



International Agreement Report

RELAP5 Assessment Against PACTEL Experimental Data (Revision 1)

Prepared by
I. Parzer, B. Mavko, S. Petelin

University of Ljubljana
"Jozef Stefan" Institute
P.O. Box 100
61111 Ljubljana
Slovenia

Office of Nuclear Regulatory Research
U.S. Nuclear Regulatory Commission
Washington, DC 20555-0001

November 1998

Prepared as part of
The Agreement on Research Participation and Technical Exchange
under the International Code Application and Maintenance Program (CAMP)

Published by
U.S. Nuclear Regulatory Commission

AVAILABILITY NOTICE

Availability of Reference Materials Cited in NRC Publications

NRC publications in the NUREG series, NRC regulations, and *Title 10, Energy, of the Code of Federal Regulations*, may be purchased from one of the following sources:

1. The Superintendent of Documents
U.S. Government Printing Office
P.O. Box 37082
Washington, DC 20402-9328
<http://www.access.gpo.gov/su_docs>
202-512-1800
2. The National Technical Information Service
Springfield, VA 22161-0002
<<http://www.ntis.gov/ordernow>>
703-487-4650

The NUREG series comprises (1) technical and administrative reports, including those prepared for international agreements, (2) brochures, (3) proceedings of conferences and workshops, (4) adjudications and other issuances of the Commission and Atomic Safety and Licensing Boards, and (5) books.

A single copy of each NRC draft report is available free, to the extent of supply, upon written request as follows:

Address: Office of the Chief Information Officer
Reproduction and Distribution
Services Section
U.S. Nuclear Regulatory Commission
Washington, DC 20555-0001
E-mail: <GRW1@NRC.GOV>
Facsimile: 301-415-2289

A portion of NRC regulatory and technical information is available at NRC's World Wide Web site:

<<http://www.nrc.gov>>

All NRC documents released to the public are available for inspection or copying for a fee, in paper, microfiche, or, in some cases, diskette, from the Public Document Room (PDR):

NRC Public Document Room
2121 L Street, N.W., Lower Level
Washington, DC 20555-0001
<<http://www.nrc.gov/NRC/PDR/pdr1.htm>>
1-800-397-4209 or locally 202-634-3273

Microfiche of most NRC documents made publicly available since January 1981 may be found in the Local Public Document Rooms (LPDRs) located in the vicinity of nuclear power plants. The locations of the LPDRs may be obtained from the PDR (see previous paragraph) or through:

<<http://www.nrc.gov/NRC/NUREGS/SR1350/V9/lpdr/html>>

Publicly released documents include, to name a few, NUREG-series reports; *Federal Register* notices; applicant, licensee, and vendor documents and correspondence; NRC correspondence and internal memoranda; bulletins and information notices; inspection and investigation reports; licensee event reports; and Commission papers and their attachments.

Documents available from public and special technical libraries include all open literature items, such as books, journal articles, and transactions, *Federal Register* notices, Federal and State legislation, and congressional reports. Such documents as theses, dissertations, foreign reports and translations, and non-NRC conference proceedings may be purchased from their sponsoring organization.

Copies of industry codes and standards used in a substantive manner in the NRC regulatory process are maintained at the NRC Library, Two White Flint North, 11545 Rockville Pike, Rockville, MD 20852-2738. These standards are available in the library for reference use by the public. Codes and standards are usually copyrighted and may be purchased from the originating organization or, if they are American National Standards, from—

American National Standards Institute
11 West 42nd Street
New York, NY 10036-8002
<<http://www.ansi.org>>
212-642-4900

DISCLAIMER

This report was prepared under an international cooperative agreement for the exchange of technical information. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for any third

party's use, or the results of such use, of any information, apparatus, product, or process disclosed in this report, or represents that its use by such third party would not infringe privately owned rights.

NUREG/IA-0145



International Agreement Report

RELAP5 Assessment Against PACTEL Experimental Data (Revision 1)

Prepared by
I. Parzer, B. Mavko, S. Petelin

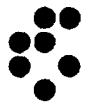
University of Ljubljana
"Jozef Stefan" Institute
P.O. Box 100
61111 Ljubljana
Slovenia

Office of Nuclear Regulatory Research
U.S. Nuclear Regulatory Commission
Washington, DC 20555-0001

November 1998

Prepared as part of
The Agreement on Research Participation and Technical Exchange
under the International Code Application and Maintenance Program (CAMP)

Published by
U.S. Nuclear Regulatory Commission



RELAP5 Assessment Against PACTEL Experimental Data

Abstract

The results of the pre-test and post-test calculations of OECD International Standard Problem no.33 (ISP-33) are presented. The frozen version of RELAP5 code version MOD2 and the latest released version MOD3.2 have been assessed against experimental data from PACTEL facility. Generally, predictions were in good agreement with experimental data, except in the most interesting part of the transient only MOD3.2 was able to follow periodic hot leg loop seal clearance phenomena and primary pressure oscillations closely.



CONTENTS

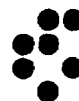
	page
INTRODUCTION	1
PACTEL FACILITY DESCRIPTION	1
PACTEL COMPUTER MODEL DEVELOPMENT	3
Characterizing test description	3
Results of the characterizing test	3
EXPERIMENT DESCRIPTION	6
IMPORTANT PHYSICAL PHENOMENA AS PREDICTED BY RELAP5	7
RESULTS	10
COMPUTER DATA AND RUN-TIME STATISTICS	15
CONCLUSIONS	16
REFERENCES	16
APPENDIX A: ISP-33 Steady State Input Deck	
APPENDIX B: ISP-33 Run Input Deck	
APPENDIX C: ISP-33 Strip Input Deck and Complete Set of Comparison Plots (post-test results)	

LIST OF FIGURES

Figure 1: Axonometric view of the PACTEL facility	2
Figure 2: PACTEL nodalization scheme for RELAP5 calculations of ISP-33	4
Figure 3: Characterizing test: pressurizer pressure	5
Figure 4: Characterizing test: pressurizer level	5
Figure 5: RELAP5/MOD3.2 - upper plenum pressure	12
Figure 6: RELAP5/MOD3.2 - pressurizer level	13
Figure 7: RELAP5/MOD2 - upper plenum pressure	13
Figure 8: RELAP5/MOD2 - pressurizer level	14
Figure 9: Comparison of RELAP5 predictions - DP over the reactor vessel	14
Figure 10: Comparison of RELAP5 predictions - maximum cladding temperatures	15

LIST OF TABLES

Table 1: Initial Conditions for the ISP-33 Experiment	6
Table 2: Run-time statistics for post-test calculations	15



INTRODUCTION

In the 1990's the interest for eastern nuclear power plants safety has increased significantly. The VVER-440 heat removal capability in accidental situations has been studied mostly. VVER-440 nuclear power plants (NPPs) differ considerably from western type Pressurized Water Reactor (PWR) plants. The main distinguishing characteristics, beside horizontal steam generators, are loop seals not only in cold but also in hot legs. The horizontal steam generator (SG) design degrades natural circulation driving force. The top of SG tubes is only at about 1 m higher elevation than hot leg connection to the reactor vessel. Along with the hot leg loop seal such construction almost disables the reflux cooling process in the case of Small Break Loss-of-Coolant Accidents (SB LOCA).

Nuclear safety oriented OECD ISP-33, focused on VVER-440 core cooling capability, started in 1992. The experiment, performed on the PACTEL integral test facility, built in Lappeenranta, Finland, simulated different stages of a Small Break Loss-of-Coolant Accident (SB LOCA). Natural circulation is essential for decay heat removal in the accident situations of the light water reactors. The experiment with stepwise reduction of primary inventory was considered relevant for VVER-440 safety since it would demonstrate the ability of the plant to remove decay heat with different amounts of primary inventory, developing different patterns of natural circulation. Since VVER-440 and PACTEL facility are equipped with horizontal steam generators, which lowers the elevation between core and steam generator tubes, the study of natural circulation was strongly desired for this kind of nuclear power plant.

PACTEL FACILITY DESCRIPTION

The PACTEL integral test facility [1, 2] in Finland (Figure 1) is a 1:305 scaled down 3-loop model of a 6-loop VVER-440 PWR NPP, ex-Soviet design, also built in Finland.

The facility consists of reactor vessel model, external downcomer, three loops with three SGs and a pressurizer connected to hot leg no. 1. Reactor core is modelled by 144 electrically heated rods, in three separated parallel triangularly shaped BWR-like channels. All the elevations in the facility are preserved as on the original plant. The same is valid for active core height, since heater rod length is 2.5 m. Axial power distribution is uniform. Maximum core power is only 1 MW which is about 20% of the scaled nominal power ($1475 \text{ MW} / 305 = 4.84 \text{ MW}$). There were no primary coolant pumps built in the facility, thus only natural circulation driven experiments were possible to be conducted on the facility at the time of the test. The Emergency Core Cooling Systems (ECCS) are also installed on the facility, but neither, high pressure, low pressure system nor passive hydroaccumulators were in action during the ISP-33 experiment. Each steam generator contains 38 horizontal heat exchange U-tubes with the average length of 8.8 m. The secondary water level control is performed by means of manual feedwater control.

There is an instrumentation system, consisting of a data acquisition unit, a controller and a workstation, dedicated to the PACTEL facility.

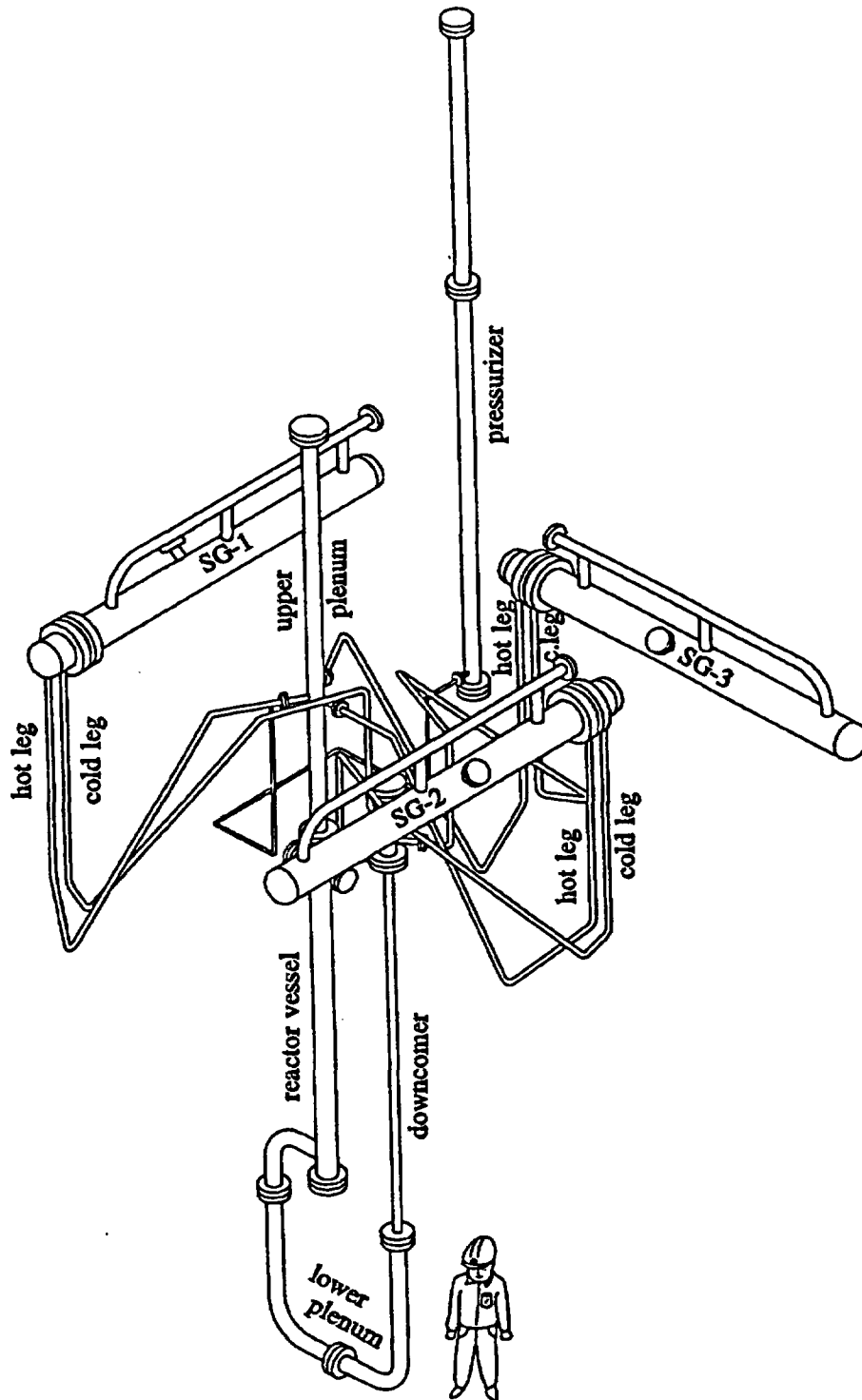
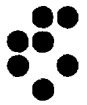
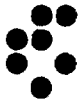


Figure 1: Axonometric view of the PACTEL facility



PACTEL COMPUTER MODEL DEVELOPMENT

The ISP-33 experiment was announced as a blind exercise. However, since it was supposed that there was not enough experience in modelling VVER-440 plants or their scaled-down models at that time, the data for a special, so called "characterizing test" were distributed among the participants in the pretest period. The characterizing test included some elements of the later ISP-33, so that the participants could tune the response of their models to a part of the SB LOCA sequence. The "characterizing test" has been performed on PACTEL facility prior to ISP-33 experiment.

A full 3-loop model has been developed at IJS [3] and is shown in Figure 2. It consists of 221 hydrodynamic volumes, 238 junctions and 259 heat structures with 1263 mesh points. Three parallel core channels were modelled lumped together as one channel. First MOD2 model [4] has been developed and initialized into another steady state condition, corresponding to the "characterizing test" data. The MOD3.2 deck was simply copied from the previously developed MOD3.0 deck, originating from MOD2 and upgraded only as much as requested in the Manual [5].

Finally, both models have been driven to 155 kW core power and initialized to the actual ISP-33 steady state conditions.

Characterizing Test Description

The characterizing test started from steady-state natural circulation at 180 kW core power. For demonstrating the system response with two pressurizer heater power levels and system behaviour with a small letdown is demonstrated with the following events:

- (A) The pressurizer heaters power has been controlled manually. It was set to 4 kW at the beginning of the test, switched to 2 kW after 1260 seconds and increased back to 4 kW at 2290 seconds.
- (B) After 2640 seconds 13.5 kg of water has been drained from the lower plenum.

In this way some of the details in the model could be tuned, especially pressurizer response to perturbations, which showed later to be of essential importance for the correct ISP-33 test simulation.

Results of the characterizing test simulation

The RELAP5 simulation started from the conditions at 1260 seconds of the transient, when the heater power was decreased to 2 kW, and followed the later sequence of events. The pressurizer pressure response (Figure 3) is shown to be adequate in both calculations. The slope of both curves from RELAP5 calculations is the same as in the experiment, which indicates that the primary system inventory distribution and thermodynamic state has been modelled adequately, as well as heat losses from different parts of the primary system. Another proof for correct modelling of the primary inventory is the pressurizer level development after the draining at 2640 seconds (Figure 4).

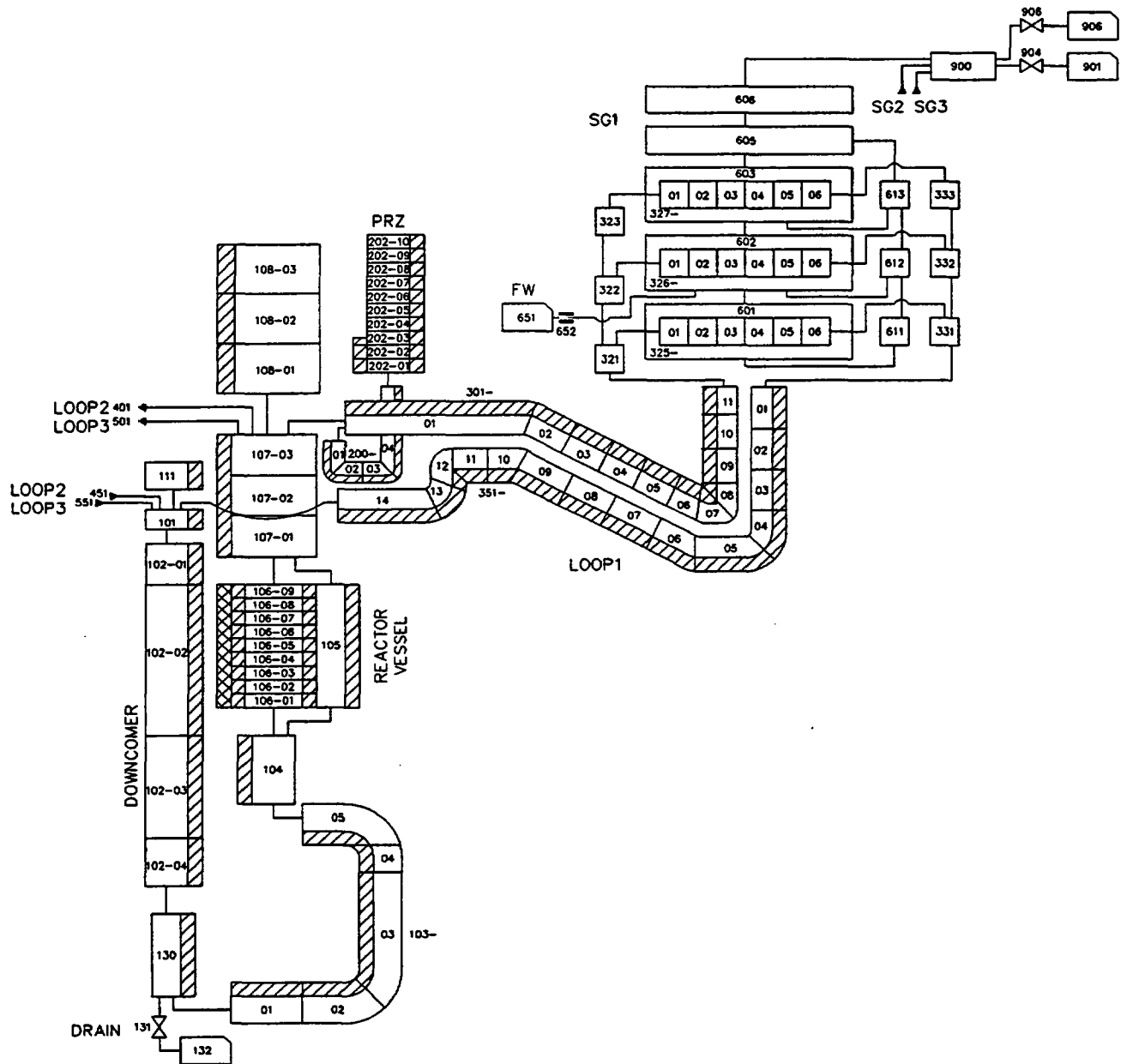
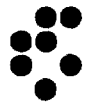


Figure 2: PACTEL nodalization scheme for RELAP5 calculations of ISP-33

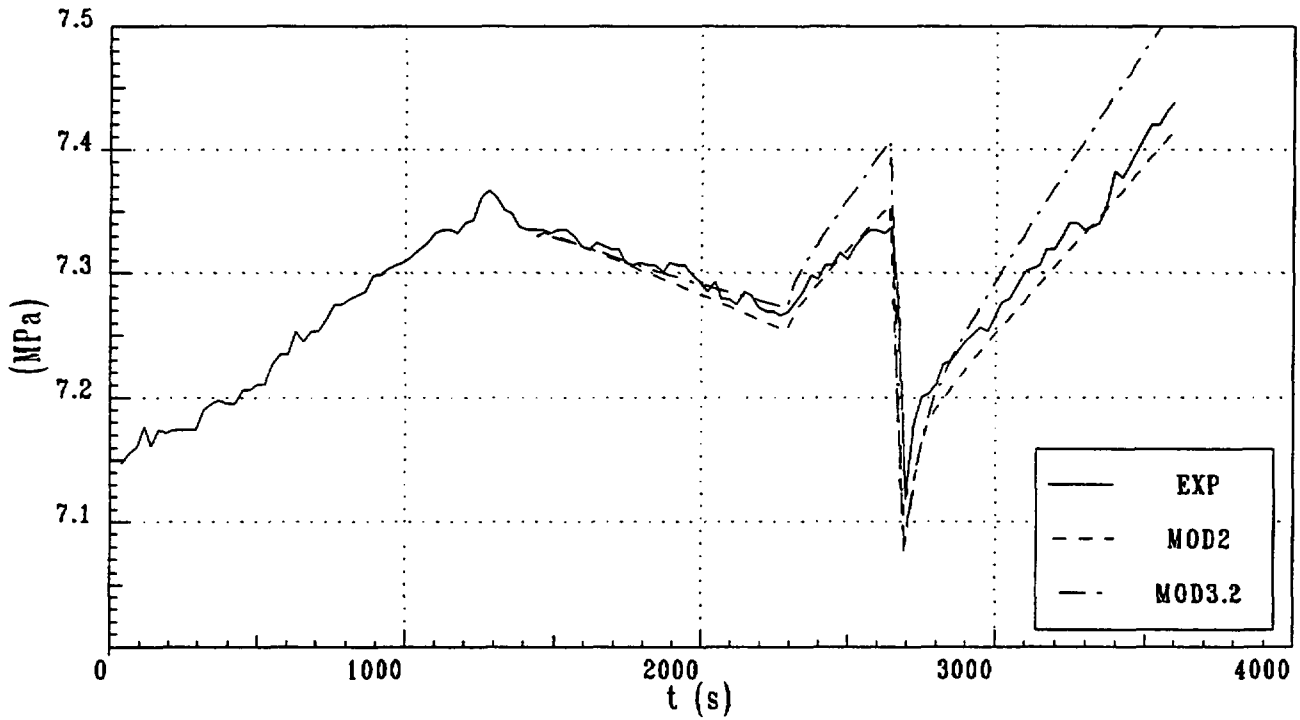
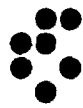


Figure 3: Characterizing test: pressurizer pressure

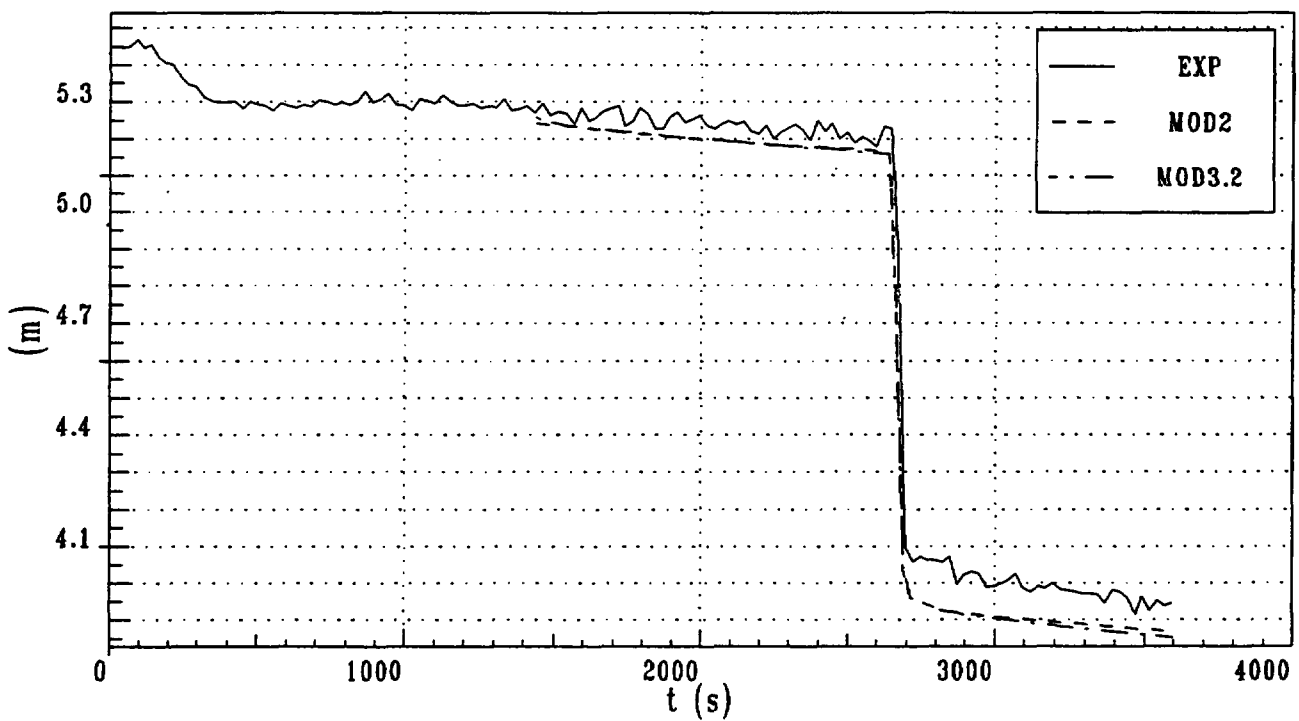
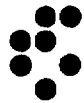


Figure 4: Characterizing test: pressurizer level



EXPERIMENT DESCRIPTION

A special SB LOCA scenario with stepwise reduction of the primary inventory has been applied for simulation on the PACTEL facility. Initial conditions, listed in Table 1, have been matched closely in MOD2 and MOD3.2 model initialization and stabilization processes.

After the initial 1200 s steady state, 1st draining from the primary system has been performed. At that time 60 kg (about 9%) of the primary liquid has been drained from the lower plenum in 180 s. During that period only the pressurizer was emptied, while reactor vessel upper head and SG tubes remained filled with subcooled liquid. In the next 720 s period, the system was allowed to reach the new steady state condition.

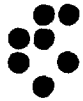
During each next draining another 60 kg of the primary inventory have been drained in period of 60 s, following by 840 s undisturbed time intervals for the system parameters to reach new quasi steady state.

PRIMARY SYSTEM		SECONDARY SYSTEM	
Core power	165 kW	SG pressure	4.18 MPa
Pressurizer pressure	7.39 MPa	SG levels: SG 1	0.271 m
Pressurizer level	5.18 m	SG 2	0.272 m
Pressurizer heater power	2 kW	SG 3	0.263 m
Downcomer flow	1.47 kg/s	SG feedwater temperature	305 K
Loop flow	0.49 kg/s		

Table 1: Initial Conditions for the ISP-33 Experiment

The most interesting phenomena took place between 2nd and 3rd draining, when single phase natural circulation was interrupted due to primary coolant depletion and steam bubble entrainment into hot legs. Oscillations of the pressurizer liquid level have been observed because of the increasing primary pressure, causing several hot leg no. 1 loop seal clearings and periodic liquid push-ups into the pressurizer.

Many other interesting phenomena were observed in the later time intervals between draining. As the primary system was emptying, single phase natural circulation switched to two-phase after the period of periodic flow blockage of single phase natural circulation. First hot legs emptied after hot leg loop seal clearance, and later the same process was observed in cold legs. Towards the end of the transient, the primary system emptied to such extent, that two-phase natural circulation was interrupted and almost all the remaining primary liquid was collected in lower part of the reactor vessel. At that time reactor core was hardly covered enough that stalled circulation



could remove the heat from the core. After the last draining core uncovered and upper part of the rods overheated. When the peak clad temperature reached 623 K (350°C) core power was switched off in the experiment and the test was ended, but the calculations were supposed to continue till the peak clad temperature of 1173 K (800°C) would be reached.

A variation case experiment was performed on the facility, when, after core heatup, operator fully opened secondary relief valves to condense the vapor in the primary system and collapse it into the reactor vessel. This caused rapid core quenching. Only after a while, when the heater rods overheated again, core power was switched off and the variation case was ended. The variation case data and the corresponding RELAP5 calculated results are not presented here.

IMPORTANT PHYSICAL PHENOMENA AS PREDICTED BY RELAP5

0) before the first draining (0 - 1200 s)

The obtained steady state in the first 100 seconds of the transient was stable in MOD2 calculation. Primary pressure was controlled by pressurizer heaters cycling, keeping it within the limits of 7.36 and 7.5 MPa. Secondary levels were controlled by automatic feedwater control and deviated insignificantly from the desired level setpoint of 0.27 m in each steam generator. Secondary pressure was controlled by appropriate opening of the valve, located on the steam line, after the joining point of three steam generator lines. All the other observed parameters behaved in a stable manner.

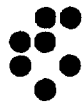
1) between 1st and 2nd draining (1200 - 2100 s)

The pressurizer was drained first. At the end of the first draining in MOD2 calculation the pressurizer was almost completely drained. The pressurizer surge line still remained filled with subcooled liquid. In both calculations the pressurizer level stayed slightly below 0.5 m till the next draining.

On the other hand the very top of the upper plenum emptied and a small vapor bubble was detected. Primary pressure dropped close to the saturating pressure, slightly below 6 MPa. Nevertheless, single-phase natural circulation proceeded with minor disturbances throughout this time interval in both calculations. MOD2 calculated mass flow interruption in cold leg no. 1 very early after the first draining.

2) between 2nd and 3rd draining (2100 - 300 s)

The reactor vessel upper plenum drained completely, while a larger amount of water was pushed back into the pressurizer, more drastically in MOD3.2 calculation. In both calculations half or more of the initial pressurizer inventory was restored. This remained till the third draining. A pressure rise was obtained in the primary system. A large pressure spike was calculated by MOD3.2, back up to the initial pressure level.



Hot leg loop seal emptying started in all the three loops. First hot leg loop seal levels decreased on the reactor vessel side, while vertical parts on the steam generator side remained almost filled up with some disturbances. MOD3.2 calculated larger hot leg loop seal emptying in all three loops on the reactor side of hot leg loop seals. Vessel inventory dropped quickly and first voiding occurred in the core region.

Heat transfer to the secondary system was interrupted during this time interval in steam generators 1 and 3 in MOD2 calculation, while MOD3.2 calculated interruption in steam generators 2 and 3. The flow through cold leg no. 2 was interrupted in both calculations. Two-phase natural circulation took place through loop 2 in MOD2 and through loop 1 in MOD3.2 calculation.

3) between 3rd and 4th draining (3000 - 3900 s)

Pressurizer was again drained completely. Primary pressure dropped below 5 MPa. More voiding took place in the core. The whole part of the reactor vessel above the core was emptied and hot leg loop seals were further emptying. The loop 2 hot leg loop seal emptied deeply on the reactor side in MOD2 calculation. Some voiding was briefly detected in cold leg 1 in MOD3.2 calculation. Exactly the reverse happened on the steam generator side of the hot leg loop seals in loop 1 and 2.

Some water was pushed through the steam generator 1 tubes from hot to cold side in MOD3.2 calculation, while MOD2 calculated the liquid transfer through the SG no. 2. Two-phase natural circulation proceeded through the same loops as in previous time interval. Vessel inventory remained almost constant in this time interval and primary level stayed well above the active part of the core.

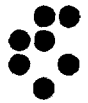
4) between 4th and 5th draining (3900 - 4800 s)

Primary pressure dropped close to the secondary pressure. A slight level rise was detected in the pressurizer, more obvious in MOD2 calculation. Heat transfer was interrupted in SG no. 2 in both calculations and restored or proceeded through the rest two steam generators. A larger amount of liquid was pushed through the SG no. 2 and 3 tubes. Hot leg loop seals no. 2 and 3 were cleared shortly after the 4th draining. Larger voiding was detected in loop 1 and 3 cold legs, but later the inventory was restored.

Steam generator tubes emptying started in loops 1 and 3. Vessel inventory slowly decreased, but the primary level still remained above the core. Two-phase natural circulation proceeded and was switched through loops 1 and 3 in both calculation.

5) between 5th and 6th draining (4800 - 5700 s)

Water continued to be pushed back into the pressurizer, but no primary pressure rise was calculated. Two-phase natural circulation was severely disturbed in all the three loops. Steam generator tubes were more than half emptied and cold legs emptying started, but the core still



remained sufficiently covered, where MOD2 calculated larger level drop. All the three hot legs were already completely emptied by this time. Heat was transferred equally through all steam generators.

6) between 6th and 7th draining (5700 - 600 s)

Steam generator tubes were drastically emptied. The level dropped in all cold legs. Two-phase natural circulation was definitely interrupted in the whole system. Stalled recirculation within reactor vessel became the mechanism of core heat removal. Still more water was pushed into the pressurizer, where close to the half inventory was again restored. Larger core uncovering was calculated especially by MOD2. First slight voiding in the reactor vessel downcomer was calculated by MOD3.2. Heat transfer proceeded through all the three steam generators.

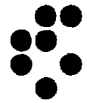
7) between 7th and 8th draining (6600 - 7500 s)

After this draining only cold leg loop seals remained filled with smaller amount of liquid and reactor vessel downcomer started voiding. The top half of the core was already filled with voids, but the heat removal remained sufficient to prevent core heatup. Larger amount of water was still kept in the pressurizer vessel. Sufficient heat transfer still proceeded through all three steam generators.

8) between the 8th draining (7500 s - core overheat to 350°C)

Core level dropped quickly and a sudden core overheat started already at the beginning of the last draining process. Level dropped in reactor vessel downcomer, mainly drained through the break and some pushed below the core. Pressurizer draining started, but that was not sufficient to cover the core sufficiently.

Heat transfer was suddenly interrupted through all three steam generators. The whole primary system, except bottom part of the reactor vessel, was empty by that time. The experiment has been prolonged after the initial core heatup, when operator applied ultimate procedure and opened SG secondary PORV. The vapor condensed in the whole primary system and collapsed into the core. Pressurizer was instantaneously drained. Heat transfer through the steam generators was restored and core heatup was stopped. However, the calculations were stopped when maximum cladding temperature reached 350°C (623 K).



RESULTS

There have been no changes introduced in any of the code versions. No deviations from the user guidelines have been introduced in the input decks. No sensitivity cases are presented in the report. The ISP-33 transient has been modelled up to the time when core heatup occurred in the defined base case and no simulation of the prolonged base case or the variation case is shown here.

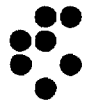
Basically, the model has been unchanged also for post-test calculations. Only a few changes have been made in the facility model in the post-test period, mainly because of some deficient or unclear initial condition data provided by the ISP-33 organizers. For the pretest calculation the core power was set 155 kW, but in the post-test period some uncertainty in core power measurement has been reported, so 165 kW was used for post-test calculation. The uncertainty of the measurement data were given by the organizers as follows:

- temperatures	± 1	K
- differential pressures	0.5 - 1	%
- absolute pressures	0.15 - 0.3	%
- flows	1 - 1.5	%
- levels	1.5 - 2.5	%
- core power	1	%

Beside the mentioned change in the input model, a small recirculation flow path has been modelled from upper plenum to upper head. This change has been introduced to achieve and stabilize initial upper head liquid temperature and match it to the experimental data. A servo valve has been modelled in the recirculation flow path governed by the difference of the actual and desired upper head temperature. In the transient the servo valve opening was fixed to the value which was stabilized in the steady-state. This procedure ensures achievement of the prescribed upper head liquid temperature, which is one of the essential parameters influencing the order of primary system emptying and bubble formation in the initial test period up to the second draining.

The procedure for the calculation was the same for MOD2 or MOD3.2. First the base input deck, given in Appendix A was run in steady-state mode. When the model has stabilized satisfactorily, the data from the output have been transferred to the base case input deck. Run mode has been switched to transient and recalculated for one time step, only to produce restart no.0. For the experiment simulation, run input deck, given in Appendix B, has been run from restart no.0. Few components for artificial pressure and level control have been deleted or controllers fixed to the final values achieved in the steady-state run. Trip logic for the experiment simulation has been added, as well as the drain valve and a part of the steam line. The transient has been then run till the stop trip has become true when the maximum cladding temperature has reached the prescribed value of 623 K.

For the completeness of the shown results the complete set of comparison plots, as requested by the ISP-33 organizers is given in Appendix C, together with the corresponding strip input deck.



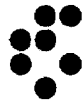
First the results of the RELAP5/MOD3.2 calculations are shown. Pre-test and post-test results are compared to the experimental data. After the 1st draining, primary pressure (Figure 5) dropped to the saturation value. Only the pressurizer has almost emptied (Figure 6), while the rest of the primary system remained filled with liquid. Single-phase natural circulation proceeded. When after the 2nd draining bubble was formed in all hot legs, single-phase natural circulation was interrupted. While the heat generated in the core could not be transported to the steam generators, primary pressure rise was observed. This pushed liquid back to the pressurizer and cleared the hot leg no. 1 loop seal (the one with the pressurizer). Several hot leg no. 1 loop seal clearings have been observed during this period [6]. Each time when the pressure peak was reached, liquid was partly drained back from the pressurizer and flooded the hot leg no. 1 loop seal. After the next draining liquid was finally drained from the pressurizer and hot leg loop seals, so the two-phase natural circulation took over the heat removal from the core. When the primary system was further emptied, liquid remained only in the reactor vessel, boiling as in a pool. Steam was carried to the steam generators, condensed there and drained back to the reactor vessel. Stalled natural circulation in the reactor vessel was shown to be sufficient to remove the heat from the core, while the core was still covered. After the 7th draining the core uncovered and heated up quickly. It can be observed that MOD3.2 calculated core heat-up one time interval too late, which means, that it was not able to predict liquid hold-up in the primary piping.

The most interesting part of the transient, between the 2nd and 3rd draining has been simulated very well by MOD3.2, already in the pretest calculation. The increased core power in the post-test calculation brought some slight improvement of the calculated parameters, but the influence of the introduced upper head recirculation can be more clearly seen. Since the upper head temperature decrease was slower, flashing occurred earlier in the upper head. This prevented total emptying of the pressurizer, which is an adverse influence, but it improved the primary pressure behaviour.

More problems were encountered in the MOD2 simulation, although it has to be mentioned, that it predicted the initial 1200 seconds of the steady state better than MOD3.2. The pressurizer heaters were supposed to maintain the primary pressure between 7.36 and 7.5 MPa automatically by switching between 2 and 6 kW power. It can be observed in Figure 7, that the primary pressure response to the pressurizer heaters cycling was correct. Some early flashing occurred in the upper head already after the 1st draining, which prevented total emptying of the pressurizer (Figure 8). The rising primary pressure pushed some liquid back to the pressurizer, but couldn't clear any of the hot leg loop seals, not even in the post-test calculation [6].

No significant differences were observed between pre-test and post-test calculations for both code versions. Some more differences between MOD2 and MOD3.2 can be seen on the following figures.

Some early flashing in the reactor vessel upper head and consequently reactor vessel inventory depletion can be observed on Figure 9 already between 1st and 2nd draining in MOD2 calculation. This prevented pressurizer to empty completely and less bubble was formed in hot legs. Single phase natural circulation has only been interrupted for a shorter time. Consequently the



primary pressure rise was not sufficient to clear any of the hot leg loop seals and push as much liquid back into the pressurizer as it happened in the experiment. The bubble has not been formed in the upper head before the second draining in MOD3.2 calculation, so the phenomena of single phase natural circulation interruption have been described correctly. After 6th draining it can be observed, that reactor vessel liquid inventory predicted by MOD3.2 was slightly lower than in MOD2 calculation, but it did not affect the further results. The calculation ended already after 7th draining, as in the experiment.

Both calculations show that core level has been kept too high in both calculations after the 6th draining. This is the indication that the liquid, which has accumulated in SG tubes in the experiment, has been drained back into the reactor vessel in RELAP5 calculations, which prevented core heat-up already after the 7th draining (Figure 10).

