

Presentations for July 26, 2018 Public Meeting Regulatory Improvements for Advanced Reactors

In order of discussion, the meeting included the following topics and presentations

- 1) NRC Slides
 - Opening / Outline
 - Update on NRC Activities
 - Licensing Modernization (see #2 for industry slides)
 - Future Stakeholder Meetings
- 2) Licensing Modernization
- 3) Molten Salt Reactor Technology Working Group (FLIBE)
- 4) INL/Framatome/ANL Natural Convection Shutdown Heat Removal





Public Meeting on Possible Regulatory Process Improvements for Advanced Reactor Designs

July 26, 2018



Telephone Bridge (888) 793-9929 Passcode: 7231346



Public Meeting

- Telephone Bridge (888) 793-9929
 Passcode: 7231346
- Opportunities for public comments and questions at designated times





Outline

Introductions
 Update on NRC Activities
 Licensing Modernization Project
 Technology Working Groups - MSR

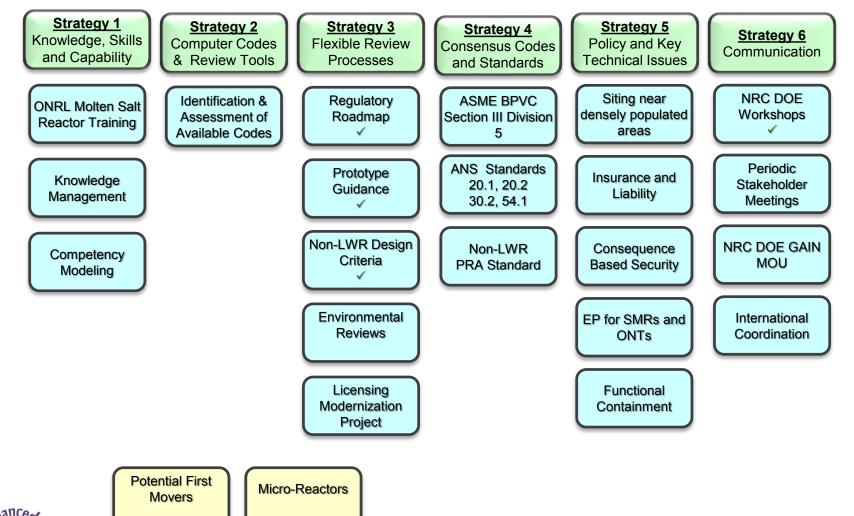
Prioritization Considering O&M
 Natural Convection Shutdown Heat Removal
 Policy Issues, Future Meetings, Public Discussion





Implementation Action Plans

Protecting People and the Environment





Strategy 2 – RES Contracts

- Reactor Kinetics and Criticality
- □ Fuel Performance
- Thermal Hydraulics
- Severe Accident Phenomena
- Offsite Consequences
- Materials Research





NRC Staff Technology Training Fuel Qualification TRISO (limited scope topical) • Metallic (legacy data) ○ MSRs Policy Resolution, Guidance Development Environmental Reviews □ RTR Guidance (MSR) □ ASME Section III Division 5

Licensing Micro Reactors





NRO Contracts - Continued

- Fuel Cycle
 - Fuel facilities
 - High level waste
- Security
- MC&A
- Technology specific barrier/consequence estimates

 $ST = MAR \cdot DR \cdot ARF \cdot RF \cdot LPF \tag{1}$

where ST is the source term (Bq), MAR is the total available material-at-risk (Bq), DR is the damage ratio (no units), ARF is the airborne release fraction (no units), RF is the respirable fraction (no units), and LPF is the leak path factor (no units).





Break Meeting/Webinar will begin shortly

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Licensing Modernization

□ Southern Company Presentation





Licensing Modernization

Protecting People and the Environment

□ Public Meeting – August 21, 2018

□ Revision to LMP Guidance (NEI 18-04)

Resolution of Questions/Comments

🖵 DG 1353

- Endorsing LMP Guidance
- Informing Content of Applications

□ September 30, 2018 – Draft Material to ACRS

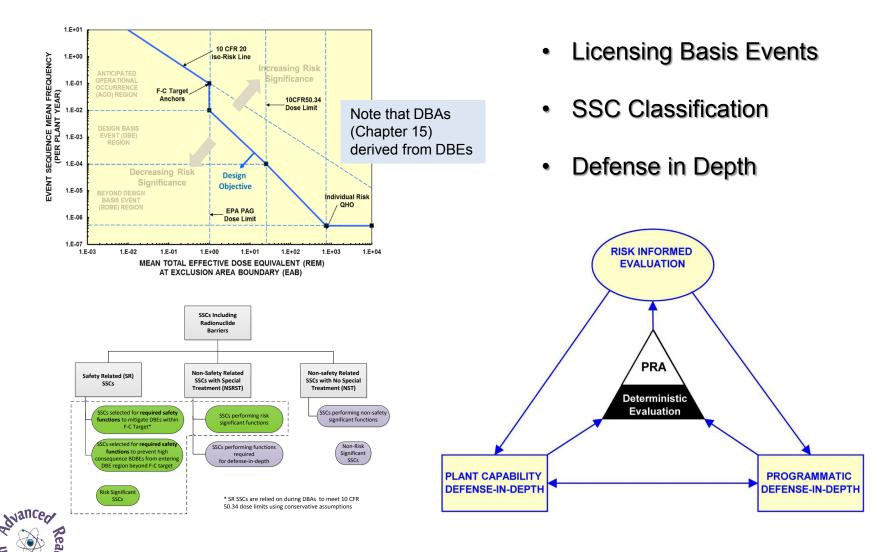
- October 30, 2018: ACRS Subcommittee
- o December 6-8, 2018: ACRS Full Committee
- o December 21, 2018: Issue DG 1353
- o Early 2019: Commission paper





Licensing Modernization

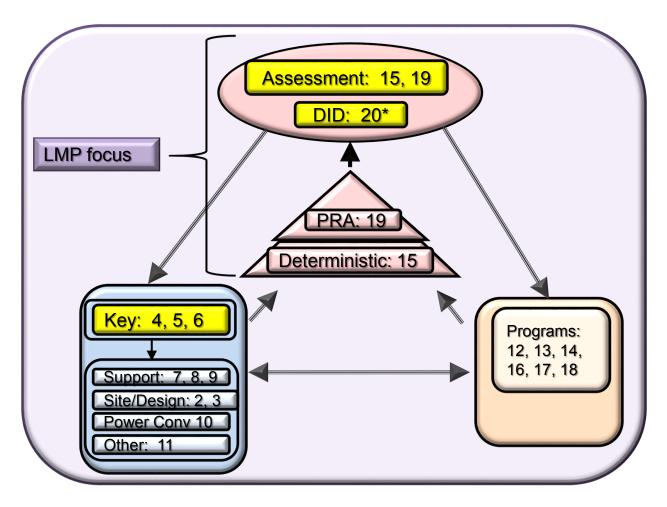
Protecting People and the Environment





DG-1353 / SECY Paper

Informing Scope and Level of Detail in Applications







Related Commission Paper

- □ LBE categories AOO, DBE, BDBE and DBAs
- F/C Target Figure with demarcations between event categories, cutoff
- □ Aggregate safety goals
- SSC Classification scheme
- Defense in Depth assessments
- □ Scope and Depth of Applications
 - Focus on Fundamental Safety Functions
 - Potential radiological consequences
 - Mechanistic source term
 - Risk-Informed approach for key systems and support systems
 - Performance-based approach





Technology Working Groups

Molten Salt Reactors
 FLIBE Presentation





Lunch Meeting/Webinar will begin at 1:00pm

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Prioritization – O&M







Break Meeting/Webinar will begin shortly

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Natural Convection Shutdown Cooling **Protecting People and the Environment**

□ Framatome





Future Stakeholder Meetings Topics ?

| | TWG – Fast Reactors, Metallic Fuel | |
|---------|--|--|
| Sept 13 | Prioritization of Issues Considering Capital Costs | |
| | Seismic Isolators | |
| | Licensing Modernization/DG 1353 | |
| | | |
| Oct 25 | TWG - HTGRs | |
| | Licensing Modernization/DG 1353 | |
| | | |
| | | |
| | | |
| Dec 13 | | |
| | | |
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| | | |



ACRS Schedule (tentative)

Protecting People and the Environment

| Date | Committee | Topic |
|---------|-----------|---------------|
| June 19 | Sub | RIPB Guidance |
| Aug 22 | Sub | EP Rulemaking |
| Oct | Full | EP Rulemaking |
| Oct 30 | Sub | RIPB Guidance |
| Dec 6 | Full | RIPB Guidance |
| 2019 | | ?? |





Public Comments / Questions





Licensing Modernization Project (LMP) Guidance Document Update

Jason Redd, PE

July 26, 2018



LMP Guidance Document Introduction



- The LMP Guidance Document represents a framework for the efficient licensing of advanced non-light water reactors (non-LWRs).
- It is the result of the LMP led by Southern Company and cost-shared by the U.S. Department of Energy (DOE).
- The LMP prepared this document for establishing licensing technical requirements to facilitate <u>risk-informed and performance-based (RIPB) design and licensing of</u> <u>advanced non-LWRs</u>.
- Such a framework acknowledges enhancements in safety achievable with advanced designs and reflects current states of knowledge regarding safety and design innovation, creating an opportunity for reduced regulatory complexity with increased levels of safety.

