

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

An Evaluation of Seismic Reflection
Studies in the Yucca Mountain Area, Nevada Test Site

by

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with an introduction by

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¹USGS, Denver, Co.

Denver, Colorado
1983

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Parker, Co.

Introduction to the Report

by

L. W. Pankratz¹ and H. D. Ackermann¹

The U.S. Geological Survey (USGS) working under an Interagency agreement, DE-AI08-78 ET 44802, with the Department of Energy is engaged in a broad program to assess and identify potential repositories for high level nuclear waste on the Nevada Test Site (NTS). The USGS program consists of integrated geologic, hydrologic and geophysical studies which range in nature from regional to site specific. This report is an evaluation of seismic reflection studies made at the Yucca Mountain potential repository site in the southwestern part of NTS.

As part of this study the U.S.G.S. contracted with three different organizations in the years 1980, 1981, and 1982 to conduct progressively more complex seismic reflection surveys focusing in the Yucca Mountain area, Southwest quadrant of the Nevada Test Site: 1.) A study was conducted by The Colorado School of Mines in 1980, which resulted in a Master of Engineering Thesis (ER-2429) by Charles Barry (1981). The results presented in this thesis emphasized the negative results of a high resolution seismic survey conducted in the presence of the high background noise environment which exists at Yucca Mountain. 2.) The second survey by Birdwell/SSC was designed with the insight gained by a noise study using elaborate receiver arrays. Extensive computer processing of these reflection data showed, either the possibility of a reflected event or a computer generated false reflection. (Later computer analysis of the noise profiles showed that the recording parameters used for the survey were still insufficient to cancel the predominant noise trains). 3.) On the basis of this possible reflected

¹U.S. Geological Survey

event, an even more extensive study was undertaken. Following thorough review, a request for bids was issued in January 1982, and a contractor selected in March, 1982. In the meantime at the request of the reviewers the services of a data acquisition processing specialist, Mr. Stanley Brasel, Seismic International Research Corporation, were used to advise the USGS on implementation of the reflection survey. The data acquisition contractor, Seisdata Services, Inc., began operations in March, 1982. Due to the untimely death of Mr. Brasel in February, 1983, SIRC hired a sub-contractor, Subsurface, Inc., to complete the final report which is presented herein.

The seismic reflection technique was predicted to provide information on the geological homogeneity of the host rock in the repository. Unfortunately, the nature of the rock structure, over 6000 feet of interbedded highly fractured densely welded and nonwelded volcanic tuffs, coupled with the highly absorptive and ringing nature of the near surface rocks (Pankratz, 1982; Barry, 1980), was not conducive to the reception of reflected events at the surface with sufficient power to be recorded above the noise level. Norman Burkhard (1983) essentially presents this same argument when he concludes that "I believe that the transmissivity of the alluvial and volcanic sections is the single most important factor". The conclusion is reached by the studies presented in the following report, that even with powerful source and receiver arrays the seismic reflection technique cannot discern a signal which can be seen above the noise level received from the tuffs that underlie Yucca Mountain. This problem coupled with the difficult terrain and the prohibitive expense of utilizing the increased power of arrays results in our recommendation that the seismic reflection method should not be employed at Yucca Mountain except as experimental surveys to evaluate new sources or techniques.

The following report by Thomas McGovern of Subsurface, Inc., presents a comprehensive analysis of the seismic reflection work performed at Yucca Mountain.

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- Barry, C. T., 1980, A study of the Verticle Vibrator Source for Seismic Profiling in the Yucca Mountain Area of the Nevada Test Site, Master of Engineering Thesis, ER 2429, Colorado School of Mines, 58 p.
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- Pankratz, L. W., 1982, Reconnaissance Seismic Refraction Studies at Calico Hills, Wahmonie and Yucca Mountain Southwest Nevada Test Site, Nye County Nevada: U.S. Geological Survey Open-File Report 82-478, 25 p.