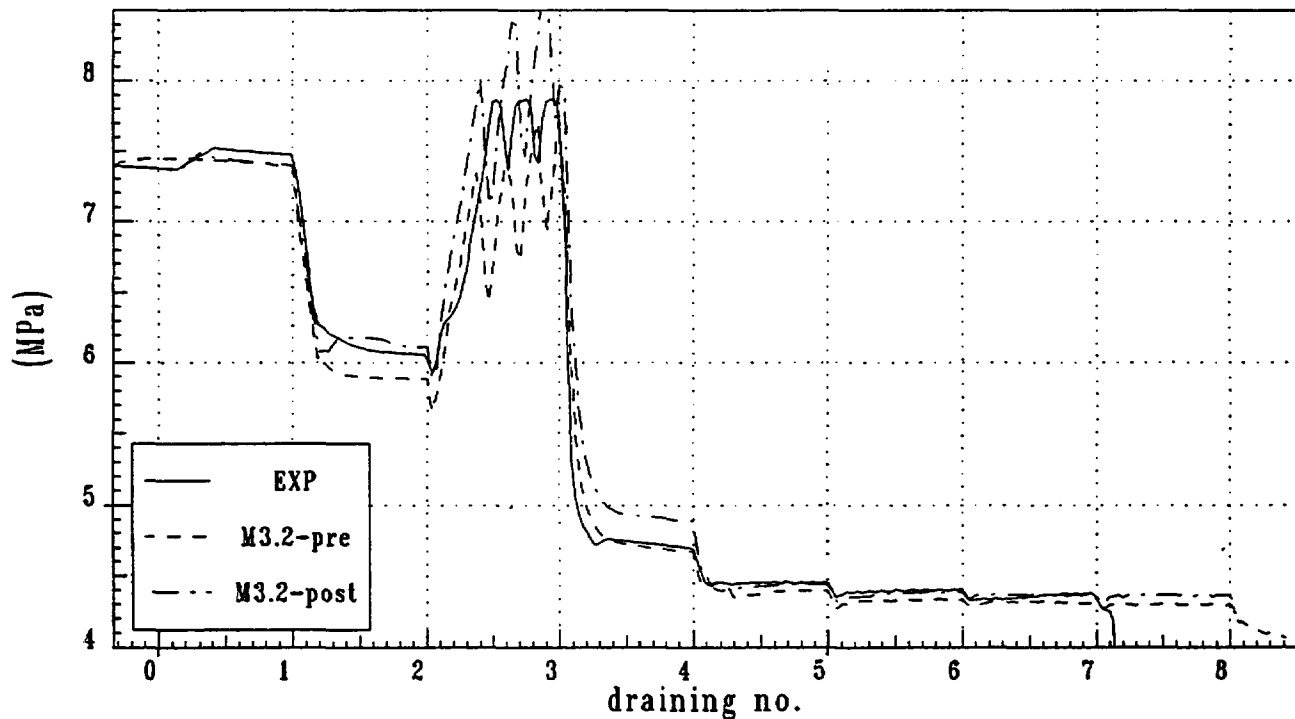


Figure 5: RELAP5/MOD3.2 - upper plenum pressure

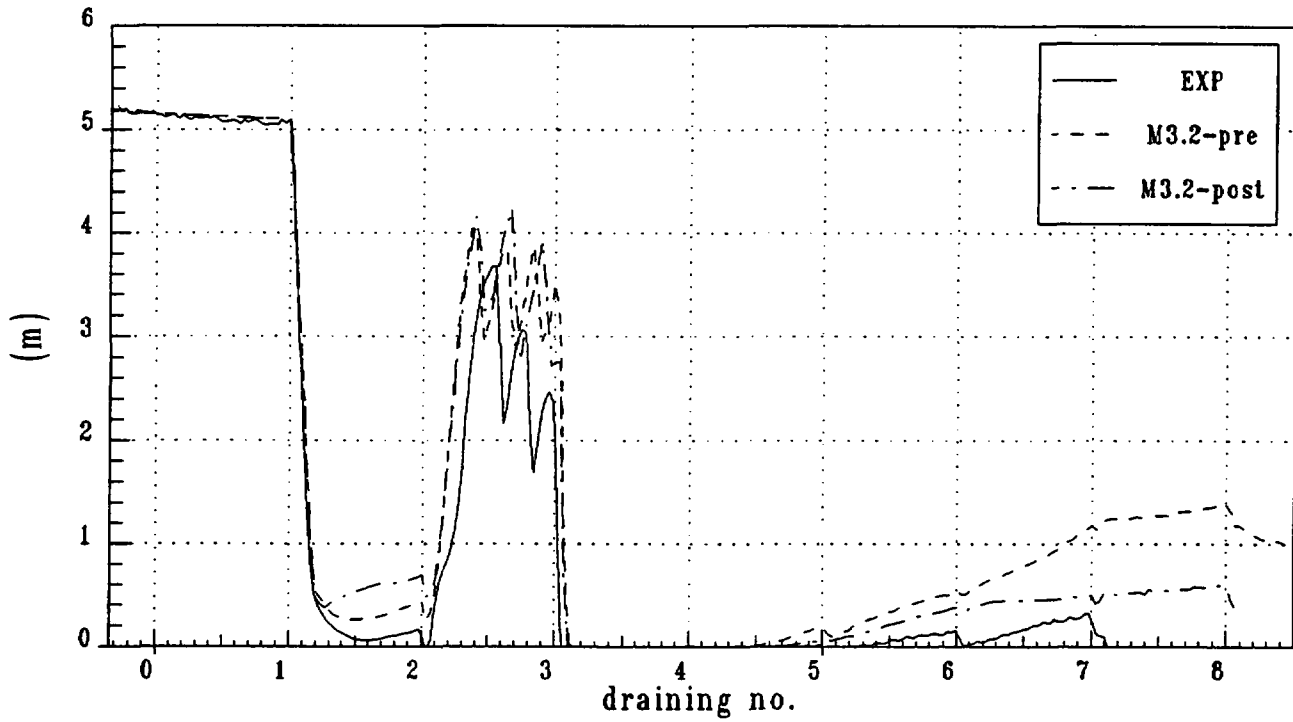
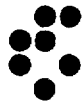


Figure 6: RELAP5/MOD3.2 - pressurizer level

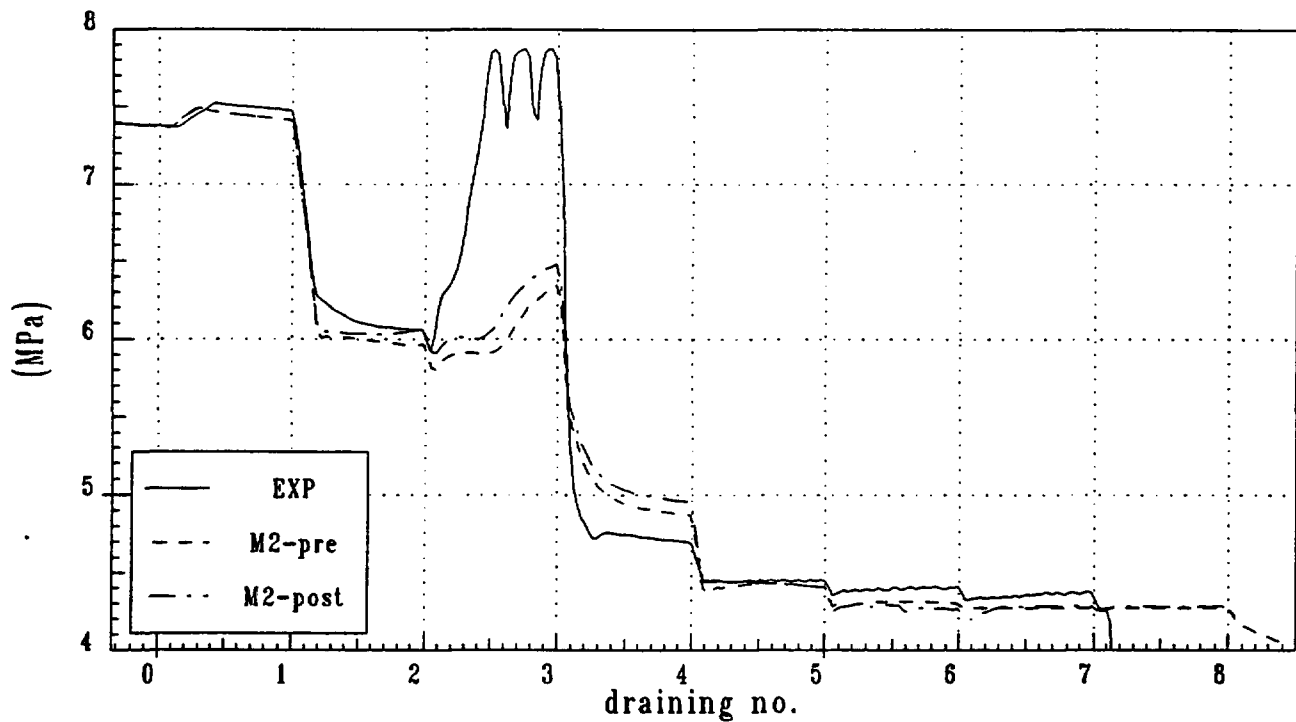


Figure 7: RELAP5/MOD2 - upper plenum pressure

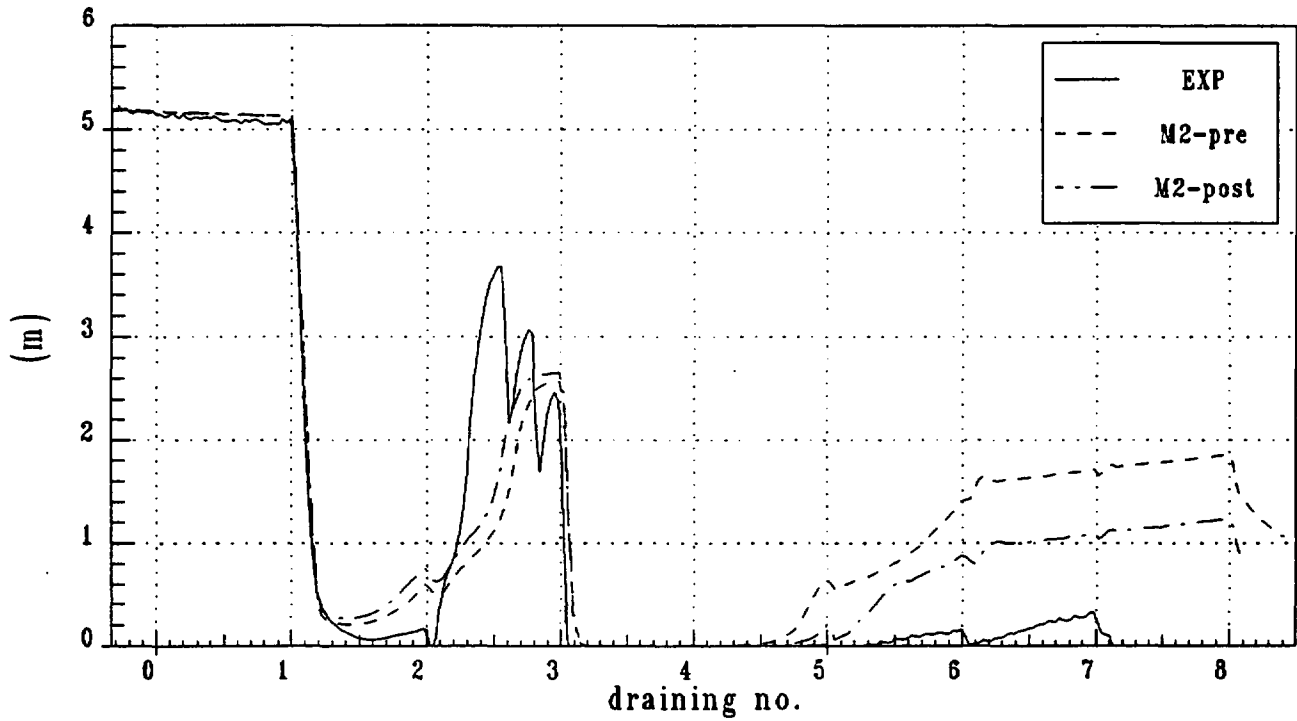
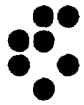


Figure 8: RELAP5/MOD2 - pressurizer level

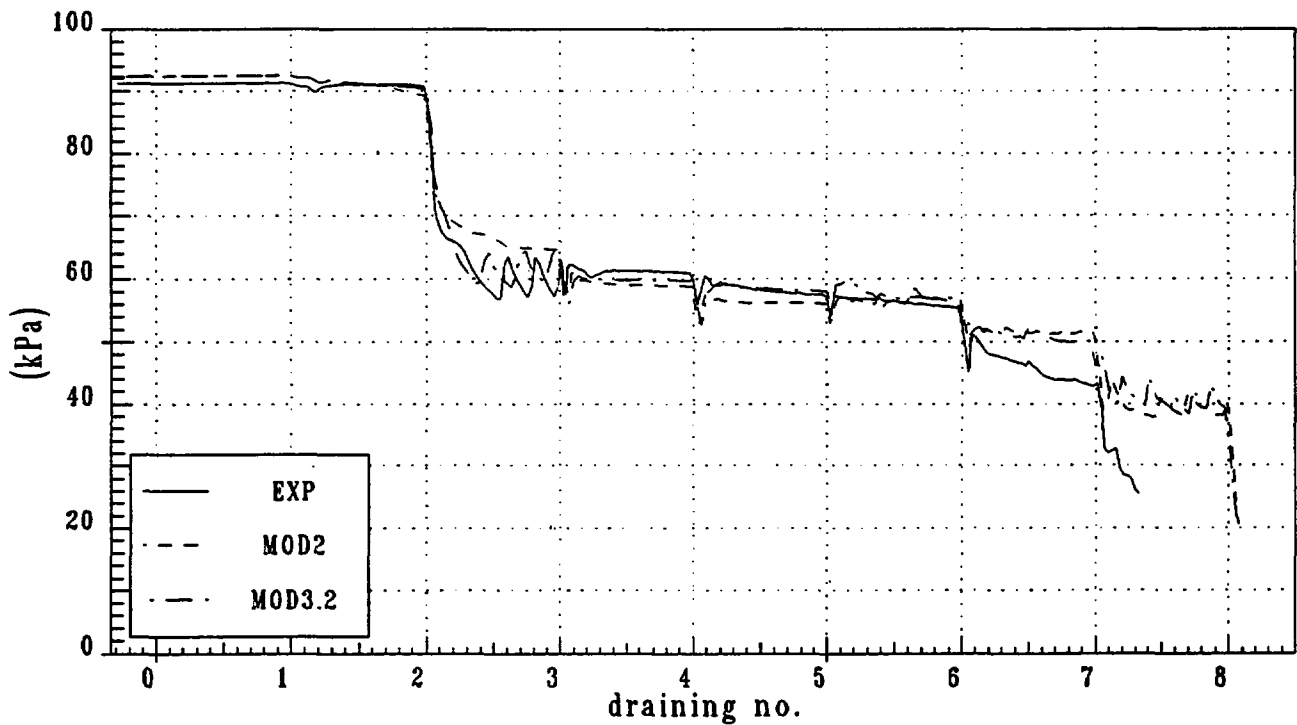


Figure 9: Comparison of RELAP5 predictions - DP over the reactor vessel

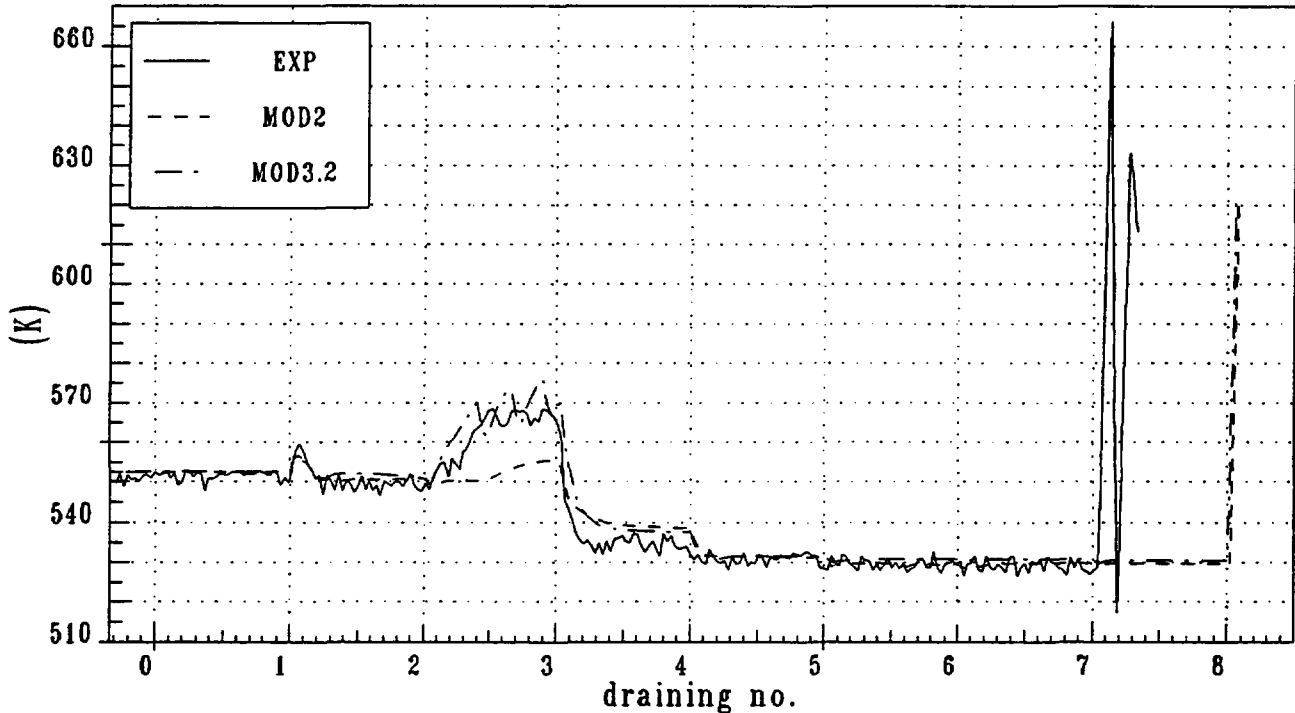
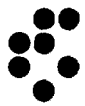


Figure 10: Comparison of RELAP5 predictions - maximum cladding temperatures

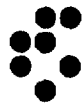
COMPUTER DATA AND RUN-TIME STATISTICS

MOD3.2 calculations have been performed on DEC Alpha with OpenVMS AXP Version V1.5 operating system, while the calculation with RELAP5/MOD2 has been performed on SUN Sparc 20 computer under SOLARIS 2.5 operating system. On average SUN computer is almost 4 times slower for RELAP5 calculations than DEC Alpha. RELAP5/MOD2 has not been installed on DEC Alpha computer, since there have been certain difficulties with the Fortran optimization option, so benchmarking was not successful.

Run-times for the pre-test and post-test calculations have been almost identical for both machines, since input models have been only slightly changed. Thus only run-time statistics for post-test calculations have been listed in Table 2. Time step has been kept constant at maximum value of 0.1 seconds for all the calculations and number of repeated time steps was less than 10.

Calculation	Computer time CPU (sec)	Total number of time steps (NT)	Number of volumes (N)	Grind time CPU/(N*DT)
RELAP5/MOD2	35308	75665	221	2.11E-3
RELAP5/MOD3.2	8957.5	75522	221	5.37E-4

Table 2: Run-time statistics for post-test calculations



CONCLUSIONS

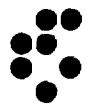
The ISP-33 experiment gives a very good basis for RELAP5 code assessment. The way it was performed, provides several sets of independent data, since each time interval between draining describes different SB LOCA phase.

Both RELAP5 code versions followed most of the transient reasonably well, with the exception that all predicted core over-heat one time interval too late. This was due to inability of both codes to hold as much water inside SG tubes, as the experiment showed. A post-test calculation with MOD2 proved, that only slight incitation of SG tubes enables RELAP5 to predict liquid hold-up in SG tubes and improves the results significantly. For MOD3.2 this was not sufficient, so water stayed more in the reactor vessel and core heatup occurred one draining later.

Some differences between the two code version results were observed in the most interesting part of the transient, after the second draining. While MOD3.2 predicted hot leg loop seal clearance and liquid push-up into the pressurizer, caused by primary pressure oscillations very well, MOD2 could not clear any of them at all. These differences can partly course in different heat transfer packages coded in the two versions. Better phase separation prediction, different interface heat transfer coefficients calculated, more vapor generation and sharper primary pressure rise in MOD3.2 calculations may origin in different heat transfer correlations and more sophisticated flow regime maps in MOD3.2 than in MOD2.

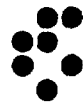
REFERENCES

- [1] H.Purhonen, J.Kouhia, H.Holmström: OECD/NEA/CSNI International Standard Problem No.33 (ISP-33), PACTEL - Natural Circulation Stepwise Coolant Inventory Reduction Experiment, Comparison Report, Draft, VTT Energy, Nuclear Energy, June 1994.
- [2] H.Purhonen, J.Miettinen: PACTEL - Parallel Channel Test Loop General Description for ISP, VTT Technical Research Centre of Finland, Nuclear Engineering Laboratory.
- [3] I.Parzer, S.Petelin, O.Gortnar, B.Mavko, M.Željko: ISP-33 PACTEL Pretest Calculation, IJS-DP-6528, Ljubljana, November 1992.
- [4] W.H.Ransom, R.J.Wagner, J.A.Trapp, L.R.Feinauer, G.W.Johnsen, D.M.Kiser, R.A.Riemke: RELAP5/MOD2 Code Manual, NUREG/CR-4321, EGG-2396, Idaho Falls, Idaho, USA, August 1985.
- [5] RELAP5/MOD3 Code Manual, NUREG/CR-5535, INEL-95/0174 (Formerly EGG-2596), Idaho Falls, Idaho, USA, June 1995.
- [6] I.Parzer, S.Petelin, O.Gortnar: Hot Leg Loop Seal Clearance Prediction in ISP-33, ASME 1993 Winter Annual Meeting, New Orleans, November 28 -December 3, 1993, PVP-Vol.267 Unsteady Flows, pp.: 17-19.



Appendix A

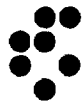
ISP-33 Steady State Input Deck



```

= isp-33: pactel (vtt, lappeenranta, finland)
*
* natural circulation test - master input deck
* created: 24-jul-1992 ; ip
* revised: 21-aug-1992 ; ip
* revised: 8-oct-1992 ; ip + mz
* revised: 16-oct-1992 ; og (??? warnings)
*
100 new transnt
*
120 103020000 0.07 h2o primary
121 601010000 9.8 h2o secondry
*
201 800.0 1.-6 0.1 3 50 40000 40000
*
*****
*               m i n o r   e d i t   r e q u e s t s               *
*****
20800001 dt 0
20800002 dtcrnt 0
*
301  cntrlvar      100 * core (heater) power
302  mflowj       106040000 * core
303  mflowj       124000000 * core bypass
305  cntrlvar      102 * core power - calorimetric
306  cntrlvar      307 * sg tubes power - calorimetric
310  p            107010000 * upper plenum
311  mflowj       101040000 * downcomer inlet
312  tempf        101010000 * downcomer inlet
313  tempf        107030000 * vessel outlet
320  p            202100000 * pressurizer
321  cntrlvar      172 * pressurizer level
322  cntrlvar      202 * pressurizer heater power
330  p            601010000 * sg-1
331  mflowj       652000000 * sg-1 feedwater
332  cntrlvar      301 * sg-1 tubes power - calorimetric
333  mflowj       301050000 * loop-1
340  p            701010000 * sg-2
341  mflowj       752000000 * sg-2 feedwater
342  cntrlvar      302 * sg-2 tubes power - calorimetric
343  mflowj       401050000 * loop-2
350  p            801010000 * sg-3
351  mflowj       852000000 * sg-3 feedwater
352  cntrlvar      303 * sg-3 tubes power - calorimetric
353  mflowj       501050000 * loop-3
*
* initialization block:
*
355  tempf        104010000 * tcold - core inlet [k]
356  mflowj       123000000 * downcomer mass flow rate [kg/s]
357  cntrlvar      930 * control valve stem position [-]
358  httemp       106000607 * tcal7h 1479
359  cntrlvar      931 * control valve stem position [-]
361  mflowj       211000000 * art. prz liquid level control [kg/s]
362  mflowj       221000000 * art. prz pressure control [kg/s]
*
365  voidf        605010000 * separator 1 [-]
366  voidf        705010000 * separator 2 [-]
367  voidf        805010000 * separator 3 [-]
371  mflowj       655000000 * art. sg-1 feedwater
372  mflowj       755000000 * art. sg-2 feedwater

```



```

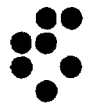
373  mflowj      855000000 * art. sg-3 feedwater
378  cntrlvar    175 * sg1 collapsed level [m]
379  cntrlvar    176 * sg2 collapsed level [m]
380  cntrlvar    177 * sg3 collapsed level [m]
*
* sg1 recirculation control
381  mflowj      605030000 * separator inlet [kg/s]
382  mflowj      613010000 * level 3 cross [kg/s]
383  mflowj      612010000 * level 2 cross [kg/s]
384  mflowj      611010000 * level 1 cross [kg/s]
*
390  p           900010000 * art. steam line pressure [pa]
391  mflowj      904000000 * steam line flow [kg/s]
392  cntrlvar    925 * total heat losses [kw]
*
* upper head temperature
395  tempf      108030000 * upper head
396  cntrlvar    179 * upper head controller
*
*****
*                               t r i p s                               *
*****
*
*
*****
*   c o n t r o l   v a r i a b l e s   f o r   m i n o r   e d i t   *
*****
*
* ctv 100: core heater power
20510000 heatpowr function 1.-3 0 1
20510001 time 0 100
*
* ctv 102: core power
20510200 corepowr sum 1.-3 0 1
20510201 0 1. q 106010000 1. q 106020000 1. q 106030000 1. q 106040000
20510202 1. q 106050000 1. q 106060000 1. q 106070000 1. q 106080000
20510203 1. q 106090000 1. q 105010000
*
* ctv 104: core heater power per channel (for minor edit only)
20510400 cor3powr sum 333. 0 1
20510401 0 1. cntrlvar 100
*
* ctv 105: core liquid mass
20510500 coremass sum 1.-3 0 1
20510501 0 3.03307 rho 106010000 3.03307 rho 106020000 3.03307 rho 106030000
20510502 3.03307 rho 106040000 3.03307 rho 106050000 3.03307 rho 106060000
20510503 3.03307 rho 106070000 3.03307 rho 106080000 3.03307 rho 106090000
*
* ctv 106: sg 1 primary inlet/outlet mass
20510600 sgliomas sum 1.-3 0 1
20510601 0 7.01350 rho 321010000 7.01350 rho 322010000 7.01350 rho 323010000
20510602 7.01350 rho 331010000 7.01350 rho 332010000 7.01350 rho 333010000
*
* ctv 107: sg 2 primary inlet/outlet mass
20510700 sg2iomass sum 1.-3 0 1
20510701 0 7.01350 rho 421010000 7.01350 rho 422010000 7.01350 rho 423010000
20510702 7.01350 rho 431010000 7.01350 rho 432010000 7.01350 rho 433010000
*
* ctv 108: sg 3 primary inlet/outlet mass
20510800 sg3iomass sum 1.-3 0 1
20510801 0 7.01350 rho 521010000 7.01350 rho 522010000 7.01350 rho 523010000
    
```



```

20510802      7.01350 rho 531010000  7.01350 rho 532010000  7.01350 rho 533010000
*
* ctv 111: vessel mass (parameter 123: vessmass = ctv 111 + ctv 105)
20511100 vessmass sum      1.-3 0 1
20511101 0  4.28300 rho 101010000  5.63112 rho 102010000  10.3237 rho 102020000
20511102      4.09536 rho 102030000  1.10916 rho 102040000  7.66400 rho 103010000
20511103      7.66400 rho 103020000  35.2237 rho 103030000  3.98528 rho 103040000
20511104      12.8295 rho 103050000  16.0416 rho 104010000  6.41300 rho 105010000
20511105      31.7800 rho 107010000  25.4169 rho 107020000  25.4169 rho 107030000
20511106      32.2170 rho 108010000  32.2170 rho 108020000  32.2170 rho 108030000
20511107      11.5186 rho 111010000  35.2237 rho 130010000
*
* ctv 112: pressurizer mass (parameter 124: przmass)
20511200 przmass sum      1.-3 0 1
20511201 0  1.17070 rho 200010000  1.11808 rho 200020000  1.11808 rho 200030000
20511202      .940306 rho 200040000  13.1889 rho 202010000  13.3047 rho 202020000
20511203      13.4528 rho 202030000  13.4886 rho 202040000  13.4886 rho 202050000
20511204      13.4886 rho 202060000  13.4886 rho 202070000  13.4886 rho 202080000
20511205      13.4886 rho 202090000  13.4886 rho 202100000
*
* ctv 113: hot leg 1 mass (parameter 125: hot11mass)
20511300 h11mass sum      1.-3 0 1
20511301 0  2.31817 rho 301010000  1.54932 rho 301020000  1.54932 rho 301030000
20511302      1.54932 rho 301040000  1.54932 rho 301050000  1.70725 rho 301060000
20511303      1.70725 rho 301070000  1.51244 rho 301080000  1.51244 rho 301090000
20511304      1.51244 rho 301100000  1.51244 rho 301110000
*
* ctv 114: hot leg 2 mass (parameter 126: hot12mass)
20511400 h12mass sum      1.-3 0 1
20511401 0  2.76689 rho 401010000  1.54932 rho 401020000  1.54932 rho 401030000
20511402      1.54932 rho 401040000  1.54932 rho 401050000  1.51674 rho 401060000
20511403      1.65559 rho 401070000  1.51244 rho 401080000  1.51244 rho 401090000
20511404      1.51244 rho 401100000  1.51244 rho 401110000
*
* ctv 115: hot leg 3 mass (parameter 127: hot13mass)
20511500 h13mass sum      1.-3 0 1
20511501 0  2.31817 rho 501010000  1.54932 rho 501020000  1.54932 rho 501030000
20511502      1.54932 rho 501040000  1.54932 rho 501050000  1.68142 rho 501060000
20511503      1.68142 rho 501070000  1.51244 rho 501080000  1.51244 rho 501090000
20511504      1.51244 rho 501100000  1.51244 rho 501110000
*
* ctv 116: sg 1 tubes mass (parameter 128: sgtubemass = ctv 116 + ctv 106)
20511600 sg1tmass sum      1.-3 0 1
20511601 0  2.50994 rho 325010000  2.50994 rho 325020000  2.50994 rho 325030000
20511602      2.50994 rho 325040000  2.50994 rho 325050000  2.50994 rho 325060000
20511603      2.91997 rho 326010000  2.91997 rho 326020000  2.91997 rho 326030000
20511604      2.91997 rho 326040000  2.91997 rho 326050000  2.91997 rho 326060000
20511605      1.94665 rho 327010000  1.94665 rho 327020000  1.94665 rho 327030000
20511606      1.94665 rho 327040000  1.94665 rho 327050000  1.94665 rho 327060000
*
* ctv 117: sg 2 tubes mass (parameter 129: sgtube2mass = ctv 117 + ctv 107)
20511700 sg2tmass sum      1.-3 0 1
20511701 0  2.50994 rho 425010000  2.50994 rho 425020000  2.50994 rho 425030000
20511702      2.50994 rho 425040000  2.50994 rho 425050000  2.50994 rho 425060000
20511703      2.91997 rho 426010000  2.91997 rho 426020000  2.91997 rho 426030000
20511704      2.91997 rho 426040000  2.91997 rho 426050000  2.91997 rho 426060000
20511705      1.94665 rho 427010000  1.94665 rho 427020000  1.94665 rho 427030000
20511706      1.94665 rho 427040000  1.94665 rho 427050000  1.94665 rho 427060000
*
* ctv 118: sg 3 tubes mass (parameter 130: sgtube3mass = ctv 118 + ctv 108)
20511800 sg3tmass sum      1.-3 0 1

```



```

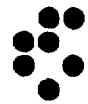
20511801 0 2.50994 rho 525010000 2.50994 rho 525020000 2.50994 rho 525030000
20511802 2.50994 rho 525040000 2.50994 rho 525050000 2.50994 rho 525060000
20511803 2.91997 rho 526010000 2.91997 rho 526020000 2.91997 rho 526030000
20511804 2.91997 rho 526040000 2.91997 rho 526050000 2.91997 rho 526060000
20511805 1.94665 rho 527010000 1.94665 rho 527020000 1.94665 rho 527030000
20511806 1.94665 rho 527040000 1.94665 rho 527050000 1.94665 rho 527060000
*
* ctv 119: cold leg 1 mass (parameter 131: coldl1mass)
20511900 cllmass sum 1.-3 0 1
20511901 0 1.51244 rho 351010000 1.51244 rho 351020000 1.51244 rho 351030000
20511902 1.51244 rho 351040000 1.32979 rho 351050000 1.46280 rho 351060000
20511903 1.46280 rho 351070000 1.46280 rho 351080000 1.46280 rho 351090000
20511904 1.25427 rho 351100000 1.25427 rho 351110000 1.71616 rho 351120000
20511905 1.71616 rho 351130000 1.11400 rho 351140000
*
* ctv 120: cold leg 2 mass (parameter 132: coldl2mass)
20512000 cl2mass sum 1.-3 0 1
20512001 0 1.51244 rho 451010000 1.51244 rho 451020000 1.51244 rho 451030000
20512002 1.51244 rho 451040000 1.43308 rho 451050000 1.46280 rho 451060000
20512003 1.46280 rho 451070000 1.46280 rho 451080000 1.46280 rho 451090000
20512004 1.34465 rho 451100000 1.34465 rho 451110000 1.71616 rho 451120000
20512005 1.71616 rho 451130000 1.11400 rho 451140000
*
* ctv 121: cold leg 3 mass (parameter 133: coldl3mass)
20512100 cl3mass sum 1.-3 0 1
20512101 0 1.51244 rho 551010000 1.51244 rho 551020000 1.51244 rho 551030000
20512102 1.51244 rho 551040000 1.25233 rho 551050000 1.46280 rho 551060000
20512103 1.46280 rho 551070000 1.46280 rho 551080000 1.46280 rho 551090000
20512104 1.29299 rho 551100000 1.29299 rho 551110000 1.71616 rho 551120000
20512105 1.71616 rho 551130000 1.11400 rho 551140000
*
* ctv 122: primary mass (parameter 122: primass)
20512200 primmass sum 1. 0 1
20512201 0 1. cntrlvar 105 1. cntrlvar 106 1. cntrlvar 107 1. cntrlvar 108
20512202 1. cntrlvar 111 1. cntrlvar 112 1. cntrlvar 113 1. cntrlvar 114
20512203 1. cntrlvar 115 1. cntrlvar 116 1. cntrlvar 117 1. cntrlvar 118
20512204 1. cntrlvar 119 1. cntrlvar 120 1. cntrlvar 121
*
* ctv 131: sg 1 secondary mass (parameter 134: sgsec1mass)
20513100 sg1smass sum 1.-3 0 1
20513101 0 78.9228 rho 601010000 71.2339 rho 602010000 48.4271 rho 603010000
20513102 75.2786 rho 605010000 83.7316 rho 606010000 19.7307 rho 611010000
20513103 17.8085 rho 612010000 12.1068 rho 613010000
*
* ctv 132: sg 2 secondary mass (parameter 135: sgsec2mass)
20513200 sg2smass sum 1.-3 0 1
20513201 0 78.9228 rho 701010000 71.2339 rho 702010000 48.4271 rho 703010000
20513202 75.2786 rho 705010000 83.7316 rho 706010000 19.7307 rho 711010000
20513203 17.8085 rho 712010000 12.1068 rho 713010000
*
* ctv 133: sg 3 secondary mass (parameter 136: sgsec3mass)
20513300 sg3smass sum 1.-3 0 1
20513301 0 78.9228 rho 801010000 71.2339 rho 802010000 48.4271 rho 803010000
20513302 75.2786 rho 805010000 83.7316 rho 806010000 19.7307 rho 811010000
20513303 17.8085 rho 812010000 12.1068 rho 813010000
*
* ctv 144: dp upper plenum (parameter 44: dp18up = dp18up_8890up_12130)
20514400 dp18up sum 1.-3 0 1
20514401 0 1. p 108010000 -1. p 108030000
20514402 4.38 rho 108010000 4.381 rho 108030000
* center 108010000 = 9.33665 ; center 108030000 = 11.68325
    
```



```

* korekcija: .44665*9.80665 = 4.38 ; .44675*9.80665 = 4.381
*
* ctv 145: dp uppl-core (parameter 45: dp17upco = dp17up_8890co_6050)
20514500 dp17upco sum 1.-3 0 1
20514501 0 1. p 107010000 -1. p 108010000
20514502 3.04 rho 107010000 -4.38 rho 108010000
* center 107010000 = 6.36 ; center 108010000 = 9.33665
* korekcija: .31*9.80665 = 3.04 ; -.44665*9.80665 = 4.38
*
* ctv 146: dp uppl-lowpl (parameter 46: dp19uplp = dp19up_12130lp_0070)
20514600 dp19uplp sum 1.-3 0 1
20514601 0 1. p 103020000 -1. p 108030000
20514602 4.381 rho 108030000
* center 103020000 = 0.07 ; center 108030000 = 11.68325
* korekcija: ; .44675*9.80665 = 4.381
*
* ctv 147: dp core (parameter 47: dp16co = dp16co_6050co_3300)
20514700 dp16co sum 1.-3 0 1
20514701 0 1. p 104010000 -1. p 107010000
20514702 -2.648 rho 104010000 -3.04 rho 107010000
* center 104010000 = 3.03 ; center 107010000 = 6.36
* korekcija: -.27*9.80665 = 2.648 ; -.31*9.80665 = 3.04
*
* ctv 148: dp downc-lowpl (parameter 48: dp23dclp = dp23dc_7900lp_0070)
20514800 dp23dclp sum 1.-3 0 1
20514801 0 1. p 103010000 -1. p 111010000
20514802 2.01 rho 111010000
* center 103010000 = 0.07 ; center 111010000 = 7.695
* korekcija: ; .205*9.80665 = 2.01
*
* ctv 149: dp pressurizer (parameter 49: dp24pz = dp24pz_16490pz_8040)
20514900 dp24pz sum 1.-3 0 1
20514901 0 1. p 202010000 -1. p 202100000
20514902 3.334 rho 202010000 2.844 rho 202100000
* center 202010000 = 8.38 ; center 202100000 = 16.2
* korekcija: .34*9.80665 = 3.334 ; .29*9.80665 = 2.844
*
* ctv 150: dp uppl-hot leg 1 (parameter 50: dp28uph1 = dp28up_8890h11_6790)
20515000 dp28uph1 sum 1.-3 0 1
20515001 0 1. p 301060000 -1. p 108010000
20515002 0.294 rho 301060000 -4.38 rho 108010000
* center 301060000 = 6.82 ; center 108010000 = 9.33665
* korekcija: .03*9.80665 = .294 ; -.44665*9.80665 = -4.38
*
* ctv 151: dp hot leg 1 (parameter 51: dp25h1 = dp25h1_9500h11_6790)
20515100 dp25h1 sum 1.-3 0 1
20515101 0 1. p 301060000 -1. p 301110000
20515102 0.294 rho 301060000 2.283 rho 301110000
* center 301060000 = 6.82 ; center 301110000 = 9.2672
* korekcija: .03*9.80665 = .294 ; .2328*9.80665 = 2.283
*
* ctv 152: dp h11-cl1 (parameter 52: dp30h11cl1 = dp30h11_9500cl1_9500)
20515200 dp30h1cl1 sum 1.-3 0 1
20515201 0 1. p 301110000 -1. p 351010000
20515202 -2.283 rho 301110000 2.283 rho 351010000
* center 301110000 = 9.2672 ; center 351010000 = 9.2672
* korekcija: -.2328*9.80665 = 2.283 ; -.2328*9.80665 = 2.283
*
* ctv 153: dp cold leg 1 (parameter 53: dp26cl1 = dp26cl1_9500cl1_6790)
20515300 dp26cl1 sum 1.-3 0 1
20515301 0 1. p 351050000 -1. p 351010000

```



```
20515302    0.294 rho 351050000    2.283 rho 351010000
* center 351050000 = 6.82 ; center 351010000 = 9.2672
* korekcija: .03*9.80665 = .294 ; .2328*9.80665 = 2.283
*
* ctv 154: dp cold leg 1 (parameter 54: dp29dcc11 = dp29dc_7900c11_6790)
20515400 dp29dcc1 sum      1.-3 0 1
20515401 0 1.    p  351050000 -1.    p  111010000
20515402    0.294 rho 351050000    2.01 rho 111010000
* center 351050000 = 6.82 ; center 111010000 = 7.695
* korekcija: .03*9.80665 = .294 ; .205*9.80665 = 2.01
*
* ctv 155: dp uppl-hot leg 2 (parameter 55: dp33uph12 = dp33up_8890h12_6790)
20515500 dp33uph2 sum      1.-3 0 1
20515501 0 1.    p  401060000 -1.    p  108010000
20515502    0.294 rho 401060000   -4.38 rho 108010000
* center 401060000 = 6.82 ; center 108010000 = 9.33665
* korekcija: .03*9.80665 = .294 ; -.44665*9.80665 = -4.38
*
* ctv 156: dp hot leg 2 (parameter 56: dp34h11 = dp34h12_9500h12_6790)
20515600 dp34h12 sum      1.-3 0 1
20515601 0 1.    p  401060000 -1.    p  401110000
20515602    0.294 rho 401060000    2.283 rho 401110000
* center 401060000 = 6.82 ; center 401110000 = 9.2672
* korekcija: .03*9.80665 = .294 ; .2328*9.80665 = 2.283
*
* ctv 157: dp h12-cl2 (parameter 57: dp32h12c12 = dp32h12_9500c12_9500)
20515700 dp32h2c2 sum      1.-3 0 1
20515701 0 1.    p  401110000 -1.    p  451010000
20515702   -2.283 rho 401110000    2.283 rho 451010000
* center 401110000 = 9.2672 ; center 451010000 = 9.2672
* korekcija: -.2328*9.80665 = 2.283 ; -.2328*9.80665 = 2.283
*
* ctv 158: dp cold leg 2 (parameter 58: dp35c12 = dp35c12_9500c12_6790)
20515800 dp35c12 sum      1.-3 0 1
20515801 0 1.    p  451050000 -1.    p  451010000
20515802    0.294 rho 451050000    2.283 rho 451010000
* center 451050000 = 6.82 ; center 451010000 = 9.2672
* korekcija: .03*9.80665 = .294 ; .2328*9.80665 = 2.283
*
* ctv 159: dp cold leg 2 (parameter 59: dp36dcc12 = dp36dc_7900c12_6790)
20515900 dp36dcc2 sum      1.-3 0 1
20515901 0 1.    p  451050000 -1.    p  111010000
20515902    0.294 rho 451050000    2.01 rho 111010000
* center 451050000 = 6.82 ; center 111010000 = 7.695
* korekcija: .03*9.80665 = .294 ; .205*9.80665 = 2.01
*
* ctv 160: dp uppl-hot leg 3 (parameter 60: dp39uph13 = dp39up_8890h13_6790)
20516000 dp39uph3 sum      1.-3 0 1
20516001 0 1.    p  501060000 -1.    p  108010000
20516002    0.294 rho 501060000   -4.38 rho 108010000
* center 501060000 = 6.82 ; center 108010000 = 9.33665
* korekcija: .03*9.80665 = .294 ; -.44665*9.80665 = -4.38
*
* ctv 161: dp hot leg 3 (parameter 61: dp40h13 = dp40h13_9500h13_6790)
20516100 dp40h13 sum      1.-3 0 1
20516101 0 1.    p  501060000 -1.    p  501110000
20516102    0.294 rho 501060000    2.283 rho 501110000
* center 501060000 = 6.82 ; center 501110000 = 9.2672
* korekcija: .03*9.80665 = .294 ; .2328*9.80665 = 2.283
*
* ctv 162: dp h13-cl3 (parameter 62: dp38h13c13 = dp38h13_9500c13_9500)
```




```

20516200 dp38h3c3 sum 1.-3 0 1
20516201 0 1. p 501110000 -1. p 551010000
20516202 -2.283 rho 501110000 2.283 rho 551010000
* center 501110000 = 9.2672 ; center 551010000 = 9.2672
* korekcija: -.2328*9.80665 = 2.283 ; -.2328*9.80665 = 2.283
*
* ctv 163: dp cold leg 3 (parameter 63: dp41cl3 = dp41cl3_9500cl3_6790)
20516300 dp41cl3 sum 1.-3 0 1
20516301 0 1. p 551050000 -1. p 551010000
20516302 0.294 rho 551050000 2.283 rho 551010000
* center 551050000 = 6.82 ; center 551010000 = 9.2672
* korekcija: .03*9.80665 = .294 ; .2328*9.80665 = 2.283
*
* ctv 164: dp cold leg 3 (parameter 64: dp42dcc13 = dp42dc_7900cl3_6790)
20516400 dp42dcc3 sum 1.-3 0 1
20516401 0 1. p 551050000 -1. p 111010000
20516402 0.294 rho 551050000 2.01 rho 111010000
* center 551050000 = 6.82 ; center 111010000 = 7.695
* korekcija: .03*9.80665 = .294 ; .205*9.80665 = 2.01
*
* ctv 165: dp sg 1 secondary (parameter 113: dp27sg1s = dp27sg1_9800sg1_9800)
20516500 dp27sg1s sum 1.-3 0 1
20516501 0 1. p 601010000 -1. p 606010000
20516502 0.545 rho 601010000
* center 601010000 = 9.8556
* korekcija: .0556*9.80665 = .545
*
* ctv 166: dp sg 2 secondary (parameter 114: dp31sg2s = dp31sg2_9800sg2_9800)
20516600 dp31sg2s sum 1.-3 0 1
20516601 0 1. p 701010000 -1. p 706010000
20516602 0.545 rho 701010000
* center 701010000 = 9.8556
* korekcija: .0556*9.80665 = .545
*
* ctv 167: dp sg 3 secondary (parameter 115: dp37sg3s = dp37sg3_9800sg3_9800)
20516700 dp37sg3s sum 1.-3 0 1
20516701 0 1. p 801010000 -1. p 806010000
20516702 0.545 rho 801010000
* center 801010000 = 9.8556
* korekcija: .0556*9.80665 = .545
*
* ctv 171: primary level (parameter 71: from dp19uplp) ; now coll.level ???
20517100 lepr sum 1. 0 1
20517101 0 2.07 voidf 103030000 .26 voidf 103040000 .3 voidf 103050000
20517102 .66 voidf 104010000 1.16 voidf 107010000 .905 voidf 107020000
20517103 .905 voidf 107030000 1. cntrlvar 74 1. cntrlvar 78
*
* ctv 172: pressurizer level (parameter 72: from dp24pz) ; now coll.level ???
20517200 lepz sum 1. 0 1
20517201 0 .68 voidf 202010000 .88 voidf 202020000 .88 voidf 202030000
20517202 .88 voidf 202040000 .88 voidf 202050000 .88 voidf 202060000
20517203 .88 voidf 202070000 .88 voidf 202080000 .88 voidf 202090000
20517204 .88 voidf 202100000
*
* ctv 173: downcomer level (parameter 73: from dp23dclp) ; now coll.level ???
20517300 ledc sum 1. 0 1
20517301 0 2.07 voidf 130010000 .26 voidf 102040000 .96 voidf 102030000
20517302 2.42 voidf 102020000 1.32 voidf 102010000 .25 voidf 101010000
20517303 .55 voidf 111010000
*
* ctv 74: upper plenum level (parameter 74: from dp18up) ; now coll.level ???

