE uncertainty in measuring the W* depth). |
| BWT | Bottom of the WEXTEX transition (in.), measured by bobbin relative to TSH. |
| UCT to BWT | Distance (in.) from the upper crack tip (UCT) to BWT, minus \(\Delta NDE_{CT-BWT} \) (Plus Point NDE uncertainty on locating the crack tip relative to the BWT). |
| UCT below W* | if the UCT is located below the W* length, then the tube is a W* tube. Any type of degradation below the W* length is acceptable. |
| UCT below BWT | If the UCT is located below BWT, then the tube is a W* candidate. |
| EOC 10 UCT | UCT location (in.) relative to TSH at the end of the next operating cycle, EOC 10, based on growing the UCT at 0.25 in./EFPY. Unit 2 Cycle 10 is projected to be 1.44 EFPY. |
| UCT below TSH at EOC 10 | If the UCT is below TSH at EOC 10, a free span indication is precluded and the tube is a W* candidate. |
| W* Tube | If the UCT is below BWT and the UCT is below TSH at EOC 10, then the tube is a W* tube. If the UCT is located below the W* length, then the tube is a W* tube. |
| Insp Ext | Inspection extent of Plus Point relative to TSH (in.). |
| W* Insp Dist | W* inspection distance (in.). This is the +Point inspection extent relative to BWT. The W* inspection distance below BWT is equal to the Plus Point inspection extent below TSH, plus measured distance from BWT to TSH, plus bobbin NDE uncertainty in locating BWT relative to TSH. The W* inspection distance must be greater than or equal to the flexible W* length. |
| Flex W* L | Flexible W* length relative to BWT (in.), equal to W* Length + ΣCl _i (total axial crack length) + N _{CL} *ΔNDE _{CL} (number of indications times Plus Point NDE uncertainty with measuring length of axial cracks) + N _{CL} *ΔCG (number of indications times crack growth allowance from prior cycle tube integrity assessment, 0.25 in./EFPY) |
| CM LR | Condition monitoring SLB leak rate at EOC 9 conditions, gpm at room temperature, based on distance of UCT to BWT using Figure 6.4-3 of WCAP-14797 Rev 1. No accident leakage is assigned to an indication with an UCT below the W* length. No accident leakage is assigned to an indication in a tube deplugged and returned to service. |
| EOC 10 UCT to | Distance of UCT to BWT (in.) at EOC 10 for operational assessment, based on growing the UCT at the latest updated |

| Column - Table 1 | Legend and Notes for Table 1 |
|------------------|---|
| BWT | industry combined 95% growth rate (0.24 in /EFPY). |
| OA LR | Operational assessment leak rate at EOC 10 conditions, gpm at room temperature, based on distance of UCT (at EOC 10) to BWT using Figure 6.4-3 of WCAP-14797 Rev 1. |
| Deplug | Tube was deplugged in 2R9. |
| Plug | Tube was plugged in 2R9. |

Table 2

DCPP Unit 2 Steam Line Break Leak Rates for Alternate Repair Criteria

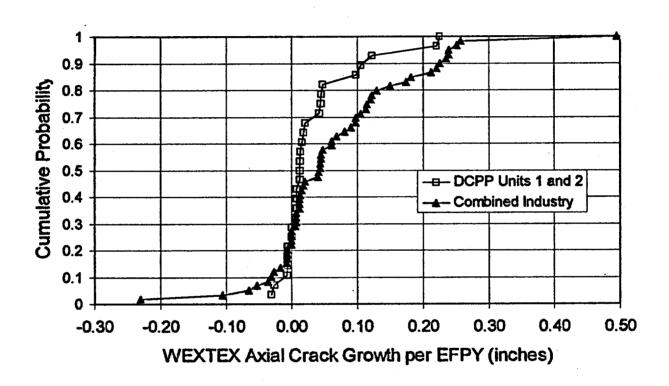
| EOC 9 Condition Monitoring Leak Rate (gpm at room temperature) | SG 2-1 | SG 2-2 | SG 2-3 | SG 2-4 |
|--|--------|--------|--------|--------|
| W* ARC | 0.1170 | 0.0383 | 0.1000 | 0.1468 |
| Voltage-Based ARC | 0.0627 | 0.0244 | 0.0312 | 0.3215 |
| Aggregate ARC | 0.1797 | 0.0627 | 0.1312 | 0.4683 |

| EOC 10 Operational Assessment Leak Rate (gpm at room temperature) | SG 2-1 | SG 2-2 | SG 2-3 | SG 2-4 |
|--|--------|--------|--------|--------|
| W* ARC | 0.2818 | 0.1765 | 0.6330 | 0.4799 |
| Voltage-Based ARC | 0.2349 | 0.1267 | 0.1500 | 1.2448 |
| Aggregate ARC | 0.5167 | 0.3032 | 0.783 | 1.7247 |

Table 3

DCPP Unit 2 Cycle 10 Growth Rate for Axial PWSCC in W* Region

Cumulative Probability Distribution for Growth of Axial PWSCC Indications in W* Region



SPECIAL REPORT 00-01

90 DAY REPORT GENERIC LETTER 95-05 VOLTAGE-BASED REPAIR CRITERIA DIABLO CANYON POWER PLANT UNIT 2 NINTH REFUELING OUTAGE