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A Geophysical Evaluation of Seismic
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Nevada Test Site

by

Thomas F. McGovern¹

ABSTRACT

As part of a total geophysical evaluation of Yucca Mountain for use as a Nuclear Waste Repository the seismic reflection technique has been applied. This study has been conducted to analyze the historical and technical efforts which have been used by three geophysical contractors employing a wide variety of techniques ranging from the most simple to very elaborate 3-D surveys. In each case elaborate noise studies were conducted, and based upon their evaluation parameters were chosen for multifold CDP recording. In every case, the signal-to-noise ratio was such that no reflections were discernable. Since the reflections cannot be separated from the noise even using very elaborate noise suppression techniques and up to 384 fold multiplicity it is apparent that in this volcanic terrain reflection surveys can not work.

¹Subsurface, Inc., Parker, Co.

INTRODUCTION

Yucca mountain (Nevada Test Site) has been the site of some recent important seismic reflection studies (Figures 1 and 1A), conducted by the following geophysical contractors: the Colorado School of Mines (1980), Birdwell/Seismograph Service Corporation (1981), Seismic International Research and Seisdata Services Inc. (1982). Each reflection survey was accompanied by an elaborate noise study. In the most recent study, Seismic International Research Corp. was responsible for the design of the field technique and data processing while Seisdata Services Inc. was responsible for data acquisition. Western Geophysical Inc. was also contracted to process one seismic reflection line as a quality control check on the Seismic International Research data processing. It is the purpose of this investigation by Subsurface Inc. to evaluate the applicability of the seismic reflection technique in the Yucca Mountain (Nevada Test Site) area.

HISTORICAL REVIEW OF SEISMIC REFLECTION SURVEYS DONE AT THE NEVADA TEST SITE

Table 1 displays the field acquisition parameters used in gathering seismic reflection surveys from the years 1972-1982 in the Nevada Test Site. It also shows the survey location areas, geologic setting and estimate of the reflection data quality. Table 1 indicates that most seismic reflection surveys at the Nevada Test Site were acquired as two dimensional profiles employing numerous input sources (Vibroseis¹, Primacord², Dynamite) and source array patterns. Many different receiver arrays were also utilized. These arrays were both short and long (up to 440 ft) and employed from 1 to 144 geophones. Our visual examination of the processed data revealed that the profiles from areas usually characterized by complex faulting, volcanics and paleozoic outcroppings (Yucca Mountain, Wahmonie, Calico Hills, and Syncline Ridge) (Christiansen and Lipman, 1965, Lipman and McKay, 1965, Hoover, 1982, Synder and Carr, 1982, and Pankratz, 1982) did not produce any accurate reflection information. However, reflection data acquired in the flat lying alluvial plain (Yucca Flat) which is not quite as complex geologically appeared of much better quality.

In 1982, a three dimensional seismic reflection survey was conducted at Yucca Mountain utilizing a field technique that produced stack fold ranging between 192 and 384. This report will illustrate that this very powerful field technique also did not produce any interpretable reflection events.

¹ Registered trademark, Continental Oil Co.

² Registered trademark, Ensign Bickford, Co.

TABLE I

Yr. & Contractor	Instrument	Channels	Amplifier	Geophone Frequency (HZ)	Geophones Trace	Geophone Pattern	Geophone Spacing (ft)	Profile Type	Source	Source Array	Source Spacing (ft)	Stack Fold	Group Interval (ft)	Source Interval (ft)
1972 SSC	T1 10000	24	Fixed-Gain	7.5	36	In Line	12.5 ft. Over 440 ft.	2-D	Vibroseis	4 Vibrators In Line	75 Apart	12	220	220
1978 Western	Litton Coda	48	Floating Point	10	36	In Line Over 440 ft.	12.5	2-D	"	"	75 Total Pattern 440	24	220	220
1978 Western	Litton Coda	48	"	10	24	In Line	19	2-D	"	"	75	24	220	220
1979 Geosource	GUS-HDDR	24	"	10	20	"	2.8	2-D	Dynamite	n/a	n/a	12	55	55
1980 CSM	DFS-5	48	"	18	1	"	55	2-D	Vibroseis	Vibrator In Line	220	24	55	55
1980 Seisdata	DFS III	48	"	10	12	"	10	2-D	Primacord	n/a	n/a	24	55	55
1980 Seisdata	DFS III	48	"	10	12	"	17	2-D	"	n/a	n/a	24	55	55
1981 Birdwell	DFS-5	48	"	10	120	In Line Weighted Array	8.5	2-D	Vibroseis	30 In Line	5	24	50	50
1982 Seisdata	MDS-10	96	"	10	96	Weighted Array	15	3-D	Dynamite	1 Deep Hole	200	192	100	200
1982 Seisdata	MDS-10	96	"	10	96	Weighted Array	15	3-D	Vibroseis	3 Vibrators 18 Sweeps	12.5	384	105 - 210	105 - 210
1982 Seisdata	MDS-10	96	"	10	12	In Line	9	3-D	Vector Pulse (Primacord)	7 Elements In Line	16	288	50	50