```

University of Ljubljana
 "Jožef Stefan" Institute, Ljubljana, Slovenia



```

20507400 leup      sum 1. 0 1
20507401 0 1.1733 voidf 108010000 1.1733 voidf 108020000 1.0334 voidf 108030000
*
* ctv 175: sg 1 level (parameter 75: from dp27sg1s) ; now collapsed level ???
20517500 lesg1    sum 1. 0 1
20517501 0.0 0.1112 voidf 601010000 0.072 voidf 602010000
20517502          0.0480 voidf 603010000 0.050 voidf 605010000
20517503          0.0852 voidf 606010000
*
* ctv 176: sg 2 level (parameter 76: from dp31sg2s) ; now collapsed level ???
20517600 lesg2    sum 1. 0 1
20517601 0.0 0.1112 voidf 701010000 0.072 voidf 702010000
20517602          0.0480 voidf 703010000 0.050 voidf 705010000
20517603          0.0852 voidf 706010000
*
* ctv 177: sg 3 level (parameter 77: from dp37sg3s) ; now collapsed level ???
20517700 lesg3    sum 1. 0 1
20517701 0.0 0.1112 voidf 801010000 0.072 voidf 802010000
20517702          0.0480 voidf 803010000 0.050 voidf 805010000
20517703          0.0852 voidf 806010000
*
* ctv 78: core level (parameter 78) ; now collapsed level ???
20507800 leco     sum 1. 0 1
20507801 0 .26889 voidf 106010000 .26889 voidf 106020000 .26889 voidf 106030000
20507802          .26889 voidf 106040000 .26889 voidf 106050000 .26889 voidf 106060000
20507803          .26889 voidf 106070000 .26889 voidf 106080000 .26889 voidf 106090000
*
* ctv 301: sg-1 tubes power - primary side
20530100 tub1ppow sum 1.-3 0 1
20530101 0 1. q 325010000 1. q 325020000 1. q 325030000 1. q 325040000
20530102          1. q 325050000 1. q 325060000 1. q 326010000 1. q 326020000
20530103          1. q 326030000 1. q 326040000 1. q 326050000 1. q 326060000
20530104          1. q 327010000 1. q 327020000 1. q 327030000 1. q 327040000
20530105          1. q 327050000 1. q 327060000
*
* ctv 302: sg-2 tubes power - primary side
20530200 tub2ppow sum 1.-3 0 1
20530201 0 1. q 425010000 1. q 425020000 1. q 425030000 1. q 425040000
20530202          1. q 425050000 1. q 425060000 1. q 426010000 1. q 426020000
20530203          1. q 426030000 1. q 426040000 1. q 426050000 1. q 426060000
20530204          1. q 427010000 1. q 427020000 1. q 427030000 1. q 427040000
20530205          1. q 427050000 1. q 427060000
*
* ctv 303: sg-3 tubes power - primary side
20530300 tub3ppow sum 1.-3 0 1
20530301 0 1. q 525010000 1. q 525020000 1. q 525030000 1. q 525040000
20530302          1. q 525050000 1. q 525060000 1. q 526010000 1. q 526020000
20530303          1. q 526030000 1. q 526040000 1. q 526050000 1. q 526060000
20530304          1. q 527010000 1. q 527020000 1. q 527030000 1. q 527040000
20530305          1. q 527050000 1. q 527060000
*
* ctv 304: sg-1 tubes power - secondary side
20530400 tub1spow sum 1.-3 0 1
20530401 0 1. q 601010000 1. q 602010000 1. q 603010000
*
* ctv 305: sg-2 tubes power - secondary side
20530500 tub2spow sum 1.-3 0 1
20530501 0 1. q 701010000 1. q 702010000 1. q 703010000
*
* ctv 306: sg-3 tubes power - secondary side
20530600 tub3spow sum 1.-3 0 1
    
```

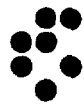


```

20530601 0 1. q 801010000 1. q 802010000 1. q 803010000
*
* ctv 307: sg tubes power - primary side
20530700 sgripow sum 1. 0 1
20530701 0 1. cntrlvar 301 1. cntrlvar 302 1. cntrlvar 303
*
* ctv 308: sg tubes power - secondary side
20530800 sgsecpow sum 1. 0 1
20530801 0 1. cntrlvar 304 1. cntrlvar 305 1. cntrlvar 306
*
*****
*
* reactor model
*
*****
*
* downcomer top part
1110000 dc-top branch
1110101 0 .69 11.5186-3 0 90. .69 2.-6 .0823 00
1111101 101000000 111000000 0 0 0 00000
*
* reactor inlet part
1010000 dc-inlet branch
1010101 0 .25 4.283-3 0 -90. -.25 2.-6 .15 00
1011101 351010000 101000000 0 0 0 00100
1012101 451010000 101000000 0 0 0 00100
1013101 551010000 101000000 0 0 0 00100
1014101 101010000 102000000 0 0 0 00100
*
* reactor downcomer
1020000 downcomr pipe
1020001 4
1020101 42.66-4 4
1020301 1.32 1 2.42 2 .96 3 .26 4
1020601 -90. 4
1020801 2.-6 .0737 4
1020901 5. 5. 1 0 0 3 * venturi nozzle: ceta=5
1021001 00 4
1021101 00000 3
*
* downcomer to lower plenum * ???
1230000 lowpljun valve
1230101 102010000 130000000 42.66-4 0 0 00000
1230300 srvvlv
1230301 930
1230401 0.01 0.01 0.01 * zaprto
1230402 1.0 10000.0 10000.0 * odprto
*
* ctv-930: stem position, ??? downcomer flow 1.47 kg/s ?
20593000 reg930 sum 1.0 2.589604e-02 0 3 0.01 1.0
20593001 0.01470 -0.01 mflowj 123000000 1.0 cntrlvar 930
*
* lower plenum - connection to downcomer
1300000 dc-lowpl branch
1300101 1.5328-2 2.298 0 0 -90. -2.07 2.-6 .1397 00
1301101 130010000 103000000 0 .13 .13 00000
*
* lower plenum
1030000 lower-pl pipe
1030001 5
1030101 1.5328-2 5

```

University of Ljubljana
 "Jožef Stefan" Institute, Ljubljana, Slovenia



```

1030301 .5 2 2.298 3 .26 4 .837 5
1030601 0 2 90. 4 45. 5
1030701 0 2 2.07 3 .26 4 .3 5
1030801 2.-6 .1397 5
1030901 0 0 1 .13 .13 2 0 0 3 .13 .13 4
1031001 00 5
1031101 00000 4
*
* below core
1040000 belowcor branch
1040101 1.671-2 .96 0 0 90. .66 2.-6 13.97-3 00
1041101 103010000 104000000 0 1.3 1.3 00100
*
* core bypass
1050000 core-byp branch
1050101 26.5-4 2.42 0 0 90. 2.42 2.-6 6.41-3 00
1051101 105010000 107000000 0 0 0 00100
*
1240000 cjun valve * ???
1240101 104010000 105000000 26.5-4 0 0 00000
1240300 srvlv
1240301 931
1240401 0.01 0.01 0.01 * zaprto
1240402 1.0 10000.0 10000.0 * odprto
*
* ctv-931: stem position, ??? 10 % bypas flow 0.147 kg/s ?
20593100 reg931 sum 1.0 1.156322e-02 0 3 0.01 1.0
20593101 0.001470 -0.01 mflowj 124000000 1.0 cntrlvar 931
*
* into core
1460000 core-bot sngljun
1460101 104010000 106000000 0 1.8 1.8 00100
*
* reactor core
1060000 rx-core pipe
1060001 9
1060101 .01128 9
1060301 .2688888 9
1060601 90. 9
1060801 2.-6 5.5-3 9
1060901 2.25 2.25 8
1061001 00 9
1061101 00000 8
*
* out of core
1670000 core-top sngljun
1670101 106010000 107000000 0 3.6 3.6 00100 * choke plate in ceta
*1670101 106010000 107000000 96.9-4 1.8 1.8 00100 * choke plate in area
*
* upper plenum
1070000 upp-plen pipe
1070001 3
1070101 0 1 2.8085-2 3
1070301 1.16 1 .905 3
1070401 .03178 1 0 3
1070601 90. 3
1070801 2.-6 28.45-3 1 2.-6 .1891 3
1071001 00 3
1071101 00100 2
*
* into hot leg no.1
    
```



```

1710000 into-hl1      sngljun
1710101 107010000 301000000 0 1. 1. 00100
*
* into hot leg no.2
1720000 into-hl2      sngljun
1720101 107010000 401000000 0 1. 1. 00100
*
* into hot leg no.3
1730000 into-hl3      sngljun
1730101 107010000 501000000 0 1. 1. 00100
*
* into upper head
1780000 intouphe      sngljun
1780101 107010000 108000000 0 0 0 00000
*
* upper head
1080000 upp-head      pipe
1080001 3
1080101 0 3
1080301 1.1733 3
*1080401 32.217-3 3
1080401 32.-3 3
1080601 90. 3
1080801 2.-6 .0966 3
1081001 00 3
1081101 00000 2
*
* upper head mixing valve
1790000 mixvalve      valve
1790101 107010000 180000000 1.8-4 0 0 00100
1790300 srvvlv
1790301 179
*
* ctv 179: upper head temperature controller
20517900 uphetemp sum .1 5.936215e-02 0 3 .01 1.
20517901 545. -1. tempf 108030000 10. cntrlvar 179
*
* upper head inflow
1800000 upheadin      branch
1800101 0 3.5199 .651-3 0 90. 3.5199 2.-6 0 10
1801101 180010000 108010000 0 0 0 00000
*
*****
* heat structure input - reactor *
*****
*
* downcomer inlet
11010000 2 5 2 1 .075
11010100 0 1
11010101 4 .09
11010201 1 4
11010301 1.0 4
11010401 480. 5
11010501 111010000 0 1 1 .69 1
11010502 101010000 0 1 1 .25 2
11010601 0 0 0 1 .69 1
11010602 0 0 0 1 .25 2
11010701 10901 0.12 0 0 1
11010702 10901 0.04 0 0 2
11010801 0 0 0 0 2
*
    
```



```

* downcomer diffusor
11011000  1 5 1 1 0
11011100  0 1
11011101  4 .004
11011201  1 4
11011301  0 4
11011401  480. 5
11011501  111010000 0 1 1 .2024 1
11011601  111010000 0 1 1 .2024 1
11011701  0 0 0 0 1
11011801  0 0 0 0 1
11011901  0 0 0 0 1
*
* downcomer
11020000  4 5 2 1 .03685
11020100  0 1
11020101  4 .04445
11020201  1 4
11020301  1.0 4
11020401  480. 5
11020501  102010000 0 1 1 1.32 1
11020502  102020000 0 1 1 2.42 2
11020503  102030000 0 1 1 .96 3
11020504  102040000 0 1 1 .26 4
11020601  0 0 0 1 1.32 1
11020602  0 0 0 1 2.42 2
11020603  0 0 0 1 .96 3
11020604  0 0 0 1 .26 4
11020701  10901 0.22 0 0 1
11020702  10901 0.42 0 0 2
11020703  10901 0.16 0 0 3
11020704  10901 0.04 0 0 4
11020801  0 0 0 0 4
*
* lower plenum
11030000  6 5 2 1 .06985
11030100  0 1
11030101  4 .08415
11030201  1 4
11030301  1.0 4
11030401  480. 5
11030501  130010000 0 1 1 2.298 1
11030502  103010000 10000 1 1 .5 3
11030503  103030000 0 1 1 2.298 4
11030504  103040000 0 1 1 .26 5
11030505  103050000 0 1 1 .837 6
11030601  0 0 0 1 2.298 1
11030602  0 0 0 1 .5 3
11030603  0 0 0 1 2.298 4
11030604  0 0 0 1 .26 5
11030605  0 0 0 1 .837 6
11030701  10902 0.34 0 0 1
11030702  10902 0.08 0 0 3
11030703  10902 0.34 0 0 4
11030704  10902 0.04 0 0 5
11030705  10902 0.12 0 0 6
11030801  0 0 0 0 6
*
* below core
11040000  1 5 2 1 .09131
11040100  0 1
    
```



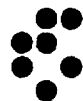
```

11040101  4 .10955
11040201  1 4
11040301  1.0 4
11040401  480. 5
11040501  104010000 0 1 1 .96 1
11040601  0 0 0 1 .96 1
11040701  10903 0.21 0 0 1
11040801  0 0 0 0 1
*
* unheated part of rods
11041000  1 5 2 1 0.
11041100  0 1
11041101  2 3.9-3 2 3.95-3
11041201  2 2 1 4
11041301  0 4
11041401  480. 5
11041501  0 0 0 1 144. 1 * = 1. * 144
11041601  104010000 0 1 1 144. 1
11041701  0 0 0 0 1
11041901  0 0 0 0 1
*
* core bypass
11050000  1 5 2 1 .09131
11050100  1040
11050400  1040
11050501  105010000 0 1 1 2.42 1
11050601  0 0 0 1 2.42 1
11050701  10903 0.53 0 0 1
11050801  0 0 0 0 1
*
* bypass-core cylinder
11051000  9 3 2 1 .086
11051100  0 1
11051101  2 .088
11051201  1 2
11051301  0 2
11051401  480. 3
11051501  106010000 10000 1 1 .2689 9
11051601  105010000 0 1 1 .2689 9
11051701  0 0 0 0 9
11051801  0 0 0 0 9
11051901  0 0 0 0 9
*
* bypass-core plate
11052000  9 3 1 1 0.
11052100  0 1
11052101  2 .002
11052201  1 2
11052301  0 2
11052401  480. 3
11052501  106010000 10000 1 1 .13875 9
11052601  105010000 0 1 1 .13875 9
11052701  0 0 0 0 9
11052801  0 0 0 0 9
11052901  0 0 0 0 9
*
* reactor core
11060000  11 7 2 1 0.
11060100  0 1
11060101  3 3.55-3 3 4.55-3
11060201  2 3 1 6
    
```



```

11060301  1. 3  0 6
11060401  580. 7
11060501  0          0      0 1 28.8  1 * = .2      * 144
11060502  0          0      0 1 38.72 10 * = (2.42/9) * 144
11060503  0          0      0 1 17.28 11 * = .12      * 144
11060601  104010000 0      1 1 28.8  1
11060602  106010000 10000 1 1 38.72 10
11060603  107010000 0      1 1 17.28 11
11060701  0 0 0 0 1
11060702  100 .0535 0 0 2
11060703  100 .0939 0 0 3
11060704  100 .1274 0 0 4
11060705  100 .1474 0 0 5
11060706  100 .1556 0 0 6
11060707  100 .1474 0 0 7
11060708  100 .1274 0 0 8
11060709  100 .0939 0 0 9
11060710  100 .0535 0 0 10
11060711  0 0 0 0 11
11060901  0 0 0 0 11
*
* tab 100: scram (no scram at initialization)
20210000 power
20210001  0. 165.+3 * isp-33
*20210002 100. 165.+3 120. 230.+3 380. 230.+3 400. 165.+3 * ??? initial.
*
* core internals (hexagonal grid)
11061000  9 3 1 1 0.
11061100  0 1
11061101  2 5.-4
11061201  1 2
11061301  0 2
11061401  480. 3
11061501  106010000 10000 1 1 .8182 9 * 2*sqrt(3)*.0061*144*2.42/9
11061601  106010000 10000 1 1 .8182 9
11061701  0 0 0 0 9
11061801  0 0 0 0 9
11061901  0 0 0 0 9
*
* outer vessel wall
11070000  1 5 2 1 .09131
11070100  1040
11070400  1040
11070501  107010000 0      1 1 1.16 1
11070601  0          0      0 1 1.16 1
11070701  10903 0.26 0 0 1
11070801  0 0 0 0 1
*
* upper plenum
11080000  5 5 2 1 .09455
11080100  0 1
11080101  4 .10955
11080201  1 4
11080301  1.0 4
11080401  480. 5
11080501  107020000 10000 1 1 .905 2
11080502  108010000 10000 1 1 1.1733 5
11080601  0          0      0 1 .905 2
11080602  0          0      0 1 1.1733 5
11080701  10904 0.17 0 0 2
11080702  10904 0.22 0 0 5
    
```

```

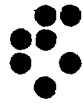
11080801  0 0 0 0 5
*
* upper plenum diffusor
11081000  3 5 2 1 .04245
11081100  0 1
11081101  4 .04468
11081201  1 4
11081301  0 4
11081401  480. 5
11081501  108010000 10000 1 1 1.2067 3
11081601  108010000 10000 1 1 1.2067 3
11081701  0 0 0 0 3
11081801  0 0 0 0 3
11081901  0 0 0 0 3
*
*****
*
*               p r e s s u r i z e r
*
*****
*
* hot leg no.1 to surge line connection (fig.8)
1990000  intosurl  sngljun
1990101  301000000 200000000 0 1. 1. 00100
*
* pressurizer surge line
2000000  surgline  pipe
2000001  4
2000101  5.8535-4 4
2000301  2. 1 1.9101 3 1.6064 4
2000601 -90. 1 0 3 90. 4
2000701 -2. 1 0 3 1.29 4
2000801  2.-6 .0273 4
2000901  .5 .5 1 .3 .3 2 .15 .15 3
2001001  00 4
2001101  00000 3
*
* surge line connection
2010000  surjunct  sngljun
2010101  200010000 202000000 0 1. 1. 00100
*
* pressurizer
2020000  pressuri  pipe
2020001  10
2020101  0 3 1.53279-2 10
2020301  .88 10
2020401  13.1889-3 1 13.3047-3 2 13.4528-3 3 0 10
2020601  90. 10
2020701  .68 1 .88 10
2020801  2.-6 .1397 10
2021001  00 10
2021101  00000 9
*
***** pressuriser for initialization *****
*
2100000  przv-art  tmdpvol
2100101  10. 10. 0 0 0 0 0 0 00
2100200  1 0 tempf 202010000
2100201 -1. 600. 0 300. 560. 0 400. 400. 0 700. 700. 0
*
2110000  char-prz  tmdpjun
    
```

University of Ljubljana
 "Jožef Stefan" Institute, Ljubljana, Slovenia



```

2110101 21000000 202000000 .05
2110200 1 0 cntrlvar 172 * prz level - collapsed
2110201 0 0 0 0 5.13 1. 0 0 5.18 0 0 0 5.23 -1. 0 0 * isp-33
*
2210000 przoutj  sngljun
2210101 202010000 222000000 0 0 0 00000
2210201 0 -2.61610e-01 1.31406e-03 0
*
2220000 prz-init  tmdpvol
2220101 10. 10. 0 0 0 0 0 0 00
2220200 2
2220201 0 73.8983+5 1. * ???? isp-33
*
*****
*          heat structure input - pressurizer          *
*****
*
* surge line
12000000 4 5 2 1 .01365
12000100 0 1
12000101 4 .01685
12000201 1 4
12000301 1.0 4
12000401 500. 5
12000501 200010000 0 1 1 2. 1
12000502 200020000 10000 1 1 1.9101 3
12000503 200040000 0 1 1 1.536 4
12000601 0 0 0 1 2. 1
12000602 0 0 0 1 1.9101 3
12000603 0 0 0 1 1.536 4
12000701 10915 0.27 0 0 1
12000702 10915 0.26 0 0 3
12000703 10915 0.21 0 0 4
12000801 0 0 0 0 4
*
* pressurizer
12020000 10 5 2 1 .06985
12020100 0 1
12020101 4 .08415
12020201 1 4
12020301 1.0 4
12020401 562. 5
12020501 202010000 10000 1 1 .88 10
12020601 0 0 0 1 .88 10
12020701 10914 0.1 0 0 10
12020801 0 0 0 0 10
*
* pressurizer heaters
12021000 3 5 2 1 0.
12021100 0 1
12021101 4 4.25-3
12021201 1 4
12021301 1. 4
12021401 580. 5
12021501 0 0 0 1 5.28 1
12021502 0 0 0 1 3.24 2
12021503 0 0 0 1 0.63 3
12021601 202010000 0 1 1 5.28 1
12021602 202020000 0 1 1 3.24 2
12021603 202030000 0 1 1 0.63 3
12021701 10202 .51 0 0 1
  
```



12021702 10202 .41 0 0 2
12021703 10202 .08 0 0 3
12021901 0 0 0 0 3

*
* ctv 202: pressurizer heaters
20520200 prz-heat sum 1.0 3354.98 0 * ??? charact. test
20520201 0.0 -1.0 cntrlvar 914 -1.0 cntrlvar 915
*

*
* cold legs *
*

* cold leg no.1

3510000 coldleg1 pipe
3510001 14
3510101 21.631-4 14
3510301 .6992 4 .61476 5 .67625 9 .57985 11 .79338 13 .515 14
3510601 -90. 4 0 5 45. 9 0 11 -90. 13 0 14
3510701 -.6992 4 0 5 .5075 9 0 11 -.75 13 0 14
3510801 2.-6 .05248 14
* venturi tube: ceta=8.2
3510901 8.2 8.2 1 0 0 3 .2 .2 5 0 0 8 .11 .11 9 0 0 10
3510902 .2 .2 11 .311 .311 12 .2 .2 13
3511001 00 14
3511101 00000 13
*

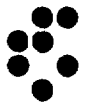
* cold leg no.2

4510000 coldleg2 pipe
4510001 14
4510101 21.631-4 14
4510301 .6992 4 .66251 5 .67625 9 .62163 11 .79338 13 .515 14
4510601 -90. 4 0 5 45. 9 0 11 -90. 13 0 14
4510701 -.6992 4 0 5 .5075 9 0 11 -.75 13 0 14
4510801 2.-6 .05248 14
* venturi tube: ceta=8.2
4510901 8.2 8.2 1 0 0 3 .2 .2 4 .27 .27 5 0 0 8 .234 .234 9 0 0 10
4510902 .2 .2 11 .311 .311 12 .2 .2 13
4511001 00 14
4511101 00000 13
*

* cold leg no.3

5510000 coldleg3 pipe
5510001 14
5510101 21.631-4 14
5510301 .6992 4 .57895 5 .67625 9 .59775 11 .79338 13 .515 14
5510601 -90. 4 0 5 45. 9 0 11 -90. 13 0 14
5510701 -.6992 4 0 5 .5075 9 0 11 -.75 13 0 14
5510801 2.-6 .05248 14
* venturi tube: ceta=8.2
5510901 8.2 8.2 1 0 0 3 .14 .14 5 0 0 8 .17 .17 9 0 0 10
5510902 .2 .2 11 .311 .311 12 .2 .2 13
5511001 00 14
5511101 00000 13
*

*
* hot legs *
*



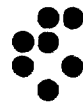
```
*
* hot leg no.1
3010000 hotleg1 pipe
3010001 11
3010101 21.631-4 11
3010301 1.07169 1 .71625 5 .78926 7 .6992 11
3010601 0. 1 -45. 5 0 7 90. 11
3010701 0. 1 -.4825 5 0 7 .6992 11
3010801 2.-6 .05248 11
3010901 .11 .11 1 0 0 4 .267 .267 5 .311 .311 6 .2 .2 7 0 0 10
3011001 00 11
3011101 00000 10
```

```
*
* hot leg no.2
4010000 hotleg2 pipe
4010001 11
4010101 21.631-4 11
4010301 1.27913 1 .71625 5 .70119 6 .76538 7 .6992 11
4010601 0. 1 -45. 5 0 7 90. 11
4010701 0. 1 -.4825 5 0 7 .6992 11
4010801 2.-6 .05248 11
4010901 .27 .27 1 0 0 4 .25 .25 5 .311 .311 6 .2 .2 7 0 0 10
4011001 00 11
4011101 00000 10
```

```
*
* hot leg no.3
5010000 hotleg3 pipe
5010001 11
5010101 21.631-4 11
5010301 1.07169 1 .71625 5 .77732 7 .6992 11
5010601 0. 1 -45. 5 0 7 90. 11
5010701 0. 1 -.4825 5 0 7 .6992 11
5010801 2.-6 .05248 11
5010901 .11 .11 1 0 0 4 .232 .232 5 .311 .311 6 .2 .2 7 0 0 10
5011001 00 11
5011101 00000 10
```

```
*****
* heat structure input - primary piping *
*****
```

```
* hot leg no.1
13010000 11 5 2 1 .02624
13010100 0 1
13010101 4 .03015
13010201 1 4
13010301 1.0 4
13010401 480. 5
13010501 301010000 0 1 1 1.07169 1
13010502 301020000 10000 1 1 .71625 5
13010503 301060000 10000 1 1 .78926 7
13010504 301080000 10000 1 1 .6942 11
13010601 0 0 0 1 1.07169 1
13010602 0 0 0 1 .71625 5
13010603 0 0 0 1 .78926 7
13010604 0 0 0 1 .6942 11
13010701 10905 0.14 0 0 1
13010702 10905 0.09 0 0 7
13010703 10905 0.08 0 0 11
13010801 0 0 0 0 11
```



```
* hot leg no.2
14010000 11 5 2 1 .02624
14010100 3010
14010400 3010
14010501 401010000 0 1 1 1.27913 1
14010502 401020000 10000 1 1 .71625 5
14010503 401060000 0 1 1 .70119 6
14010504 401070000 0 1 1 .76538 7
14010505 401080000 10000 1 1 .6942 11
14010601 0 0 0 1 1.27913 1
14010602 0 0 0 1 .71625 5
14010603 0 0 0 1 .70119 6
14010604 0 0 0 1 .76538 7
14010605 0 0 0 1 .6942 11
14010701 10908 0.14 0 0 1
14010702 10908 0.09 0 0 7
14010703 10908 0.08 0 0 11
14010801 0 0 0 0 11
```

```
*
* hot leg no.3
15010000 11 5 2 1 .02624
15010100 3010
15010400 3010
15010501 501010000 0 1 1 1.07169 1
15010502 501020000 10000 1 1 .71625 5
15010503 501060000 10000 1 1 .77732 7
15010504 501080000 10000 1 1 .6942 11
15010601 0 0 0 1 1.07169 1
15010602 0 0 0 1 .71625 5
15010603 0 0 0 1 .77732 7
15010604 0 0 0 1 .6942 11
15010701 10911 0.14 0 0 1
15010702 10911 0.09 0 0 7
15010703 10911 0.08 0 0 11
15010801 0 0 0 0 11
```

```
*
* cold leg no.1
13510000 14 5 2 1 .02624
13510100 3010
13510400 3010
13510501 351010000 10000 1 1 .6942 4
13510502 351050000 0 1 1 .61476 5
13510503 351060000 10000 1 1 .67625 9
13510504 351100000 10000 1 1 .57985 11
13510505 351120000 10000 1 1 .79338 13
13510506 351140000 0 1 1 .515 14
13510601 0 0 0 1 .6942 4
13510602 0 0 0 1 .61476 5
13510603 0 0 0 1 .67625 9
13510604 0 0 0 1 .57985 11
13510605 0 0 0 1 .79338 13
13510606 0 0 0 1 .515 14
13510701 10906 0.07 0 0 11
13510702 10906 0.085 0 0 13
13510703 10906 0.06 0 0 14
13510801 0 0 0 0 14
```

```
*
* cold leg no.2
14510000 14 5 2 1 .02624
14510100 3010
14510400 3010
```



```

14510501 451010000 10000 1 1 .6942 4
14510502 451050000 0 1 1 .66251 5
14510503 451060000 10000 1 1 .67625 9
14510504 451100000 10000 1 1 .62163 11
14510505 451120000 10000 1 1 .79338 13
14510506 451140000 0 1 1 .515 14
14510601 0 0 0 1 .6942 4
14510602 0 0 0 1 .66251 5
14510603 0 0 0 1 .67625 9
14510604 0 0 0 1 .62163 11
14510605 0 0 0 1 .79338 13
14510606 0 0 0 1 .515 14
14510701 10909 0.07 0 0 11
14510702 10909 0.085 0 0 13
14510703 10909 0.06 0 0 14
14510801 0 0 0 0 14
    
```

*

* cold leg no.3

```

15510000 14 5 2 1 .02624
15510100 3010
15510400 3010
15510501 551010000 10000 1 1 .6942 4
15510502 551050000 0 1 1 .57895 5
15510503 551060000 10000 1 1 .67625 9
15510504 551100000 10000 1 1 .59775 11
15510505 551120000 10000 1 1 .79338 13
15510506 551140000 0 1 1 .515 14
15510601 0 0 0 1 .6942 4
15510602 0 0 0 1 .57895 5
15510603 0 0 0 1 .67625 9
15510604 0 0 0 1 .59775 11
15510605 0 0 0 1 .79338 13
15510606 0 0 0 1 .515 14
15510701 10912 0.07 0 0 11
15510702 10912 0.085 0 0 13
15510703 10912 0.06 0 0 14
15510801 0 0 0 0 14
    
```

*

```

*****
* additional rcs heat losses - unisolated rcs valves *
*****
    
```

```

* rcs heat losses 20 kw: 12.433 kw corresponding to given r5/mod3
* heat sink distribution
* 7.567 kw (38%) added for unisolated rcs valves
* to obtain total 20 kw (isp-33 data)
*
    
```

* hot leg valves: 1,2,3

```

13011000 3 5 2 1 .02624
13011100 0 1
* 13011101 4 .03015
13011101 4 .05 * ???? rout = 5 cm
13011201 1 4
13011301 1.0 4
13011401 480. 5
13011501 301070000 100000000 1 1 0.2 3 * ???? l=20 cm (high w/m2 !)
13011601 0 0 0 1 0.2 3 * ???? l=20 cm
13011701 10951 1.0 0 0 1
13011702 10952 1.0 0 0 2
13011703 10953 1.0 0 0 3
13011801 0 0 0 0 3
    
```



```

*
* ctv 951: hl1 valve heat losses [w]
20595100 hl1vloss sum -4.60 -1081.0 1
20595101 -308.0 1.0 tempf 301070000
*
* ctv 952: hl2 valve heat losses [w]
20595200 hl2vloss sum -4.60 -1081.0 1
20595201 -308.0 1.0 tempf 401070000
*
* ctv 953: hl3 valve heat losses [w]
20595300 hl3vloss sum -4.60 -1081.0 1
20595301 -308.0 1.0 tempf 501070000
*
*
* cold leg valves: 1,2,3
13511000 3 5 2 1 .02624
13511100 3011
13511400 3011
13511501 351130000 100000000 1 1 0.2 3 * ??? l=20 cm
13511601 0 0 0 1 0.2 3 * ??? l=20 cm
13511701 10954 1.0 0 0 1
13511702 10955 1.0 0 0 2
13511703 10956 1.0 0 0 3
13511801 0 0 0 0 3
*
* ctv 954: cl1 valve heat losses [w]
20595400 cl1vloss sum -4.80 -1081.0 1
20595401 -308.0 1.0 tempf 351130000
*
* ctv 955: cl2 valve heat losses [w]
20595500 cl2vloss sum -4.80 -1081.0 1
20595501 -308.0 1.0 tempf 451130000
*
* ctv 956: cl3 valve heat losses [w]
20595600 cl3vloss sum -4.80 -1081.0 1
20595601 -308.0 1.0 tempf 551130000
*
* surge line valve
12001000 1 5 2 1 .01365
12001100 0 1
* 12001101 4 .016
12001101 4 .03 * ??? rout=3 cm
12001201 1 4
12001301 1.0 4
12001401 480. 5
12001501 200010000 0 1 1 0.2 1 * ??? l=20 cm
12001601 0 0 0 1 0.2 1 * ??? l=20 cm
12001701 10957 1.0 0 0 1
12001801 0 0 0 0 1
*
* ctv 957: sl valve heat losses [w]
* 20595700 slvloss sum -4.60 -1081.0 1
20595700 slvloss sum -1.53 -360.0 1 * ??? zmanjsano na 1/3
20595701 -308.0 1.0 tempf 200010000
*
*****
*
* steam generators - primary side *
*
*****
*

```



```

*****
*                               s g   n o . 1                               *
*****
*
* sg no.1 inlet chamber - level 1
3210000 ut11-inl  branch
3210101 .012264 0 5.26-3 0 90. .0632 2.-6 .2128 00
3211101 301010000 321000000 0 0 0 00100
3212101 321010000 325000000 0 1. 1. 00100
*
* sg no.1 inlet chamber - level 2
3220000 ut12-inl  branch
3220101 .012264 0 5.26-3 0 90. .084 2.-6 .2128 00
3221101 321010000 322000000 0 0 0 00100
3222101 322010000 326000000 0 1. 1. 00100
*
* sg no.1 inlet chamber - level 3
3230000 ut13-inl  branch
3230101 .024528 0 10.52-3 0 90. .06 2.-6 .2128 00
3231101 322010000 323000000 0 0 0 00100
3232101 323010000 327000000 0 1. 1. 00100
*
* sg no.1 u-tubes - level 1 (13 tubes)
3250000 utub-1-1  pipe
3250001 6
3250101 17.2552-4 6
3250301 1.4546 6
3250601 -3. 3 3. 6
3250701 -.07 3 .07 6
3250801 1.-6 .013 6
3250901 0 0 2 .175 .175 3 0 0 5
3251001 00 6
3251101 00000 5
*
* sg no.1 u-tubes - level 2 (15 tubes)
3260000 utub-1-2  pipe
3260001 6
3260101 19.9098-4 6
3260301 1.4666 6
3260601 0 6
3260801 1.-6 .013 6
3260901 0 0 2 .18 .18 3 0 0 5
3261001 00 6
3261101 00000 5
*
* sg no.1 u-tubes - level 3 (10 tubes)
3270000 utub-1-3  pipe
3270001 6
3270101 13.2732-4 6
3270301 1.4666 6
3270601 0 6
3270801 1.-6 .013 6
3270901 0 0 2 .18 .18 3 0 0 5
3271001 00 6
3271101 00000 5
*
* sg no.1 outlet chamber - level 1
3310000 ut11-out  branch
3310101 .012264 0 5.26-3 0 -90. -.0632 2.-6 .2128 00
3311101 325010000 331000000 0 1. 1. 00100
3312101 331010000 351000000 0 0 0 00100
    
```



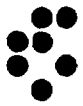

```

*
* sg no.1 outlet chamber - level 2
3320000 ut12-out branch
3320101 .012264 0 5.26-3 0 -90. -.084 2.-6 .2128 00
3321101 326010000 332000000 0 1. 1. 00100
3322101 332010000 331000000 0 0 0 00100
*
* sg no.1 outlet chamber - level 3
3330000 ut13-out branch
3330101 .024528 0 10.52-3 0 -90. -.06 2.-6 .2128 00
3331101 327010000 333000000 0 1. 1. 00100
3332101 333010000 332000000 0 0 0 00100
*
*****
*                               s g   n o . 2                               *
*****
*
* sg no.2 inlet chamber - level 1
4210000 ut21-inl branch
4210101 .012264 0 5.26-3 0 90. .0632 2.-6 .2128 00
4211101 401010000 421000000 0 0 0 00100
4212101 421010000 425000000 0 1. 1. 00100
*
* sg no.2 inlet chamber - level 2
4220000 ut22-inl branch
4220101 .012264 0 5.26-3 0 90. .084 2.-6 .2128 00
4221101 421010000 422000000 0 0 0 00100
4222101 422010000 426000000 0 1. 1. 00100
*
* sg no.2 inlet chamber - level 3
4230000 ut23-inl branch
4230101 .024528 0 10.52-3 0 90. .06 2.-6 .2128 00
4231101 422010000 423000000 0 0 0 00100
4232101 423010000 427000000 0 1. 1. 00100
*
* sg no.2 u-tubes - level 1 (13 tubes)
4250000 utub-2-1 pipe
4250001 6
4250101 17.2552-4 6
4250301 1.4546 6
4250601 -3. 3 3. 6
4250701 -.07 3 .07 6
4250801 1.-6 .013 6
4250901 0 0 2 .175 .175 3 0 0 5
4251001 00 6
4251101 00000 5
*
* sg no.2 u-tubes - level 2 (15 tubes)
4260000 utub-2-2 pipe
4260001 6
4260101 19.9098-4 6
4260301 1.4666 6
4260601 0 6
4260801 1.-6 .013 6
4260901 0 0 2 .18 .18 3 0 0 5
4261001 00 6
4261101 00000 5
*
* sg no.2 u-tubes - level 3 (10 tubes)
4270000 utub-2-3 pipe
4270001 6
    
```



```

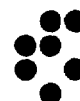
4270101 13.2732-4 6
4270301 1.4666 6
4270601 0 6
4270801 1.-6 .013 6
4270901 0 0 2 .18 .18 3 0 0 5
4271001 00 6
4271101 00000 5
*
* sg no.2 outlet chamber - level 1
4310000 ut21-out branch
4310101 .012264 0 5.26-3 0 -90. -.0632 2.-6 .2128 00
4311101 425010000 431000000 0 1. 1. 00100
4312101 431010000 451000000 0 0 0 00100
*
* sg no.2 outlet chamber - level 2
4320000 ut22-out branch
4320101 .012264 0 5.26-3 0 -90. -.084 2.-6 .2128 00
4321101 426010000 432000000 0 1. 1. 00100
4322101 432010000 431000000 0 0 0 00100
*
* sg no.2 outlet chamber - level 3
4330000 ut23-out branch
4330101 .024528 0 10.52-3 0 -90. -.06 2.-6 .2128 00
4331101 427010000 433000000 0 1. 1. 00100
4332101 433010000 432000000 0 0 0 00100
*
*****
*                               s g   n o . 3                               *
*****
*
* sg no.3 inlet chamber - level 1
5210000 ut31-inl branch
5210101 .012264 0 5.26-3 0 90. .0632 2.-6 .2128 00
5211101 501010000 521000000 0 0 0 00100
5212101 521010000 525000000 0 1. 1. 00100
*
* sg no.3 inlet chamber - level 2
5220000 ut32-inl branch
5220101 .012264 0 5.26-3 0 90. .084 2.-6 .2128 00
5221101 521010000 522000000 0 0 0 00100
5222101 522010000 526000000 0 1. 1. 00100
*
* sg no.3 inlet chamber - level 3
5230000 ut33-inl branch
5230101 .024528 0 10.52-3 0 90. .06 2.-6 .2128 00
5231101 522010000 523000000 0 0 0 00100
5232101 523010000 527000000 0 1. 1. 00100
*
* sg no.3 u-tubes - level 1 (13 tubes)
5250000 utub-3-1 pipe
5250001 6
5250101 17.2552-4 6
5250301 1.4546 6
5250601 -3. 3 3. 6
5250701 -.07 3 .07 6
5250801 1.-6 .013 6
5250901 0 0 2 .175 .175 3 0 0 5
5251001 00 6
5251101 00000 5
*
* sg no.3 u-tubes - level 2 (15 tubes)
    
```



```

5260000 utub-3-2 pipe
5260001 6
5260101 19.9098-4 6
5260301 1.4666 6
5260601 0 6
5260801 1.-6 .013 6
5260901 0 0 2 .18 .18 3 0 0 5
5261001 00 6
5261101 00000 5
*
* sg no.3 u-tubes - level 3 (10 tubes)
5270000 utub-3-3 pipe
5270001 6
5270101 13.2732-4 6
5270301 1.4666 6
5270601 0 6
5270801 1.-6 .013 6
5270901 0 0 2 .18 .18 3 0 0 5
5271001 00 6
5271101 00000 5
*
* sg no.3 outlet chamber - level 1
5310000 ut31-out branch
5310101 .012264 0 5.26-3 0 -90. -.0632 2.-6 .2128 00
5311101 525010000 531000000 0 1. 1. 00100
5312101 531010000 551000000 0 0 0 00100
*
* sg no.3 outlet chamber - level 2
5320000 ut32-out branch
5320101 .012264 0 5.26-3 0 -90. -.084 2.-6 .2128 00
5321101 526010000 532000000 0 1. 1. 00100
5322101 532010000 531000000 0 0 0 00100
*
* sg no.3 outlet chamber - level 3
5330000 ut33-out branch
5330101 .024528 0 10.52-3 0 -90. -.06 2.-6 .2128 00
5331101 527010000 533000000 0 1. 1. 00100
5332101 533010000 532000000 0 0 0 00100
*
*****
*
*   s t e a m   g e n e r a t o r s   -   s e c o n d a r y   s i d e   *
*
*****
*
*                               s g   n o .   1                               *
*****
*
* sg no.1 secondary side - level 1
6010000 sg-sec11 branch
6010101 0 .1112 78.9228-3 0 90. .1112 2.-6 .011 00 * ??? dh=1.0cm
6011101 601010000 602000000 0 0 0 00000
*
* sg no.1 secondary side - downcomer - level 1
6110000 sg1-dc-1 branch
6110101 0 .1112 19.7307-3 0 -90. -.1112 2.-6 .011 00 * ??? dh=1.0cm
6111101 611010000 601000000 0 0 0 00000
*
* sg no.1 secondary side - level 2
6020000 sg-sec12 branch

```



```

6020101 0 .072 71.2339-3 0 90. .072 2.-6 .011 00 * ???? dh=1.0cm
6021101 602010000 603000000 0 0 0 00000
*
* sg no.1 secondary side - downcomer - level 2
6120000 sgl-dc-2 branch
6120101 0 .072 17.8085-3 0 -90. -.072 2.-6 .011 00 * ???? dh=1.0cm
6121101 612010000 602000000 0 0 0 00000
6122101 612010000 611000000 0 0 0 00000
*
* sg no.1 secondary side - level 3
6030000 sg-sec13 snglvol
6030101 0 .048 48.4271-3 0 90. .048 2.-6 .011 00 * ???? dh=1.0cm
*
* sg no.1 secondary side - downcomer - level 3
6130000 sgl-dc-3 branch
6130101 0 .048 12.1068-3 0 -90. -.048 2.-6 .011 00 * ???? dh=1.0cm
6131101 613010000 603000000 0 0 0 00000
6132101 613010000 612000000 0 0 0 00000
*
* sg no.1 steam separator
6050000 sgl-sepa separatr
6050101 0 .05 75.2786-3 0 90. .05 2.-6 0 00
6051101 605010000 606000000 0 0 0 01000 * 0.01 * ???? default?
6052101 605000000 613000000 0 0 0 01000 * 0.01
6053101 603010000 605000000 0 0 0 01000
*
* sg no.1 steam dome
6060000 sgl-stdm snglvol
6060101 0 .0852 83.7316-3 0 90. .0852 2.-6 0 00
*
*****
*                               s g   n o . 2                               *
*****
*
* sg no.2 secondary side - level 1
7010000 sg-sec21 branch
7010101 0 .1112 78.9228-3 0 90. .1112 2.-6 .011 00 * ???? dh=1.0cm
7011101 701010000 702000000 0 0 0 00000
*
* sg no.2 secondary side - downcomer - level 1
7110000 sg2-dc-1 branch
7110101 0 .1112 19.7307-3 0 -90. -.1112 2.-6 .011 00 * ???? dh=1.0cm
7111101 711010000 701000000 0 0 0 00000
*
* sg no.2 secondary side - level 2
7020000 sg-sec22 branch
7020101 0 .072 71.2339-3 0 90. .072 2.-6 .011 00 * ???? dh=1.0cm
7021101 702010000 703000000 0 0 0 00000
*
* sg no.2 secondary side - downcomer - level 2
7120000 sg2-dc-2 branch
7120101 0 .072 17.8085-3 0 -90. -.072 2.-6 .011 00 * ???? dh=1.0cm
7121101 712010000 702000000 0 0 0 00000
7122101 712010000 711000000 0 0 0 00000
*
* sg no.2 secondary side - level 3
7030000 sg-sec23 snglvol
7030101 0 .048 48.4271-3 0 90. .048 2.-6 .011 00 * ???? dh=1.0cm
*
* sg no.2 secondary side - downcomer - level 3
7130000 sg2-dc-3 branch
    
```



```

7130101  0 .048 12.1068-3 0 -90. -.048 2.-6 .011 00 * ???? dh=1.0cm
7131101  713010000 703000000 0 0 0 00000
7132101  713010000 712000000 0 0 0 00000
*
* sg no.2 steam separator
7050000  sg2-sepa  separatr
7050101  0 .05 75.2786-3 0 90. .05 2.-6 0 00
7051101  705010000 706000000 0 0 0 01000 * 0.01 * ???? default?
7052101  705000000 713000000 0 0 0 01000 * 0.01
7053101  703010000 705000000 0 0 0 01000
*
* sg no.2 steam dome
7060000  sg2-stdm  snglvol
7060101  0 .0852 83.7316-3 0 90. .0852 2.-6 0 00
*
*****
*                               s g   n o . 3                               *
*****
*
* sg no.3 secondary side - level 1
8010000  sg-sec31  branch
8010101  0 .1112 78.9228-3 0 90. .1112 2.-6 .011 00 * ???? dh=1.0cm
8011101  801010000 802000000 0 0 0 00000
*
* sg no.3 secondary side - downcomer - level 1
8110000  sg3-dc-1  branch
8110101  0 .1112 19.7307-3 0 -90. -.1112 2.-6 .011 00 * ???? dh=1.0cm
8111101  811010000 801000000 0 0 0 00000
*
* sg no.3 secondary side - level 2
8020000  sg-sec32  branch
8020101  0 .072 71.2339-3 0 90. .072 2.-6 .011 00 * ???? dh=1.0cm
8021101  802010000 803000000 0 0 0 00000
*
* sg no.3 secondary side - downcomer - level 2
8120000  sg3-dc-2  branch
8120101  0 .072 17.8085-3 0 -90. -.072 2.-6 .011 00 * ???? dh=1.0cm
8121101  812010000 802000000 0 0 0 00000
8122101  812010000 811000000 0 0 0 00000
*
* sg no.3 secondary side - level 3
8030000  sg-sec33  snglvol
8030101  0 .048 48.4271-3 0 90. .048 2.-6 .011 00 * ???? dh=1.0cm
*
* sg no.3 secondary side - downcomer - level 3
8130000  sg3-dc-3  branch
8130101  0 .048 12.1068-3 0 -90. -.048 2.-6 .011 00 * ???? dh=1.0cm
8131101  813010000 803000000 0 0 0 00000
8132101  813010000 812000000 0 0 0 00000
*
* sg no.3 steam separator
8050000  sg3-sepa  separatr
8050101  0 .05 75.2786-3 0 90. .05 2.-6 0 00
8051101  805010000 806000000 0 0 0 01000 * 0.01 * ???? default?
8052101  805000000 813000000 0 0 0 01000 * 0.01
8053101  803010000 805000000 0 0 0 01000
*
* sg no.3 steam dome
8060000  sg3-stdm  snglvol
8060101  0 .0852 83.7316-3 0 90. .0852 2.-6 0 00
*