LMP Guidance Document Recent Activities



- April First table top demonstration of the LMP RIPB processes on a current advanced non-LWR design completed. Lessons learned and best practices identified during this demonstration were incorporated into the LMP Guidance Document.
- June 5-6 NRC Public Workshop discussing LMP Guidance Document (Working Draft M). [ML18150A344 – LMP Guidance Document][ML18177A462 – meeting summary]
- June 18 LMP members delivered a training opportunity on the LMP RIPB process for NRC Staff at the White Flint offices.
 - The Staff posed many excellent questions during this training opportunity and provided constructive feedback which is being addressed in ongoing updates to the LMP Guidance Document.

LMP Guidance Document Recent Activities



- June 19 The LMP Guidance Document (Working Draft M) was reviewed and discussed by the Advisory Committee on Reactor Safeguards (ACRS) Future Plants Subcommittee.
 - As with the Staff, the ACRS FPS engaged in a robust discussion of the LMP Guidance Document and provided feedback to both the LMP team and the NRO Staff. Likewise, this feedback is being addressed in ongoing updates to the LMP Guidance Document.

LMP Guidance Document Upcoming Meetings and Milestones



- August 21 NRC Public Workshop on LMP Guidance Document. Agenda focused on resolution of June NRC and ACRS comments.
- September 13 NRC advanced reactors stakeholder meeting. LMP team to provide update on LMP progress to date.
- October 30 ACRS Future Plants Subcommittee meeting to review and discuss the working draft of the LMP Guidance Document, draft NRC SECY, and draft NRC Regulatory Guide addressing the LMP Guidance Document.
- December 6-8 Full ACRS meeting to review and discuss the working draft of the LMP Guidance Document, draft NRC SECY, and draft NRC Regulatory Guide addressing the LMP Guidance Document.

LMP Guidance Document Upcoming Opportunities for Industry and Public Participation



- August 21 NRC Public Workshop on LMP Guidance Document. Agenda focused on resolutions of June NRC and ACRS comments.
 - Proposed comment resolutions will be shared with NEI ARRTF in advance; a full revision of the LMP Guidance Document will not be performed for this workshop.
- September 9 Updated LMP Guidance Document working draft incorporating NRC and ACRS FPS feedback distributed to NEI ARRTF for two week review and comment cycle supporting September 28 submittal of updated document to ACRS FPS Chair for review.
- TBD By 2Q19 we expect between four and six designs to have exercised the LMP RIPB processes on their designs to obtain potential insights. <u>The LMP team is</u> <u>interested in demonstrating the LMP RIPB processes with additional vendors</u>.
- Anytime The LMP team always welcomes questions, comments, and feedback. Please contact me at jpredd@southernco.com or 205-992-6435.

Questions?

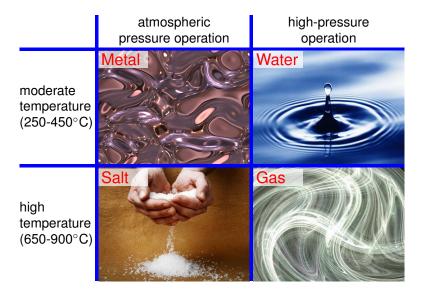


Molten-Salt Reactor Technology

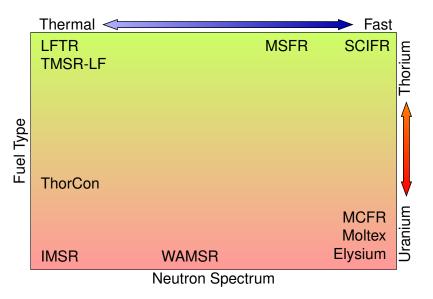
Matthew Lish Flibe Energy

Nuclear Regulatory Commission July 26, 2018

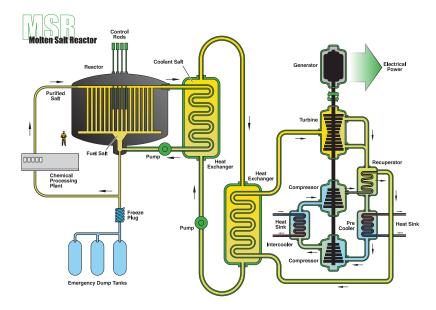
Coolant Choices for a Nuclear Reactor



Molten Salt Reactor Design Space



Gen-4 Molten Salt Reactor Concept



The MSRE successfully operated for over 20,000 hours, from 1965-1969

the part of the second second second second

COOLANT SALT SYSTEM



-7.2 MW

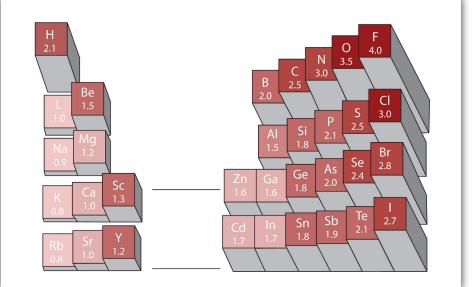
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6000 FULL POWER

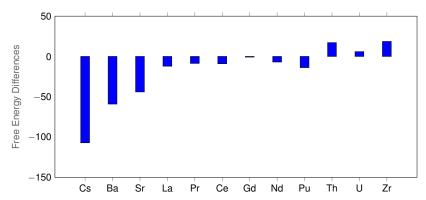
UNEAR POWER

-



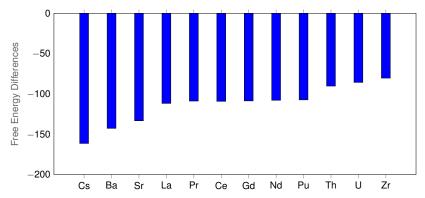
Oxygen is very electronegative and forms strong bonds with metals, however fluorine, and only fluorine, is even more electronegative.

Free energy differences (oxides/chlorides) at 1000 K



Alkaline fission products are stable in chloride salt, and will not volatilize if introduced to air. Actinides may form oxides in air, but will not volatilize.

Free energy differences (oxides/fluorides) at 1000 K



In fluoride form all actinides and alkaline fission products, most notably cesium and strontium, remain in fluoride salt form in the presence of air, do not form volatile species. In molten salts, the first barrier to fission product release is the chemical form of the fuel salt, rather than the mechanical integrity of the fuel pin.

MSR Material Compatibility



Through proper material choices, molten-salt reactors can operate in a state of fundamental chemical equilibrium. This was demonstrated by the MSRE with FLiBe salt, graphite, and Hastelloy-N alloy. This is very different than the environment inside PWRs.

Conclusions

- MSRs feature circulating fuel dissolved in stable form in the coolant.
- Molten salts chemically bind most fission products, but do not retain noble gas fission products at all, thus the standard operating approach for noble gases should bound potential accidents.
- Properly chosen materials operate in chemical equilibrium with the coolant without stored energy terms or driving forces for radionuclide release.
- Off-gas treatment and sequestration is of paramount importance.

Regulatory Framework Development Passive Heat Removal

Jim Kinsey Idaho National Laboratory

July 26, 2018



dov.



Background



- Reactor technologies and associated designs address a set of fundamental safety functions
- The LWR-based operating fleet generally relies on a group of interrelated active systems for the heat removal function, as reflected in the GDCs:
 - Residual heat removal
 - Emergency core cooling
 - Containment heat removal
 - Cooling water systems



NRC Advanced Reactor Policy (2008 - Excerpts)

Commission policy encourages:

- Use of inherent or passive means of reactor shutdown and heat removal
- Longer time constants
- Simplified safety systems which reduce required operator actions
- Minimizing the potential for severe accidents and their consequences
- Safety-system independence from balance of plant
- Incorporation of defense-in-depth philosophy by maintaining multiple barriers against radiation release and by reducing the potential for consequences of severe accidents
- Using existing technology or technology that can be satisfactorily established by commitment to a suitable technology development program



Regulatory Framework - Areas of Focus

The "Regulatory Framework" consists of four key parts that are the areas of focus:

- What are the rules?
 - 1) Establish Commission policy on advanced non-LWR topics
 - 2) Develop adaptations and updates to NRC's existing LWR-based rules and regulatory guidance
- What are the technology-specific technical requirements for implementing those rules?
 - 3) Define requirements based on testing and R&D (fuel performance, high temperature materials, heat removal, etc.)
- What is the process for predictable and timely NRC review of a license application?
 - 4) Establish method for incremental and frequent NRC feedback on specific technology development and early design efforts ("staged licensing review")

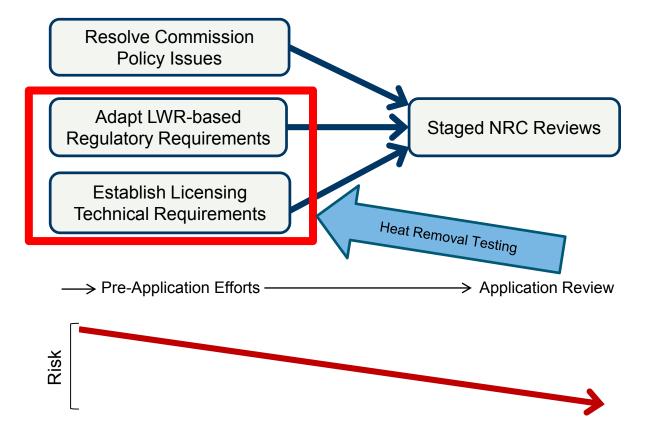


Passive Heat Removal System Testing

- NRC's Non-Light Water Reactor Near Term Implementation Action Plans highlight the need to establish "Decision Criteria" as a key part of the framework
 - Criteria must be established for non-LWRs that allow the NRC to reach a safety, security, and environmental finding for a particular technology and design.
- Today's presentation material will summarize DOE Advanced Reactor Technology Program testing underway to gather representative performance data to inform passive heat removal system design and modeling efforts
 - Core heat removal path to Ultimate Heat Sink
 - Passive system doesn't rely on active components
 - Informs reactor developers, future license applicants, and NRC