TABLE 1 [cont'd]

Yr. & Contractor	Near Offset (ft)	Far Offset (ft)	Sweep (Hz)	No. of Sweeps	Sweep Duration (sec)	Listening Time (sec)	Sampling Interval (ms)	Field Filter (Hz)	Area	Data Quality	Geological Setting
1972 SSC	880	3300	17-56	16	7	10	4	14-70	Syncline Ridge	poor	VR over PH
1978 Western	660	5720	14-56	16	16	5	4	out-62	Syncline Ridge	poor	"
1978 Western	880	11220	6-32	up 32	12	3	4	out-62	Syncline Ridge	very poor-poor	"
1979 Geosource	n/a	n/a	n/a	n/a	n/a	n/a	25	23-180	Yucca Flats	poor-fair	Alluvium over VR
1980 CSM	55	1320	30-120	9	6	3	2	12-180	Wahmonie Yucca Mt. Calico Hills	very poor	AFT over IC & VR
1980 Seisdata	192	1457	n/a	n/a	n/a	n/a	2	18-124	Yucca Flats	poor-fair	Alluvium over VR
1980 Seisdata	220	1465	n/a	n/a	n/a	n/a	2	18-124	Yucca Flats	poor-fair	"
1981 Birdwell	500	1650	48-6	30	16	6	4	out-128	Yucca Mt.	very poor	AFT in MT
1982 Seisdata	800	3100	n/a	n/a	n/a	n/a	2	12-125	Yucca Mt.	very poor	"
1982 Seisdata	840	1940	10-56 22-84 16-62	16	14	4	2	out-125	Yucca Mt.	very poor	"
1982 Seisdata	840	2415	n/a	n/a	n/a	n/a	2	12-125	Yucca Mt.	poor	"

LEGEND

n/a - Not Available
 IC - Intrusive Complex
 PH - Paleozoic High
 VR - Volcanic Rock
 AFT - Ash Flow Tuff
 MT - Mountainous Terrain

COLORADO SCHOOL OF MINES REFLECTION SURVEY

In 1980, The Colorado School of Mines (CSM) (Barry, 1980) conducted seismic reflection surveys in three areas of the southwest Nevada Test Site. These areas were: Yucca Mountain, Wahmonie, and Calico Hills (Figures 1 and 1A). Their objective was to obtain detailed shallow subsurface geologic information. With this objective in mind, their field technique was directed toward high resolution acquisition utilizing short geophone arrays and high source frequencies. Initially, a detailed noise analysis was conducted in each of the three areas. Each noise profile consisted of a small common depth point reflection line, various geophone arrays and a broad range of input sweep frequencies (8 to 120 hz.). Detailed computer analysis of the noise data indicated that noise patterns, in all three areas, were not effectively cancelled by the suite of receiver arrays tested. Table 2 is a summary of the CSM measured velocities of noise patterns in all the three areas.

In accordance with their high resolution objective, the CSM selected as final production acquisition parameters a receiver array consisting of one buried geophone and a sweep frequency of 30 to 120 hz. Additional acquisition parameters included: 18 hz. geophones, 55 ft. station intervals, 6 second up sweep at nine vibrator positions, 6 ft. vibrator move up, 48 channel recording, 24 fold stack, 2 millisecond sampling interval, and near and far offsets of 55/1320 ft. This survey produced no interpretable subsurface reflection information. It also demonstrated that simple high resolution data acquisition techniques are not applicable in the Yucca Mountain vicinity (Barry, 1980, pp. 36-40).