```



```

*****
*                               sg feedwater control                               *
*****
*
6510000 feedwat1 tmdpvol
6510101 10. 10. 0 0 0 0 0 0 0 0
6510200 3
6510201 0 45.+5 305.
*
7510000 feedwat2 tmdpvol
7510101 10. 10. 0 0 0 0 0 0 0 0
7510200 3
7510201 0 45.+5 305.
*
8510000 feedwat3 tmdpvol
8510101 10. 10. 0 0 0 0 0 0 0 0
8510200 3
8510201 0 45.+5 305.
*
* max. fw capacity for one sg: 0.063 kg/s
* initial isp-33 fw flow: 0.018 kg/s
* isp-33 steady state secondary levels are 0.27 m -> separator voidf=0.776
* controlled manually within +-0.01 m band (+-0.2 separator total volume)
* (ijs steady heat sink calculation: 0.016 kg/s)
*
6520000 fw1-junc tmdpjun
6520101 651000000 602000000 25.73-4
6520200 1 0 voidf 605010000
6520201 0.576 0.063 0 0 0.776 0.018 0 0 0.876 0.0 0 0 * ??? isp-33
* -0.01m ref. +0.005m
*
7520000 fw2-junc tmdpjun
7520101 751000000 702000000 25.73-4
7520200 1 0 voidf 705010000
7520201 0.576 0.063 0 0 0.776 0.018 0 0 0.876 0.0 0 0 * ??? isp-33
*
8520000 fw3-junc tmdpjun
8520101 851000000 802000000 25.73-4
8520200 1 0 voidf 805010000
8520201 0.576 0.063 0 0 0.776 0.018 0 0 0.876 0.0 0 0 * ??? isp-33
*
*****
*                               secondary pressure control                               *
*****
*
* art. sg-relief initialization:
* no pi control description available
* 42.0 bar: presumed 2 x 0.05 kg/s (approx. simulating nek
* 2 x 10% sg relief)
*
9000000 stem1 branch
9000101 0.022 5.0 0.0 0 0. 0. 2.-6 0 00 * ??? approxim. geom.
9001101 606010000 900000000 0 0 0 00100
9002101 706010000 900000000 0 0 0 00100
9003101 806010000 900000000 0 0 0 00100
*
9040000 sec_porv valve
9040101 900010000 901000000 7.92034e-05 1.0 1.0 00100 1.0 1.0
9040300 srvvlv
9040301 940
*
    
```



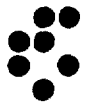
```

20594000 stempos function 1.0 1.0 1
20594001 p 900010000 940
*
20294000 reac-t
20294001 41.9e+05 0.0 43.5e+05 1.0
* when the pressure is approaching the setpoint 4.19 mpa the control valve
* starts to open and the pressure reaches 4.35 mpa before the control valve
* is opened for reducing the pressure
*
9010000 steamex tmdpvol
9010101 10. 10. 0 0 0 0 0 0 00
9010200 2
9010201 0 1.0e+05 1.0
*
*****
* heat structure input - steam generators *
*****
*
* sg no.1 divide plate
13210000 3 5 1 1 0
13210100 0 1
13210101 4 .02
13210201 1 4
13210301 0 4
13210401 450. 5
13210501 321010000 1000000 1 1 .052 3
13210601 331010000 1000000 1 1 .052 3
13210701 0 0 0 0 3
13210801 0 0 0 0 3
13210901 0 0 0 0 3
*
* sg no.2 divide plate
14210000 3 5 1 1 0
14210100 3210
14210400 3210
14210501 421010000 1000000 1 1 .052 3
14210601 431010000 1000000 1 1 .052 3
14210701 0 0 0 0 3
14210801 0 0 0 0 3
14210901 0 0 0 0 3
*
* sg no.3 divide plate
15210000 3 5 1 1 0
15210100 3210
15210400 3210
15210501 521010000 1000000 1 1 .052 3
15210601 531010000 1000000 1 1 .052 3
15210701 0 0 0 0 3
15210801 0 0 0 0 3
15210901 0 0 0 0 3
*
* sg no.1 shell - primary side
13211000 6 5 2 1 .183
13211100 0 1
13211101 4 .203
13211201 1 4
13211301 0 4
13211401 450. 5
13211501 321010000 1000000 1 1 .1 3
13211502 331010000 1000000 1 1 .1 6
13211601 0 0 0 1 .1 3
    
```



```

13211602  0      0      0 1 .1 6
13211701  0 0 0 0 6
13211801  0 0 0 0 6
*
* sg no.2 shell - primary side
14211000  6 5 2 1 .183
14211100  3211
14211400  3211
14211501  421010000 1000000 1 1 .1 3
14211502  431010000 1000000 1 1 .1 6
14211601  0      0      0 1 .1 3
14211602  0      0      0 1 .1 6
14211701  0 0 0 0 6
14211801  0 0 0 0 6
*
* sg no.3 shell - primary side
15211000  6 5 2 1 .183
15211100  3211
15211400  3211
15211501  521010000 1000000 1 1 .1 3
15211502  531010000 1000000 1 1 .1 6
15211601  0      0      0 1 .1 3
15211602  0      0      0 1 .1 6
15211701  0 0 0 0 6
15211801  0 0 0 0 6
*
* u-tubes sg-1
13250000  18 5 2 1 .0065
13250100  0 1
13250101  4 .008
13250201  1 4
13250301  0 4
13250401  450. 5
13250501  325010000 10000 1 1 18.9098 6 * 1.4546 m * 13 tubes
13250502  326010000 10000 1 1 22. 12 * 1.4666 m * 15 tubes
13250503  327010000 10000 1 1 14.6667 18 * 1.4666 m * 10 tubes
13250601  601010000 0      1 1 18.9098 6
13250602  602010000 0      1 1 22. 12
13250603  603010000 0      1 1 14.6667 18
13250701  0 0 0 0 18
13250801  0 0 0 0 18
13250901  0 0 0 0 18
*
* u-tubes sg-2
14250000  18 5 2 1 .0065
14250100  3250
14250400  3250
14250501  425010000 10000 1 1 18.9098 6 * 1.4546 m * 13 tubes
14250502  426010000 10000 1 1 22. 12 * 1.4666 m * 15 tubes
14250503  427010000 10000 1 1 14.6667 18 * 1.4666 m * 10 tubes
14250601  701010000 0      1 1 18.9098 6
14250602  702010000 0      1 1 22. 12
14250603  703010000 0      1 1 14.6667 18
14250701  0 0 0 0 18
14250801  0 0 0 0 18
14250901  0 0 0 0 18
*
* u-tubes sg-3
15250000  18 5 2 1 .0065
15250100  3250
15250400  3250
    
```

```

15250501  525010000 10000 1 1 18.9098  6 * 1.4546 m * 13 tubes
15250502  526010000 10000 1 1 22.        12 * 1.4666 m * 15 tubes
15250503  527010000 10000 1 1 14.6667 18 * 1.4666 m * 10 tubes
15250601  801010000  0         1 1 18.9098  6
15250602  802010000  0         1 1 22.        12
15250603  803010000  0         1 1 14.6667 18
15250701  0 0 0 0 18
15250801  0 0 0 0 18
15250901  0 0 0 0 18

```

*
* sg no.1 shell - secondary side

```

16010000  5 5 2 1 .183
16010100  3211
16010401  426. 5
16010501  601010000 0 1 1 1.72647 1
16010502  602010000 0 1 1 .59853 2
16010503  603010000 0 1 1 .39283 3
16010504  605010000 0 1 1 .44363 4
16010505  606010000 0 1 1 1.48854 5
16010601  0         0 0 1 1.72647 1
16010602  0         0 0 1 .59853 2
16010603  0         0 0 1 .39283 3
16010604  0         0 0 1 .44363 4
16010605  0         0 0 1 1.48854 5
16010701  10907 0.37 0 0 1
16010702  10907 0.13 0 0 2
16010703  10907 0.085 0 0 3
16010704  10907 0.095 0 0 4
16010705  10907 0.32 0 0 5
16010801  0 0 0 0 5

```

*
* sg no.2 shell - secondary side

```

17010000  5 5 2 1 .183
17010100  3211
17010400  6010
17010501  701010000 0 1 1 1.72647 1
17010502  702010000 0 1 1 .59853 2
17010503  703010000 0 1 1 .39283 3
17010504  705010000 0 1 1 .44363 4
17010505  706010000 0 1 1 1.48854 5
17010601  0         0 0 1 1.72647 1
17010602  0         0 0 1 .59853 2
17010603  0         0 0 1 .39283 3
17010604  0         0 0 1 .44363 4
17010605  0         0 0 1 1.48854 5
17010701  10910 0.37 0 0 1
17010702  10910 0.13 0 0 2
17010703  10910 0.085 0 0 3
17010704  10910 0.095 0 0 4
17010705  10910 0.32 0 0 5
17010801  0 0 0 0 5

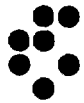
```

*
* sg no.3 shell - secondary side

```

18010000  5 5 2 1 .183
18010100  3211
18010400  6010
18010501  801010000 0 1 1 1.72647 1
18010502  802010000 0 1 1 .59853 2
18010503  803010000 0 1 1 .39283 3
18010504  805010000 0 1 1 .44363 4
18010505  806010000 0 1 1 1.48854 5

```



```

18010601  0          0 0 1 1.72647 1
18010602  0          0 0 1 .59853 2
18010603  0          0 0 1 .39283 3
18010604  0          0 0 1 .44363 4
18010605  0          0 0 1 1.48854 5
18010701  10913 0.37  0 0 1
18010702  10913 0.13  0 0 2
18010703  10913 0.085 0 0 3
18010704  10913 0.095 0 0 4
18010705  10913 0.32  0 0 5
18010801  0 0 0 0 5
*
*****
*          initial conditions - primary side          *
*****
*          volumes          *
*****
*
1110200  3  7.43060e+06  5.20089e+02
1010200  3  7.43430e+06  5.26263e+02
1021201  3  7.44034e+06  5.26238e+02  0 0 0 1
1021202  3  7.45457e+06  5.26192e+02  0 0 0 2
1021203  3  7.46777e+06  5.26177e+02  0 0 0 3
1021204  3  7.47254e+06  5.26174e+02  0 0 0 4
1300200  3  7.48155e+06  5.26103e+02
1031201  3  7.48965e+06  5.26088e+02  0 0 0 1
1031202  3  7.48965e+06  5.26071e+02  0 0 0 2
1031203  3  7.48154e+06  5.25997e+02  0 0 0 3
1031204  3  7.47241e+06  5.25987e+02  0 0 0 4
1031205  3  7.47022e+06  5.25961e+02  0 0 0 5
1040200  3  7.46644e+06  5.25940e+02
1050200  3  7.45437e+06  5.36239e+02
1061201  3  7.46277e+06  5.27629e+02  0 0 0 1
1061202  3  7.46064e+06  5.30258e+02  0 0 0 2
1061203  3  7.45852e+06  5.33555e+02  0 0 0 3
1061204  3  7.45642e+06  5.37224e+02  0 0 0 4
1061205  3  7.45433e+06  5.40938e+02  0 0 0 5
1061206  3  7.45226e+06  5.44257e+02  0 0 0 6
1061207  3  7.45020e+06  5.46992e+02  0 0 0 7
1061208  3  7.44816e+06  5.48844e+02  0 0 0 8
1061209  3  7.44612e+06  5.49682e+02  0 0 0 9
1071201  3  7.44075e+06  5.48322e+02  0 0 0 1
1071202  3  7.43304e+06  5.48282e+02  0 0 0 2
1071203  3  7.42628e+06  5.48093e+02  0 0 0 3
1081201  3  7.41844e+06  5.40095e+02  0 0 0 1
1081202  3  7.40953e+06  5.42284e+02  0 0 0 2
1081203  3  7.40067e+06  5.45022e+02  0 0 0 3
1800200  3  7.40939e+06  5.48056e+02
2001201  3  7.43046e+06  5.47000e+02  0 0 0 1
2001202  3  7.43807e+06  5.47000e+02  0 0 0 2
2001203  3  7.43807e+06  5.47000e+02  0 0 0 3
2001204  3  7.43322e+06  5.47000e+02  0 0 0 4
2021201  2  7.42594e+06  5.71600e-04  0 0 0 1
2021202  2  7.42041e+06  9.43500e-04  0 0 0 2
2021203  2  7.41420e+06  9.45000e-04  0 0 0 3
2021204  2  7.40797e+06  8.53800e-04  0 0 0 4
2021205  2  7.40174e+06  8.17200e-04  0 0 0 5
2021206  2  7.39546e+06  1.37700e-04  0 0 0 6
2021207  2  7.39157e+06  1.84000e-01  0 0 0 7
2021208  2  7.39067e+06  1.00000e+00  0 0 0 8
2021209  2  7.39033e+06  9.98000e-01  0 0 0 9
    
```



2021210	2	7.39000e+06	9.99000e-01	0	0	0	10
3011201	3	7.42281e+06	5.47996e+02	0	0	0	1
3011202	3	7.42460e+06	5.47941e+02	0	0	0	2
3011203	3	7.42819e+06	5.47894e+02	0	0	0	3
3011204	3	7.43179e+06	5.47853e+02	0	0	0	4
3011205	3	7.43539e+06	5.47817e+02	0	0	0	5
3011206	3	7.43717e+06	5.47784e+02	0	0	0	6
3011207	3	7.43715e+06	5.47314e+02	0	0	0	7
3011208	3	7.43452e+06	5.47283e+02	0	0	0	8
3011209	3	7.42927e+06	5.47251e+02	0	0	0	9
3011210	3	7.42403e+06	5.47215e+02	0	0	0	10
3011211	3	7.41879e+06	5.47178e+02	0	0	0	11
4011201	3	7.42281e+06	5.47993e+02	0	0	0	1
4011202	3	7.42459e+06	5.47939e+02	0	0	0	2
4011203	3	7.42819e+06	5.47893e+02	0	0	0	3
4011204	3	7.43178e+06	5.47852e+02	0	0	0	4
4011205	3	7.43538e+06	5.47815e+02	0	0	0	5
4011206	3	7.43717e+06	5.47780e+02	0	0	0	6
4011207	3	7.43715e+06	5.47304e+02	0	0	0	7
4011208	3	7.43451e+06	5.47272e+02	0	0	0	8
4011209	3	7.42927e+06	5.47238e+02	0	0	0	9
4011210	3	7.42403e+06	5.47201e+02	0	0	0	10
4011211	3	7.41878e+06	5.47162e+02	0	0	0	11
5011201	3	7.42281e+06	5.47996e+02	0	0	0	1
5011202	3	7.42460e+06	5.47941e+02	0	0	0	2
5011203	3	7.42819e+06	5.47895e+02	0	0	0	3
5011204	3	7.43179e+06	5.47854e+02	0	0	0	4
5011205	3	7.43539e+06	5.47818e+02	0	0	0	5
5011206	3	7.43717e+06	5.47785e+02	0	0	0	6
5011207	3	7.43715e+06	5.47315e+02	0	0	0	7
5011208	3	7.43452e+06	5.47285e+02	0	0	0	8
5011209	3	7.42927e+06	5.47252e+02	0	0	0	9
5011210	3	7.42403e+06	5.47217e+02	0	0	0	10
5011211	3	7.41879e+06	5.47179e+02	0	0	0	11
3511201	3	7.41875e+06	5.27193e+02	0	0	0	1
3511202	3	7.42393e+06	5.27158e+02	0	0	0	2
3511203	3	7.42939e+06	5.27123e+02	0	0	0	3
3511204	3	7.43484e+06	5.27088e+02	0	0	0	4
3511205	3	7.43756e+06	5.27052e+02	0	0	0	5
3511206	3	7.43556e+06	5.27015e+02	0	0	0	6
3511207	3	7.43159e+06	5.26978e+02	0	0	0	7
3511208	3	7.42761e+06	5.26941e+02	0	0	0	8
3511209	3	7.42363e+06	5.26903e+02	0	0	0	9
3511210	3	7.42163e+06	5.26866e+02	0	0	0	10
3511211	3	7.42163e+06	5.26830e+02	0	0	0	11
3511212	3	7.42454e+06	5.26786e+02	0	0	0	12
3511213	3	7.43039e+06	5.26303e+02	0	0	0	13
3511214	3	7.43331e+06	5.26272e+02	0	0	0	14
4511201	3	7.41875e+06	5.27193e+02	0	0	0	1
4511202	3	7.42394e+06	5.27157e+02	0	0	0	2
4511203	3	7.42939e+06	5.27121e+02	0	0	0	3
4511204	3	7.43485e+06	5.27086e+02	0	0	0	4
4511205	3	7.43757e+06	5.27049e+02	0	0	0	5
4511206	3	7.43557e+06	5.27011e+02	0	0	0	6
4511207	3	7.43159e+06	5.26973e+02	0	0	0	7
4511208	3	7.42761e+06	5.26934e+02	0	0	0	8
4511209	3	7.42363e+06	5.26896e+02	0	0	0	9
4511210	3	7.42163e+06	5.26858e+02	0	0	0	10
4511211	3	7.42163e+06	5.26821e+02	0	0	0	11
4511212	3	7.42454e+06	5.26776e+02	0	0	0	12
4511213	3	7.43039e+06	5.26287e+02	0	0	0	13



4511214	3	7.43331e+06	5.26256e+02	0	0	0	14
5511201	3	7.41875e+06	5.27193e+02	0	0	0	1
5511202	3	7.42393e+06	5.27158e+02	0	0	0	2
5511203	3	7.42939e+06	5.27123e+02	0	0	0	3
5511204	3	7.43484e+06	5.27088e+02	0	0	0	4
5511205	3	7.43756e+06	5.27052e+02	0	0	0	5
5511206	3	7.43556e+06	5.27015e+02	0	0	0	6
5511207	3	7.43159e+06	5.26978e+02	0	0	0	7
5511208	3	7.42761e+06	5.26940e+02	0	0	0	8
5511209	3	7.42363e+06	5.26903e+02	0	0	0	9
5511210	3	7.42164e+06	5.26866e+02	0	0	0	10
5511211	3	7.42163e+06	5.26829e+02	0	0	0	11
5511212	3	7.42454e+06	5.26786e+02	0	0	0	12
5511213	3	7.43039e+06	5.26303e+02	0	0	0	13
5511214	3	7.43331e+06	5.26273e+02	0	0	0	14
3210200	3	7.41594e+06	5.47027e+02				
3220200	3	7.41539e+06	5.46799e+02				
3230200	3	7.41485e+06	5.46286e+02				
3251201	3	7.41568e+06	5.35385e+02	0	0	0	1
3251202	3	7.41566e+06	5.30473e+02	0	0	0	2
3251203	3	7.41564e+06	5.28353e+02	0	0	0	3
3251204	3	7.41562e+06	5.27416e+02	0	0	0	4
3251205	3	7.41560e+06	5.26983e+02	0	0	0	5
3251206	3	7.41558e+06	5.26771e+02	0	0	0	6
3261201	3	7.41504e+06	5.35397e+02	0	0	0	1
3261202	3	7.41502e+06	5.30523e+02	0	0	0	2
3261203	3	7.41500e+06	5.28390e+02	0	0	0	3
3261204	3	7.41498e+06	5.27432e+02	0	0	0	4
3261205	3	7.41495e+06	5.26981e+02	0	0	0	5
3261206	3	7.41493e+06	5.26755e+02	0	0	0	6
3271201	3	7.41459e+06	5.35265e+02	0	0	0	1
3271202	3	7.41457e+06	5.30506e+02	0	0	0	2
3271203	3	7.41454e+06	5.28401e+02	0	0	0	3
3271204	3	7.41452e+06	5.27447e+02	0	0	0	4
3271205	3	7.41449e+06	5.26995e+02	0	0	0	5
3271206	3	7.41447e+06	5.26768e+02	0	0	0	6
3310200	3	7.41582e+06	5.27228e+02				
3320200	3	7.41524e+06	5.27209e+02				
3330200	3	7.41468e+06	5.27301e+02				
4210200	3	7.41593e+06	5.47009e+02				
4220200	3	7.41538e+06	5.46779e+02				
4230200	3	7.41484e+06	5.46265e+02				
4251201	3	7.41568e+06	5.35359e+02	0	0	0	1
4251202	3	7.41566e+06	5.30453e+02	0	0	0	2
4251203	3	7.41564e+06	5.28340e+02	0	0	0	3
4251204	3	7.41562e+06	5.27408e+02	0	0	0	4
4251205	3	7.41560e+06	5.26978e+02	0	0	0	5
4251206	3	7.41558e+06	5.26768e+02	0	0	0	6
4261201	3	7.41504e+06	5.35373e+02	0	0	0	1
4261202	3	7.41502e+06	5.30506e+02	0	0	0	2
4261203	3	7.41500e+06	5.28379e+02	0	0	0	3
4261204	3	7.41497e+06	5.27426e+02	0	0	0	4
4261205	3	7.41495e+06	5.26977e+02	0	0	0	5
4261206	3	7.41493e+06	5.26752e+02	0	0	0	6
4271201	3	7.41459e+06	5.35243e+02	0	0	0	1
4271202	3	7.41456e+06	5.30490e+02	0	0	0	2
4271203	3	7.41454e+06	5.28391e+02	0	0	0	3
4271204	3	7.41451e+06	5.27441e+02	0	0	0	4
4271205	3	7.41449e+06	5.26991e+02	0	0	0	5
4271206	3	7.41447e+06	5.26766e+02	0	0	0	6
4310200	3	7.41582e+06	5.27230e+02				



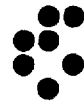
1061306		1.52590e-01	1.52590e-01	0	6
1061307		1.53570e-01	1.53570e-01	0	7
1061308		1.54260e-01	1.54260e-01	0	8
1460201	0	1.46800e-01	1.46800e-01	0	
1670201	0	1.54570e-01	1.54570e-01	0	
1071300	0				
1071301		7.04819e-02	7.04819e-02	0	1
1071302		6.87486e-02	8.05652e-02	0	2
1710201	0	2.98110e-01	2.98110e-01	0	
1720201	0	2.95330e-01	2.95330e-01	0	
1730201	0	2.98800e-01	2.98800e-01	0	
1780201	0	-2.34172e-04	-2.34784e-04	0	
1790201	0	3.79289e-02	3.79289e-02	0	
1800001	1 0				
1801201		3.79297e-02	3.79297e-02	0	
1081300	0				
1081301		-2.41574e-04	-2.42224e-04	0	1
1081302		-2.49246e-04	-2.49937e-04	0	2
1990201	0	-2.26005e-05	-2.26006e-05	0	
2001300	0				
2001301		-3.37845e-04	-3.37845e-04	0	1
2001302		-4.60400e-04	-4.60400e-04	0	2
2001303		-5.83323e-04	-5.83323e-04	0	3
2010201	0	-7.08604e-04	1.13530e-01	0	
2021300	0				
2021301		-1.63006e-05	1.59050e-01	0	1
2021302		-8.79318e-05	1.70120e-01	0	2
2021303		-9.09411e-05	1.69180e-01	0	3
2021304		-8.01654e-05	1.68750e-01	0	4
2021305		-6.81552e-05	1.57680e-01	0	5
2021306		-3.26816e-04	8.44920e-01	0	6
2021307		-3.88120e+00	2.68635e-03	0	7
2021308		-2.35490e-01	1.88757e-03	0	8
2021309		-2.71480e-01	1.60097e-03	0	9
3511300	0				
3511301		2.84930e-01	2.84930e-01	0	1
3511302		2.84910e-01	2.84910e-01	0	2
3511303		2.84880e-01	2.84880e-01	0	3
3511304		2.84860e-01	2.84860e-01	0	4
3511305		2.84840e-01	2.84840e-01	0	5
3511306		2.84820e-01	2.84820e-01	0	6
3511307		2.84800e-01	2.84800e-01	0	7
3511308		2.84780e-01	2.84780e-01	0	8
3511309		2.84760e-01	2.84760e-01	0	9
3511310		2.84740e-01	2.84740e-01	0	10
3511311		2.84720e-01	2.84720e-01	0	11
3511312		2.84700e-01	2.84700e-01	0	12
3511313		2.84430e-01	2.84430e-01	0	13
4511300	0				
4511301		2.82260e-01	2.82260e-01	0	1
4511302		2.82240e-01	2.82240e-01	0	2
4511303		2.82220e-01	2.82220e-01	0	3
4511304		2.82190e-01	2.82190e-01	0	4
4511305		2.82170e-01	2.82170e-01	0	5
4511306		2.82150e-01	2.82150e-01	0	6
4511307		2.82130e-01	2.82130e-01	0	7
4511308		2.82110e-01	2.82110e-01	0	8
4511309		2.82090e-01	2.82090e-01	0	9
4511310		2.82070e-01	2.82070e-01	0	10
4511311		2.82050e-01	2.82050e-01	0	11
4511312		2.82030e-01	2.82030e-01	0	12



4511313		2.81760e-01	2.81760e-01	0	13
5511300	0				
5511301		2.85570e-01	2.85570e-01	0	1
5511302		2.85550e-01	2.85550e-01	0	2
5511303		2.85530e-01	2.85530e-01	0	3
5511304		2.85510e-01	2.85510e-01	0	4
5511305		2.85490e-01	2.85490e-01	0	5
5511306		2.85470e-01	2.85470e-01	0	6
5511307		2.85450e-01	2.85450e-01	0	7
5511308		2.85430e-01	2.85430e-01	0	8
5511309		2.85410e-01	2.85410e-01	0	9
5511310		2.85390e-01	2.85390e-01	0	10
5511311		2.85370e-01	2.85370e-01	0	11
5511312		2.85340e-01	2.85340e-01	0	12
5511313		2.85070e-01	2.85070e-01	0	13
3011300	0				
3011301		2.98070e-01	2.98070e-01	0	1
3011302		2.98030e-01	2.98030e-01	0	2
3011303		2.98000e-01	2.98000e-01	0	3
3011304		2.97970e-01	2.97970e-01	0	4
3011305		2.97940e-01	2.97940e-01	0	5
3011306		2.97910e-01	2.97910e-01	0	6
3011307		2.97560e-01	2.97560e-01	0	7
3011308		2.97540e-01	2.97540e-01	0	8
3011309		2.97510e-01	2.97510e-01	0	9
3011310		2.97480e-01	2.97480e-01	0	10
4011300	0				
4011301		2.95280e-01	2.95280e-01	0	1
4011302		2.95240e-01	2.95240e-01	0	2
4011303		2.95210e-01	2.95210e-01	0	3
4011304		2.95180e-01	2.95180e-01	0	4
4011305		2.95140e-01	2.95140e-01	0	5
4011306		2.95110e-01	2.95110e-01	0	6
4011307		2.94770e-01	2.94770e-01	0	7
4011308		2.94740e-01	2.94740e-01	0	8
4011309		2.94720e-01	2.94720e-01	0	9
4011310		2.94690e-01	2.94690e-01	0	10
5011300	0				
5011301		2.98740e-01	2.98740e-01	0	1
5011302		2.98710e-01	2.98710e-01	0	2
5011303		2.98680e-01	2.98680e-01	0	3
5011304		2.98650e-01	2.98650e-01	0	4
5011305		2.98610e-01	2.98610e-01	0	5
5011306		2.98580e-01	2.98580e-01	0	6
5011307		2.98240e-01	2.98240e-01	0	7
5011308		2.98210e-01	2.98210e-01	0	8
5011309		2.98190e-01	2.98190e-01	0	9
5011310		2.98160e-01	2.98160e-01	0	10
3210001	2 0				
3211201		2.97460e-01	2.97460e-01	0	
3212201		1.18000e-01	1.18000e-01	0	
3220001	2 0				
3221201		3.58444e-02	4.07029e-02	0	
3222201		1.29590e-01	1.29590e-01	0	
3230001	2 0				
3231201		1.47885e-02	1.60414e-02	0	
3232201		1.36480e-01	1.36480e-01	0	
3251300	0				
3251301		1.14960e-01	1.14960e-01	0	1
3251302		1.13810e-01	1.13810e-01	0	2
3251303		1.13320e-01	1.13320e-01	0	3



3251304		1.13120e-01	1.13120e-01	0	4
3251305		1.13020e-01	1.13020e-01	0	5
3261300	0				
3261301		1.26330e-01	1.26330e-01	0	1
3261302		1.25060e-01	1.25060e-01	0	2
3261303		1.24530e-01	1.24530e-01	0	3
3261304		1.24300e-01	1.24300e-01	0	4
3261305		1.24190e-01	1.24190e-01	0	5
3271300	0				
3271301		1.33170e-01	1.33170e-01	0	1
3271302		1.31870e-01	1.31870e-01	0	2
3271303		1.31310e-01	1.31310e-01	0	3
3271304		1.31070e-01	1.31070e-01	0	4
3271305		1.30950e-01	1.30950e-01	0	5
3310001	2 0				
3311201		1.12970e-01	1.12970e-01	0	
3312201		2.84950e-01	2.84950e-01	0	
3320001	2 0				
3321201		1.24130e-01	1.24130e-01	0	
3322201		3.43483e-02	3.89211e-02	0	
3330001	2 0				
3331201		1.30890e-01	1.30890e-01	0	
3332201		1.41812e-02	1.53532e-02	0	
4210001	2 0				
4211201		2.94660e-01	2.94660e-01	0	
4212201		1.16710e-01	1.16710e-01	0	
4220001	2 0				
4221201		3.55320e-02	4.03304e-02	0	
4222201		1.28410e-01	1.28410e-01	0	
4230001	2 0				
4231201		1.46676e-02	1.59043e-02	0	
4232201		1.35360e-01	1.35360e-01	0	
4251300	0				
4251301		1.13710e-01	1.13710e-01	0	1
4251302		1.12570e-01	1.12570e-01	0	2
4251303		1.12090e-01	1.12090e-01	0	3
4251304		1.11890e-01	1.11890e-01	0	4
4251305		1.11790e-01	1.11790e-01	0	5
4261300	0				
4261301		1.25180e-01	1.25180e-01	0	1
4261302		1.23930e-01	1.23930e-01	0	2
4261303		1.23400e-01	1.23400e-01	0	3
4261304		1.23170e-01	1.23170e-01	0	4
4261305		1.23060e-01	1.23060e-01	0	5
4271300	0				
4271301		1.32080e-01	1.32080e-01	0	1
4271302		1.30790e-01	1.30790e-01	0	2
4271303		1.30240e-01	1.30240e-01	0	3
4271304		1.30000e-01	1.30000e-01	0	4
4271305		1.29880e-01	1.29880e-01	0	5
4310001	2 0				
4311201		1.11750e-01	1.11750e-01	0	
4312201		2.82280e-01	2.82280e-01	0	
4320001	2 0				
4321201		1.23010e-01	1.23010e-01	0	
4322201		3.40504e-02	3.85667e-02	0	
4330001	2 0				
4331201		1.29830e-01	1.29830e-01	0	
4332201		1.40658e-02	1.52227e-02	0	
5210001	2 0				
5211201		2.98130e-01	2.98130e-01	0	



5212201		1.18310e-01	1.18310e-01	0	
5220001	2 0				
5221201		3.59198e-02	4.07927e-02	0	
5222201		1.29870e-01	1.29870e-01	0	
5230001	2 0				
5231201		1.48178e-02	1.60746e-02	0	
5232201		1.36750e-01	1.36750e-01	0	
5251300	0				
5251301		1.15270e-01	1.15270e-01	0	1
5251302		1.14110e-01	1.14110e-01	0	2
5251303		1.13620e-01	1.13620e-01	0	3
5251304		1.13410e-01	1.13410e-01	0	4
5251305		1.13320e-01	1.13320e-01	0	5
5261300	0				
5261301		1.26600e-01	1.26600e-01	0	1
5261302		1.25340e-01	1.25340e-01	0	2
5261303		1.24800e-01	1.24800e-01	0	3
5261304		1.24570e-01	1.24570e-01	0	4
5261305		1.24460e-01	1.24460e-01	0	5
5271300	0				
5271301		1.33430e-01	1.33430e-01	0	1
5271302		1.32130e-01	1.32130e-01	0	2
5271303		1.31570e-01	1.31570e-01	0	3
5271304		1.31330e-01	1.31330e-01	0	4
5271305		1.31210e-01	1.31210e-01	0	5
5310001	2 0				
5311201		1.13270e-01	1.13270e-01	0	
5312201		2.85590e-01	2.85590e-01	0	
5320001	2 0				
5321201		1.24400e-01	1.24400e-01	0	
5322201		3.44203e-02	3.90067e-02	0	
5330001	2 0				
5331201		1.31150e-01	1.31150e-01	0	
5332201		1.42091e-02	1.53848e-02	0	

*

 * initial conditions - secondary side *

 * volumes *

 *

6010200	2	4.20863e+06	6.38600e-05
6020200	2	4.20791e+06	9.21800e-05
6030200	2	4.20745e+06	4.56300e-05
6050200	2	4.20711e+06	7.76300e-03
6110200	2	4.20862e+06	0.00000e+00
6120200	2	4.20791e+06	0.00000e+00
6130200	2	4.20744e+06	0.00000e+00
6060200	2	4.20695e+06	1.00000e+00
7010200	2	4.20863e+06	6.33200e-05
7020200	2	4.20791e+06	9.14700e-05
7030200	2	4.20745e+06	4.51600e-05
7050200	2	4.20711e+06	7.73100e-03
7110200	2	4.20862e+06	0.00000e+00
7120200	2	4.20791e+06	0.00000e+00
7130200	2	4.20744e+06	0.00000e+00
7060200	2	4.20695e+06	1.00000e+00
8010200	2	4.20863e+06	6.39800e-05
8020200	2	4.20791e+06	9.23200e-05
8030200	2	4.20745e+06	4.57100e-05
8050200	2	4.20711e+06	7.77500e-03



```
8110200 2 4.20862e+06 0.00000e+00
8120200 2 4.20791e+06 0.00000e+00
8130200 2 4.20744e+06 0.00000e+00
8060200 2 4.20695e+06 1.00000e+00
9000200 2 4.20694e+06 1.00000e+00
```

```
*
*****
*                               junctions                               *
*****
```

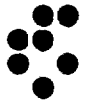
```
*
6010001 1 0
6011201      2.83073e-02  2.19560e-01  0
6020001 1 0
6021201      3.46215e-02  1.95920e-01  0
6050001 3 0
6051201     -3.81000e-01  1.93312e-03  0
6052201      1.43540e-01 -9.84810e-01  0
6053201      3.59443e-02  5.40720e-01  0
6110001 1 0
6111201      1.13010e-01  9.31748e-02  0
6120001 2 0
6121201      5.69313e-02  2.23045e-02  0
6122201      1.13010e-01  1.13010e-01  0
6130001 2 0
6131201      8.21489e-03 -3.16753e-02  0
6132201      1.38000e-01  1.38000e-01  0
7010001 1 0
7011201      2.81816e-02  2.18700e-01  0
7020001 1 0
7021201      3.44755e-02  1.95130e-01  0
7050001 3 0
7051201     -3.80690e-01  1.91798e-03  0
7052201      1.42830e-01 -9.84660e-01  0
7053201      3.57666e-02  5.40280e-01  0
7110001 1 0
7111201      1.12510e-01  9.28345e-02  0
7120001 2 0
7121201      5.67114e-02  2.23134e-02  0
7122201      1.12510e-01  1.12510e-01  0
7130001 2 0
7131201      8.07486e-03 -3.15248e-02  0
7132201      1.37420e-01  1.37420e-01  0
8010001 1 0
8011201      2.83344e-02  2.19730e-01  0
8020001 1 0
8021201      3.46484e-02  1.96060e-01  0
8050001 3 0
8051201     -3.81110e-01  1.93451e-03  0
8052201      1.43670e-01 -9.84950e-01  0
8053201      3.59766e-02  5.40850e-01  0
8110001 1 0
8111201      1.13120e-01  9.32478e-02  0
8120001 2 0
8121201      5.69601e-02  2.22911e-02  0
8122201      1.13120e-01  1.13120e-01  0
8130001 2 0
8131201      8.23907e-03 -3.17040e-02  0
8132201      1.38110e-01  1.38110e-01  0
9000001 3 0
9001201      3.91824e-02  3.91824e-02  0
9002201      3.87501e-02  3.87501e-02  0
```



```

9003201      3.92572e-02  3.92572e-02  0
9040201      0  1.17190e-01  1.17190e-01  0
*
*****
*                               heat losses                               *
*****
*
* given mod3 sg heat losses distribution: 3 x -2.8 kw
*                                       --> 3 x -2.5 kw for isp-33
*
* ctv 901: downcomer heat losses [w]
20590100 dwchloss sum -3.83 -862.0 1
20590101 -308.0 1.0 tempf 102010000
*
* ctv 902: lower plenum heat losses [w]
20590200 lphloss sum -6.76 -1521.0 1
20590201 -308.0 1.0 tempf 103010000
*
* ctv 903: core section heat losses [w]
20590300 chloss sum -3.04 -715.0 1
20590301 -308.0 1.0 tempf 105010000
*
* ctv 904: upper plenum heat losses [w]
20590400 uphloss sum -7.09 -1666.0 1
20590401 -308.0 1.0 tempf 108010000
*
* ctv 905: h11 heat losses [w]
20590500 h11hloss sum -5.37 -1262.0 1
20590501 -308.0 1.0 tempf 301050000
*
* ctv 906: c11 heat losses [w]
20590600 c11hloss sum -5.68 -1277.0 1
20590601 -308.0 1.0 tempf 351070000
*
* ctv 907: sg1 heat losses [w]
20590700 sg1hloss sum -11.63 -2500.0 1
20590701 -308.0 1.0 tempf 611010000
*
* ctv 908: h12 heat losses [w]
20590800 h12hloss sum -5.46 -1284.0 1
20590801 -308.0 1.0 tempf 401050000
*
* ctv 909: c12 heat losses [w]
20590900 c12hloss sum -5.77 -1298.0 1
20590901 -308.0 1.0 tempf 451070000
*
* ctv 910: sg2 heat losses [w]
20591000 sg2hloss sum -11.63 -2500.0 1
20591001 -308.0 1.0 tempf 711010000
*
* ctv 911: h13 heat losses [w]
20591100 h13hloss sum -5.39 -1266.0 1
20591101 -308.0 1.0 tempf 501050000
*
* ctv 912: c13 heat losses [w]
20591200 c13hloss sum -5.70 -1282.0 1
20591201 -308.0 1.0 tempf 551070000
*
* ctv 913: sg3 heat losses [w]
20591300 sg3hloss sum -11.63 -2500.0 1
20591301 -308.0 1.0 tempf 811010000

```



```

*
* ctv 914: pressurizer heat losses [w]
* 20591400 przhloss sum -9.24 -2171.0 1
20591400 przhloss sum -9.92 -2331.0 1 * +1/5 razlike (160 w) za
*                                     ugl. padanja tlaka v ch. testu
20591401 -308.0 1.0 tempf 202020000
*
* ctv 915: surge line heat losses [w]
20591500 slhloss sum -3.50 -788.0 1
20591501 -308.0 1.0 tempf 200020000
*
* ctv 916: total vessel losses [w]
20591600 veshloss sum 1. -4764. 1
20591601 0.0 1.0 cntrlvar 901 1.0 cntrlvar 902 1.0 cntrlvar 903
20591602 1.0 cntrlvar 904
*
* ctv 917: total loop 1 losses [w]
20591700 lplhloss sum 1. -2539. 1
20591701 0.0 1.0 cntrlvar 905 1.0 cntrlvar 906 1.0 cntrlvar 951
20591702 1.0 cntrlvar 954
*
* ctv 918: total loop 2 losses [w]
20591800 lp2hloss sum 1. -2582. 1
20591801 0.0 1.0 cntrlvar 908 1.0 cntrlvar 909 1.0 cntrlvar 952
20591802 1.0 cntrlvar 955
*
* ctv 919: total loop 3 losses [w]
20591900 lp3hloss sum 1. -2548. 1
20591901 0.0 1.0 cntrlvar 911 1.0 cntrlvar 912 1.0 cntrlvar 953
20591902 1.0 cntrlvar 956
*
* ctv 920: total pressurizer losses [w]
20592000 pzshloss sum 1. -2959. 1
20592001 0.0 1.0 cntrlvar 914 1.0 cntrlvar 915 1.0 cntrlvar 957
*
* ctv 925: total heat losses [kw]
20592500 sumhloss sum 1.0e-03 -30.5 1
20592501 0.0 1.0 cntrlvar 907 1.0 cntrlvar 910 1.0 cntrlvar 913 * sgs
20592502 1.0 cntrlvar 916 1.0 cntrlvar 917 1.0 cntrlvar 918 * vess,11,12
20592503 1.0 cntrlvar 919 1.0 cntrlvar 920 * 13,prz
*
*****
* heat structure thermal property data *
*****
*
20100100 tbl/fctn 1 1 * aisi 3041
20100101 293. 15.0 373. 15.5 473. 17.5 673. 20.0 873. 22.5 1073. 25.5
20100151 293. 3.9+1 373. 3.9+1 473. 4.07+1 573. 4.23+1 673. 4.33+1
20100152 1000. 4.5+1 * ???? initialization
*
20100200 tbl/fctn 2 2 * boron nitride (heater rods) - bethsy data !!!
20100201 293. 1473. 2. 0 0 0 0 0
20100251 293. 1473. 1.46+1 1.62-2 0 0 0 0 0 * ???? initialization
*
*****
* fast artifitial sg level control *
*****
*
6540000 afeed1 tmdpv0l
6540101 10. 10. 0 0 0 0 0 0 0
6540200 3 0 tempf 603010000
    
```




```
*
* mod3 ccfl data
*
1111110 0.15      0 1. 1.
1011110 0.05248 0 1. 1.
1012110 0.05248 0 1. 1.
1013110 0.05248 0 1. 1.
1014110 0.0737   0 1. 1.
1021401 0.0737   0 1. 1. 3
1230110 0.0737   0 1. 1.
1301110 0.1397   0 1. 1.
1031401 0.1397   0 1. 1. 4
1041110 0.1397   0 1. 1.
1460110 0.0055   0 1. 1.
1240110 0.00641  0 1. 1.
1051110 0.00641  0 1. 1.
1061401 0.0055   0 1. 1. 8
1670110 0.0055   0 1. 1.
1071401 0.02845  0 1. 1. 1
1071402 0.1891   0 1. 1. 2
1710110 0.05248  0 1. 1.
1720110 0.05248  0 1. 1.
1730110 0.05248  0 1. 1.
1780110 0.1891   0 1. 1.
1790110 0.0151   0 1. 1.
1081401 0.1891   0 1. 1. 2
1801110 0.0153   0 1. 1.
1990110 0.0273   0 1. 1.
2001401 0.0273   0 1. 1. 3
2010110 0.0273   0 1. 1.
2021401 0.1397   0 1. 1. 9
3011401 0.05248  0 1. 1. 10
3511401 0.05248  0 1. 1. 13
4011401 0.05248  0 1. 1. 10
4511401 0.05248  0 1. 1. 13
5011401 0.05248  0 1. 1. 10
5511401 0.05248  0 1. 1. 13
3211110 0.05248  0 1. 1.
3212110 0.013    0 1. 1.
3221110 0.2128   0 1. 1.
3222110 0.013    0 1. 1.
3231110 0.2128   0 1. 1.
3232110 0.013    0 1. 1.
3251401 0.013    0 1. 1. 5
3261401 0.013    0 1. 1. 5
3271401 0.013    0 1. 1. 5
3311110 0.013    0 1. 1.
3312110 0.05248  0 1. 1.
3321110 0.013    0 1. 1.
3322110 0.2128   0 1. 1.
3331110 0.013    0 1. 1.
3332110 0.2128   0 1. 1.
4211110 0.05248  0 1. 1.
4212110 0.013    0 1. 1.
4221110 0.2128   0 1. 1.
4222110 0.013    0 1. 1.
4231110 0.2128   0 1. 1.
4232110 0.013    0 1. 1.
4251401 0.013    0 1. 1. 5
4261401 0.013    0 1. 1. 5
4271401 0.013    0 1. 1. 5
```