Support of Regulatory Framework Development



Idaho National Laboratory

framatome

Reactor Cavity Cooling System

Matthew Miller

Regulatory Process Improvements for Advanced Reactor Designs

NEI - Washington, DC. July 26, 2018



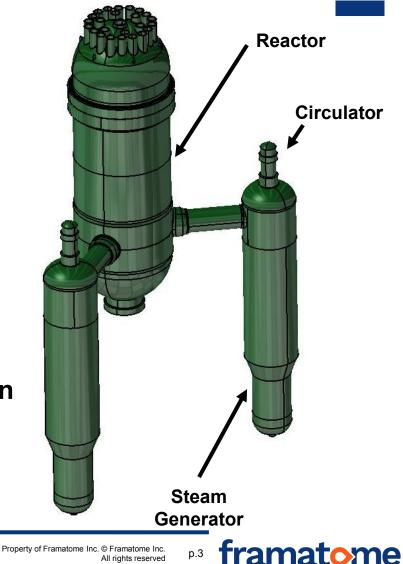
Overall SC-HTGR Description

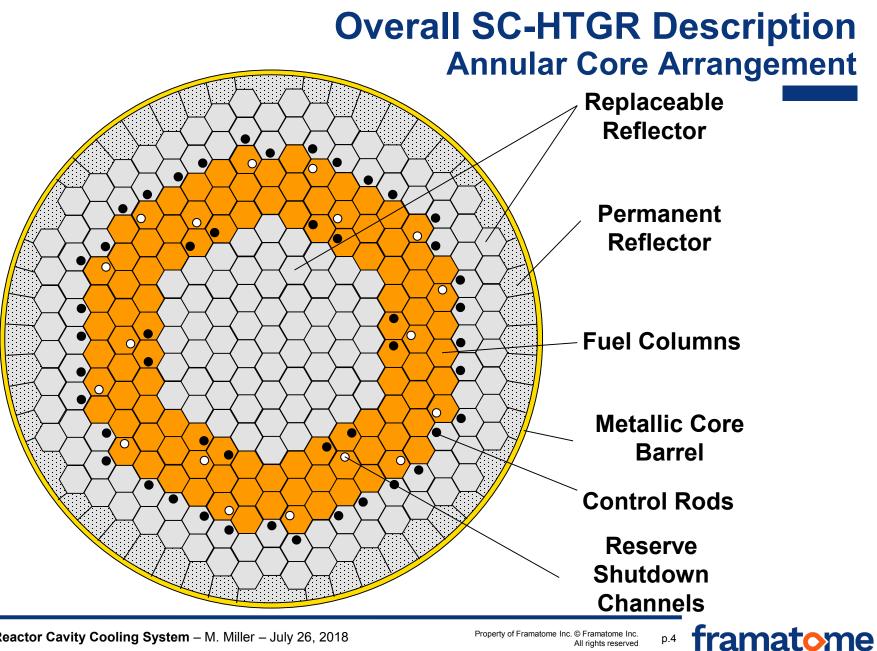
- SC-HTGR RCCS Description
- SC-HTGR RCCS Pre-Conceptual Performance
- Importance of RCCS R&D
- Conclusions



Overall SC-HTGR Description Key Features

- Prismatic block annular core
- Conventional steam cycle
- Modular reactors
- Inherent safety characteristics
 - Passive decay heat removal
 - Large thermal inertia
 - Negative reactivity feedback
- Minimal reliance on active safety systems
- Sized to minimize steam production cost (625 MWt)
- Fully embedded reactor building





Reactor Cavity Cooling System – M. Miller – July 26, 2018

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Overall SC-HTGR Description Passive Heat Removal Considerations

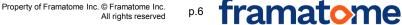
Passive cooling is a key characteristic of modular HTGRs

- Loss of forced circulation
- Loss of all coolant
- No power or system actuation required
- Passive cooling capability is inherently determined by fundamental HTGR design characteristics
 - Reactor geometry
 - Reactor materials
 - Reactor power level
 - Reactor operating temperature
 - Passive reactor cavity cooling
- These fundamental characteristics must be established early in the design process (before detailed safety analyses are available)

p.5

Overall SC-HTGR Description SC-HTGR Passive Cooling Design

- SC-HTGR is in Conceptual Design phase
- Scoping evaluations of passive cooling design important at this design stage
- Depressurized Loss of Forced Circulation (DLOFC) is used as representative limiting event (aka "Depressurized Conduction Cooldown" or DCC)
 - Maximum fuel temperature
 - Maximum vessel temperature
- Scoping criteria established to screen results
- Results (fuel temperatures) depend primarily on reactor configuration, power level, and initial conditions
- RCCS important to maintaining vessel and concrete temperatures



Overall SC-HTGR Description

Reactor Cavity Cooling System Design Considerations

- Modular HTGR designers have considered a variety of RCCS configurations
 - Air-cooled
 - Water-cooled (various different concepts)
 - Natural circulation
 - Active cooling
- Various tradeoffs must be addressed in selecting configuration
 - Functionality (normal operation and accidents)
 - Robustness
 - Passive cooling duration (unlimited or "n" days)
 - Physical interfaces
 - External hazards
 - Constructability and cost

Framatome SC-HTGR utilizes a water cooled RCCS design.

p.7



- Overall SC-HTGR description
- SC-HTGR RCCS Description
- SC-HTGR RCCS Pre-Conceptual Performance
- Importance of RCCS R&D
- Conclusions



SC-HTGR RCCS Description SC-HTGR RCCS System Functions

Safety Functional Requirements

- Maintain reactor pressure vessel mean wall temperatures within ASME limits during all DBE
- Maintain reactor cavity concrete temperatures within acceptable limits during all DBE

Normal Operation Functional Requirements

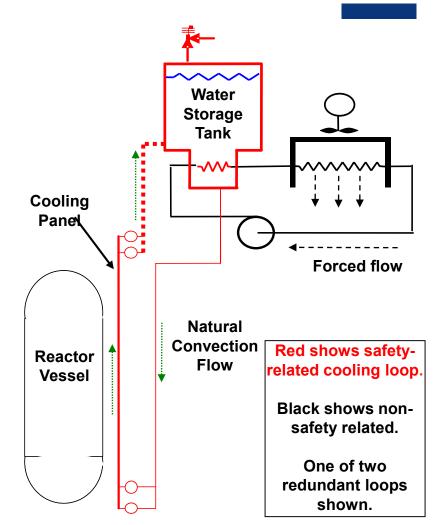
- Maintain acceptable reactor pressure vessel mean wall temperatures limits during power operation, startup and shutdown, and AOOs
- Maintain acceptable reactor cavity concrete temperatures during power operation, startup and shutdown, and AOOs
- Cooling vessel supports at building interface
 - Local thermal protection strategy being developed as design progresses
 - Vessel supports are not at hottest location
 - RCCS role for supports still to be defined

p.9

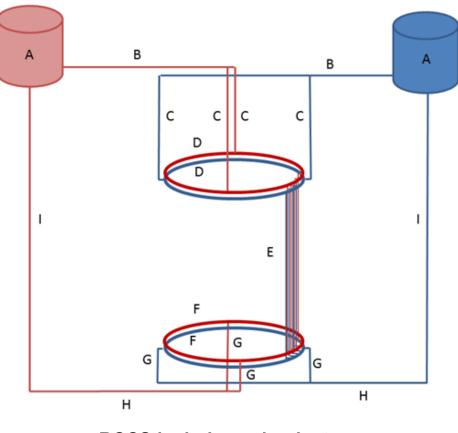
SC-HTGR RCCS Description SC-HTGR RCCS Concept Overview

Reactor Cavity Cooling System

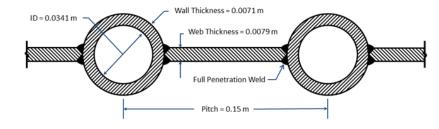
- Safety-related heat removal system
- Passive cooling of vessel and surrounding cavity (operates continuously)
- Active cooling of water storage tank during normal operation (non-safety)
- Initial RCCS analysis and design focused on cavity natural circulation loop
 - Building integration
 - Component sizing
 - Performance evaluation



SC-HTGR RCCS Description SC-HTGR RCCS Design Elements



RCCS includes redundant and separate loops

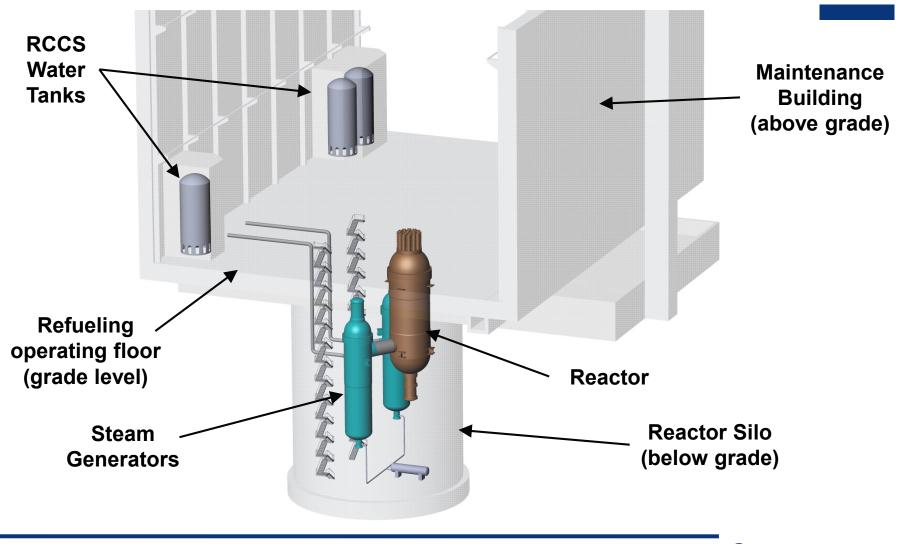


RCCS panel collects heat and transfers it to water loop

(panel cross section shown)