TABLE 2

<u>NOISE TYPE</u>	<u>VELOCITY ft./sec.</u>
Refraction	11500
Direct Wave	4000-4200
Groundroll	1600-2000
Airwave	1100

BIRDWELL REFLECTION SURVEY

In 1981, Birdwell conducted a seismic reflection survey at Yucca Mountain near Drill Hole Wash from drill holes USW-G1 to USW-H1 (Figure 1A). The objective of this study was to further test the feasibility of the reflection method at Yucca Mountain and establish a tie between the two drill holes. The noise study and a reflection survey were recorded within a few days of each other. The noise study used elaborate receiver arrays (Figure 2) which allowed the testing of various configurations of geophone receiver arrays using different channels in a simultaneous recording. This method utilized the VibroseisTM source walkaway technique (Sheriff, 1974) where receiver arrays remain stationary as the source moves away in a linear pattern. This profile differed from a standard walkaway procedure in that it utilized closely spaced source points that were received by various array patterns configured on each recording channel. This procedure can provide many types of walkaway profiles by computer plotting of each recording channel for each source point. Analysis of the noise profiles revealed that all receiver arrays tested exhibited similar noise attenuation properties.

Figure 3 is a typical noise profile with automatic gain control. Table 3 is a summary of the measured velocities of the noise patterns as recorded by the Birdwell survey.

TABLE 3

<u>NOISE TYPE</u>	<u>VELOCITY ft/sec.</u>
Refraction	6000, 8000, 10000
Direct Wave	4000-4200
Groundroll	1600-2000
Airwave	1100

Recording parameters for the reflection survey were chosen on the basis of field examination of the noise profiles. They consisted of a rectangular 100 x 200 ft. receiver array containing 10 rows of 12 geophones each separated 8.5 ft. and a 48 to 6 hz. downsweep. Additional parameters included: 24 channels, 24 stack fold, 16 second downsweep, 3 vibrators 50 ft. apart inline with a 5 ft. move up, 50 ft. station intervals, 4 millisecond sampling interval and near and far offsets of 500/2850 ft.

The raw unstacked records were dominated by several types of noise the character of which appears to change with shot-receiver offset distance (fig. 4). For the near receiver offsets, the seismic records are dominated by high frequency random noise, probably produced by instrument electronics, wind and seismic crew related activities. For far offsets the records are dominated by low frequency source generated coherent noise which propagates horizontally through the near surface. No reflections could be observed on the raw reflection records. Processing was done by Seismograph Service Corporation (SSC). The data were initially demultiplexed, summed, cross-correlated,

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edited and CDP sorted using standard procedures (Anstey, 1977). Various tests were then employed (e.g. autocorrelation, power spectrum analysis, filtering, deconvolution, and scaling) to help determine further processing procedures. The data set was filtered with a 14 to 48 hz. bandpass and constant velocity stacks run to determine normal moveout.

At this point, a source and receiver simulation test was performed to determine if a larger array interval would effectively cancel dominant noise patterns. (This procedure mathematically transforms one recorded source and receiver array configuration to another by means of a running sum mix of adjacent traces). Selective stacking was performed using varying offset distances to determine whether lateral continuity of reflection events could possibly be enhanced by using only the near, or the intermediate, or the far offset traces. These specific stacks led to the conclusion that both the near and medium to far offsets were dominated by noise. Figure 4 displays a typical field recording which exhibits very coherent noise patterns in most areas of the seismic reflection record.