1011101	351010000	101000000	0	0	0	100100	
1012101	451010000	101000000	0	0	0	100100	
1013101	551010000	101000000	0	0	0	100100	
1014101	101010000	102000000	0	0	0	100100	
1021101						100000	3
1230101	102010000	130000000	42.66-4	0	0	100000	
1301101	130010000	103000000	0	.13	.13	100000	
1031101						100000	4
1041101	103010000	104000000	0	1.3	1.3	100100	
1240101	104010000	105000000	26.5-4	0	0	100000	
1051101	105010000	107000000	0	0	0	100100	
1460101	104010000	106000000	0	1.8	1.8	100100	
1061101						100000	8
1670101	106010000	107000000	0	3.6	3.6	100100	
1071101						100100	2
1710101	107010000	301000000	0	1.	1.	100100	
1720101	107010000	401000000	0	1.	1.	100100	
1730101	107010000	501000000	0	1.	1.	100100	
1780101	107010000	108000000	0	0	0	100000	
1790101	107010000	180000000	1.8-4	0	0	100100	
1081101						100000	2
1801101	180010000	108010000	0	0	0	100000	
1990101	301000000	200000000	0	1.	1.	100100	
2001101						100000	3
2010101	200010000	202000000	0	1.	1.	100100	
2021101						100000	9
3511101						100000	13
4511101						100000	13
5511101						100000	13
3011101						100000	10
4011101						100000	10
5011101						100000	10
3211101	301010000	321000000	0	0	0	100100	
3212101	321010000	325000000	0	1.	1.	100100	
3221101	321010000	322000000	0	0	0	100100	
3222101	322010000	326000000	0	1.	1.	100100	
3231101	322010000	323000000	0	0	0	100100	
3232101	323010000	327000000	0	1.	1.	100100	
3251101						100000	5
3261101						100000	5
3271101						100000	5
3311101	325010000	331000000	0	1.	1.	100100	
3312101	331010000	351000000	0	0	0	100100	
3321101	326010000	332000000	0	1.	1.	100100	
3322101	332010000	331000000	0	0	0	100100	
3331101	327010000	333000000	0	1.	1.	100100	
3332101	333010000	332000000	0	0	0	100100	
4211101	401010000	421000000	0	0	0	100100	
4212101	421010000	425000000	0	1.	1.	100100	
4221101	421010000	422000000	0	0	0	100100	
4222101	422010000	426000000	0	1.	1.	100100	
4231101	422010000	423000000	0	0	0	100100	
4232101	423010000	427000000	0	1.	1.	100100	
4251101						100000	5
4261101						100000	5
4271101						100000	5
4311101	425010000	431000000	0	1.	1.	100100	
4312101	431010000	451000000	0	0	0	100100	
4321101	426010000	432000000	0	1.	1.	100100	
4322101	432010000	431000000	0	0	0	100100	
4331101	427010000	433000000	0	1.	1.	100100	



```

4332101 433010000 432000000 0      0  0  100100
5211101 501010000 521000000 0      0  0  100100
5212101 521010000 525000000 0      1. 1. 100100
5221101 521010000 522000000 0      0  0  100100
5222101 522010000 526000000 0      1. 1. 100100
5231101 522010000 523000000 0      0  0  100100
5232101 523010000 527000000 0      1. 1. 100100
5251101                100000 5
5261101                100000 5
5271101                100000 5
5311101 525010000 531000000 0      1. 1. 100100
5312101 531010000 551000000 0      0  0  100100
5321101 526010000 532000000 0      1. 1. 100100
5322101 532010000 531000000 0      0  0  100100
5331101 527010000 533000000 0      1. 1. 100100
5332101 533010000 532000000 0      0  0  100100
6011101 601010000 602000000 0      0  0  100000
6111101 611010000 601000000 0      0  0  100000
6021101 602010000 603000000 0      0  0  100000
6121101 612010000 602000000 0      0  0  100000
6122101 612010000 611000000 0      0  0  100000
6131101 613010000 603000000 0      0  0  100000
6132101 613010000 612000000 0      0  0  100000
6051101 605010000 606000000 0      0  0  001000 * 0.01 * ???? default?
6052101 605000000 613000000 0      0  0  001000 * 0.01
6053101 603010000 605000000 0      0  0  001000
7011101 701010000 702000000 0      0  0  100000
7111101 711010000 701000000 0      0  0  100000
7021101 702010000 703000000 0      0  0  100000
7121101 712010000 702000000 0      0  0  100000
7122101 712010000 711000000 0      0  0  100000
7131101 713010000 703000000 0      0  0  100000
7132101 713010000 712000000 0      0  0  100000
7051101 705010000 706000000 0      0  0  001000 * 0.01 * ???? default?
7052101 705000000 713000000 0      0  0  001000 * 0.01
7053101 703010000 705000000 0      0  0  001000
8011101 801010000 802000000 0      0  0  100000
8111101 811010000 801000000 0      0  0  100000
8021101 802010000 803000000 0      0  0  100000
8121101 812010000 802000000 0      0  0  100000
8122101 812010000 811000000 0      0  0  100000
8131101 813010000 803000000 0      0  0  100000
8132101 813010000 812000000 0      0  0  100000
8051101 805010000 806000000 0      0  0  001000 * 0.01 * ???? default?
8052101 805000000 813000000 0      0  0  001000 * 0.01
8053101 803010000 805000000 0      0  0  001000
9001101 606010000 900000000 0      0  0  100100
9002101 706010000 900000000 0      0  0  100100
9003101 806010000 900000000 0      0  0  100100
9040101 900010000 901000000 7.92034-5 1. 1. 100100 1. 1.

```

```

*
*****
*           mod3 heat structure changes           *
*****

```

```

*
11010801  0 10. 10. 0 0 0 0 1.  2
11011801  0 10. 10. 0 0 0 0 1.  1
11011901  0 10. 10. 0 0 0 0 1.  1
11020801  0 10. 10. 0 0 0 0 1.  4
11030801  0 10. 10. 0 0 0 0 1.  6
11040801  0 10. 10. 0 0 0 0 1.  1

```



```

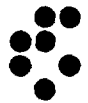
11041901  0 10. 10. 0 0 0 0 1.  1
11050801  0 10. 10. 0 0 0 0 1.  1
11051801  0 10. 10. 0 0 0 0 1.  9
11051901  0 10. 10. 0 0 0 0 1.  9
11052801  0 10. 10. 0 0 0 0 1.  9
11052901  0 10. 10. 0 0 0 0 1.  9
11060901  0 10. 10. 0 0 0 0 1. 11
11061801  0 10. 10. 0 0 0 0 1.  9
11061901  0 10. 10. 0 0 0 0 1.  9
11070801  0 10. 10. 0 0 0 0 1.  1
11080801  0 10. 10. 0 0 0 0 1.  5
11081801  0 10. 10. 0 0 0 0 1.  3
11081901  0 10. 10. 0 0 0 0 1.  3
12000801  0 10. 10. 0 0 0 0 1.  4
12001801  0 10. 10. 0 0 0 0 1.  1
12020801  0 10. 10. 0 0 0 0 1. 10
12021901  0 10. 10. 0 0 0 0 1.  3
13010801  0 10. 10. 0 0 0 0 1. 11
13011801  0 10. 10. 0 0 0 0 1.  3
14010801  0 10. 10. 0 0 0 0 1. 11
15010801  0 10. 10. 0 0 0 0 1. 11
13210801  0 10. 10. 0 0 0 0 1.  3
13210901  0 10. 10. 0 0 0 0 1.  3
14210801  0 10. 10. 0 0 0 0 1.  3
14210901  0 10. 10. 0 0 0 0 1.  3
15210801  0 10. 10. 0 0 0 0 1.  3
15210901  0 10. 10. 0 0 0 0 1.  3
13211801  0 10. 10. 0 0 0 0 1.  6
14211801  0 10. 10. 0 0 0 0 1.  6
15211801  0 10. 10. 0 0 0 0 1.  6
13510801  0 10. 10. 0 0 0 0 1. 14
13511801  0 10. 10. 0 0 0 0 1.  3
14510801  0 10. 10. 0 0 0 0 1. 14
15510801  0 10. 10. 0 0 0 0 1. 14
13250801  0 10. 10. 0 0 0 0 1. 18
13250901  0 10. 10. 0 0 0 0 1. 18
14250801  0 10. 10. 0 0 0 0 1. 18
14250901  0 10. 10. 0 0 0 0 1. 18
15250801  0 10. 10. 0 0 0 0 1. 18
15250901  0 10. 10. 0 0 0 0 1. 18
16010801  0 10. 10. 0 0 0 0 1.  5
17010801  0 10. 10. 0 0 0 0 1.  5
18010801  0 10. 10. 0 0 0 0 1.  5
*
*****
*                ??? replacement block                *
*****
*
* prepare restart at 0 seconds
201 .1  1.-6  .1  3  2000  20000  20000
*
* restore volumetric heat capacities
20100151 293. 3.90+6 373. 3.90+6 473. 4.07+6 573. 4.23+6 673. 4.33+6
20100152 1000. 4.50+6
20100251 293. 1473. 1.46+6 1.62+3 0. 0. 0. 0. 0.
.
    
```



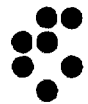
Appendix B

ISP-33 Run Input Deck





```
=isp-33: pactel (vtt, lappeenranta, finland)
* natural circulation test
*
100 restart transnt
103 0
201 1200. 1.-6 0.1 3 300 12000 12000
202 8000. 1.-6 0.1 3 300 9000 9000
*
*****
*               m i n o r   e d i t   r e q u e s t s               *
*****
*
301  cntrlvar      100 * core (heater) power
302  mflowj       101040000 * downcomer inlet
303  tempf        101010000 * downcomer inlet
304  tempf        107030000 * vessel outlet
305  p            202100000 * pressurizer
306  cntrlvar      172 * pressurizer level
307  cntrlvar      202 * pressurizer heater power
308  p            606010000 * secondary
309  mflowj       652000000 * sg-1 feedwater
310  mflowj       301050000 * loop-1
311  mflowj       401050000 * loop-2
312  mflowj       501050000 * loop-3
313  mflowj       904000000 * steam out
314  mflowj       131000000 * break flow
315  cntrlvar      190 * integral break flow
316  cntrlvar      999 * maxcladt
317  cntrlvar      171 * primary level
318  cntrlvar      153 * dp 2 cold leg 1
319  mflowj       201000000 * surge line flow
*
*****
*               t r i p s               *
*****
*
401  p            202100000 ge null 0 73.6+5 n * low.limit - prz press.control
402  p            202100000 ge null 0 75.0+5 n * upp.limit - prz press.control
*
501  time          0 ge null 0 1200. n * draining starts,prz heaters off
599  cntrlvar      999 ge null 0 623. n * cladding overheat
*
600  599 * stop trip - cladding overheat
*
* prz pressure control (2 or 6 kw)
701  702 or -401 n
702  701 and -402 n
*
*****
*               c o n t r o l s               *
*****
*
20517900 uphetemp constant 2.500000e-02 * upper head temperature
20593000 reg930 constant 2.589604e-02 * rcs flow
20593100 reg931 constant 1.156322e-02 * core bypass flow
*
* ctv 199: switch pressurizer heaters off at first draining
20519900 przh-swi tripunit 1. 0 0
20519901 -501
*
* ctv 200: switch higher level of pressurizer heaters
```

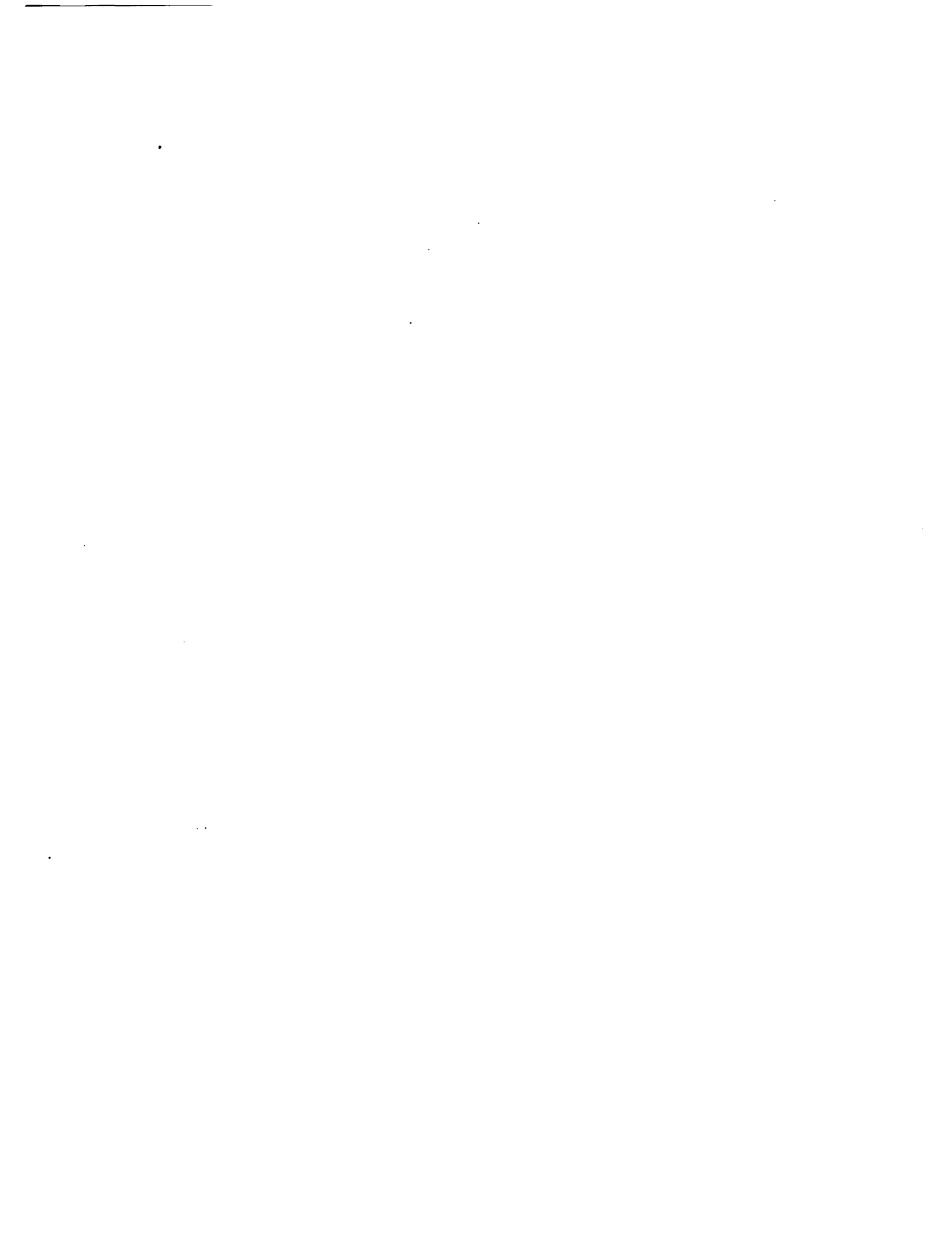


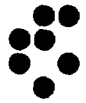
```

20520000 przhswit tripunit 1. 0 0
20520001 702
*
* ctv 201: pressurizer heaters
20520100 przheats sum 1.+3 2.+3 0
20520101 2. 4. cntrlvar 200
*
* ctv 202: pressurizer heaters final switch
20520200 prz-heat mult 1. 2.+3 0
20520201 cntrlvar 199 cntrlvar 201
*
* ctv 999: maximum cladding outer temperature
20599900 maxcladt stdfctn 1. 0 1
20599901 max httemp 106000107 httemp 106000207 httemp 106000307
20599902 httemp 106000407 httemp 106000507 httemp 106000607
20599903 httemp 106000707 httemp 106000807 httemp 106000907
*
*****
* hydrodynamic components *
*****
*
2100000 noname delete * art. pressurizer control
2110000 noname delete
2210000 noname delete
2220000 noname delete
*
6540000 noname delete * art. feedwater
6550000 noname delete
7540000 noname delete
7550000 noname delete
8540000 noname delete
8550000 noname delete
*
* drain valve
1310000 drain tmdppjun
1310101 130010000 132000000 5.067-4
1310200 1 501
1310201 -1. 0 0 0 0 0 0 0 0 * drain: amount duration
1310202 0 .33 0 0 182. .33 0 0 182. 0 0 0 900. 0 0 0 * 60 kg 182 sec
1310203 900. 1. 0 0 960. 1. 0 0 960. 0 0 0 1800. 0 0 0 * 60 kg 60 sec
1310204 1800. 1. 0 0 1860. 1. 0 0 1860. 0 0 0 2700. 0 0 0 * -- --
1310205 2700. 1. 0 0 2760. 1. 0 0 2760. 0 0 0 3600. 0 0 0 * -- --
1310206 3600. 1. 0 0 3660. 1. 0 0 3660. 0 0 0 4500. 0 0 0 * -- --
1310207 4500. 1. 0 0 4560. 1. 0 0 4560. 0 0 0 5400. 0 0 0 * -- --
1310208 5400. 1. 0 0 5460. 1. 0 0 5460. 0 0 0 6300. 0 0 0 * -- --
1310209 6300. 1. 0 0 6360. 1. 0 0 6360. 0 0 0 7200. 0 0 0 * etc. etc.
*
* ctv 190: integral of break mass flow [kg]
20519000 intbreak integral 1. 0 0
20519001 mflowj 131000000
*
1320000 draintnk tmdpvvol
1320101 10. 10. 0 0 0 0 0 0 0 0
1320200 2
1320201 0 1.+5 1.
*
* steam line
19000000 1 5 2 1 .0485
19000100 0 1
19000101 4 .05715
19000201 1 4
    
```



19000301 1.0 4
19000401 480. 5
19000501 900010000 0 1 1 5. 1
19000601 0 0 0 1 5. 1
19000701 0 0 0 0 1
19000801 0 10. 10. 0 0 0 0 1. 1





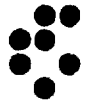
Appendix C

ISP-33 Strip Input Deck and Complete Set of Comparison Plots (post-test results)

Parameters 2- 77: base set of requested parameters

Parameters 78-121: supplementing parameters

Parameters 122-150: parameters calculated but not measured



=isp-33 pactel - requested parameters strip
 100 strip
 103 0

```

*****
*
*                               strip requests                               *
*****
*      alph.code  num.code  calc.id      description
***** main parameters *****
*
*      heat structure temperatures
1002 httemp      104100105  * tca17h_-100 - channel a, rod 17, elev. -100 mm
1003 httemp      106000407  * tca17h_0941 - channel a, rod 17, elev. 941 mm
1004 httemp      106000507  * tca17h_1210 - channel a, rod 17, elev. 1210 mm
1005 httemp      106000607  * tca17h_1479 - channel a, rod 17, elev. 1479 mm
1006 httemp      106000807  * tca17h_2017 - channel a, rod 17, elev. 2017 mm
1007 httemp      104100105  * tca25h_-330 - channel a, rod 25, elev. -330 mm
1008 httemp      106000307  * tca25h_0672 - channel a, rod 25, elev. 672 mm
1009 httemp      106000507  * tca25h_1210 - channel a, rod 25, elev. 1210 mm
1010 httemp      106000707  * tca25h_1748 - channel a, rod 25, elev. 1748 mm
1011 httemp      106000907  * tca25h_2286 - channel a, rod 25, elev. 2286 mm
*      temperatures
1012 tempf      107030000  * tfuph_8340  - upper plenum, elevation 8340 mm
1013 tempf      108030000  * tfuph_11440 - upper plenum, elevation 11440 mm
1014 tempf      301110000  * tfh11h_9600 - hot leg 1, elevation 9600 mm
1015 tempf      351010000  * tfcl1h_9600 - cold leg 1, elevation 9600 mm
1016 tempf      401110000  * tfh12h_9600 - hot leg 2, elevation 9600 mm
1017 tempf      451010000  * tfcl2h_9600 - cold leg 2, elevation 9600 mm
1018 tempf      501110000  * tfh13h_9600 - hot leg 3, elevation 9600 mm
1019 tempf      551010000  * tfcl3h_9600 - cold leg 3, elevation 9600 mm
1020 tempf      325010000  * tfsg1pr26a  - sg 1 prim, tube 26, location a
1021 tempf      325030000  * tfsg1pr26b  - sg 1 prim, tube 26, location b
1022 tempf      325050000  * tfsg1pr26c  - sg 1 prim, tube 26, location c
1023 tempf      601010000  * tfsg1se26b  - sg 1 sec, tube 26, location b
1024 tempf      602010000  * tfsg1se23b  - sg 1 sec, tube 23, location b
1025 tempf      603010000  * tfsg1se11b  - sg 1 sec, tube 11, location b
1026 tempf      425010000  * tfsg2pr26a  - sg 2 prim, tube 26, location a
1027 tempf      425030000  * tfsg2pr26b  - sg 2 prim, tube 26, location b
1028 tempf      425050000  * tfsg2pr26c  - sg 2 prim, tube 26, location c
1029 tempf      701010000  * tfsg2se26b  - sg 2 sec, tube 26, location b
1030 tempf      702010000  * tfsg2se23b  - sg 2 sec, tube 23, location b
1031 tempf      703010000  * tfsg2se11b  - sg 2 sec, tube 11, location b
1032 tempf      525010000  * tfsg3pr26a  - sg 3 prim, tube 26, location a
1033 tempf      525030000  * tfsg3pr26b  - sg 3 prim, tube 26, location b
1034 tempf      525050000  * tfsg3pr26c  - sg 3 prim, tube 26, location c
1035 tempf      801010000  * tfsg3se26b  - sg 3 sec, tube 26, location b
1036 tempf      802010000  * tfsg3se23b  - sg 3 sec, tube 23, location b
1037 tempf      803010000  * tfsg3se11b  - sg 3 sec, tube 11, location b
1038 tempf      102020000  * tfdch_4620  - downcomer, elevation 4620 mm
1039 tempf      103020000  * tf1ph_0070  - lower plenum, elevation 0070 mm
1040 tempf      104010000  * tfcoh_2800  - core/lp, elevation 2800 mm
1041 tempf      107010000  * tfach_6150  - core/up, elevation 6150 mm
*      pressures
1042 p          202100000  * p02pz      - pressure in pressurizer
1043 p          606010000  * p04sg1     - secondary pressure, sg 1
*      differential pressures
1044 cntrlvar    144      * dp18up     - diff. pressure up
1045 cntrlvar    145      * dp17upco   - diff. pressure up-co
1046 cntrlvar    146      * dp19uplp   - diff. pressure up-lp
1047 cntrlvar    147      * dp16co     - diff. pressure core
1048 cntrlvar    148      * dp23dclp  - diff. pressure dc-lp
1049 cntrlvar    149      * dp24pz     - diff. press. pressurizer
    
```



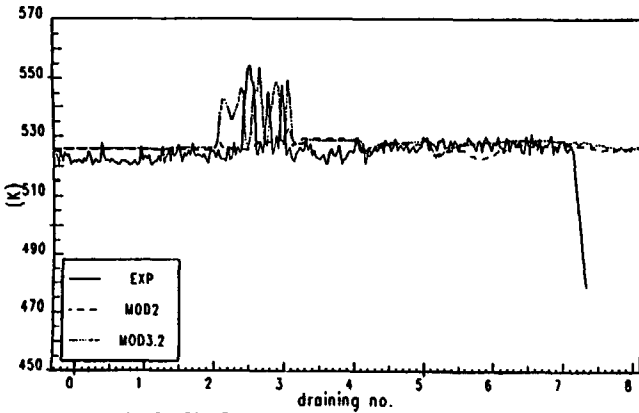
```

1050 cntrlvar      150 * dp28uph11 - dp 1, hot leg 1
1051 cntrlvar      151 * dp25h11   - dp 2, hot leg 1
1052 cntrlvar      152 * dp30h11c11 - dp over sg 1
1053 cntrlvar      153 * dp26c11   - dp 1, cold leg 1
1054 cntrlvar      154 * dp29dcc11 - dp 2, cold leg 1
1055 cntrlvar      155 * dp33uph12 - dp 1, hot leg 2
1056 cntrlvar      156 * dp34h12   - dp 2, hot leg 2
1057 cntrlvar      157 * dp32h12c12 - dp over sg 2
1058 cntrlvar      158 * dp35c12   - dp 1, cold leg 1
1059 cntrlvar      159 * dp36dcc12 - dp 2, cold leg 2
1060 cntrlvar      160 * dp39uph13 - dp 1, hot leg 3
1061 cntrlvar      161 * dp40h13   - dp 2, hot leg 3
1062 cntrlvar      162 * dp38h13c13 - dp over sg 3
1063 cntrlvar      163 * dp41c13   - dp 1, cold leg 1
1064 cntrlvar      164 * dp42dcc13 - dp 2, cold leg 3
* mass flows
1065 mflowj        351010000 * fcl1      - mass flow, cold leg 1
1066 mflowj        451010000 * fcl2      - mass flow, cold leg 2
1067 mflowj        551010000 * fcl3      - mass flow, cold leg 3
1068 mflowj        102010000 * fdc       - mass flow, downcomer
1069 mflowj        131000000 * flp       - outlet mass flow
* heating power
1070 cntrlvar      100 * e_total   - total core power
* levels
1071 cntrlvar      171 * lepr     ??? - primary level, from d19
1072 cntrlvar      172 * lepz     ??? - pressurizer level, from d24
1073 cntrlvar      173 * ledc     ??? - downcomer level, from d23
1074 cntrlvar       74 * leup     ??? - upper plenum level, from d18
1075 cntrlvar      175 * lesg1    ??? - sg 1 secondary level, from d27
1076 cntrlvar      176 * lesg2    ??? - sg 2 secondary level, from d31
1077 cntrlvar      177 * lesg3    ??? - sg 3 secondary level, from d37
*
***** supplementing parameters *****
*
* temperatures
1078 tempf         301070000 * tfh11h_6820 - hot leg 1, elevation 6820 mm
1079 tempf         301010000 * tfh11h_8750 - hot leg 1, elevation 8750 mm
1080 tempf         351140000 * tfcl1h_7350 - cold leg 1, elevation 7350 mm
1081 tempf         351050000 * tfcl1h_6820 - cold leg 1, elevation 6820 mm
1082 tempf         401070000 * tfh12h_6820 - hot leg 2, elevation 6820 mm
1083 tempf         401010000 * tfh12h_8750 - hot leg 2, elevation 8750 mm
1084 tempf         451140000 * tfcl2h_7350 - cold leg 2, elevation 7350 mm
1085 tempf         451050000 * tfcl2h_6820 - cold leg 2, elevation 6820 mm
1086 tempf         501070000 * tfh13h_6820 - hot leg 3, elevation 6820 mm
1087 tempf         501010000 * tfh13h_8750 - hot leg 3, elevation 8750 mm
1088 tempf         551140000 * tfcl3h_7350 - cold leg 3, elevation 7350 mm
1089 tempf         551050000 * tfcl3h_6820 - cold leg 3, elevation 6820 mm
1090 tempf         326010000 * tfsg1pr23a - sg 1 prim, tube 23, location a
1091 tempf         326030000 * tfsg1pr23b - sg 1 prim, tube 23, location b
1092 tempf         326050000 * tfsg1pr23c - sg 1 prim, tube 23, location c
1093 tempf         426010000 * tfsg2pr23a - sg 2 prim, tube 23, location a
1094 tempf         426030000 * tfsg2pr23b - sg 2 prim, tube 23, location b
1095 tempf         426050000 * tfsg2pr23c - sg 2 prim, tube 23, location c
1096 tempf         526010000 * tfsg3pr23a - sg 3 prim, tube 23, location a
1097 tempf         526030000 * tfsg3pr23b - sg 3 prim, tube 23, location b
1098 tempf         526050000 * tfsg3pr23c - sg 3 prim, tube 23, location c
1099 tempf         111010000 * tfdch_7900 - downcomer, elevation 7900 mm
1100 tempf         130010000 * tfdch_1700 - downcomer, elevation 1700 mm
1101 tempf         103030000 * tf1ph_1700 - lower plenum, elevation 1700 mm
1102 tempf         107010000 * tfbch_6150 - core/up, elevation 6150 mm
1103 tempf         107010000 * tfcch_6150 - core/up, elevation 6150 mm
    
```

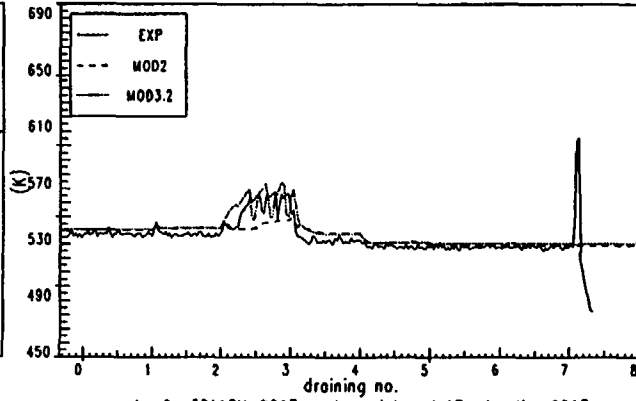


1104	tempf	202050000	* tfpzh_12240	- pressurizer, elevation 12240 mm
1105	tempf	202100000	* tfpzh_16090	- pressurizer, elevation 16090 mm
1106	tempf	651010000	* tfsg1fw	- sg 1 feed water temp
1107	tempf	751010000	* tfsg2fw	- sg 2 feed water temp
1108	tempf	851010000	* tfsg3fw	- sg 3 feed water temp
1109	sattemp	108030000	* sat_temp	- upper plenum sat temp
* pressures				
1110	p	108030000	* p01up	- pressure in upper plenum
1111	p	706010000	* p05sg2	- secondary pressure, sg 2
1112	p	806010000	* p06sg3	- secondary pressure, sg 3
* differential pressures				
1113	cntrlvar	165	* dp27sg1s	- sg 1, secondary dp
1114	cntrlvar	166	* dp31sg2s	- sg 2, secondary dp
1115	cntrlvar	167	* dp37sg3s	- sg 3, secondary dp
* mass flows				
1116	mflowj	652000000	* fih01	- sg 1 feed water mass flow
1117	mflowj	752000000	* fih02	- sg 2 feed water mass flow
1118	mflowj	852000000	* fih03	- sg 3 feed water mass flow
* heating power				
1119	cntrlvar	104	* eac	- core power, channel a
1120	cntrlvar	104	* ebc	- core power, channel b
1121	cntrlvar	104	* ecc	- core power, channel c
* ***** parameters calculated but not measured ***** *				
* coolant mass				
1122	cntrlvar	122	* primas	- primary mass
1123	cntrlvar	111	* vessmass	- vessel mass
1124	cntrlvar	112	* przmass	- pressurizer mass
1125	cntrlvar	113	* hot11mass	- hot leg 1 mass
1126	cntrlvar	114	* hot12mass	- hot leg 2 mass
1127	cntrlvar	115	* hot13mass	- hot leg 3 mass
1128	cntrlvar	116	* sgtubelmass	- sg 1 tube mass
1129	cntrlvar	117	* sgtube2mass	- sg 2 tube mass
1130	cntrlvar	118	* sgtube3mass	- sg 3 tube mass
1131	cntrlvar	119	* cold11mass	- cold leg 1 mass
1132	cntrlvar	120	* cold12mass	- cold leg 2 mass
1133	cntrlvar	121	* cold13mass	- cold leg 3 mass
1134	cntrlvar	131	* sgsec1mass	- sg 1 mass
1135	cntrlvar	132	* sgsec2mass	- sg 2 mass
1136	cntrlvar	133	* sgsec3mass	- sg 3 mass
* heat fluxes				
1137	cntrlvar	102	* corehflux	- heat from core
1138	cntrlvar	304	* sgen1hflux	- sg 1 heat flux
1139	cntrlvar	305	* sgen2hflux	- sg 2 heat flux
1140	cntrlvar	306	* sgen3hflux	- sg 3 heat flux
* heat losses				
1141	cntrlvar	916	* vesshloss	- vessel heat loss
1142	cntrlvar	917	* loop1hloss	- loop 1 heat loss
1143	cntrlvar	918	* loop2hloss	- loop 2 heat loss
1144	cntrlvar	919	* loop3hloss	- loop 3 heat loss
1145	cntrlvar	920	* przhloss	- pressurizer heat loss
1146	cntrlvar	907	* sec1hloss	- sg 1 sec. heat loss
1147	cntrlvar	910	* sec3hloss	- sg 2 sec. heat loss
1148	cntrlvar	913	* sec2hloss	- sg 3 sec. heat loss
* mass flow				
1149	mflowj	904000000	* steamout	- steam flow out
* level				
1150	cntrlvar	78	* corelevel	- core level ????

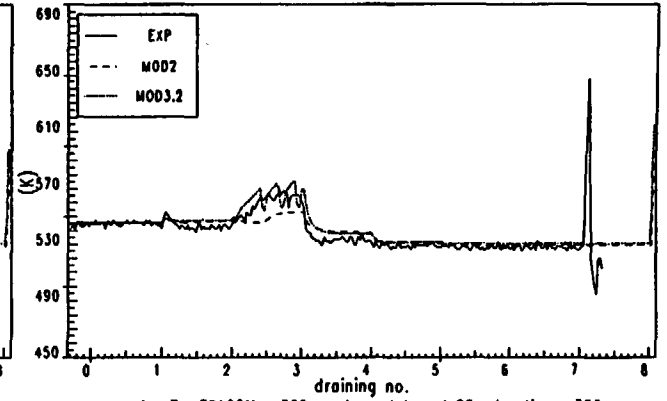
parameter 2 : TCA17H_-100 - channel A, rod 17, elevation -100 mm



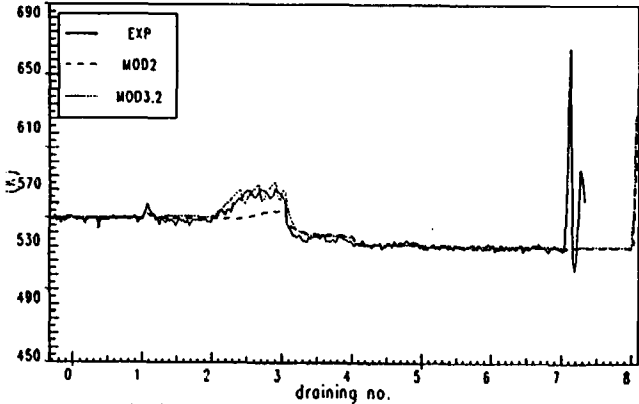
parameter 3 : TCA17H_0941 - channel A, rod 17, elevation 941 mm



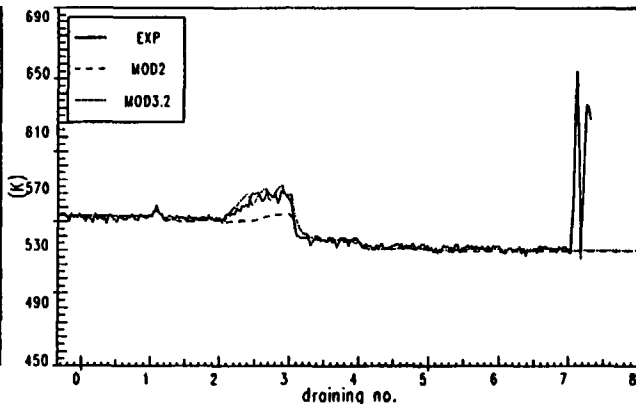
parameter 4 : TCA17H_1210 - channel A, rod 17, elevation 1210 mm



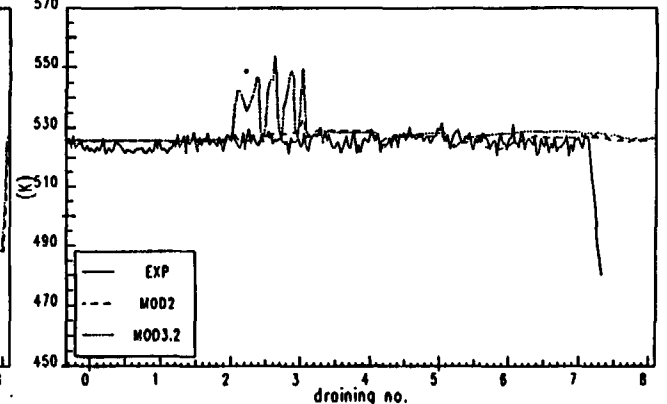
parameter 5 : TCA17H_1479 - channel A, rod 17, elevation 1479 mm



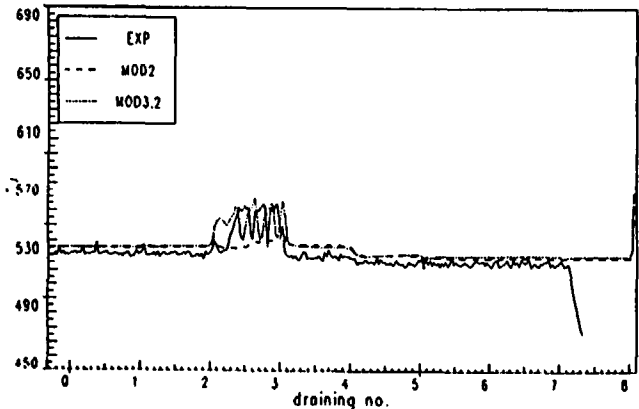
parameter 6 : TCA17H_2017 - channel A, rod 17, elevation 2017 mm



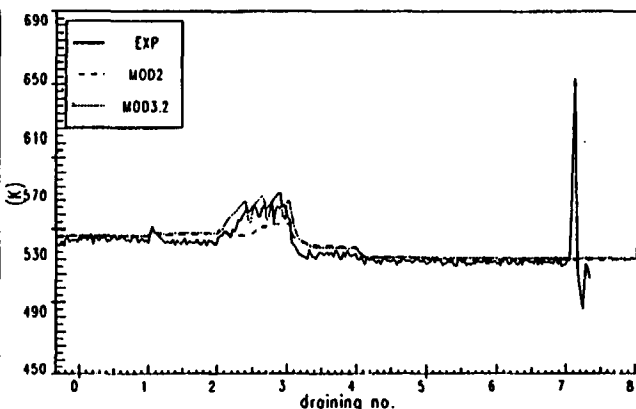
parameter 7 : TCA25H_-330 - channel A, rod 25, elevation -330 mm



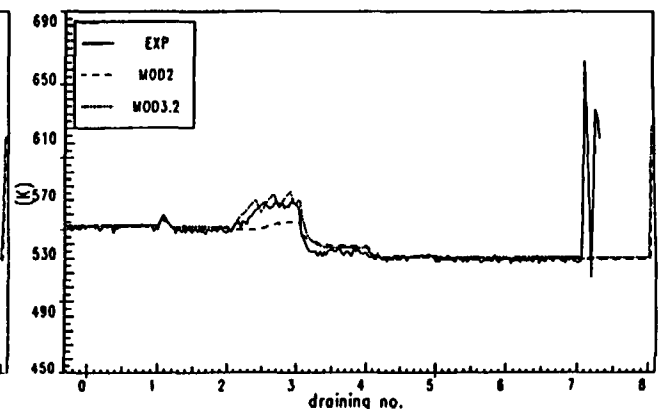
parameter 8 : TCA25H_0672 - channel A, rod 25, elevation 672 mm



parameter 9 : TCA25H_1210 - channel A, rod 25, elevation 1210 mm

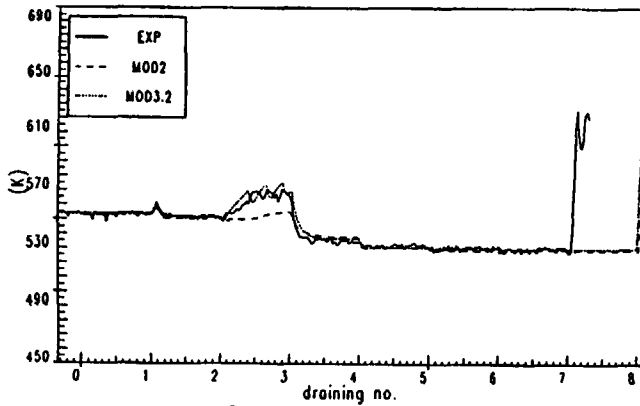


parameter 10 : TCA25H_1748 - channel A, rod 25, elevation 1748 mm

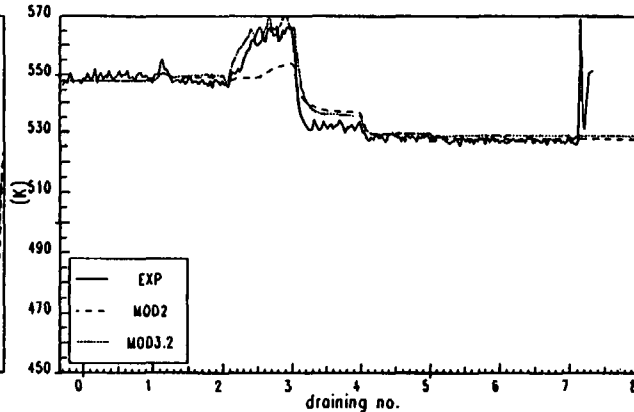


C-4

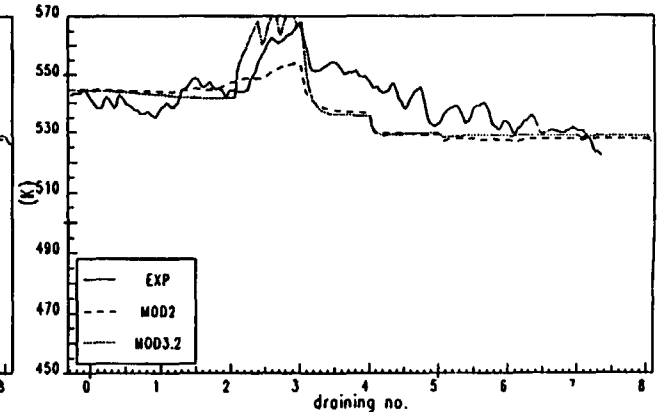
parameter 11 : TCA25H_2286 - channel A, rod 25, elevation 2286 mm