SC-HTGR RCCS Description Single Reactor Module - Arrangement



SC-HTGR RCCS Description Operating Modes

Normal System Operation

- Two loop operation
- Nominal heat load (~1.4 MWt)
- Natural circulation in cavity loop
- Active cooling of water tanks
- Active Accident System
 Operation
 - Two loop operation
 - Variable heat load (~2.1 MWt max.)
 - Natural circulation in cavity loop
 - Active cooling of water tanks

Passive Accident System Operation

- Two loop operation
- Variable heat load (~2.1 MWt max.)
- Natural circulation in cavity loop
- Evaporation from water tanks
- DBA System Operation
 - Single loop operation
 - Variable heat load (~2.1 MWt max.)
 - Natural circulation in cavity loop
 - Evaporation from water tanks



SC-HTGR RCCS Description Key RCCS Technical Requirements

- Passive cooling during accidents
- Water heat sink cooling
 - Active secondary cooling during normal operation
 - Evaporation cooling during accidents (assume active cooling and power supply not available)
- No change in component state for accident cooling
 - Cavity cooling natural circulation for normal operation and accidents
- Redundant independent loops
- Required water inventory refill interval
 - ♦ Single loop operation: ≥ 7 days
 - ◆ Two loop operation : ≥ 14 days
- Continuous performance monitoring
- Must accommodate reactor building structural interfaces





- Overall SC-HTGR description
- SC-HTGR RCCS Description
- SC-HTGR RCCS Pre-Conceptual Performance
- Importance of RCCS R&D
- Conclusions



SC-HTGR RCCS Pre-Conceptual Performance RCCS Thermodynamic States

Normal operation

- Subcooled natural circulation
- Steady system temperatures (controlled by active tank cooling)
- Initial heatup conditions
 - Subcooled natural circulation, but
 - Gradually increasing loop temperatures

Approaching saturation conditions

- Downcomer and lower riser subcooled
- Saturation reached in heated riser panels
- Boiling occurs in hot part of riser
- Very low quality two phase natural circulation

- Saturation conditions
 - Tank at saturation condition
 - Downcomer single phase flow
 - Low quality two phase natural circulation
- Tank empty
 - Circulation blocked (stagnant loop)
 - Downcomer single phase
 - "Pool" boiling in hot leg
 - Water gradually boils out of panels
- Refill water tank (stagnant loop)
 - Water goes down downcomer, collects in bottom of loop, rises in hot leg riser and panel inlet
 - Flashing occurs when water reaches heated sections
 - Depending on geometry, may have to purge trapped gases



SC-HTGR RCCS Pre-Conceptual Performance RCCS Operating Modes and TD States

| | | Thermodynamic State | | | | | |
|-----------|---|---------------------|-------------------|--------------------------------------|--------------------------|---------------|-------------------------|
| | | Normal Operation | Initial Heatup | Approach Saturation Conditions | Saturation Conditions | Tank Empty | Refill Empty Loop |
| de | Normal Plant Operation | | | | | | |
| g Mode | Active Accident System Operation | | | | | | |
| Operating | Passive Accident System Operation | | | | | | |
| ŎĎ | DBA System Operation | | | | | | |
| | System Dryout and Long-Term Recovery (outside design envelope) | | | | | | |



SC-HTGR RCCS Pre-Conceptual Performance Preliminary Performance Characteristics

For subcooled operation

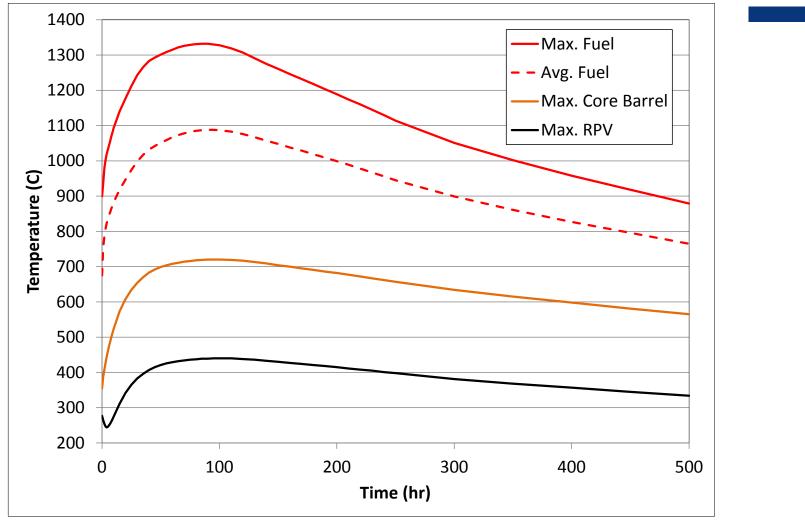
- Cold leg ΔP is ~80% of total ΔP
- System ΔT is ~10-20°C

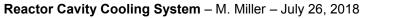
For saturated operation

- Cold leg ΔP is less than 50% of total ΔP
- System return quality is < 1% (but still significant void fraction)
- Stability not expected to be concern for overheating/burnout
- Dynamic structural loading must be addressed
- Panel performance (conduction heat transfer)
 - Large temperature variations for single loop operation (especially w/ SS)
 - RPV cooling not particularly sensitive to panel temperature variations
 - Thermal stresses in panel are detailed design challenge to be addressed
 - Impact of large panel temperature variations on concrete surfaces and necessary thermal protection still to be evaluated



SC-HTGR RCCS Pre-Conceptual Performance Nominal DLOFC Results

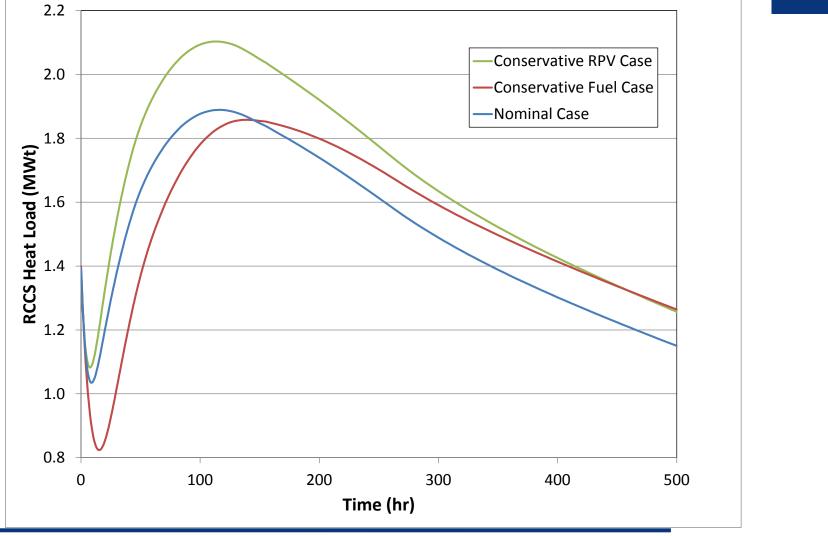




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SC-HTGR RCCS Pre-Conceptual Performance RCCS Heat Load During DLOFC



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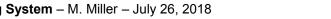
SC-HTGR RCCS Pre-Conceptual Performance Summary of Results

| Component | Nominal Case | Conservative Case* | Scoping Criterion |
|------------------------------|-----------------|-----------------------|----------------------|
| Fuel peak temperature | 1332°C | 1635°C | 1650°C |
| Core Barrel peak temperature | 720°C | 784°C | 800°C |
| RPV peak temperature | 440°C | 482°C | 538°C |
| Duration RPV above 371°C | 305 hr | 446 hr | 750 hr |
| Duration RPV above 427°C | 96 hr | 233 hr | 250 hr |

Different conservative case for each Figure of Merit

All scoping criteria satisfied

- Safety functions are not impaired
- Components remain within design limits
- Meeting these criteria provides confidence that final design will be successful







- Overall SC-HTGR description
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Importance of RCCS R&D

Need for RCCS R&D

- Provide data to qualify RCCS analysis tools
- Provide data to address specific design issues
- Provide confidence in overall system concept

Designer perspective:

- Basic performance of buoyancy-driven natural circulation loop is well understood
- Basic performance of radiation heat transfer from RPV to RCCS is well understood
- Main areas of interest are with specific details
 - Impact of specific design details on system performance
 - Dynamics associated with two phase operating modes