During the normal data processing routine, several CDP stacks were generated for quality control and these, curiously, led to some interesting conclusions. First, a CDP stack was produced that had only a normal moveout correction applied (Figure 5). This type of stack is normally produced as a quality control check before application of automatic residual statics. This CDP stack yielded no interpretable continuous reflection events. Then automatic residual statics were applied to the data (Figure 6) which produced an apparent reflection at 1.2 seconds. In reference to Figure 4, we note that the shallow part of the seismic reflection record above 2.0 sec is dominated by coherent noise which may be the source of this apparent reflection. To test this concept (Taner et al, 1974), a CDP stack was produced without the

presence of this coherent noise (Figure 7) using velocity filtering (Sheriff, 1974) and selective muting to eliminate these coherent noise patterns. Automatic statics were also applied and the CDP stack (Saghy and Zelei, 1975) yielded no apparent continuous reflection information, therefore, we conclude that the automatic statics routine aligned noise trains to produce an inferred reflected event. A discussion of this routine necessarily follows. The automatic statics routine used by SSC employed a seven CDP correlation model and a 0.5 - 1.2 second correlation window. Seven common depth points and their respective traces were stacked to produce this model which was then cross-correlated with each trace within the central common depth point. The time shifts observed between the model and the CDP traces are assumed to be residual static errors and these time shifts are then applied to the traces. This cross-correlation technique is amplitude dependent. If high amplitude events existed within the correlation window, they were shifted to align with corresponding high amplitude events contained in the model. If these high amplitude events represented coherent noise, the resulting stack would have aligned coherent noise. Therefore, the reflection at 1.2 seconds observed in figure 6 is no more than alignment produced by the automatic statics routine. Despite this maximum processing effort no interpretable reflections were observed.

In 1982, Seismic International Research Corp. (SIRC) and Seisdata Services Inc. (SSI) conducted a three dimensional seismic reflection survey in the Yucca Mountain vicinity. (Figure 1A). A historical analysis of previous reflection surveys proved that standard simple acquisition techniques could not be applied in this area. This reflection survey had to maximize all field efforts if reflection information was to be obtained. A three dimensional effort was proposed and accepted because it favored an extremely high stack fold (192 to 384) for common depth points and provided a very effective method of attenuating noise patterns thereby improving the signal to noise ratio.

The VibroseisTM method was chosen for use as long as the terrain was flat and accessible, however, where the terrain was rugged and inaccessible, surface source explosives (PrimacordTM) were employed. Previous acquisition efforts utilized simple receiver and source arrays. Serious consideration had to be given to the concept of employing complicated source and receiver arrays which with their combined effort offered a very powerful technique for coherent noise attenuation.

Several conclusions can be reached from the two previous reflection surveys conducted in the Yucca Mountain vicinity. First, the CSM survey was designed with high resolution acquisition in mind. Therefore, they utilized short geophone arrays and high source frequencies. This technique employed a simple 9 element single vibrator source array and a single geophone array. However, this method was much too simple for an area where the dominant recorded energy is noise. Figure 8 is an array response curve for the total combined technique (Halzman, 1963) used in the CSM reflection survey. This technique resulted in a maximum effort of 12 db. attenuation for noise

wavelengths of 10 to 70 ft. The Birdwell reflection survey differed from the CSM survey in that it did not employ high resolution acquisition techniques, only a complicated receiver array and a simple source array. The input source frequencies were fairly low (6 to 48 hz.) Figure 9 is an array response pattern for the combined field technique used in the Birdwell reflection survey. The maximum effort is a 29 db. attenuation for noise wavelengths of 12 to 160 ft. Because no reflection information was obtained, this still proved too low of an attenuation factor for this noise dominated area.

SIRC/SSI designed a much stronger method using receiver arrays consisting of 120 geophones, and either 3-4 vibrator trucks or Vector PulseTM for source arrays. Figure 10 is a response curve for a total combined source and receiver array using 3 vibrator trucks (Gayer, 1970), 54 sweeps with 12 foot spacing and a 96 geophone array at 15 foot spacing. This combined technique produced an attenuation power of 68 db. for noise wavelengths of 18 to 122 feet. Figure 11 shows the response curve employing the same receiver array but a Vector PulseTM source array consisting of 12 equally spaced elements. This combined effort is also very powerful because it provides a 53 db. attenuation for noise wavelengths of 18 to 122 feet.

- 1.) Vector Pulse is a Registered Trademark, Seisdata Services Inc. It employs elements consisting of 0.5 in steel rods approximately 4 ft long loaded with PrimacordTM emplaced in the earth.