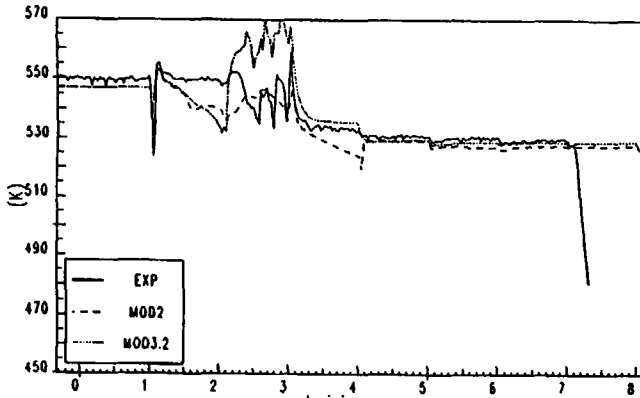
parameter 12 : TFUPH_8340 - upper plenum, elevation 8340 mm



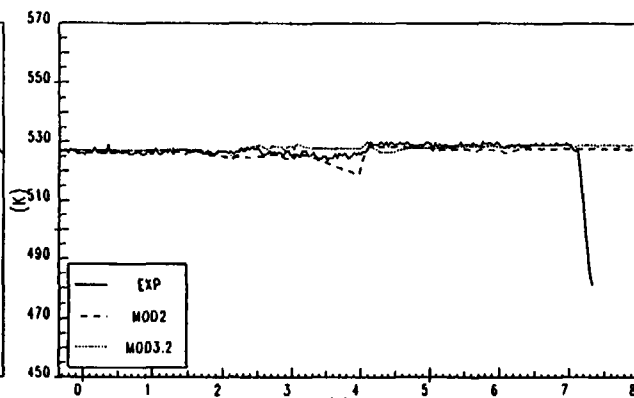
parameter 13 : TFUPH_11440 - upper plenum, elevation 11440 mm



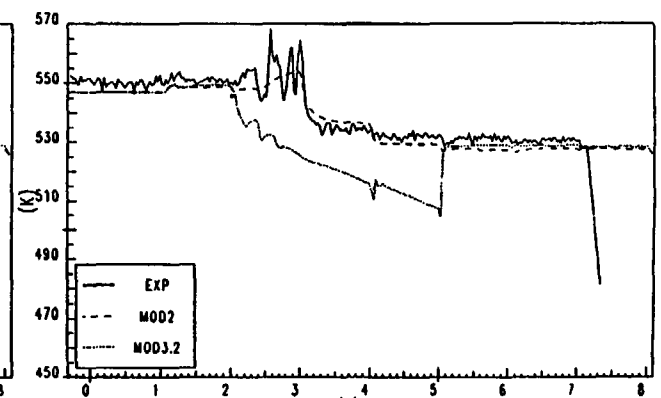
parameter 14 : TFHL1H_9600 - hot leg 1, elevation 9600 mm



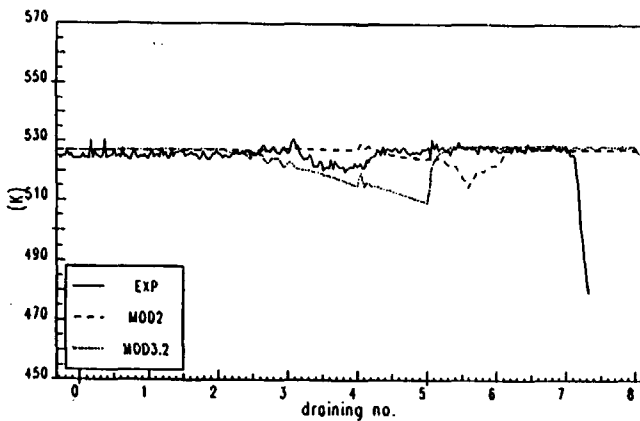
parameter 15 : TFCL1H_9600 - cold leg 1, elevation 9600 mm



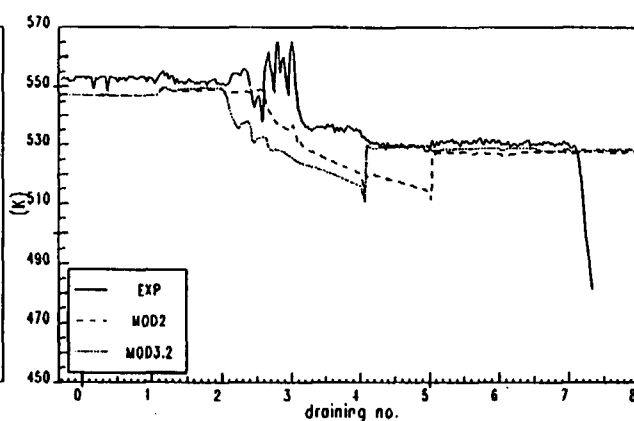
parameter 16 : TFHL2H_9600 - hot leg 2, elevation 9600 mm



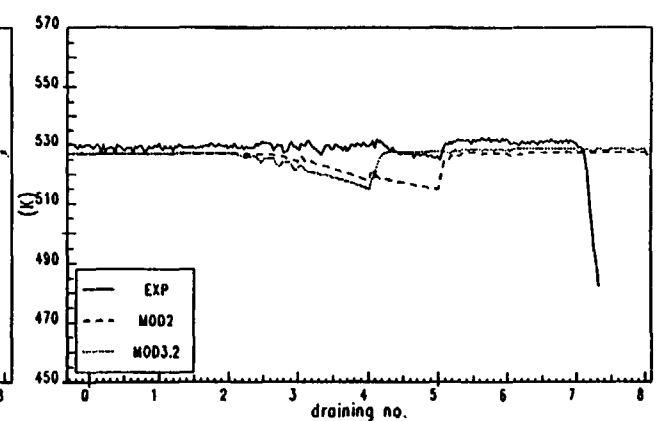
parameter 17 : TFCL2H_9600 - cold leg 2, elevation 9600 mm



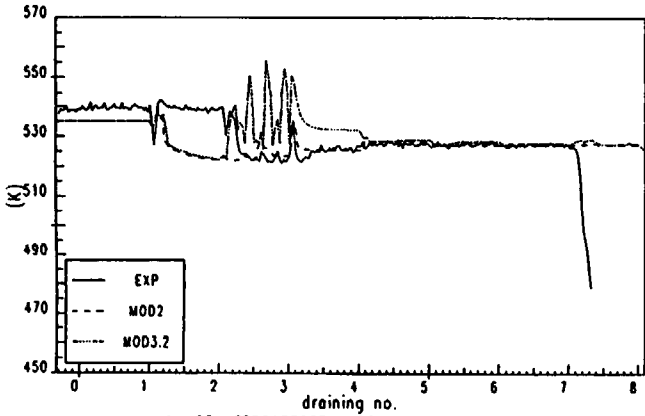
parameter 18 : TFHL3H_9600 - hot leg 3, elevation 9600 mm



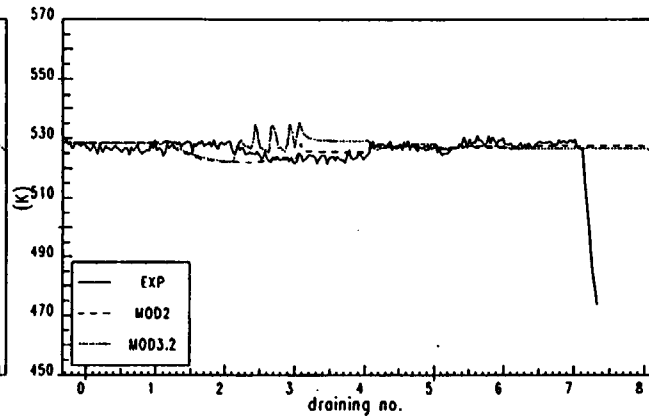
parameter 19 : TFCL3H_9600 - cold leg 3, elevation 9600 mm



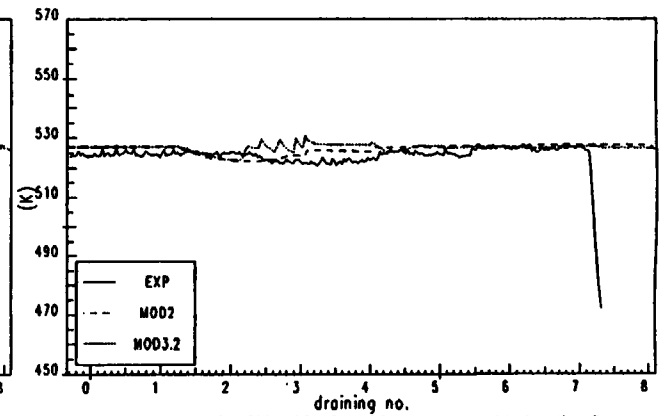
parameter 20 : TFSG1PR26A - SG 1 prim, tube 26, location A



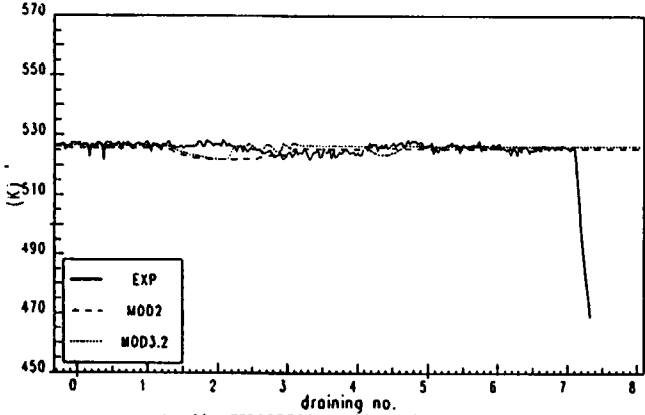
parameter 21 : TFSG1PR26B - SG 1 prim, tube 26, location B



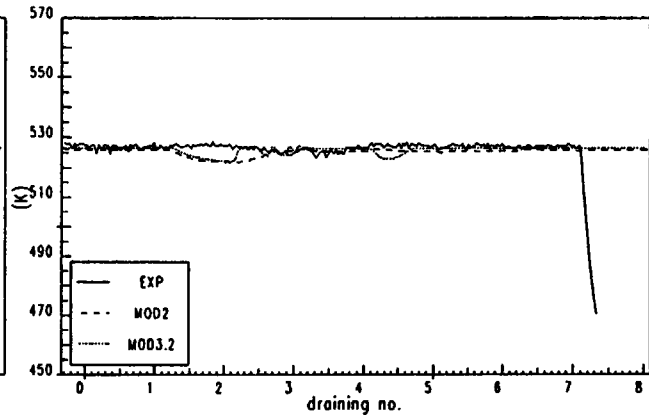
parameter 22 : TFSG1PR26C - SG 1 prim, tube 26, location C



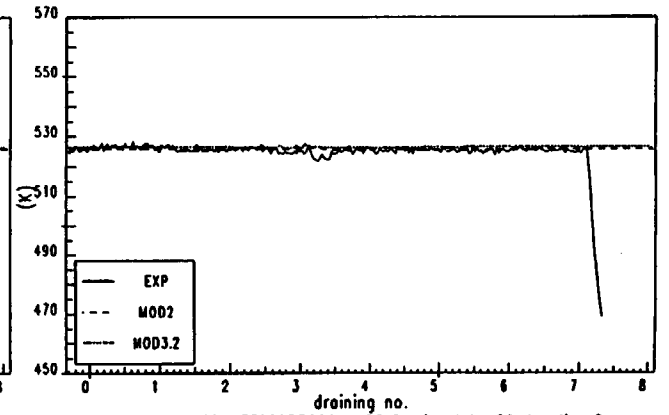
parameter 23 : TFSG1SE26B - SG 1 sec, tube 26, location B



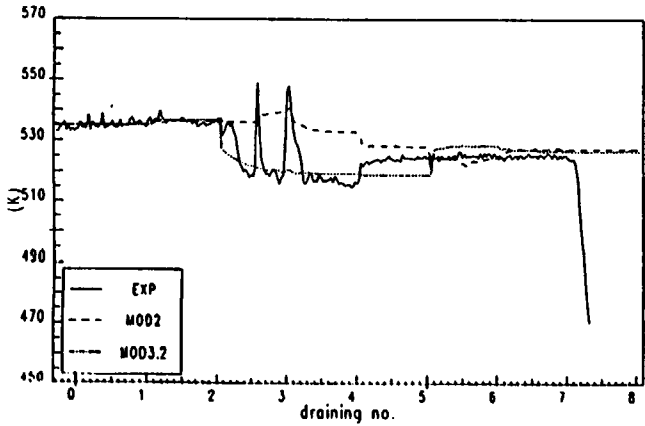
parameter 24 : TFSG1SE23B - SG 1 sec, tube 23, location B



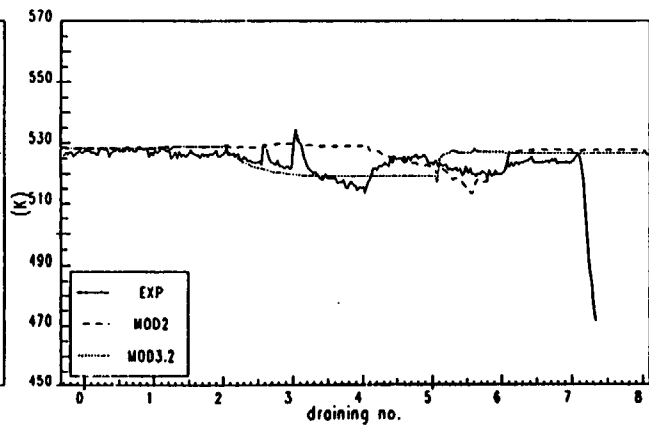
parameter 25 : TFSG1SE11B - SG 1 sec, tube 11, location B



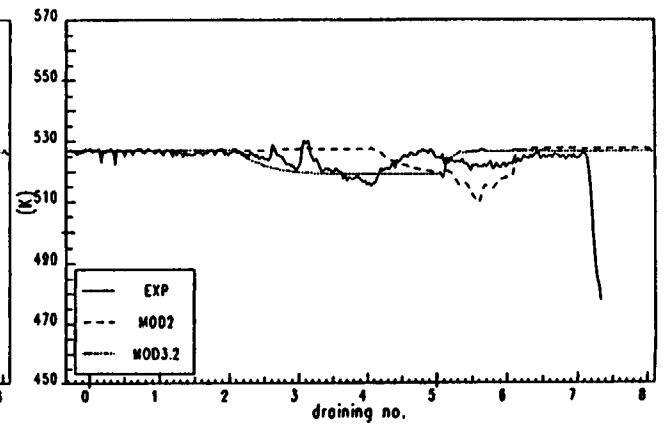
parameter 26 : TFSG2PR26A - SG 2 prim, tube 26, location A



parameter 27 : TFSG2PR26B - SG 2 prim, tube 26, location B

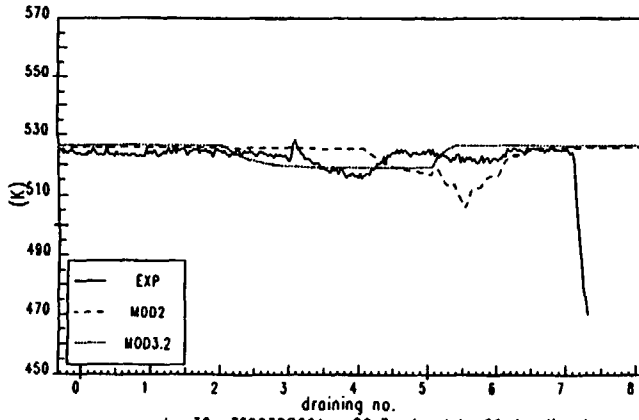


parameter 28 : TFSG2PR26C - SG 2 prim, tube 26, location C

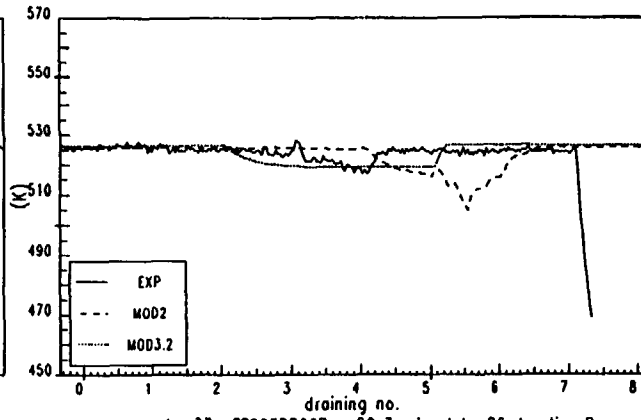


C-6

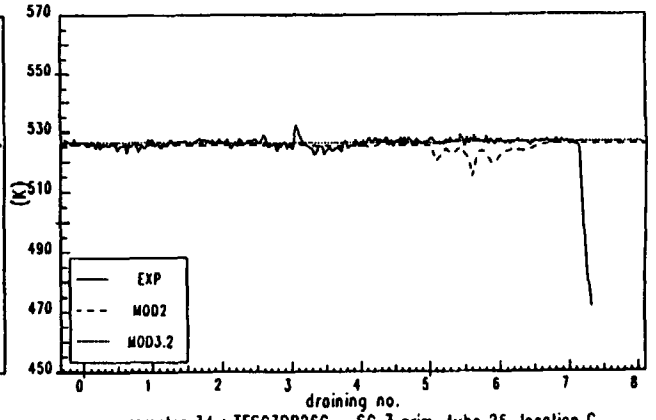
parameter 29 : TFSG2SE26B - SG 2 sec, tube 26, location B



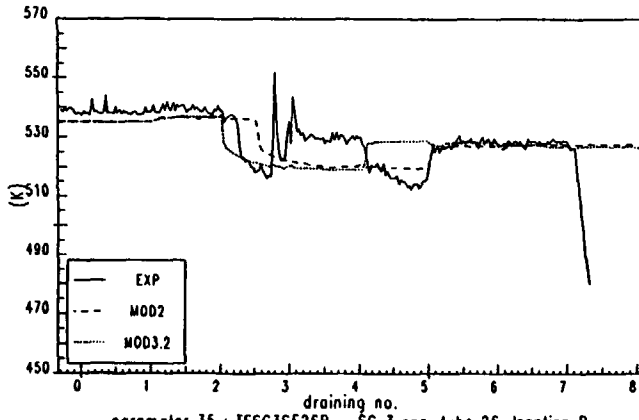
parameter 30 : TFSG2SE23B - SG 2 sec, tube 23, location B



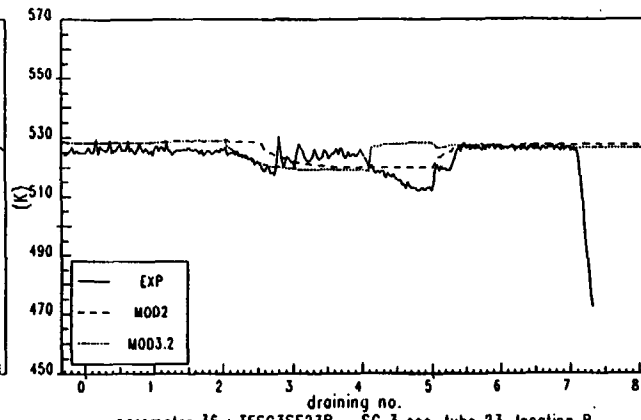
parameter 31 : TFSG2SE11B - SG 2 sec, tube 11, location B



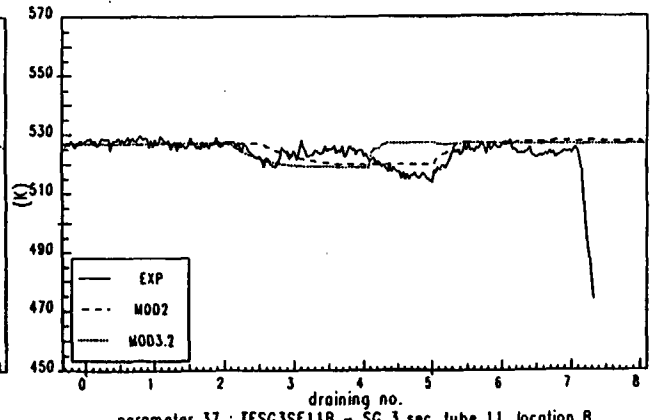
parameter 32 : TFSG3PR26A - SG 3 prim, tube 26, location A



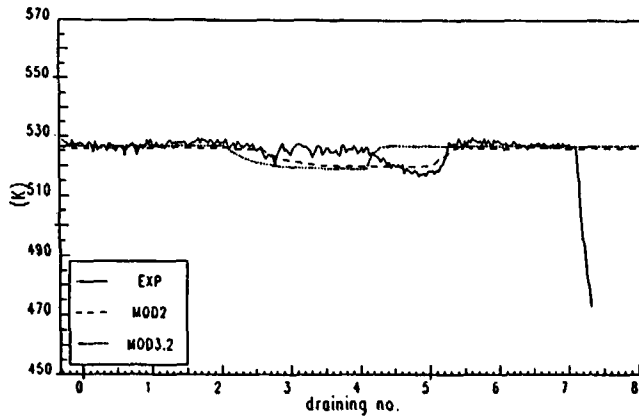
parameter 33 : TFSG3PR26B - SG 3 prim, tube 26, location B



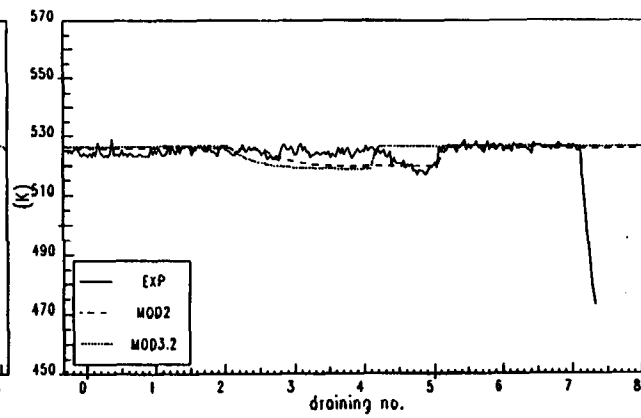
parameter 34 : TFSG3PR26C - SG 3 prim, tube 26, location C



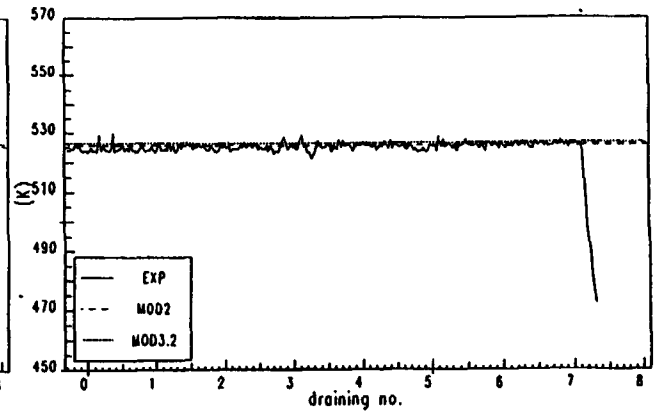
parameter 35 : TFSG3SE26B - SG 3 sec, tube 26, location B



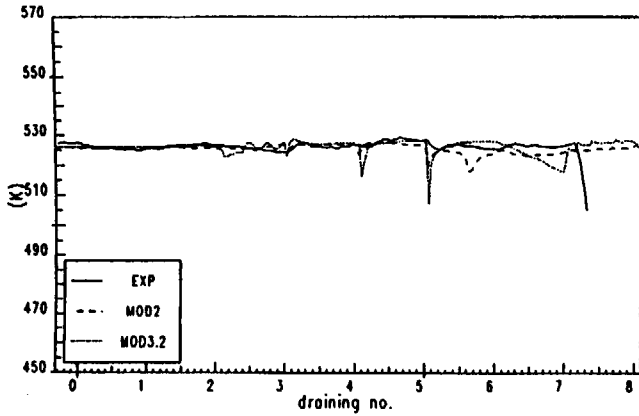
parameter 36 : TFSG3SE23B - SG 3 sec, tube 23, location B



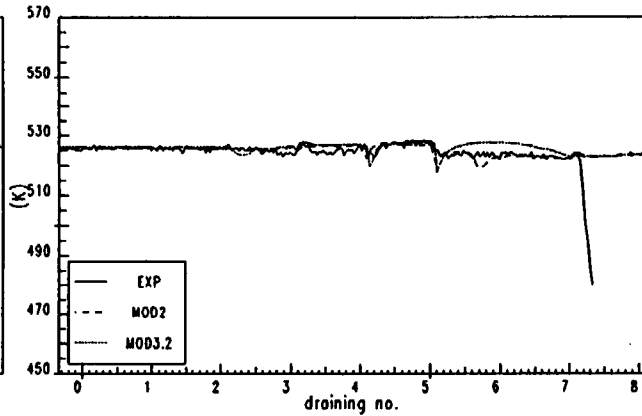
parameter 37 : TFSG3SE11B - SG 3 sec, tube 11, location B



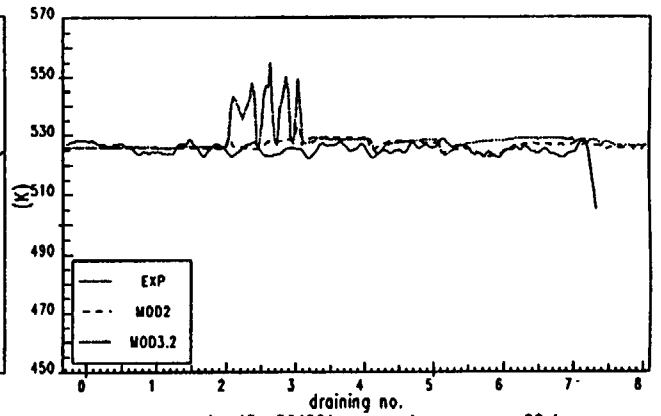
parameter 38 : TFDCH_4620 - downcomer, elevation 4620 mm



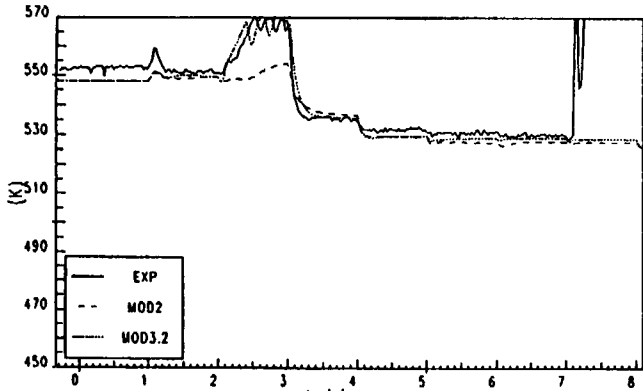
parameter 39 : TFLPH_0070 - lower plenum, elevation 0070 mm



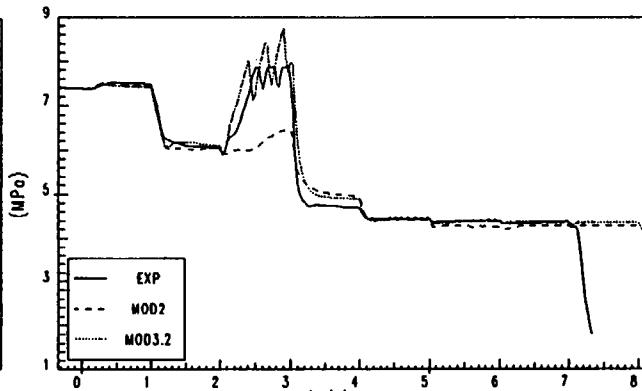
parameter 40 : TFCOH_2800 - core/lower plenum, elevation 2800 mm



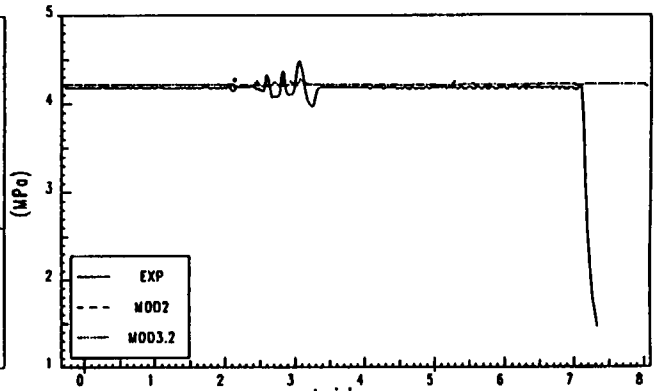
parameter 41 : TFACH_6150 - core/upper plenum, elevation 6150 mm



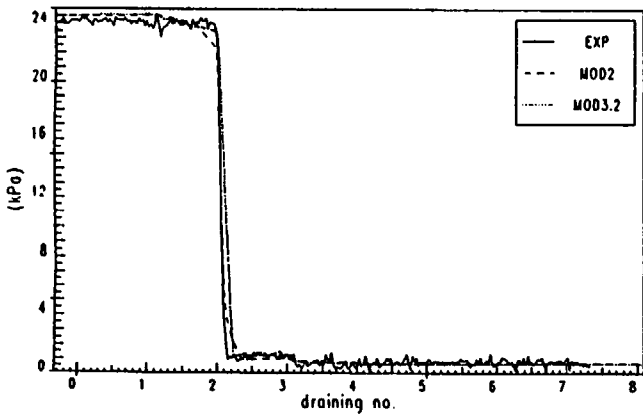
parameter 42 : P02PZ - pressurizer pressure



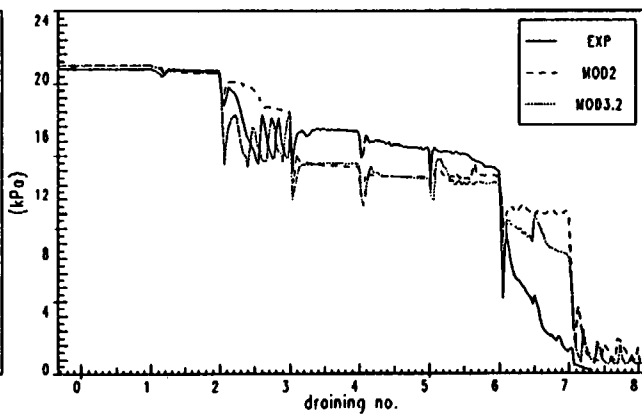
parameter 43 : P04SG1 - secondary pressure, SG 1



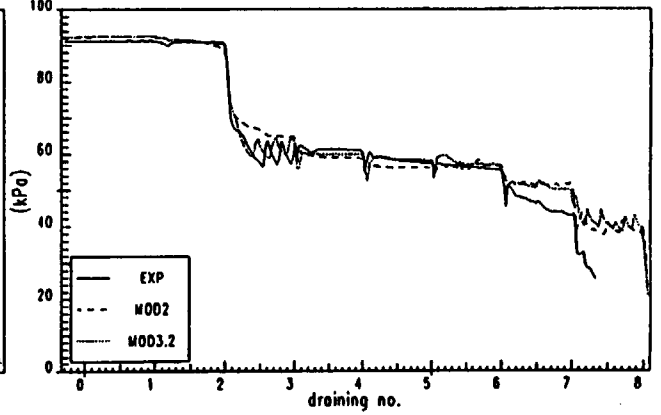
parameter 44 : DP18UP - DP upper plenum



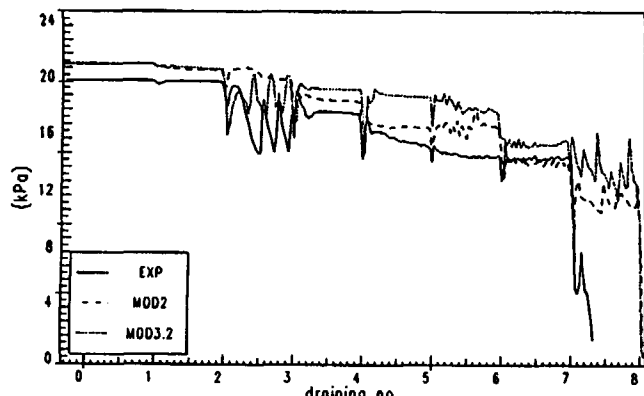
parameter 45 : DP17UPCO - DP upper plenum-core



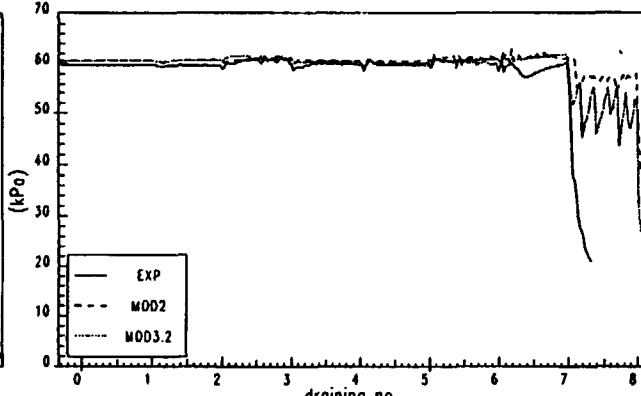
parameter 46 : DP19UPLP - DP upper plenum-lower plenum



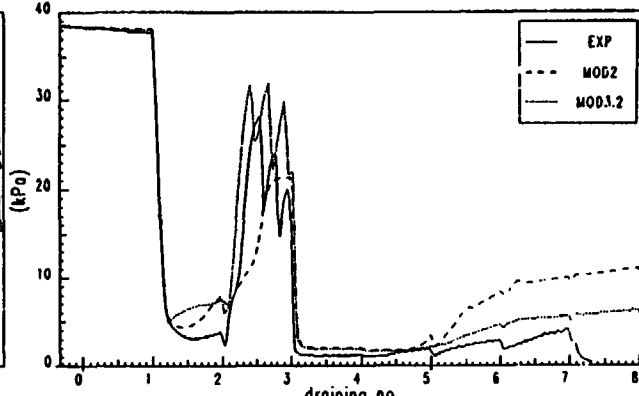
parameter 47 : DP16CO - DP core



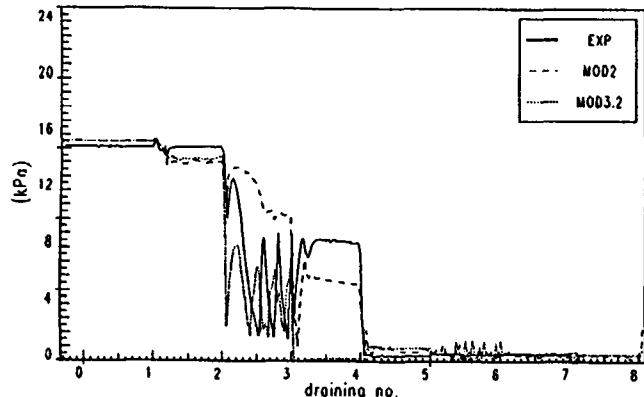
parameter 48 : DP230CLP - DP downcomer-lower plenum



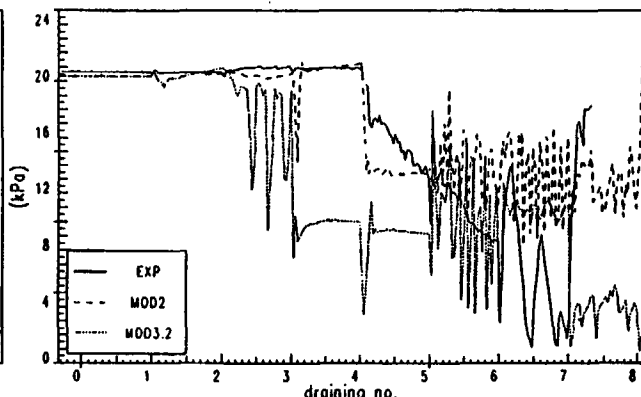
parameter 49 : DP24PZ - DP pressurizer



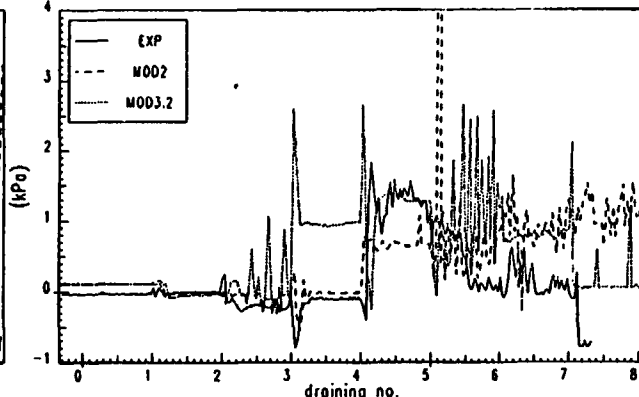
parameter 50 : DP28UPHL1 - DP 1, hot leg 1



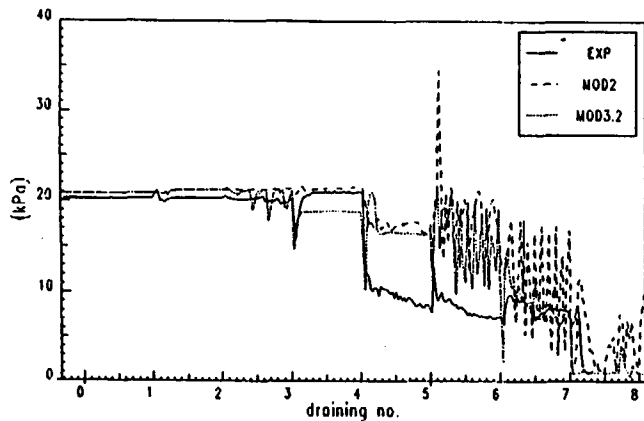
parameter 51 : DP25HL1 - DP 2, hot leg 1



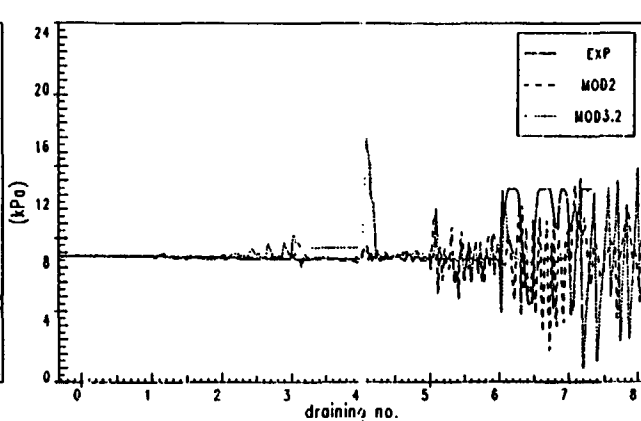
parameter 52 : DP30HL1CL1 - DP over SG 1



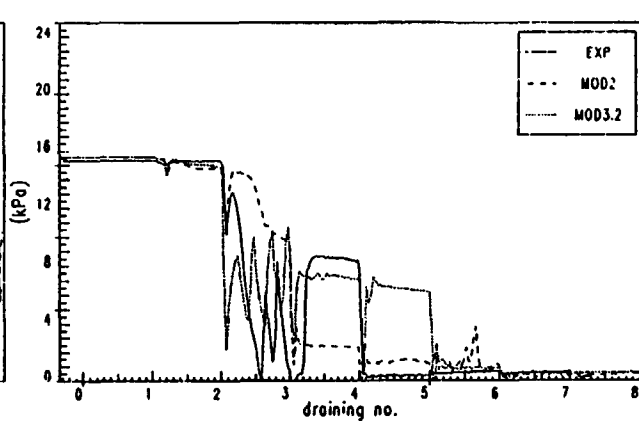
parameter 53 : DP26CL1 - DP 1, cold leg 1



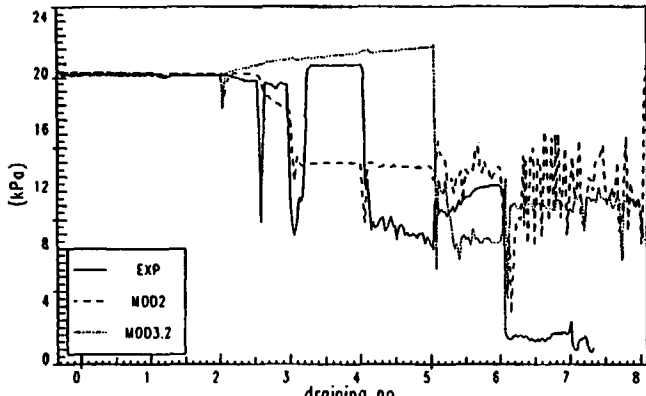
parameter 54 : DP29DCCL1 - DP 2, cold leg 1



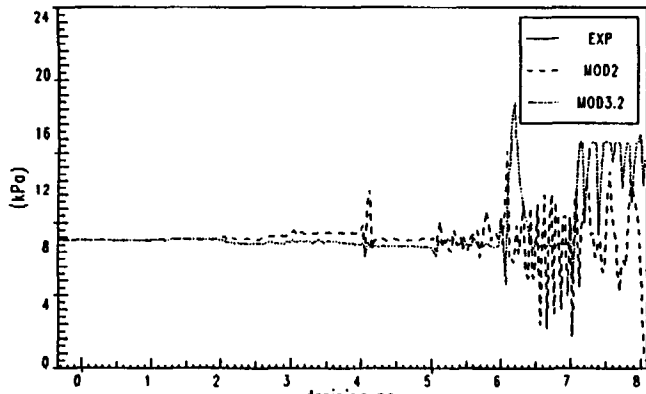
parameter 55 : DP33UPHL2 - DP 1, hot leg 2



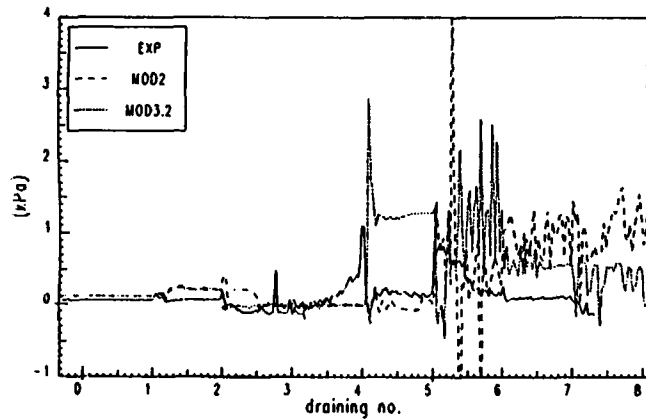
parameter 56 : DP34HL2 - DP 2, hot leg 2



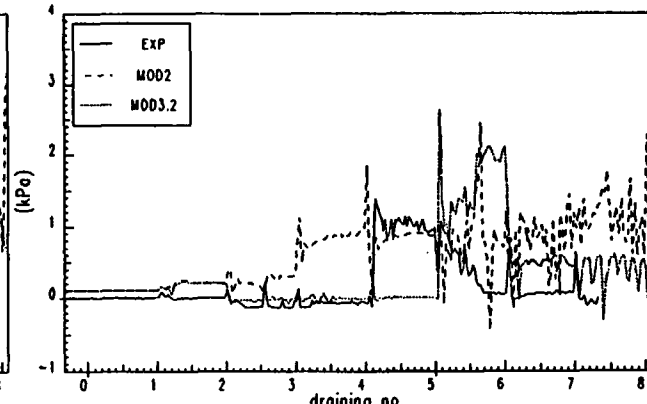
parameter 59 : DP36DCCL2 - DP 2, cold leg 2



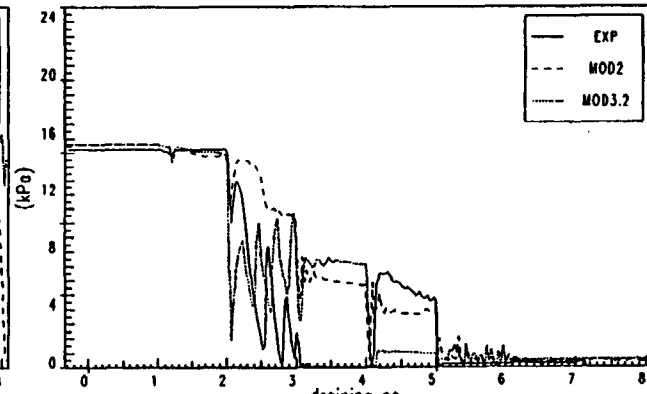
parameter 62 : DP38HL3CL3 - DP over SG 3