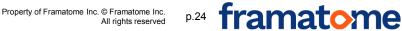


Importance of RCCS R&D Points of Interest

- Impact of riser panel tube dimensions on system performance and dynamic stability
- Need for inlet orificing (at riser tube inlets from bottom header)
- Dynamic performance characteristics
- Impact of system piping details due to building interface issues, etc.
- Impact of panel riser tube discontinuities

| AREVA | 20004-021 (01/30/2014 |
|--|---|
| | AREVA Inc. |
| | Technical Data Record |
| | Document No.: <u>12 - 9239789 - 000</u> |
| | RCCS Designer Input Report |
| United States Government subcontractors, makes any w completeness, or usefulness of not infringe privately owned name, trademark, manufactu or favoring by the United Sta | Disclaimer an account of work spensored by an agency of the United States Government, Neither the, ner any agency thereof, nor any of their employees, nor their contractors and arranty, capters or implied or assumes may lead liability or responsibility for the accuracy, of any information, apparatus, product, or process disclosed, or represents that its use would rights. Reference berien to any specific commercial product, process, arrives by trade reference of the service of the service of the service of trade ref. or otherwise does not necessarily constitute or imply its endorsement, recommendation, the Government or any agency three. The views and expiniso of authors expressed herein flect those of the United States Government or any agency thereof. |
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- Overall SC-HTGR description
- SC-HTGR RCCS Description
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Conclusions

framatome

- SC-HTGR being developed for a variety of process heat, electricity, and cogeneration markets
- Reactor Cavity Cooling System (RCCS) is only safety-related heat removal system for SC-HTGR
- Preliminary analytical assessments indicate RCCS maintains acceptable system temperatures
 - Reactor cavity wall (normal operation and accident)
 - Reactor vessel (accident)
- Basic behavior of natural circulation system and radiation heat transfer well understood
- RCCS R&D needed to
 - Provide data to qualify design and safety analysis evaluation models
 - Provide data to address specific system characteristics
 - Provide confirmation of overall system concept



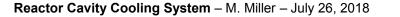


Reactor Cavity Cooling System - M. Miller - July 26, 2018



Wrap-up

- Industry is working with the national labs to develop testing and the associated test plans to support design validation
- Industry needs the data developed in the national labs to support future license applications and submittals:
 - Demonstrate basic concept feasibility
 - Provide insights on detailed design issues for RCCS designers
 - Generate data required to validate general computational methods for RCCS analysis
- Current data gathering and proposed test plans are expected to meet the necessary quality requirements specified by industry standards and the regulator







Natural convection Shutdown heat removal Test Facility (NSTF) Overview

Darius D. Lisowski

Nuclear Science & Engineering Division – Argonne National Laboratory

presented at: Nuclear Regulatory Commission

July 26th 2018 Washington, DC. USA.



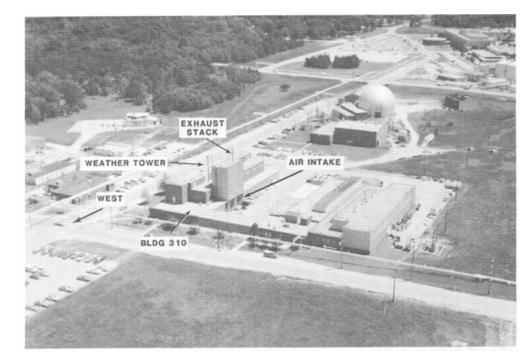
Introduction

- GenIV initiative defines 8 technological goals, of which 3 are safety related:
 - "S&R 1 System operations will excel in safety and reliability"
 - "S&R 2 Very low likelihood and degree of reactor core damage"
 - "S&R 3 Eliminate the need for offsite emergency response"
- The reactor cavity cooling system (RCCS) has emerged as a leading concept for meeting these goals
 - Possibility to provide simple and fully passive means of decay heat removal
 - Offers a high level of performance with relative simplicity in design
 - Has been under consideration since 1950's
- Multi-institutional effort has brought together federal, industry, national laboratories, universities, and countries.



NSTF at Argonne (legacy)

- Original NSTF built to provide confirmatory data for the GE PRISM RVACS design
- Successfully operated through the late 1980's



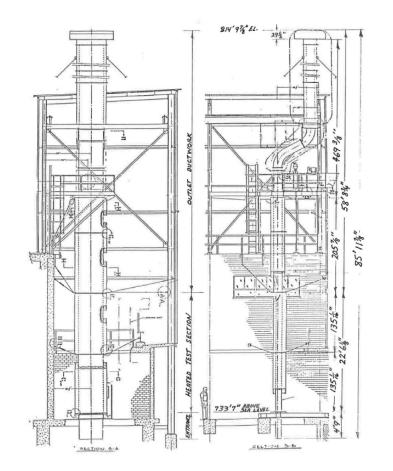


Figure 3-1. ANL Shutdown Heat Removal Test Assembly (Reduction of ANL Dwg. No. R0408-0004-DE, Sheet 1 of 4).



NSTF at Argonne (legacy)

- Beginning in 2010, the aging facility was revisited
- Several design aspects were re-used, however focus shifted to include features of newer high temperature gas-cooled reactors
- Many components were updated to latest technologies...

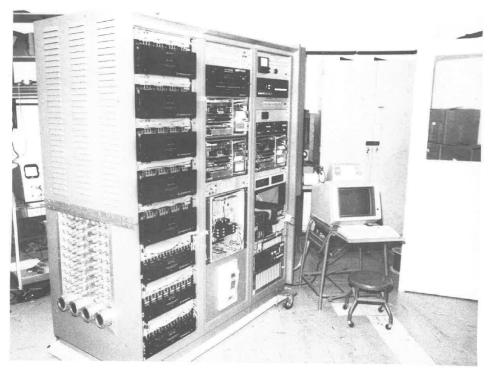
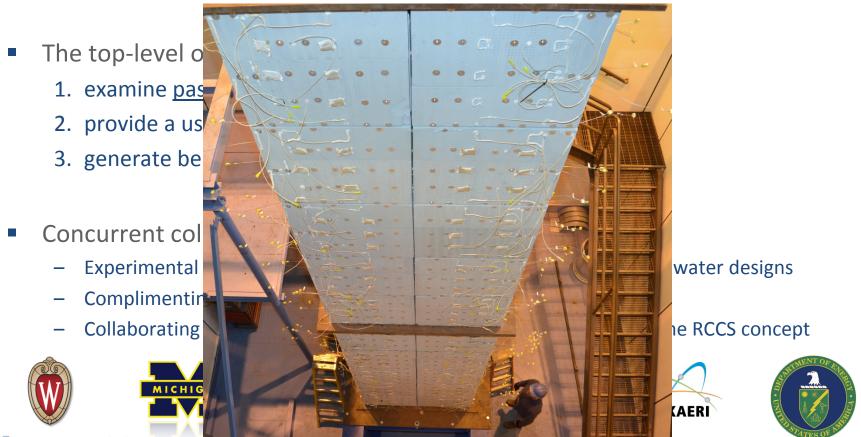


Figure 3-17. Computer Control and Data Acquisition Console.

NSTF at Argonne (present)

- The <u>Natural Convection Shutdown Heat Removal Test Facility</u> (NSTF) was initiated in FY2010 in support of DOE programs NGNP, SMR, and now ART
 - Program is compliant to Nuclear Quality Assurance (NQA)-1 2008/2009a



NSTF Quality Assurance

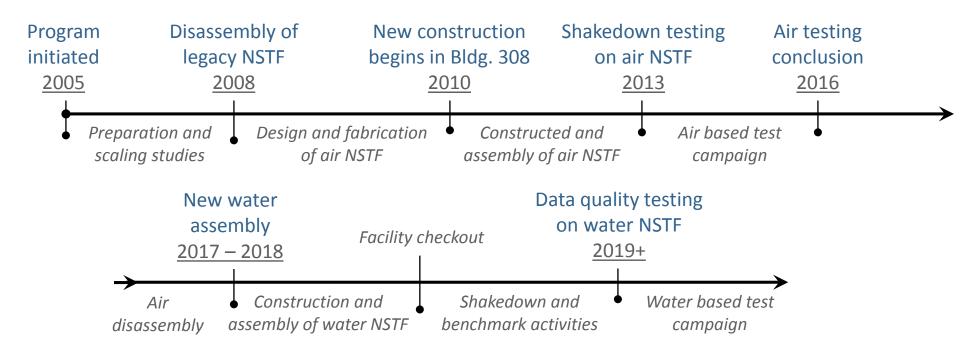
- Regular audits, or assessments, maintain compliance to NQA-1
 - Following requirements of ASME NQA-1 2008 with 2009 addendum
 - Small team of dedicated individuals with strong management support
 - Primary purpose is generating and packaging high-quality data
- Audit frequency
 - Management assessments are conducted by Argonne leadership every 3 9 months
 - Internal audits by NQA-1/ASQ certified staff every 12 18 months
 - External audits by NQA-1 certified consultants every 18 24 months or after major programmatic changes
- Compliance status
 - "All required ASTM-NQA-1-2008/1a-2009 criteria are addressed and compliant. The overall effectiveness rating of the ANL NTSF Program is Effective." - ASMT 2018-022
- Program will maintain NQA-1 compliance through entire active program period