SEISMIC INTERNATIONAL RESEARCH CORP./SEISDATA SERVICES INC. NOISE STUDIES

Noise studies conducted by SIRC/SSI consisted of both inline (walkway) and circular (tornado) profiles. These noise profiles were recorded in the alluvial valley directly east of Yucca Mountain which afforded accessibility and mild terrain and also allowed the use of both VibroseisTM and Vector PulseTM source methods. The objectives of these noise studies at Yucca Mountain were:

- a) to measure the range in velocity of all source generated noise,
- b) to test for reflected or broadside noise,
- c) to determine the dominant noise patterns,
- d) to test several input frequency ranges for penetrating and resolving power,
- e) to compare VibroseisTM and Vector PulseTM energy sources,
- f) to generate a physical model of noise distribution, and
- g) to seek a window between noise patterns for observing reflection information.

INLINE NOISE PROFILE

The inline noise spread was designed to measure velocity, frequency and wavelength of source generated noise in the line of profile. It consisted of 96 recording stations each with 12 bunched geophones 10 feet apart. Four shotpoints were used, each 950 feet apart as illustrated in Figure 12. Both Vector PulseTM and VibroseisTM energy sources were tested. The VibroseisTM sweep frequencies used were 10 to 56, 16 to 72, 22 to 84, 32 to 96 and 38 to

104 hz. This profile simulated a standard walkway procedure (Sheriff, 1974) with the source moving away at selected increments from a stationary recording cable. Table 4 is a summary of the measured velocities, frequencies and wavelengths of the dominant noise patterns.

TABLE 4

NOISE RELATED PROPERTIES FOR THE INLINE SPREAD

<u>Noise Type</u>	<u>Velocity (ft/sec)</u>	<u>Frequency(hz.)</u>	<u>Wavelength(ft.)</u>
Groundroll	1640-2000	12-20	82-166
Direct	3170	20-35	91-159
Reflected	none observed	N/A	N/A
Refracted	none observed	N/A	N/A

CIRCULAR NOISE PROFILE

In addition to identifying the functions of noise in the line of profile a circular noise spread was used to identify noise patterns originating as reflected-refractions or broadside noise from hills, mountain ranges or man-made objects. It is ideal, therefore, in the Yucca Mountain area. This profile used concentric circular spreads (Brasel, 1979) with 32 stations at 10 foot spacing on the inner circle of 52 ft. radius and 64 stations at 10 foot spacing on the outer circle of 102 ft. radius (fig. 13). Each station consisted of 12 bunched geophones. The radii were chosen to effectively measure the smallest noise wavelength which may exist in this area. Source points (VP-1) began at the center of the circles and progressed outward in a straight line at 200 foot intervals. Several input sources were tested in

this study. Shotpoints 1-19 were recorded using VibroseisTM with 32-96 hz. sweeps. Shotpoints 1, 3, 6, 9, 12, 15, and 18 were recorded with both Vector PulseTM and VibroseisTM using sweep frequencies of 10 to 56, 16 to 72, 22 to 84, 38 to 104, 44 to 108 hz.

Table 5 displays the measured velocities, frequencies, and wavelengths of dominant noise patterns interpreted from offset distances of 400 to 2850 feet from the circular noise spreads.

TABLE 5

NOISE RELATED PROPERTIES FOR THE CIRCULAR SPREAD

<u>NOISE Type</u>	<u>Velocity(ft/sec)</u>	<u>Frequency(hz.)</u>	<u>Wavelength(ft.)</u>
Groundroll	1800	15-25	72-144
Direct	2100	20-50	65-156
Reflected	none observed	N/A	N/A
Refracted	none observed	N/A	N/A

ANALYSIS OF NOISE PROFILES

The final acquisition parameters for the three dimensional reflection survey were selected based upon the analysis of the properties observed in the noise profile data. The dominant noise recorded on both inline and circular noise spreads is groundroll and direct. The noise wavelength range observed for groundroll and direct noise is 65 to 166 feet. These wavelengths are well within the attenuation power of the combined source and receiver arrays discussed in a previous section (Figures 10 and 11).