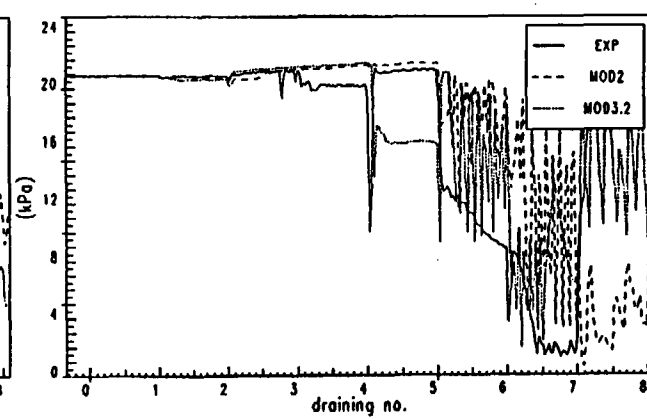
parameter 57 : DP32HL2CL2 - DP over SG 2



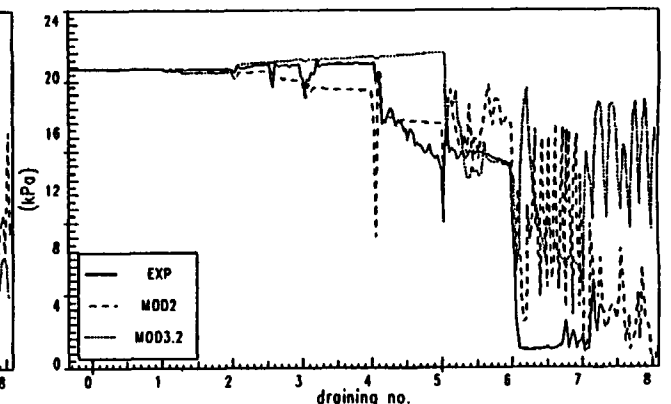
parameter 60 : DP39UPLH3 - DP 1, hot leg 3



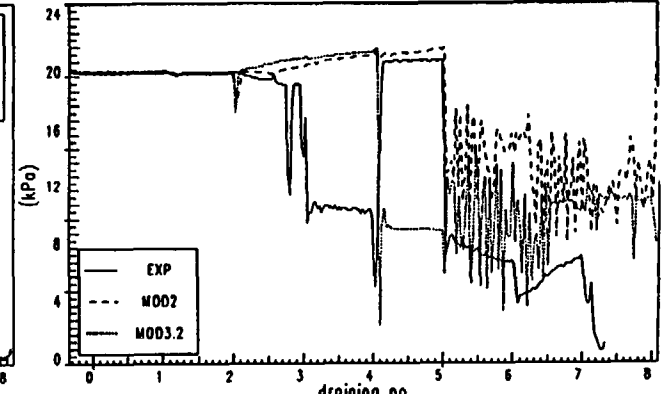
parameter 63 : DP41CL3 - DP 1, cold leg 3



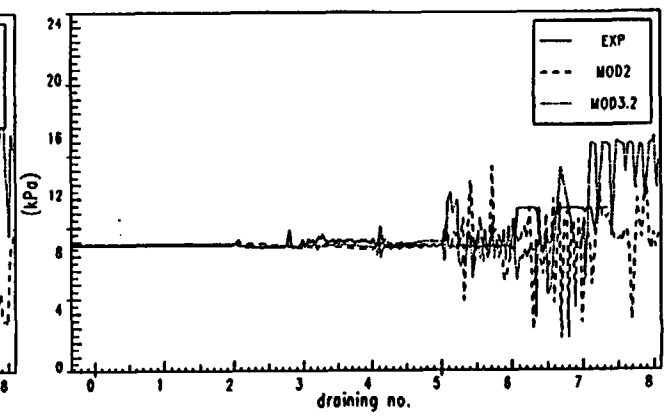
parameter 58 : DP35CL2 - DP 1, cold leg 2



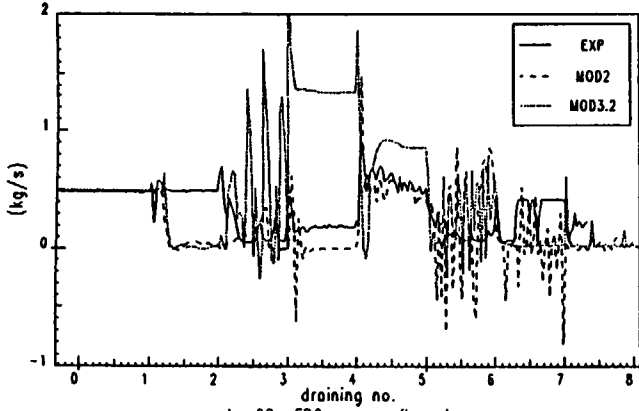
parameter 61 : DP40HL3 - DP 2, hot leg 3



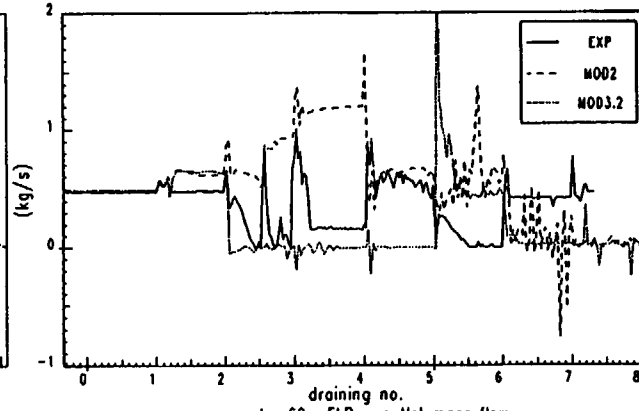
parameter 64 : DP42DCCL3 - DP 2, cold leg 3



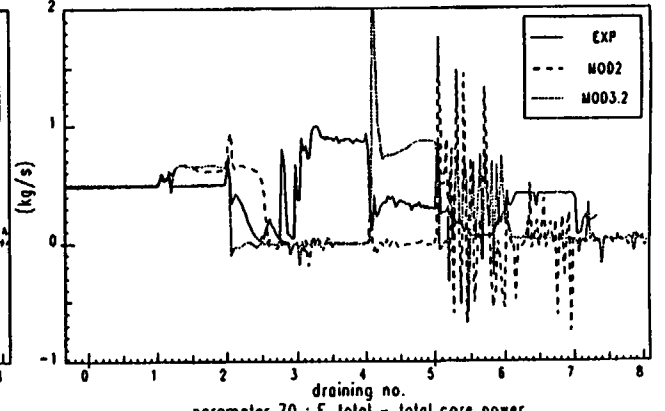
parameter 65 : FCL1 - mass flow, cold leg 1



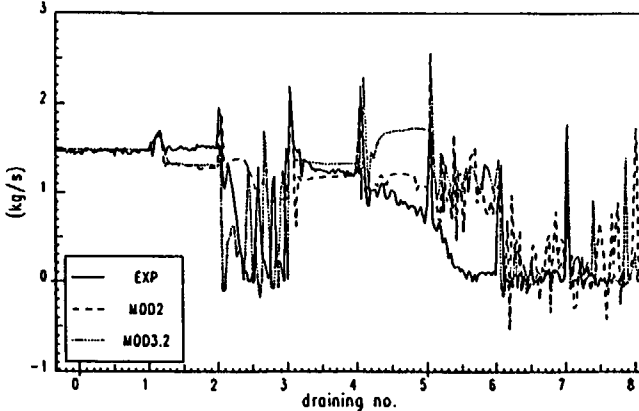
parameter 66 : FCL2 - mass flow, cold leg 2



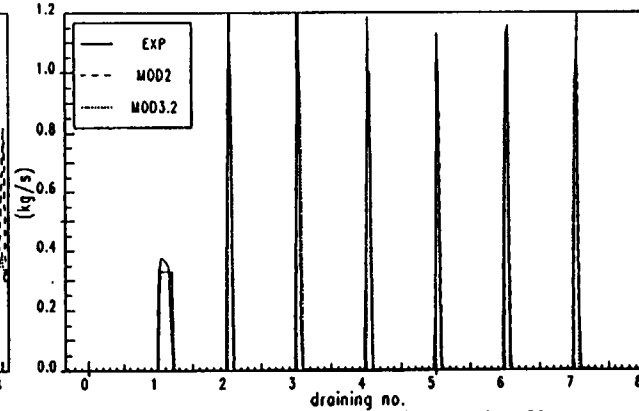
parameter 67 : FCL3 - mass flow, cold leg 3



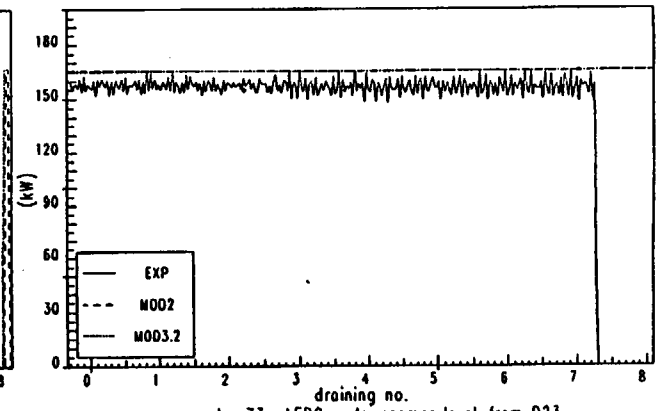
parameter 68 : FDC - mass flow, downcomer



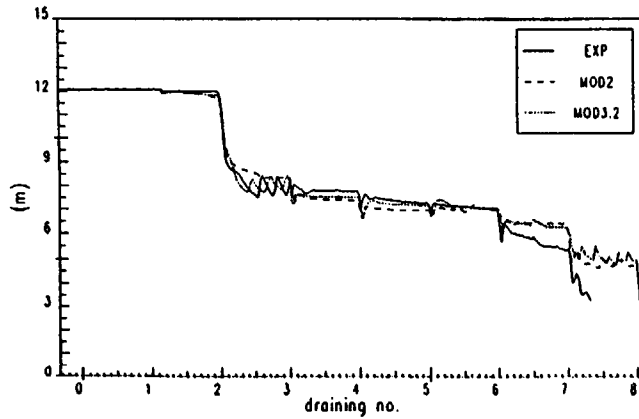
parameter 69 : FLP - outlet mass flow



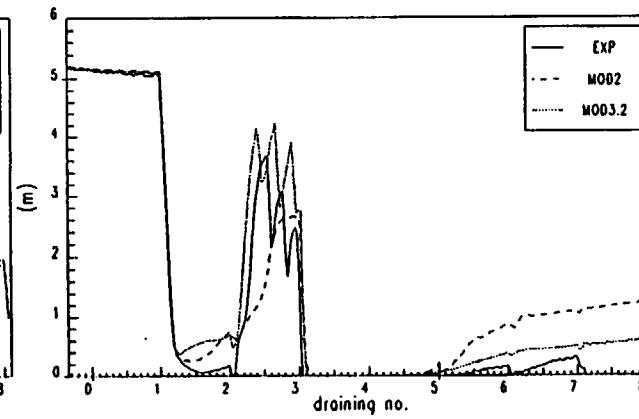
parameter 70 : E_total - total core power



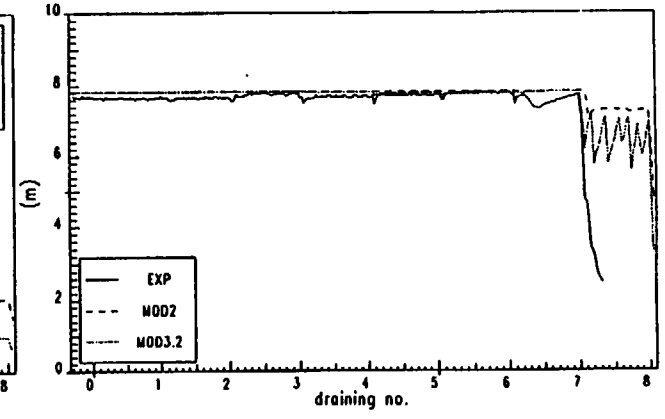
parameter 71 : LEPR - primary level, from D19



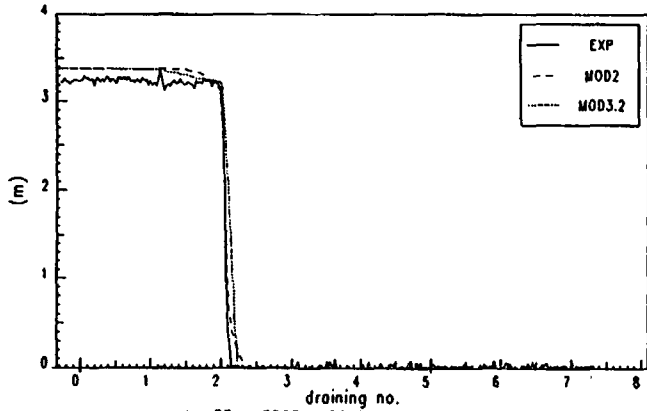
parameter 72 : LEPR - pressurizer level, from D24



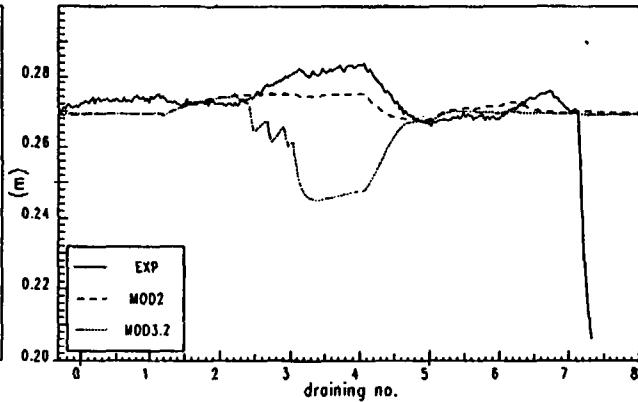
parameter 73 : LEDC - downcomer level, from D23



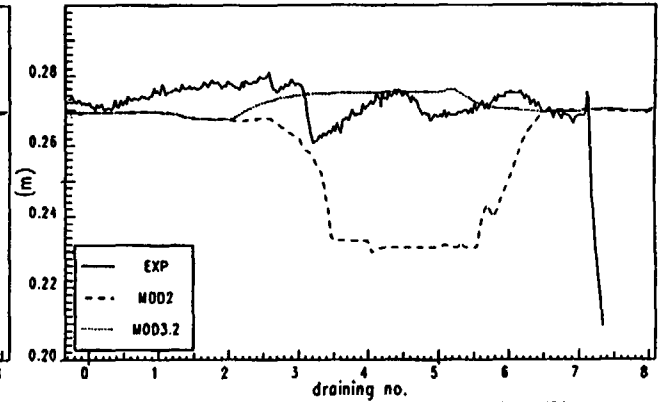
parameter 74 : LEUP - upper plenum level, from D18



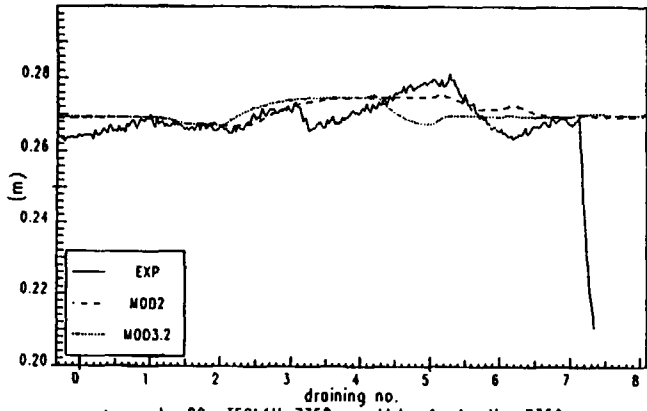
parameter 75 : LESG1 - SG 1 secondary level, from D27



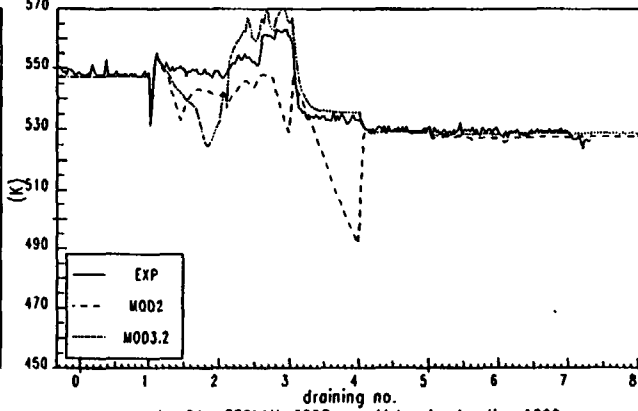
parameter 76 : LESG2 - SG 2 secondary level, from D31



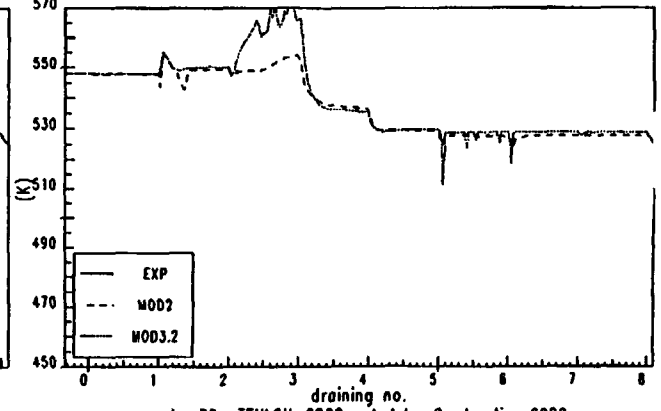
parameter 77 : LESG3 - SG 3 secondary level, from D37



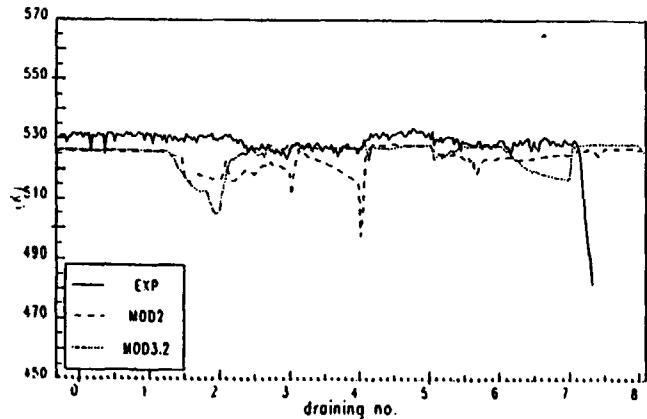
parameter 78 : TFHL1H_6820 - hot leg 1, elevation 6820 mm



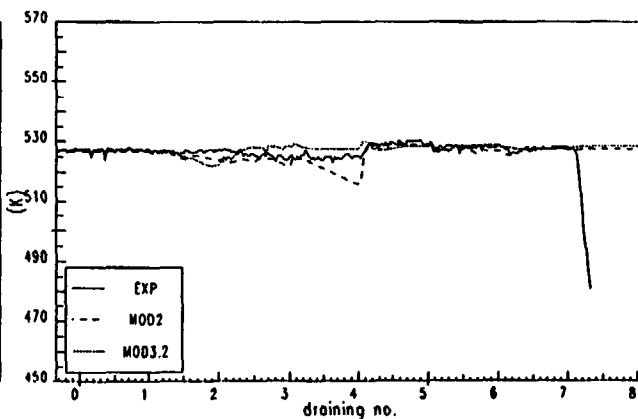
parameter 79 : TFHL1H_8750 - hot leg 1, elevation 8750 mm



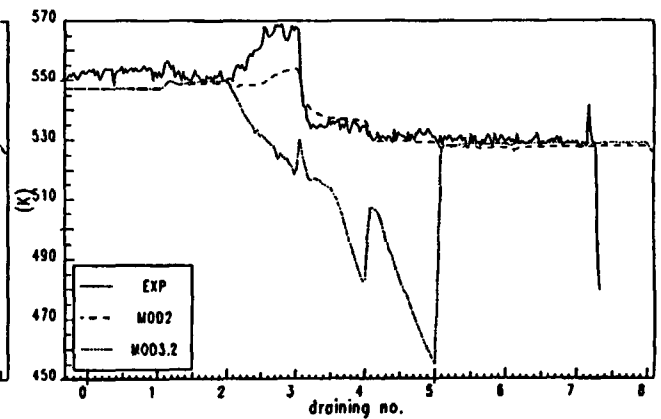
parameter 80 : TFCL1H_7350 - cold leg 1, elevation 7350 mm



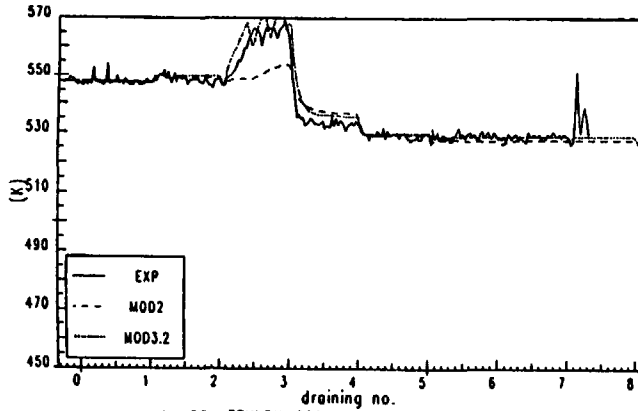
parameter 81 : TFCL1H_6820 - cold leg 1, elevation 6820 mm



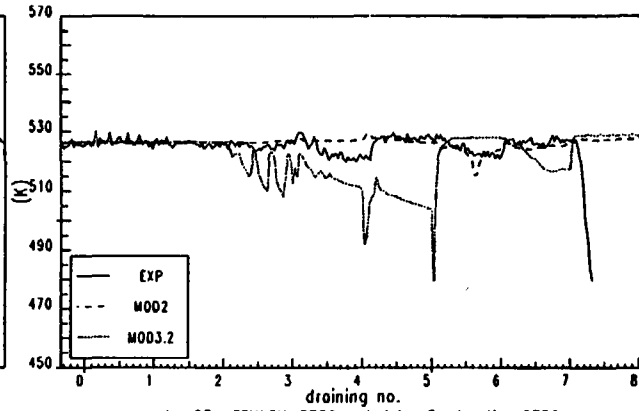
parameter 82 : TFHL2H_6820 - hot leg 2, elevation 6820 mm



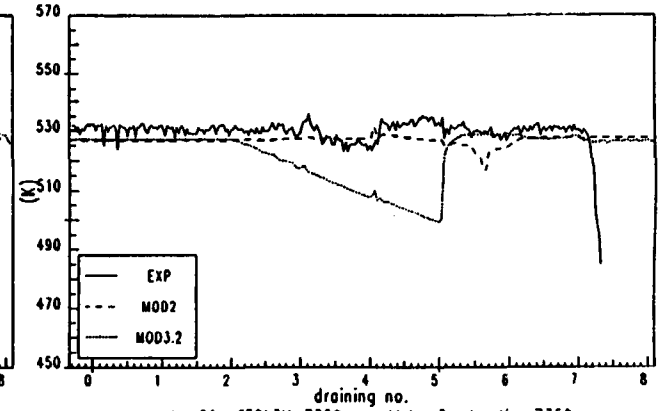
parameter 83 : TFHL2H_8750 - hot leg 2, elevation 8750 mm



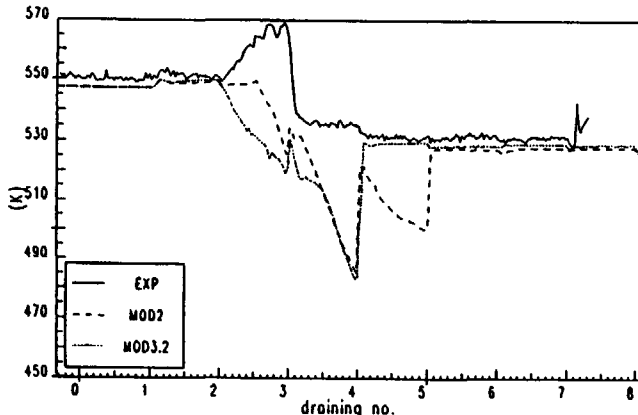
parameter 84 : TFCL2H_7350 - cold leg 2, elevation 7350 mm



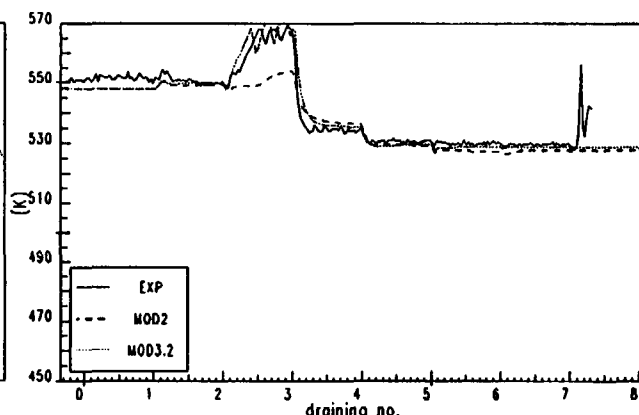
parameter 85 : TFCL2H_6820 - cold leg 2, elevation 6820 mm



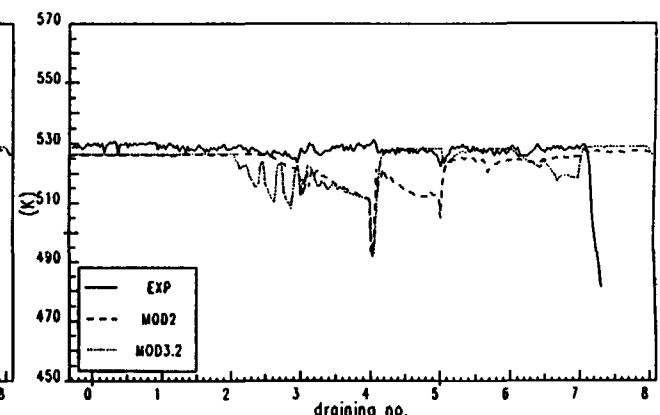
parameter 86 : TFHL3H_6820 - hot leg 3, elevation 6820 mm



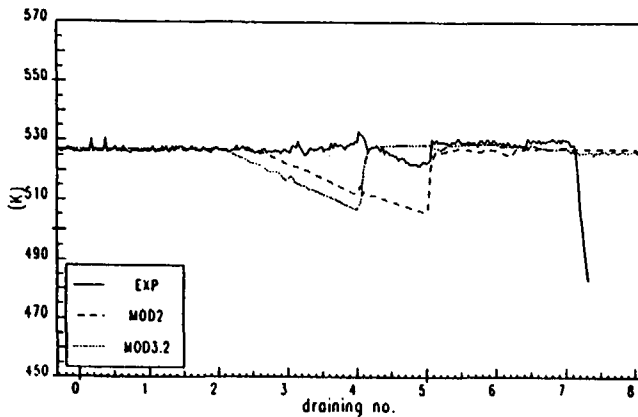
parameter 87 : TFHL3H_8750 - hot leg 3, elevation 8750 mm



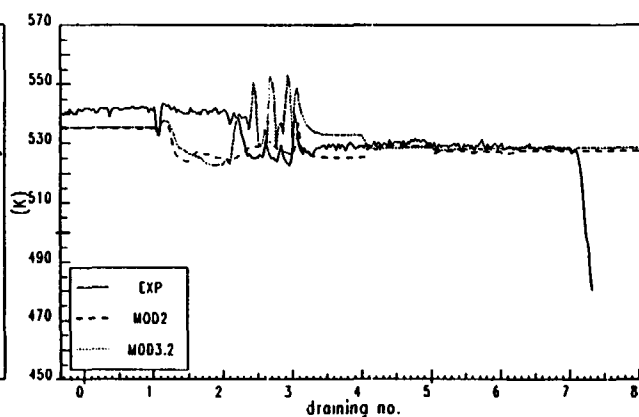
parameter 88 : TFCL3H_7350 - cold leg 3, elevation 7350 mm



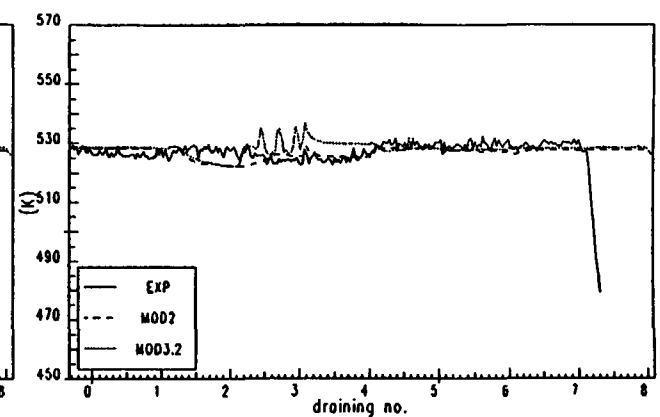
parameter 89 : TFCL3H_6820 - cold leg 3, elevation 6820 mm



parameter 90 : TFSG1PR23A - SG 1 prim, tube 23, location A

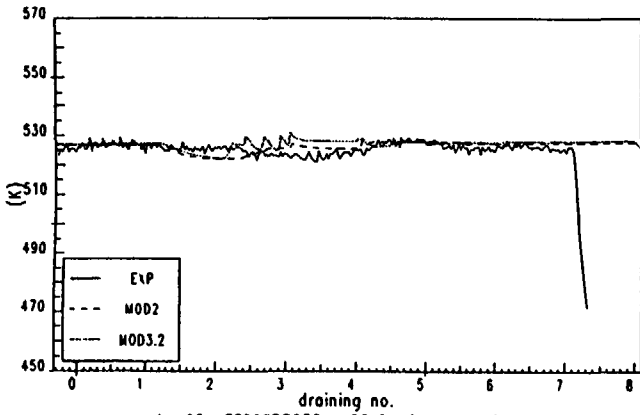


parameter 91 : TFSG1PR23B - SG 1 prim, tube 23, location B

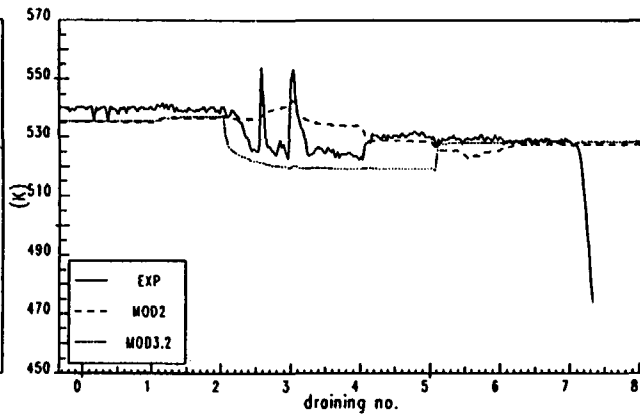


C-13

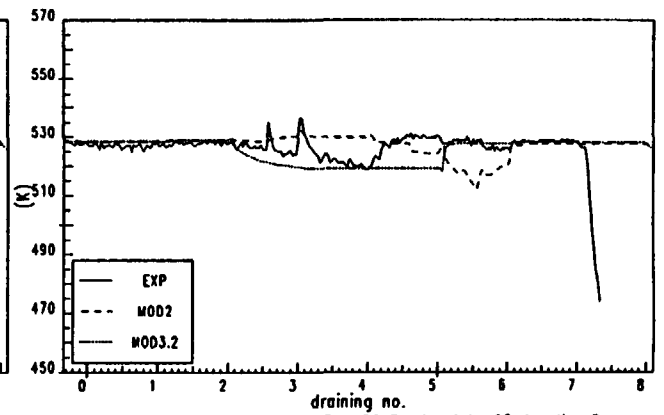
parameter 92 : TFSG1PR23C - SG 1 prim, tube 23, location C



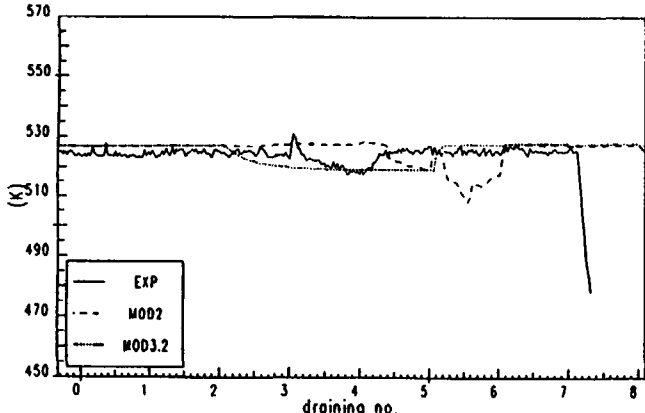
parameter 93 : TFSG2PR23A - SG 2 prim, tube 23, location A



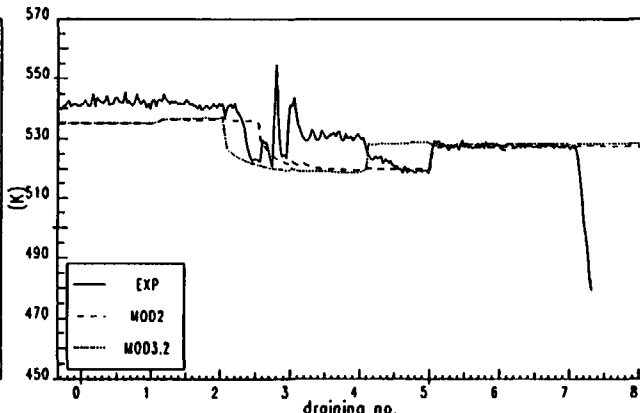
parameter 94 : TFSG2PR23B - SG 2 prim, tube 23, location B



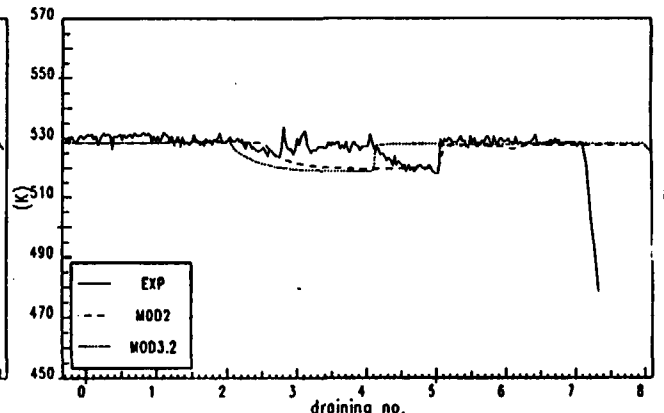
parameter 95 : TFSG2PR23C - SG 2 prim, tube 23, location C



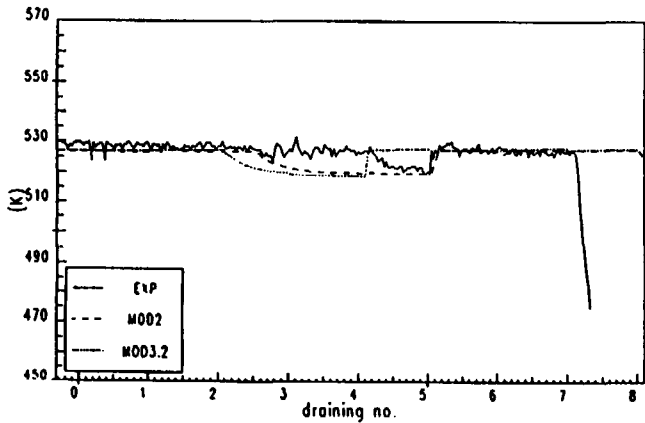
parameter 96 : TFSG3PR23A - SG 3 prim, tube 23, location A



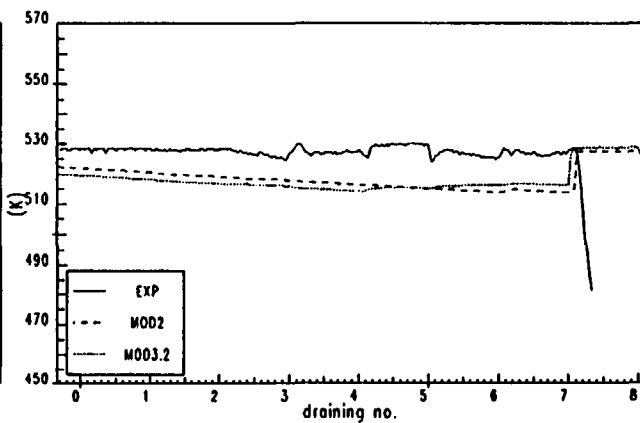
parameter 97 : TFSG3PR23B - SG 3 prim, tube 23, location B



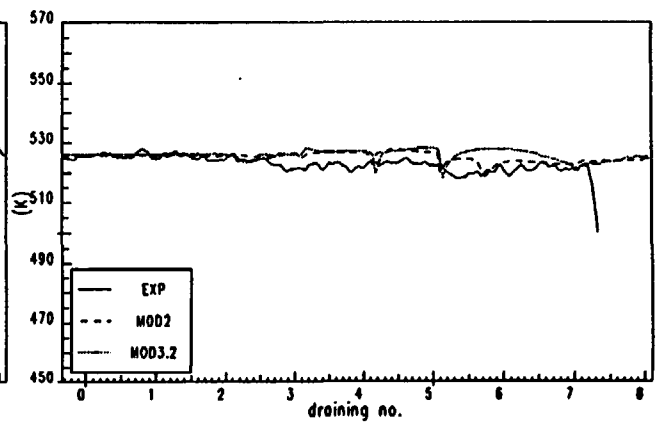
parameter 98 : TFSG3PR23C - SG 3 prim, tube 23, location C



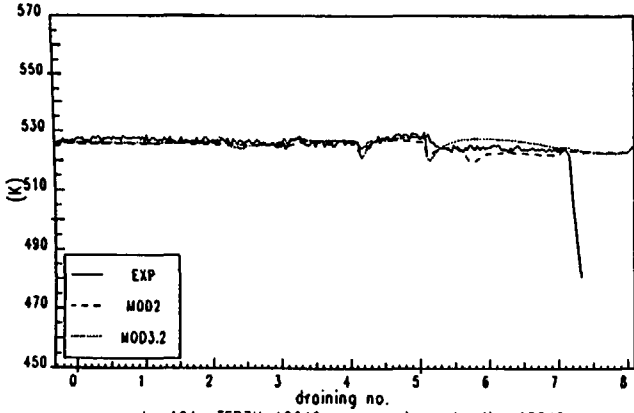
parameter 99 : TFDCH_7900 - downcomer, elevation 7900 mm



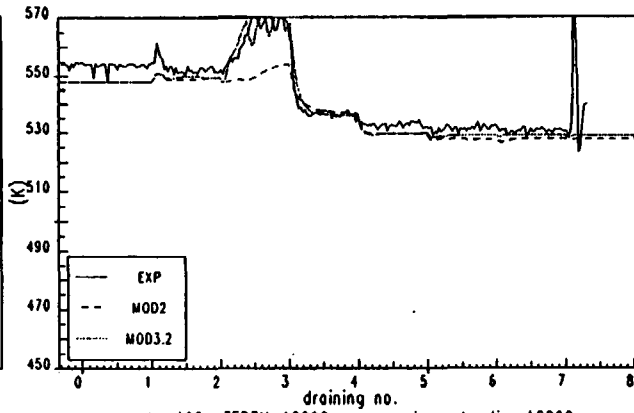
parameter 100 : TFDCH_1700 - downcomer, elevation 1700 mm



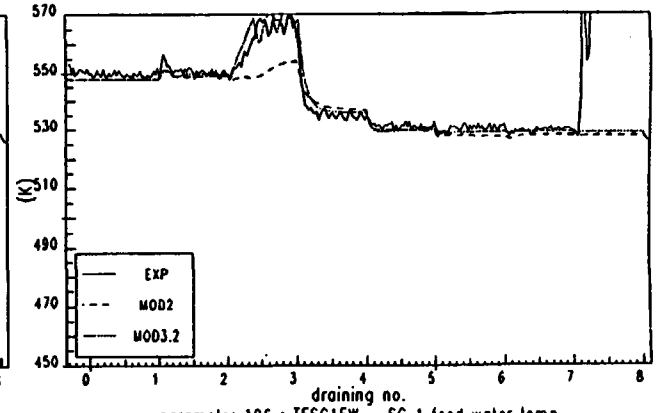
parameter 101 : TFLPH_1700 - lower plenum, elevation 1700 mm



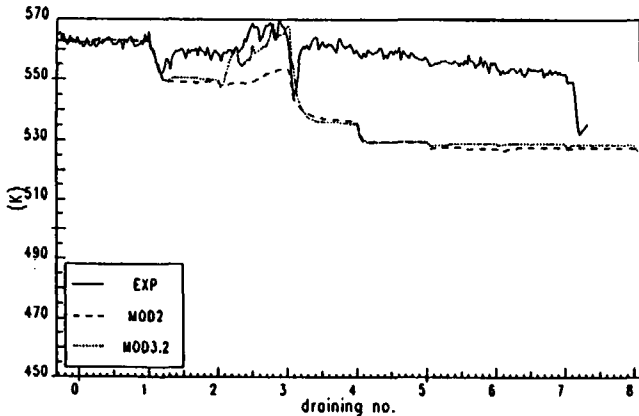
parameter 102 : TFBCH_6150 - core/upper plenum, elevation 6150 mm



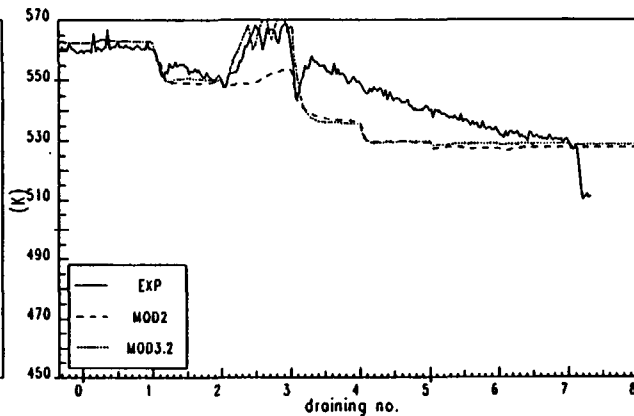
parameter 103 : TFCCH_6150 - core/upper plenum, elevation 6150 mm