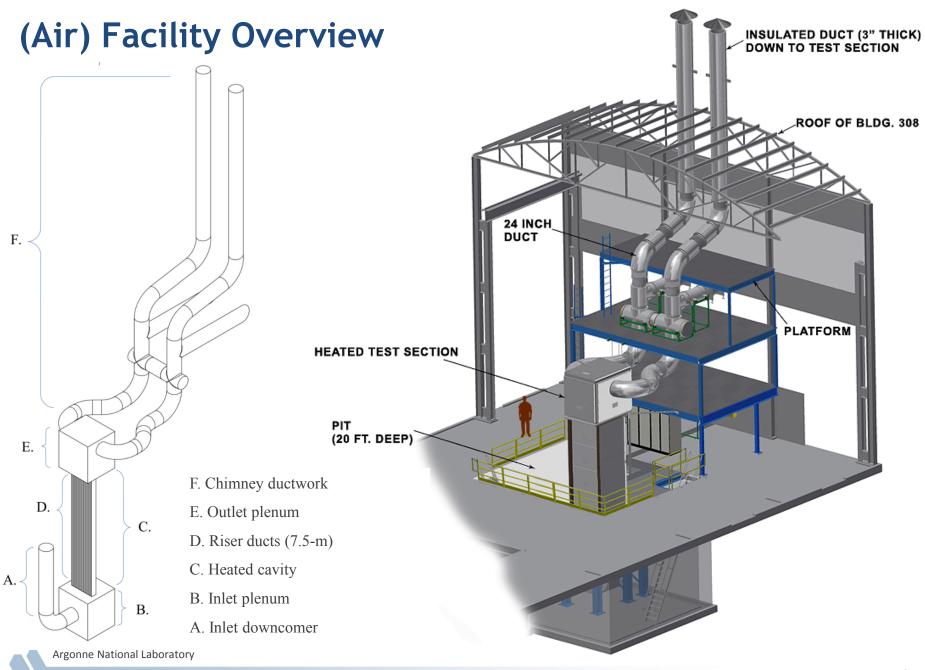
NSTF Project Documentation

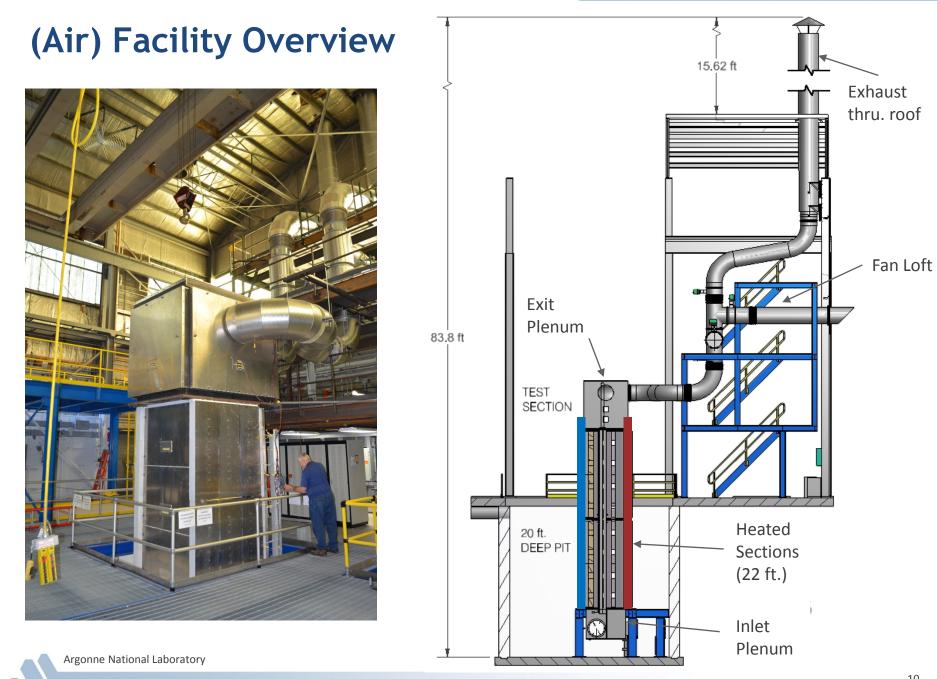
- We document all aspects of the project and engineering details of our facility
 - 80+ documents on programmatic structure, technical specifications, procurement reports, etc.
 - 300+ engineering drawings of facility design (machine shop delivery)
- Published report on scaling studies and preparation tasks
 - "RCCS Studies and NSTF Preparation Air-Cooled Option" ANL-GenIV-142 (2010)
 - "Progress Report on Water Conversion of the NSTF" ANL-ART-69 (2016)
- Compiled technical document outlining test matrix for air & water installations
 - "NSTF Data Test Matrix and Operating Parameters" ANL-NSTF-000000-TECH-010-R1 (2014, 2015)
 - "Water-based NSTF Data Quality Testing Objectives" ANL-NSTF-000000-TECH-021-R (2017)
- Published detailed design report that provides key dimensions of significant features and components of NSTF
 - "Design Report for the ½ Scale Air-Cooled RCCS Tests in the NSTF" ANL-SMR-8 (2014)
 - "Water NSTF Design, Instrumentation, and Test Planning" ANL-ART-98 (2017)
- Active contributions to scientific community
 - Regular attendance and publication in conferences, journal submissions in-review

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High-Level Status of NSTF Program







NEI/NRC, July 2018

Matrix Testing Procedures

- All matrix tests are performed with strict procedures and are documented in full
 - Test procedure (20+ pages)
 - Engineering drawings of all instrumentation positions
 - Channel listing for all instruments (NIST calibrated) into data acquisition
 - Software configuration listing
 - Archived computer software (e.g. LabVIEW .vi)
 - Full data sets saved in raw format (e.g. original voltage signals for flow instruments)
- Facility and instrument check outs are performed prior and after each test, verifying working measurements and physical connections
- If a completed test meets the stated test objective, it is suggested for classification as "Type-A" data and is followed by a Preliminary test acceptance report (PTAR)
- Those tests that do not meet objective may be classified as "Trending"



Completed Air Testing Parameters

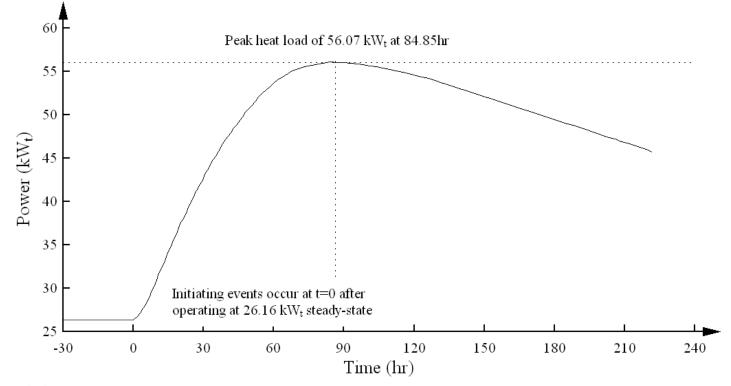
- 1. Shakedown/Calibration/Isothermal Characterization
- 2. Baseline testing ($Q_R = 1$, $\Delta T = 1$)
- 3. Scaling verification
 - Integral power variation
 - Reduced physical scale
- 4. Heated profile shaping
- 5. GA-MHTGR accident scenario
 - Full time history of decay power profile
- 6. Performance testing
 - Single chimney configuration
 - Forced flow operation
 - Blocked riser channels (incrementally block up to 6 out of 12 ducts)
 - Adjacent chimney roles (N. vertical stack inlet, S. vertical stack outlet)
- 7. Repeatability / Weather
 - Repeat tests performed at baseline, GA-MHTGR accident scenario
 - Repeat tests performed in unfavorable or varied weather conditions
 - Regular repeats of baseline case

GA-MHTGR Accident Scenario

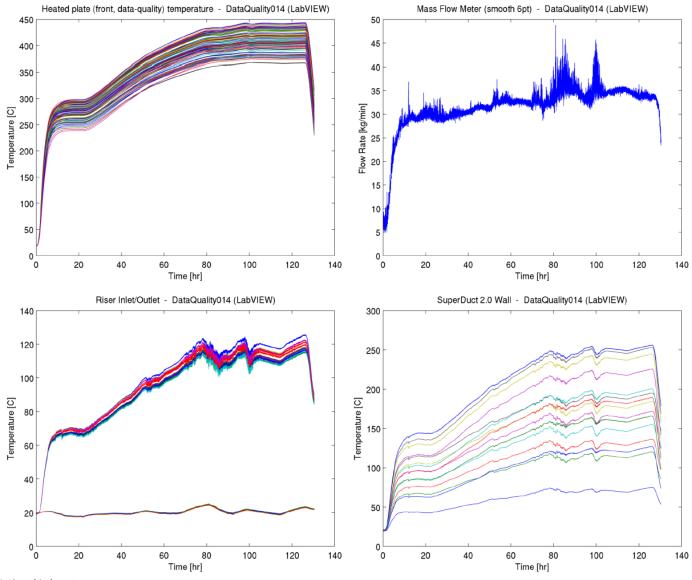
RCCS heat removal is a function of vessel temperature and ambient air temperature. A constant 43°C (II0°F) ambient air temperature is assumed for this analysis. For the depressurized cooldown accident, there is very little convective heat transfer from the core to the top head. Decay heat is primarily removed by conduction horizontally through the reflector to the vessel sidewall. Vessel temperature peaks at 441°C (826°F) just above the core midplane at 120 hours after shutdown. All major RCCS parameters also peak at 120 hours. Peak RCCS parameters are as follows:

| RCCS heat removal | 1.50 MW |
|---------------------------|---------------------------------|
| Air flow rate | 12.2 kg/sec (9.68 x 104 lbm/hr) |
| Maximum panel temperature | 219°C (426°F) |
| Air outlet temperature | 164°C (326°F) |

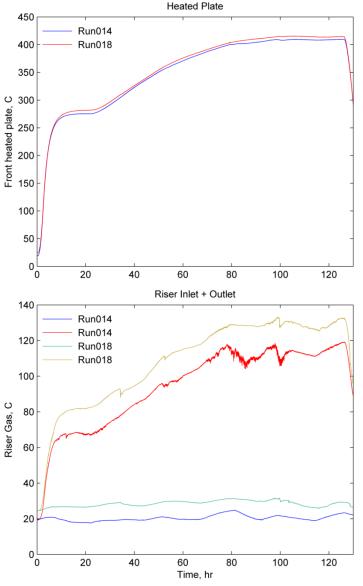
"Preliminary Safety Information Document for the Standard MHTGR," HTGR-86-024, Vol. 1, Amendment 13, U.S. Department of Energy, (1992)



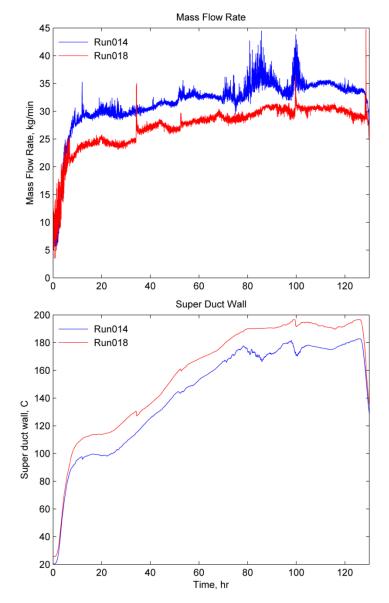
GA-MHTGR Accident Scenario



GA-MHTGR Weather Influences

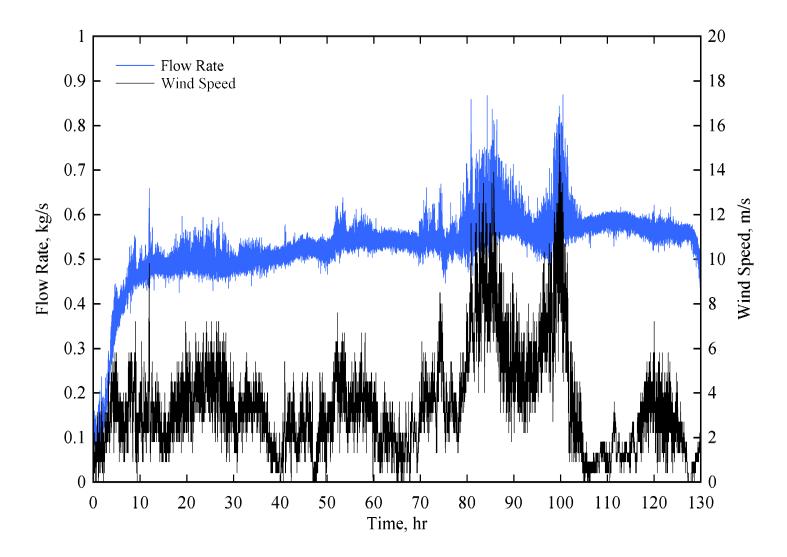


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Influences of Wind



Summary of Accepted Air-Based Test Runs

| Test Type | Test Number | Date | Duration | Classification | Primary Objectives | Flow Path |
|----------------------|----------------|----------------|--------------------------------|----------------|----------------------------|----------------------------|
| | DataQuality004 | April 2014 | 49h 52m | Accepted | Test series kick-off | Natural, Dual vertical |
| Baseline | DataQuality011 | January 2015 | 52h $47m$ | Accepted | Mid-project baseline | Natural, Dual vertical |
| | DataQuality020 | September 2015 | 52h 8m | Accepted | Hot weather baseline | Natural, Dual vertical |
| Scaling | DataQuality005 | May 2014 | $30h\ 05m$ | Accepted | Low power study | Natural, Dual vertical |
| Scaling | DataQuality008 | July 2014 | $51h \ 09m$ | Accepted | Reduced chimney discharge | Natural, Reduced discharge |
| Chimney roles | DataQuality017 | June 2015 | 58h $38m$ | Accepted | Adjacent chimney study | Natural, Adjacent |
| Children Poles | DataQuality024 | April 2016 | $145h\ 50m$ | Accepted | Single chimney | Natural, Single vericcal. |
| | DataQuality013 | March 2015 | 72h 05m | Accepted | Mid-plane cosine | Forced, Reduced discharge |
| Power Shaping | DataQuality022 | January 2016 | $120\mathrm{h}~8\mathrm{m}$ | Accepted | Bottom-peaked cosine | Natural, Dual vertical |
| | DataQuality026 | May 2016 | 97h~38m | Accepted | Azimuthal, $65/35\%$ | Natural, Dual vertical |
| GA-MHTGR | DataQuality014 | April 2015 | 130h 28m | Accepted | SRDC-II, winter months | Natural, Dual vertical |
| GA-MITGR | DataQuality018 | August 2015 | $129 \mathrm{h}~55 \mathrm{m}$ | Accepted | SRDC-II, summer months | Natural, Dual vertical |
| Performance | DataQuality015 | May 2015 | 82h $53m$ | Accepted | Blocked riser tubes | Natural, Single vertical |
| | DataQuality027 | June 2016 | $30h\ 07m$ | Accepted | Heavy gas (argon) ingress | Natural, Single vertical |
| Weather | DataQuality007 | June 2014 | $13h\ 28m$ | Accepted | Inclement weather start-up | Natural, Reduced discharge |
| Collaboration driven | DataQuality023 | February 2016 | 190h 20m | Accepted | INERI test series | Forced, Reduced discharge |

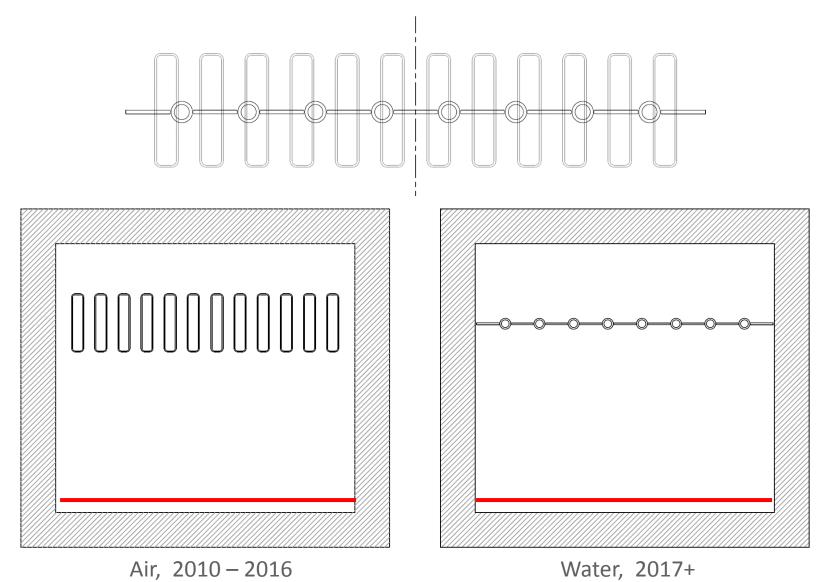
Air-based Program Summary

- Air-based testing program officially concluded on July 5th 2016
 - Final modeling report documented in ANL-ART-46 (M2AT-16AN1702078)
 - Final project report documented in ANL-ART-47 (M2AT-16AN1702077)
 - Formal internal audit for all 18 elements of NQA-1 2008 June 29th 2016
- All program requirements were completed
 - High level program objectives drafted in 2005, prior to facility design and assembly
 - Experimental objectives drafted in 2013, prior to testing campaign
 - Items identified during early 2016 data review meeting, prior to testing conclusion
 - Attendees included the DOE, NRC, INL, AREVA, GA, and US Universities
 - Stenographer hired and transcribed full meeting minutes
- Program accomplishments
 - 33-month testing campaign duration
 - 2,250 active hours of heating
 - 27 conducted tests (16 accepted)
 - Multiple baseline repeats, GA-MHTGR accident scenario, blocked risers, power variations, azimuthal and cosine skew, adjacent chimney roles, meteorological variations, I-NERI test series
 - 24 publications since inception (numbered reports, journals, and conference)

Water based transformation & Design study

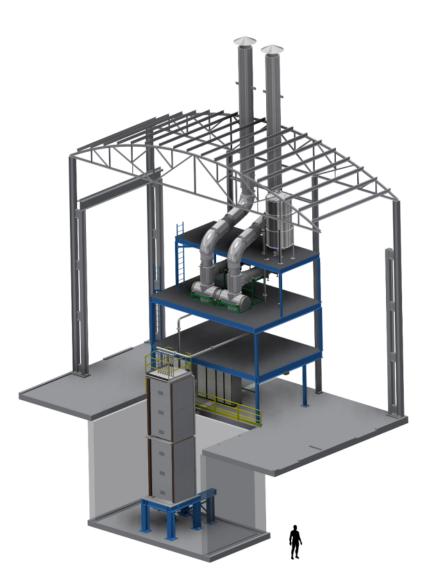
- Water-cooled NSTF is based on concept design for Framatome's water based RCCS
 - DOE sponsored HTGR Technology Economic/Business Analysis and Trade Studies
 - RCCS team performed scaling studies, geometric simulations, thermal and stress calculations, tank depletion time estimates, steam quality/flow rate determinations, etc.
- Close collaboration with Frametome, whose RCCS included as part of their 625 MW_t SC-HTGR served as the primary design basis for incorporation into the NSTF
 - "RCCS Designer Input Report, Technical Data Record, 12-9239789-000, AREVA"
 - "Design Proposal for the Water-Based NSTF Test Section and Network Piping Argonne National Laboratory", Technical Report, ANL-NSTF-000000-TECH-016-R0, ANL"
 - "Water-Cooled RCCS R&D Designer Observation Report, Technical Data Record, 12-9237246-000, AREVA"
 - "Design Proposal for the Water-Based NSTF Test Section and Network Piping Argonne National Laboratory", Technical Report, ANL-NSTF-000000-TECH-016-R1, ANL"
- Participation from Framatome, INL, DOE, NRC, and US Universities
 - Design review meeting held at Argonne in February of 2015
 - Test planning and program readiness meeting held March of 2018
 - Consensus reached on a design and test plan that reflects a representative yet bounding configuration for future implementation into a full scale design
- The final facility meets ANL/DOE project goals, and will provide industry with data suitable for characterizing the RCCS of their full scale HTGR design