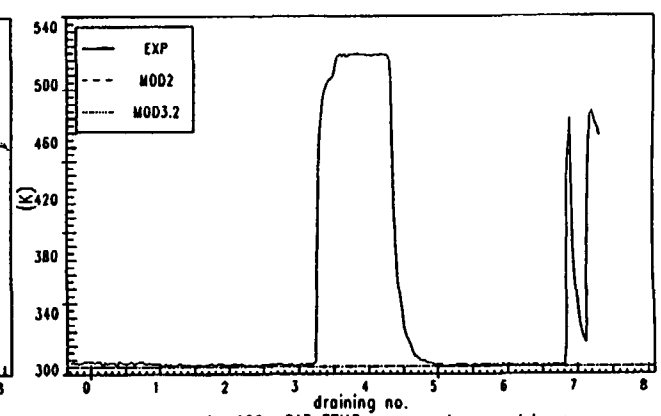
parameter 104 : TFPZH_12240 - pressurizer, elevation 12240 mm



parameter 105 : TFPZH_16090 - pressurizer, elevation 16090 mm

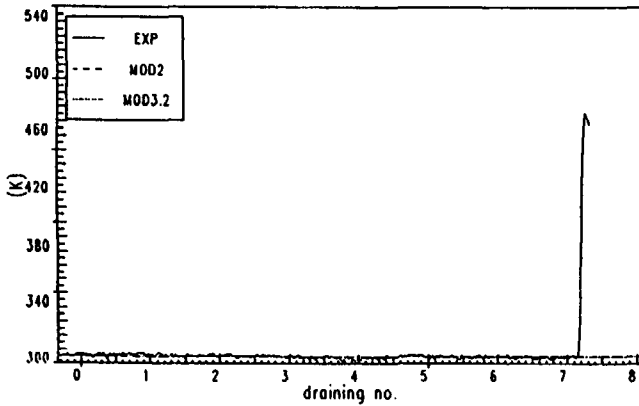


parameter 106 : TFG1FW - SG 1 feed water temp

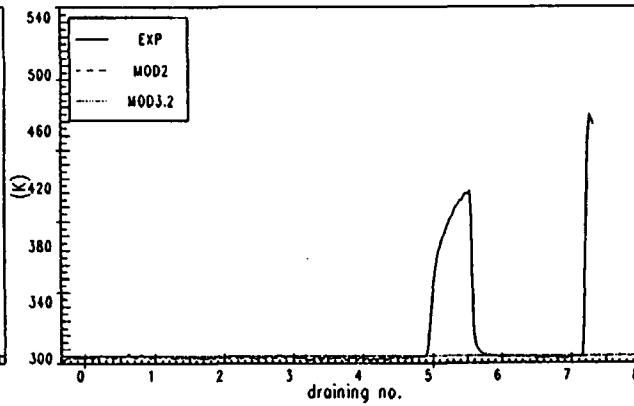


C-15

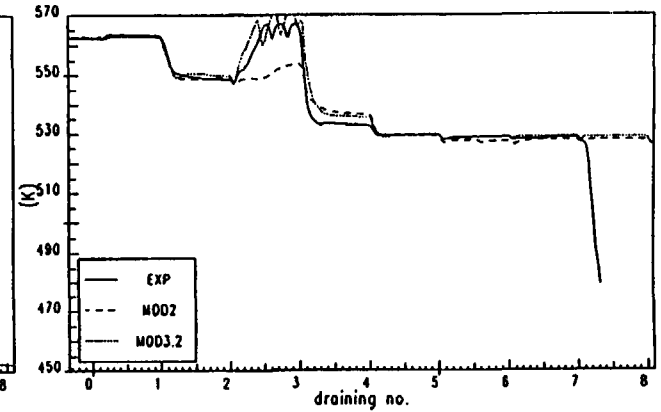
parameter 107 : TFG2FW - SG 2 feed water temp

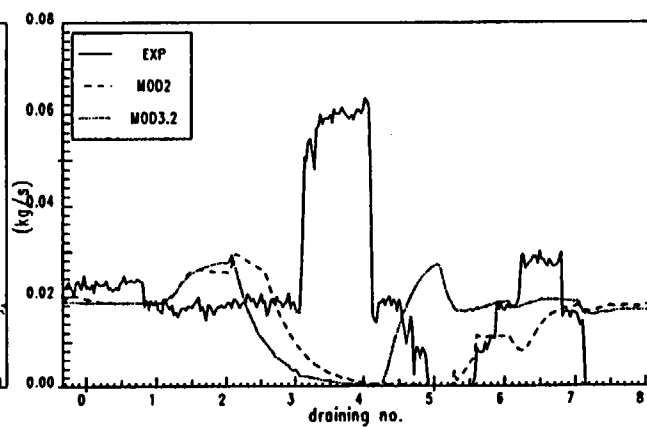
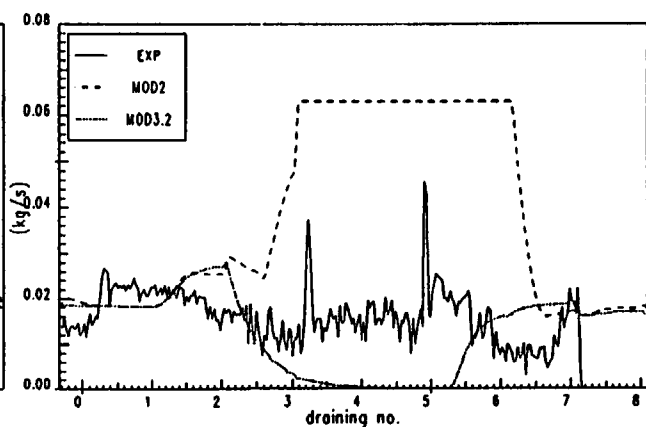
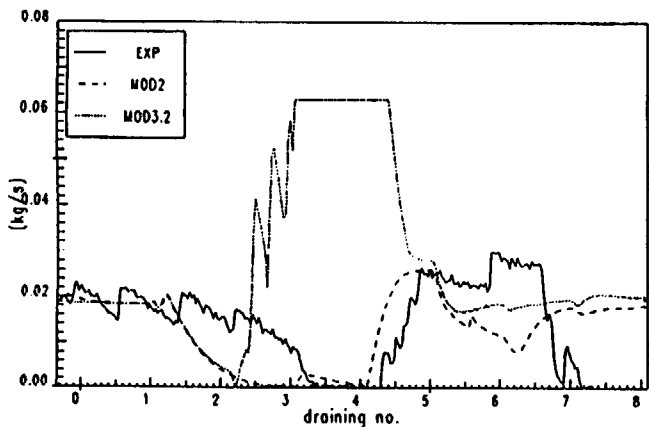
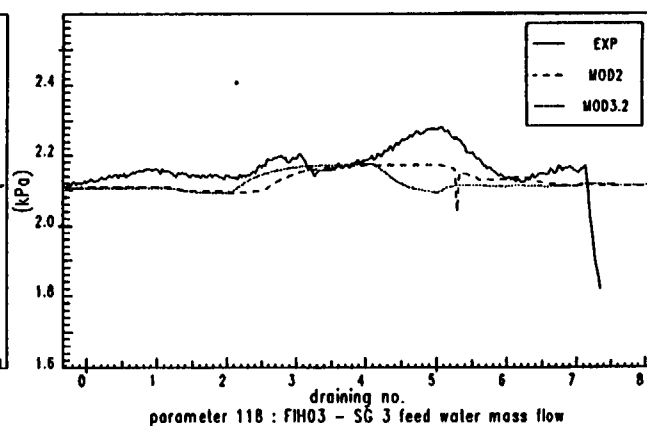
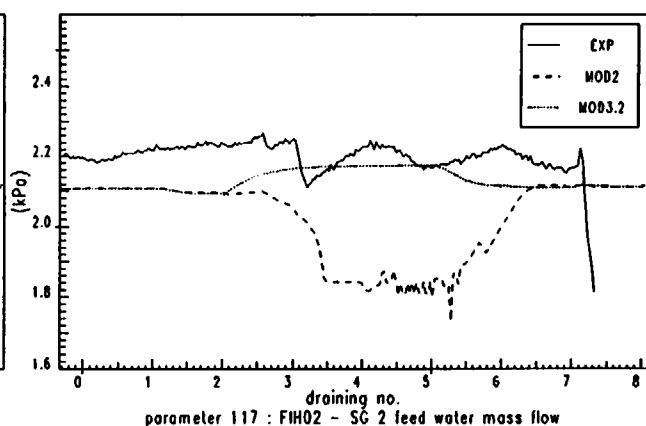
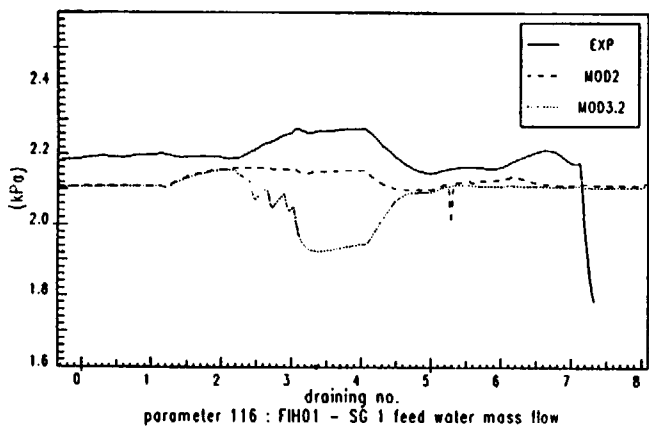
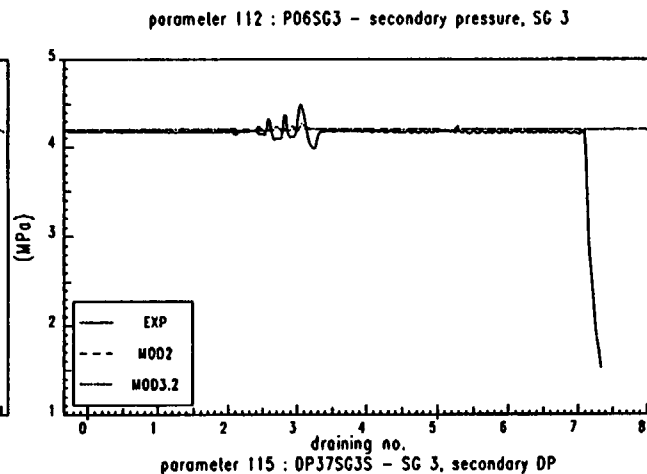
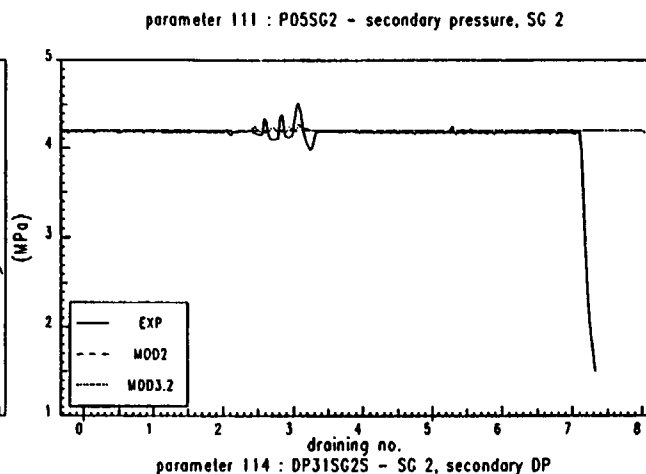
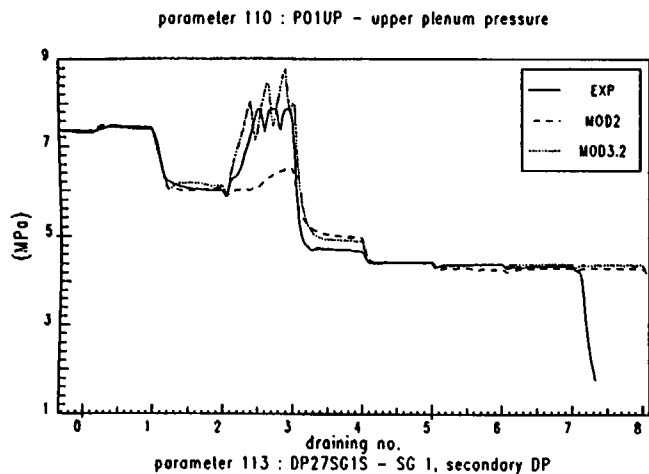


parameter 108 : TFG3FW - SG 3 feed water temp

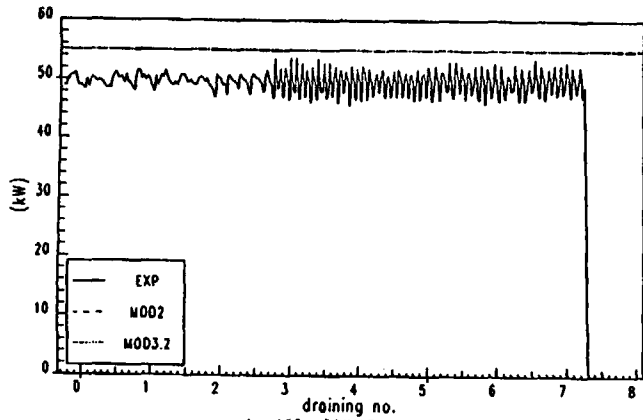


parameter 109 : SAT_TEMP - upper plenum sat temp

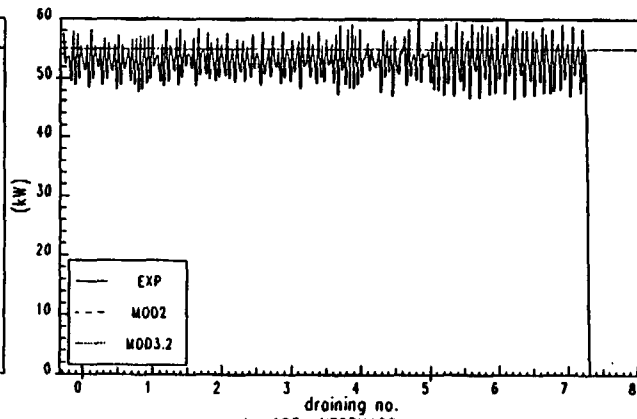




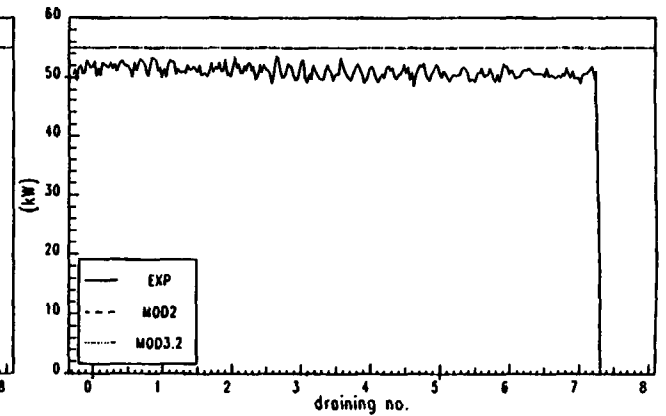
parameter 119 : EAC - core power, channel A



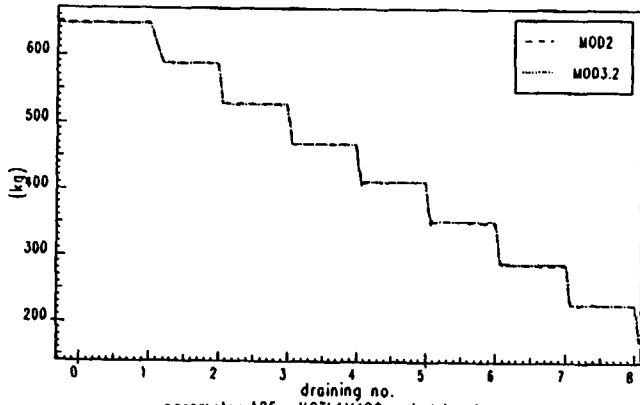
parameter 120 : EBC - core power, channel B



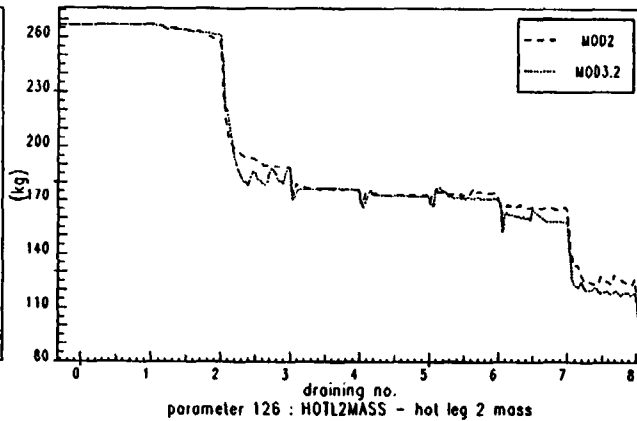
parameter 121 : ECC - core power, channel C



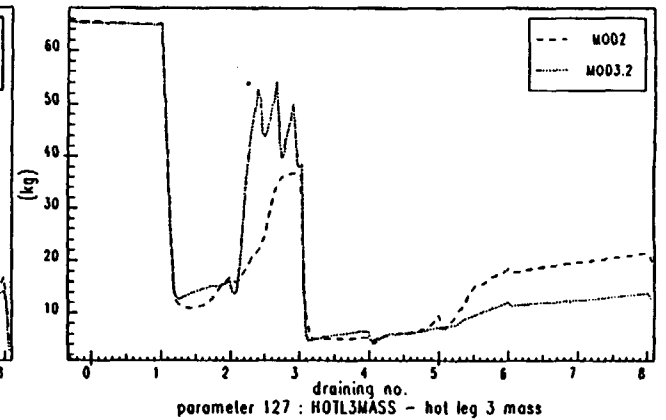
parameter 122 : PRIMAS - primary mass



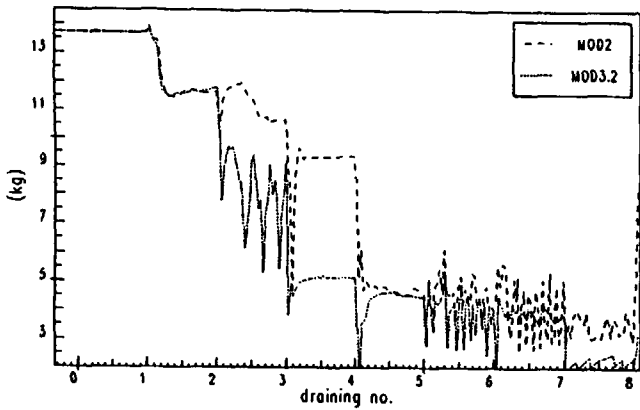
parameter 123 : VESSMASS - vessel mass



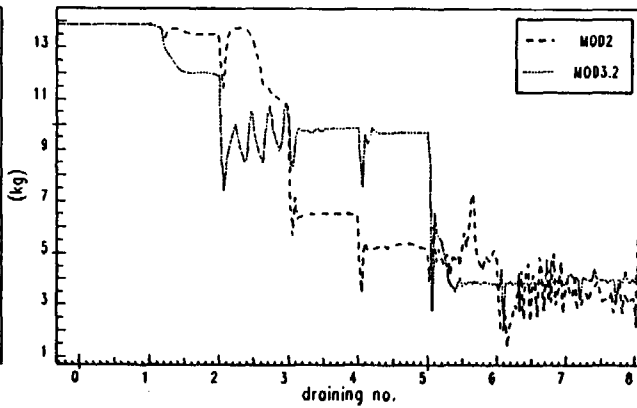
parameter 124 : PRZMASS - pressurizer mass



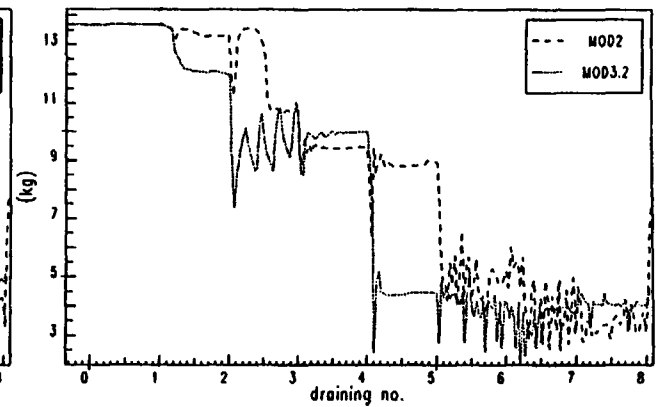
parameter 125 : HOTL1MASS - hot leg 1 mass



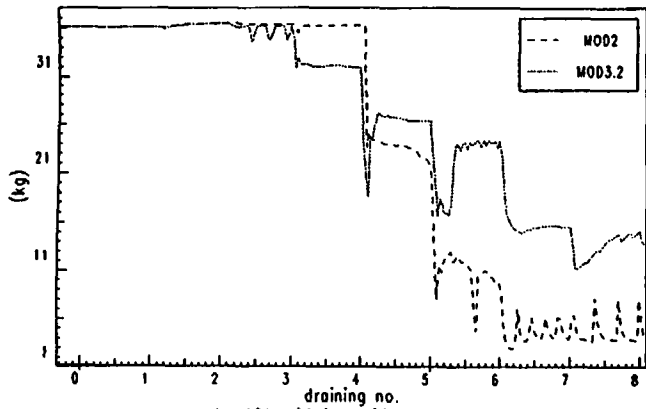
parameter 126 : HOTL2MASS - hot leg 2 mass



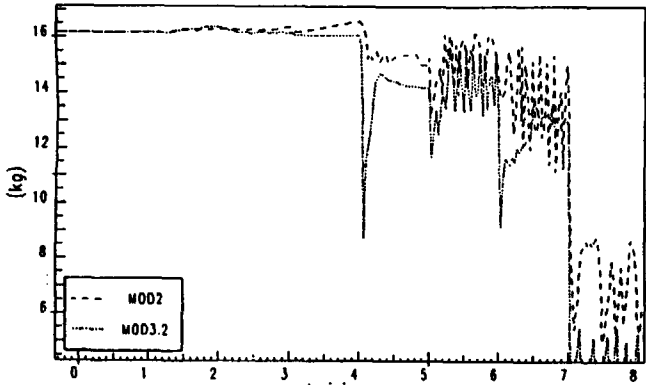
parameter 127 : HOTL3MASS - hot leg 3 mass



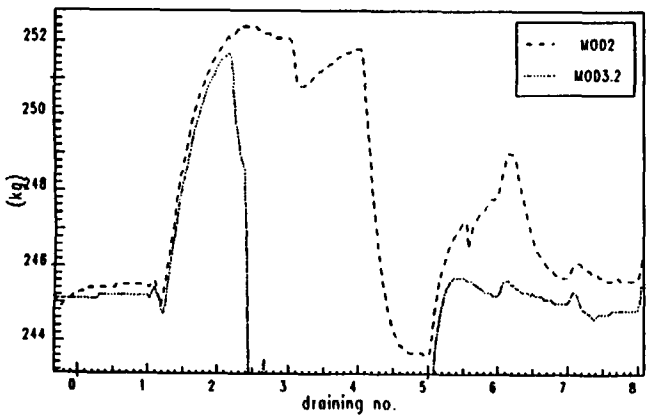
parameter 128 : SGTUBE1MASS - SG 1 tube mass



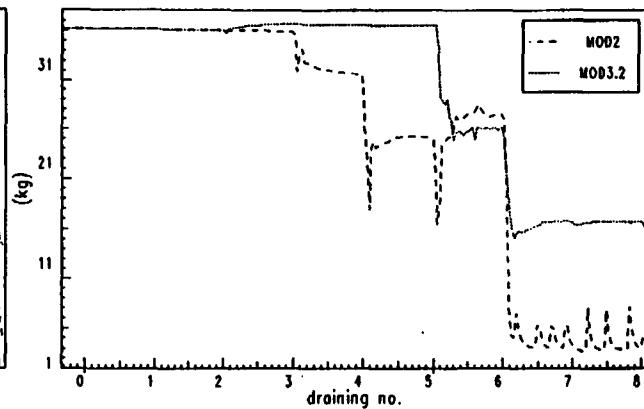
parameter 131 : COLDL1MASS - cold leg 1 mass



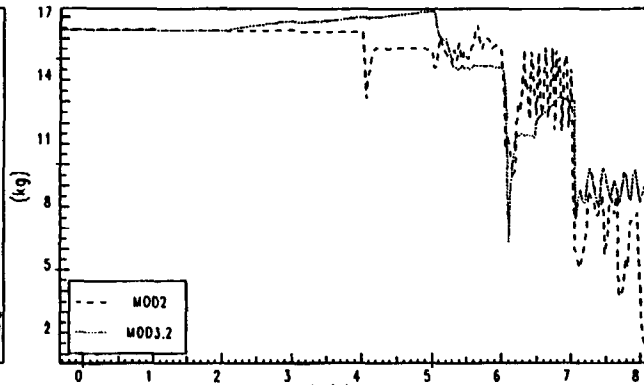
parameter 134 : SGSEC1MASS - SG 1 mass



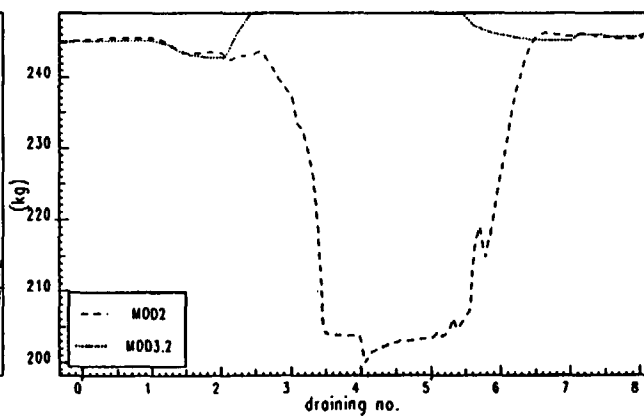
parameter 129 : SGTUBE2MASS - SG 2 tube mass



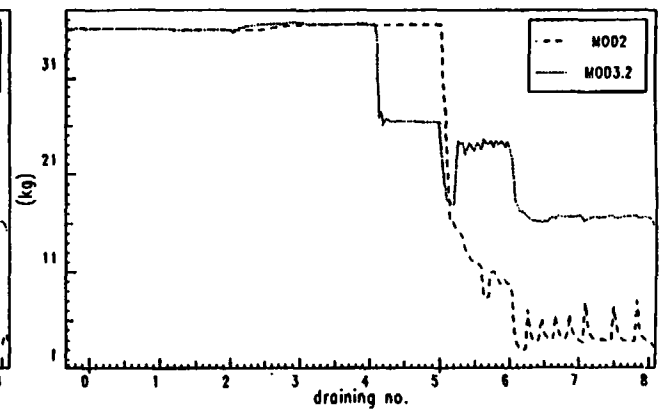
parameter 132 : COLDL2MASS - cold leg 2 mass



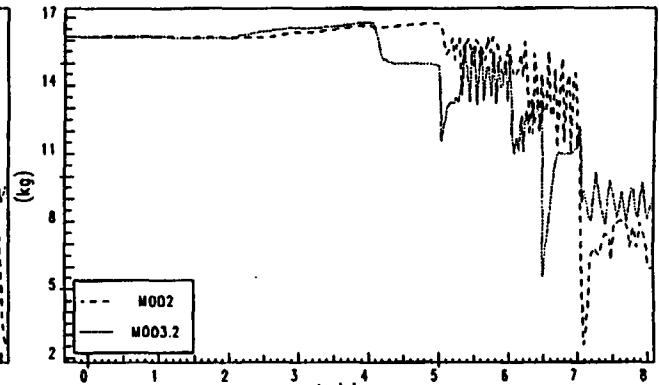
parameter 135 : SGSEC2MASS - SG 2 mass



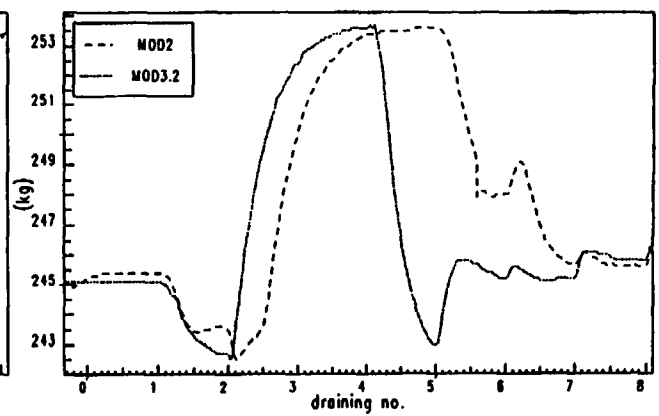
parameter 130 : SGTUBE3MASS - SG 3 tube mass



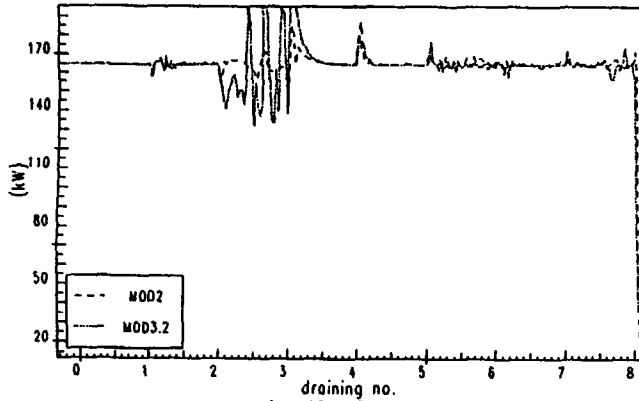
parameter 133 : COLDL3MASS - cold leg 3 mass



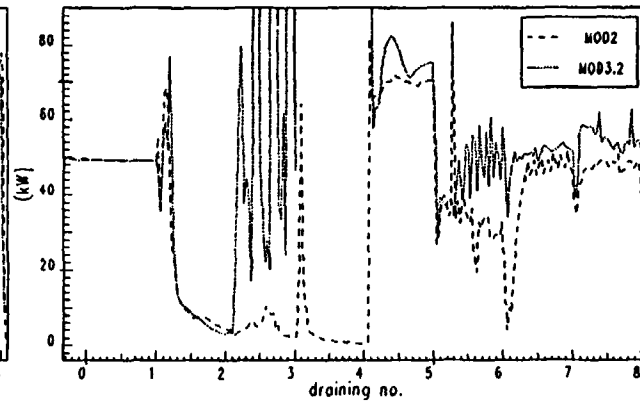
parameter 136 : SGSEC3MASS - SG 3 mass



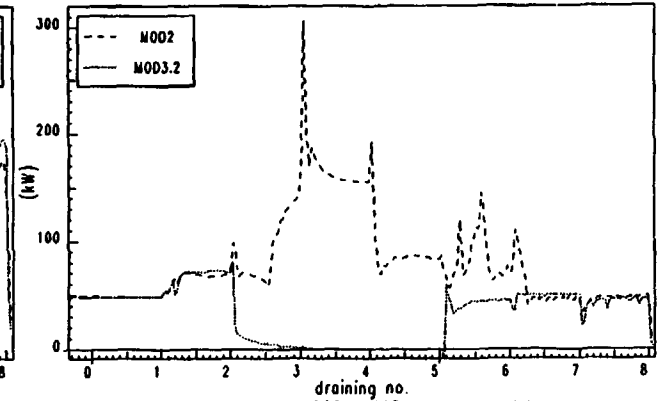
parameter 137 : COREFLUX - heat from core



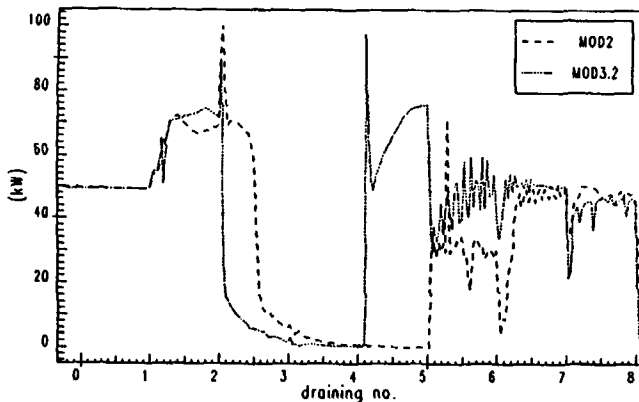
parameter 138 : SGEN1HFLUX - SG 1 heat flux



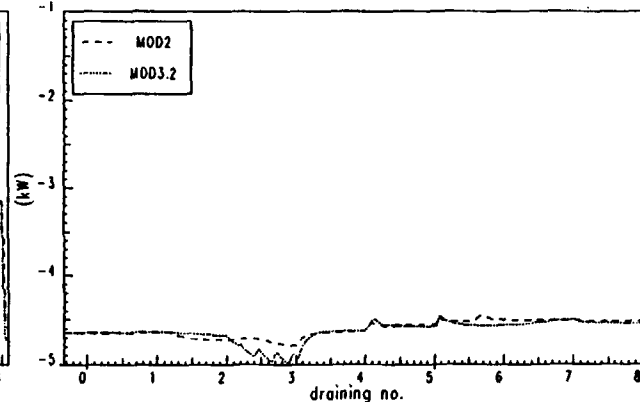
parameter 139 : SGEN2HFLUX - SG 2 heat flux



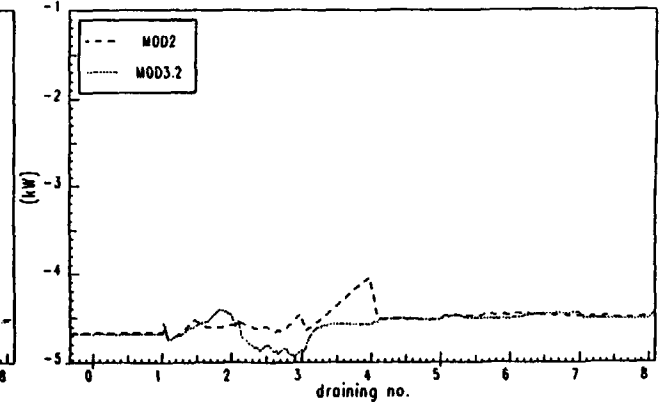
parameter 140 : SGEN3HFLUX - SG 3 heat flux



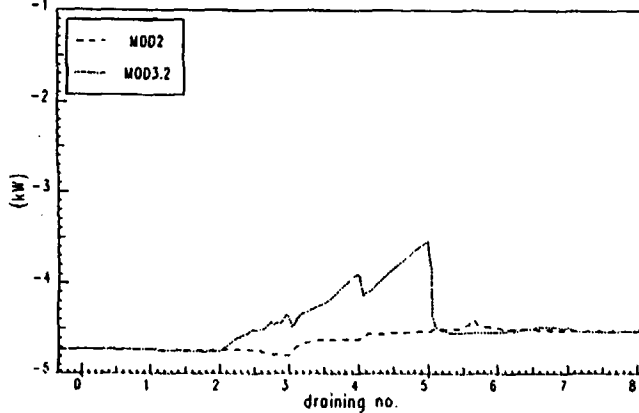
parameter 141 : VESSHLOSS - vessel heat loss



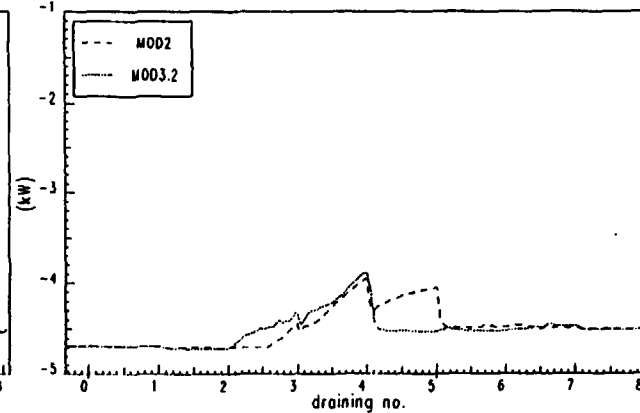
parameter 142 : LOOP1HLOSS - loop 1 heat loss



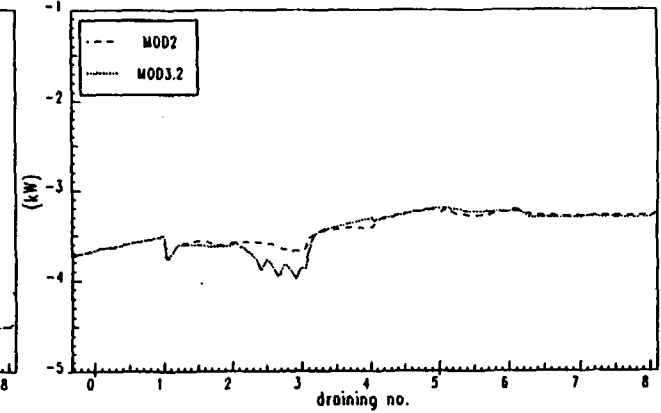
parameter 143 : LOOP2HLOSS - loop 2 heat loss



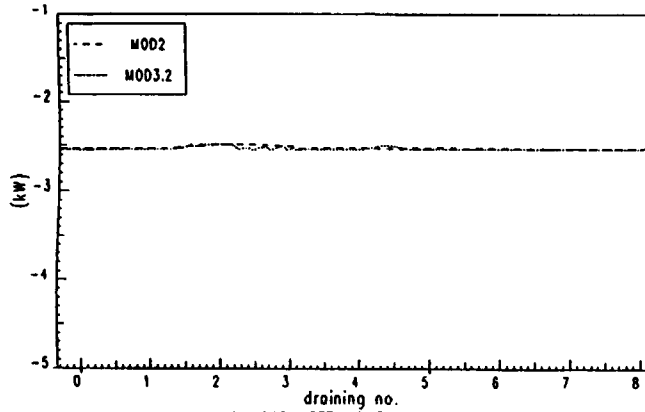
parameter 144 : LOOP3HLOSS - loop 3 heat loss



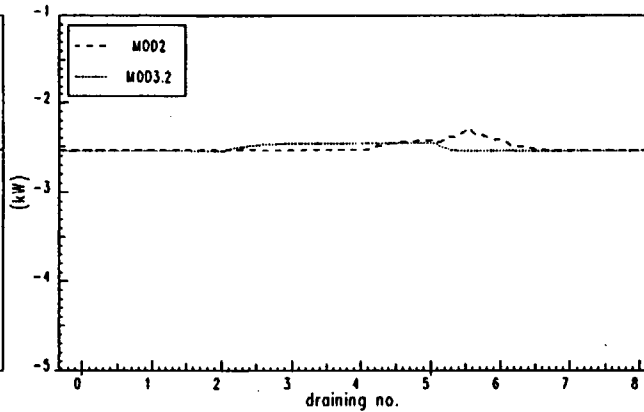
parameter 145 : PRZHLOSS - pressurizer heat loss



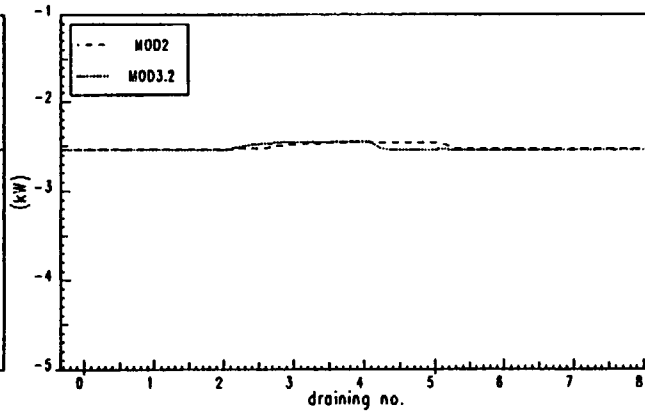
parameter 146 : SEC1HLOSS - SG 1 sec. heat loss



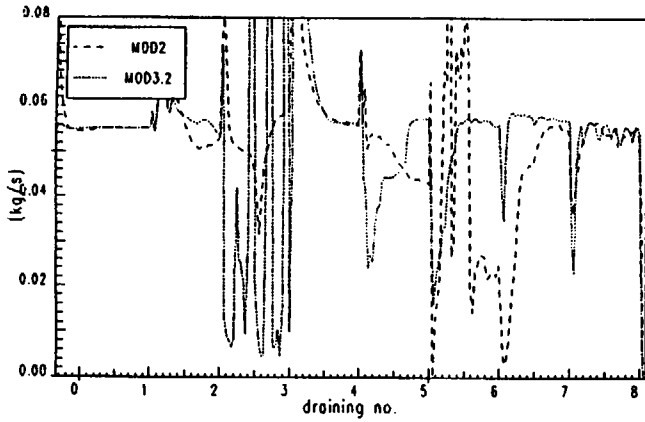
parameter 147 : SEC3HLOSS - SG 2 sec. heat loss



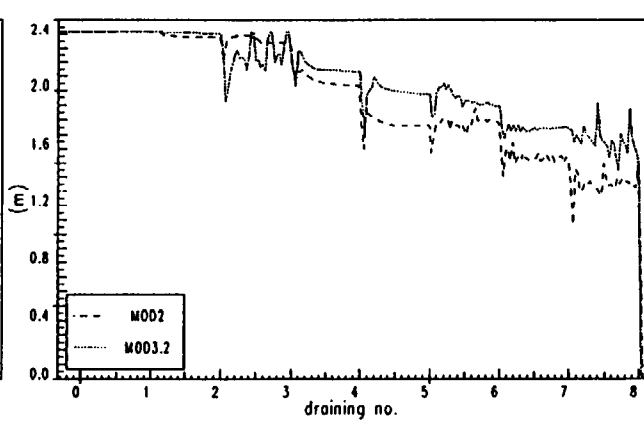
parameter 148 : SEC2HLOSS - SG 3 sec. heat loss



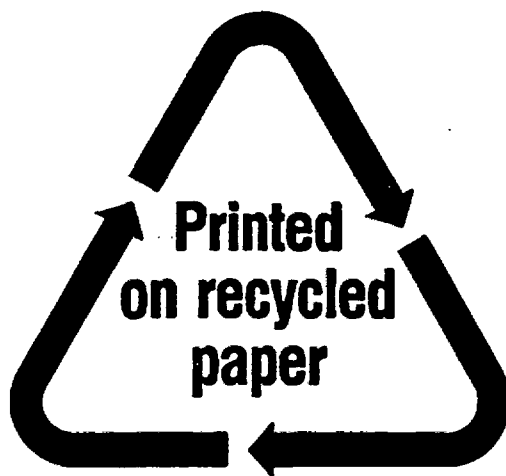
parameter 149 : STEAMOUT - steam flow out



parameter 150 : CORELEVEL - core level



NRC FORM 335 (2-89) NRCM 1102, 3201, 3202	U.S. NUCLEAR REGULATORY COMMISSION BIBLIOGRAPHIC DATA SHEET <i>(See instructions on the reverse)</i>	1. REPORT NUMBER (Assigned by NRC, Add Vol., Supp., Rev., and Addendum Numbers, if any.) NUREG/IA-0145			
2. TITLE AND SUBTITLE RELAPAssessment Against PACTEL Experimental Data (Revision 1)	3. DATE REPORT PUBLISHED <table border="1" style="width: 100%;"> <tr> <td style="width: 50%;">MONTH</td> <td style="width: 50%;">YEAR</td> </tr> <tr> <td>November</td> <td>1998</td> </tr> </table>	MONTH	YEAR	November	1998
MONTH	YEAR				
November	1998				
5. AUTHOR(S) I. Parzer, B. Mavko, S. Petelin	4. FIN OR GRANT NUMBER W6238				
8. PERFORMING ORGANIZATION - NAME AND ADDRESS <i>(If NRC, provide Division, Office or Region, U.S. Nuclear Regulatory Commission, and mailing address; if contractor, provide name and mailing address.)</i> University of Ljubljana "Jozef Stefan" Institute P.O. Box 100 61111 Ljubljana, Slovenia	6. TYPE OF REPORT Technical				
9. SPONSORING ORGANIZATION - NAME AND ADDRESS <i>(If NRC, type "Same as above"; if contractor, provide NRC Division, Office or Region, U.S. Nuclear Regulatory Commission, and mailing address.)</i> Office of Nuclear Regulatory Research U.S. Nuclear Regulatory Commission Washington, DC 20555-0001	7. PERIOD COVERED <i>(Inclusive Dates)</i>				
10. SUPPLEMENTARY NOTES J. Uhle, NRC Project Manager					
11. ABSTRACT <i>(200 words or less)</i> The results of the pre-test and post-test calculations of OECD International Standard Problem no.33 (ISP-33) are presented. The frozen version of RELAP5 code version MOD2 and the latest released version MOD3.2 have been assessed against experimental data from PACTEL facility. Generally, predictions were in good agreement with experimental data, except in the most interesting part of the transient only MOD3.2 was able to follow periodic hot leg loop seal clearance phenomena and primary pressure oscillations closely.					
12. KEY WORDS/DESCRIPTORS <i>(List words or phrases that will assist researchers in locating the report.)</i> RELAP5/MOD3.2 SB-LOCA	13. AVAILABILITY STATEMENT unlimited <hr/> 14. SECURITY CLASSIFICATION <i>(This Page)</i> unclassified <hr/> <i>(This Report)</i> unclassified <hr/> 15. NUMBER OF PAGES <hr/> 16. PRICE				



Federal Recycling Program

NUREG/IA-0145

RELAP5 ASSESSMENT AGAINST PACTEL EXPERIMENTAL DATA
(REVISION 1)

NOVEMBER 1998

UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, DC 20555-0001

OFFICIAL BUSINESS
PENALTY FOR PRIVATE USE, \$300

SPECIAL STANDARD MAIL
POSTAGE AND FEES PAID
USNRC
PERMIT NO. G-67