Air / Water Comparison



Water Facility Overview

- ½ axial scale
 - Total height of 18 m (59-ft)
 - Heated length of 6.7 m (22-ft)
- Natural circulation boiling water test loop
 - Operating modes of natural or forced
- 4,260 liter water storage tank
 - H/D ratio of 2.0, rated to 2 bar over pressure
- Heat transfer panel:
 - Eight riser tubes and ten heat transfer panels
 - 316L stainless tubes, 1018 carbon fins
 - Full penetration HLAW weld to risers
- Network piping: 4.0" Sch. 40, 316L stainless

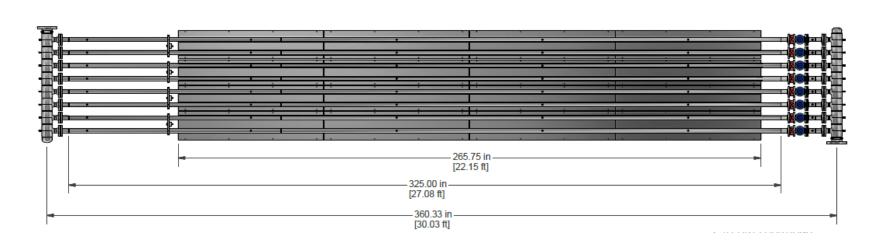


| Cooling Panel Design | | Material | k (W/m-K) | ε (-) |
|--|------|----------------|-----------|-------|
| | | 1018 carbon | 51.9 | > 0.8 |
| | Pipe | 316L stainless | 16.2 | < 0.3 |
| - 1-1/2" PIPE, SCH 160, 1.900" OD X 1.337" ID X 0.281" WALL | | | | |

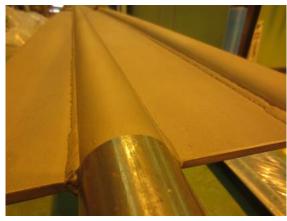
0.313 in

-4.01 in -

-5.91 in -



Cooling Panel Installation



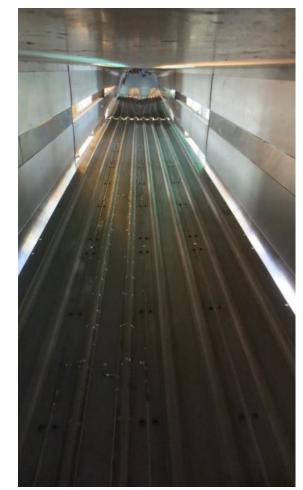
Bead blasted cooling panel surface



Assembled panel staged for 180° flip



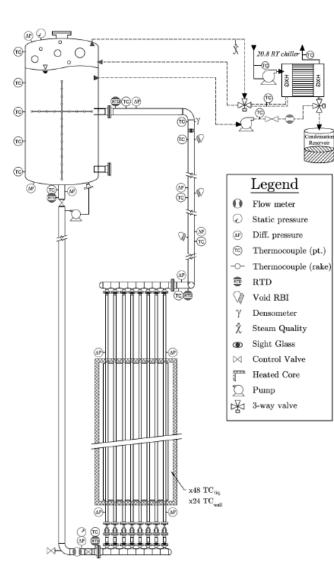
Panel hoisted vertical prior to install



Installed test section, view in heated cavity

Water Instrumentation

| Measurement | Sensor | Location | Qty. | Mfg. | Model | Range |
|---------------------|--------------|--------------|------|--------------|---------------|-------------------------|
| Flowrate | Magnetic | Inlet header | x1 | Krohne | Optiflux 4000 | ±5kg/s |
| Flowrate | Magnetic | Inlet riser | x8 | Krohne | Optiflux 4000 | ±1kg/s |
| Static head | Strain | Inlet header | x1 | Rosemount | 3051S | 0 - 10bar |
| Steam pressure | Strain | Gas space | x1 | Rosemount | 3051S | 0 - 2bar _{abs} |
| ΔP | Strain | Chimney | x2 | Rosemount | 3051S | ±6kPa |
| ΔP | Strain | Risers | x3 | Rosemount | 3051S | ±62kPa |
| Liquid level | Strain | Tank | x1 | Rosemount | 3051S | 0 - 3m |
| Void fraction | Optical | Chimney | x2 | RBI | Twin-tip | 0 - 100% |
| Void fraction | γ-Density | Chimney | x1 | ThermoFisher | DensityPRO | 0 - 100% |
| Temperature | RTD | Fluid | x4 | Omega | UP1/10DIN | 0 - 250°C |
| Temperature | T-type TC | Fluid | x128 | ARi | T-31N | 0 - 400°C |
| Temperature | K-type TC | Test section | x24 | ARi | T-31N | 0 - 600°C |
| Temperature | K-type TC | Strain | x286 | ARi | Silica20AWG | 0 - 600°C |
| Temperature | DTS | Test section | x20 | LUNA | ODiSI-A | 0 - 300°C |
| Water pH | pH meter | Inlet header | x1 | Emerson | RBI547 | 0 - 14pH |
| TrDO O ₂ | Amperometric | Inlet header | x1 | Emerson | 499A | 0.1ppb-20ppm |
| Conductivity | Magnetic | Inlet header | x1 | Krohne | Optiflux 4000 | $1-6000\mu S/cm$ |





Electromagnetic flow meters



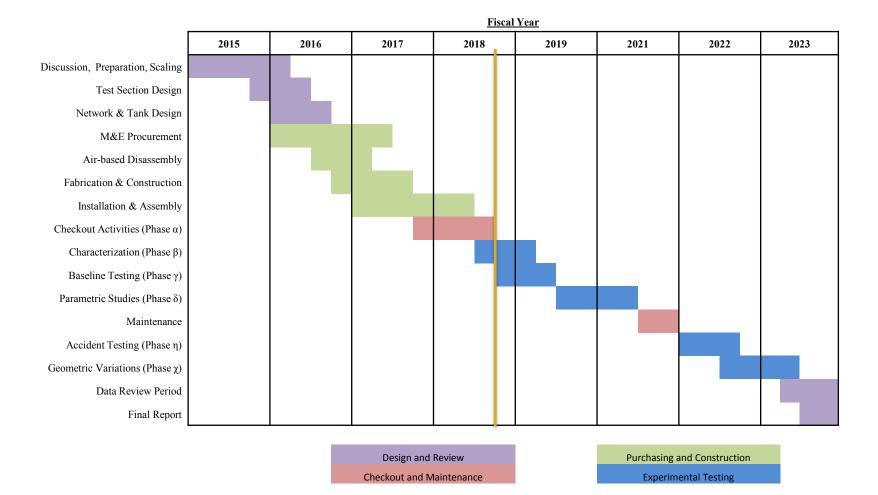
Gamma densometer

Path forward for Water Testing

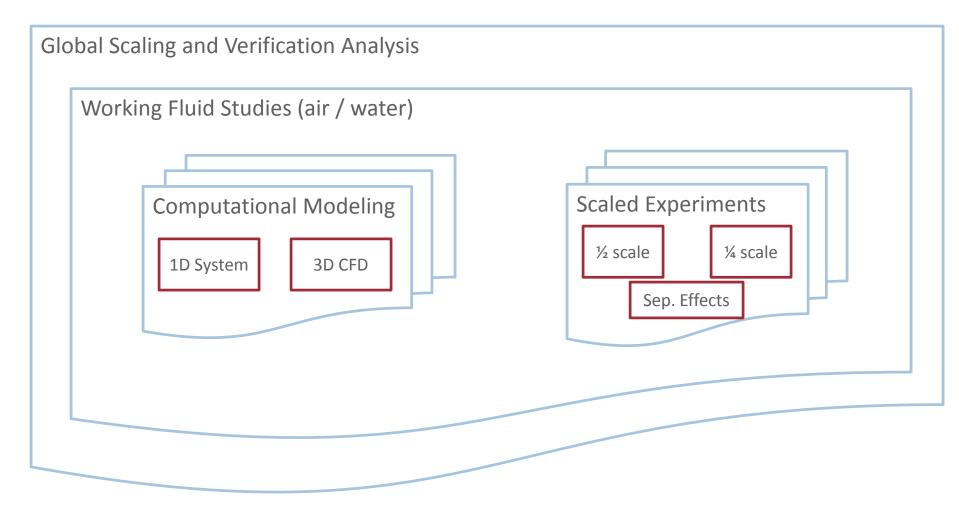
- Basis and detail of test planning included in ANL-ART-98 (M2, August 2017)
 - Checkout activities are in-progress
- Test planning & review meeting has been held prior to initiating matrix testing
 - Invitation included programs to key players
- External audit of program and test procedures prior to initiating matrix testing
 - Completed without any findings
- Baseline testing to begin by FY2019
- Continue communication with industry & NRC

| Phase | Activities Conducted | Duration |
|---------------|--|----------|
| Ι | Power, electrical, data acquisition checkout, hydrostatic leak testing | 6 mo. |
| II | Gross system mass and energy balance, isothermal testing | 9 mo. |
| III | Single- and two-phase baseline test cases | 6 mo. |
| IV | Single parameter variations of power, inventory, pressure | 24 mo. |
| \mathbf{V} | Accident scenarios (design-basis) | 6 mo. |
| \mathbf{VI} | Geometric variations, off-normal scenarios | 12 mo. |

Water Program Timeline



Realization of Full Scale Deployment of the RCCS



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Acknowledgments

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| Argonne Project Personnel | | Program Sponsors | | Analysis Support Team | |
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Questions?



http://www.ne.anl.gov/capabilities/rsta/NSTF