Source frequency tests showed that of the five sweep frequencies tested (Figures 14 to 25), 16 to 72 and 22 to 84 hz. provided the least noise generation and best resolving power. The Vector PulseTM method generate sufficient resolving power but a large amount of coherent source noise.

In order to understand the relationship between noise distribution and reflection information, a signal and noise schematic was made (Figure 26) which graphically displays all noise distribution common to the Yucca Mountain vicinity. From this graph an offset dependent recording window for observing reflection information can be defined. Analysis of this schematic suggested that a window of 750-2000 feet be utilized if reflection information, for example from the base of the Topopah Spring Tuff, is to be observed. Any defined offset lying outside the perimeters of this window would be overwhelmed by shot generated noise.

THREE DIMENSIONAL PRODUCTION ACQUISITION PHASE

Initial production acquisition parameters were based on results of the noise studies and existing terrain limitations. Three dimensional grids (Figure 27) were designed which employed 96 recording channels and an optimum offset recording window.

Line W-4 (Figure 1) was recorded initially with an 8 x 12 three dimensional receiver array grid consisting of 105 foot station intervals and 800 to 1900 foot receiver offsets. A weighted receiver array of 96 geophones spaced at 15 feet over pattern length of 210 feet, was used. A source array of 3 vibrators sweeping 18 times at a spacing of 12.5 feet and a pattern length of 156 feet was utilized. The initial sweep was 10 to 56 hz. which due to mechanical difficulties caused decoupling effects. The sweep was later

changed to 16 to 62 hz. which eliminated these effects. Due to excessive mechanical failures, VibroseisTM activity was temporarily halted and a Vector PulseTM source array of 11 elements spaced at 9 feet was employed. VibroseisTM was once again employed until mechanical failures forced the use of Vector PulseTM until termination of the project. Because of operational equipment problems and the decision to attempt to record reflections from the beds lying less than 500 feet deep, lines S-2, and S-4 were recorded using different source and receiver arrays. The source array consisted of 7 Vector PulseTM elements spaced at 16 feet while the receiver array was shifted to a linear pattern of 12 geophones spaced at 9 feet. The three dimensional grid was also changed to a 6 x 16 grid (Figure 27) employing 50 foot station intervals.

Line G-2 which is located along one of the ridges was recorded with a different source and receiver array. The source consisted of 10 pounds of dynamite detonated in 200 foot deep holes and was recorded by receiver arrays of 96 geophones spaced at 15 feet with a total pattern length of 210 feet. The three dimensional grid was changed to a 4 x 24 grid (Figure 27) employing 100 foot station intervals.

THREE DIMENSIONAL DATA PROCESSING METHODS

All of the three-dimensional data were processed by SIRC. Western Geophysical was also contracted to process line S-4 as a quality control check.

SIRC's data processing began with a standard demultiplex and VibroseisTM cross-correlation. Raw records were plotted for editing and shooting pattern review. Geometry is coded and placed in the trace headers assigning each

record trace to it's respective common depth point within the 3-D grid. Several tests were performed on the data at this stage which included: filter tests, autocorrelations, power spectra, deconvolution tests and scaling tests. These test results were analyzed for optimum processing parameters. The data were then filtered with a 10 to 30 hz. operator. Constant velocity stacks were run on the data to provide accurate normal moveout corrections. SIRC elected not to apply automatic residual statics because tests concluded that no apparent reflection information was present for the automatic static picking technique to function properly. The data were stacked in many different configurations (figures 28 to 30) to seek any relevant reflection information. SIRC chose for their final presentation, a stacking configuration that would produce the highest stack fold for each common depth point (figures 31 to 34). The data were filtered with a 10 to 36 hz. operator and scaled with automatic gain control. Western Geophysical, however, elected to apply automatic residual statics and for their final presentation chose to break up line S-4 into 11 CDP lines each consisting of 48 stack fold. Each company produced final CDP stacks that contained no interpretable reflection information. Horizontal time slices were produced by both companies during their data processing efforts, which are discussed in the following section.

SIRC 3-D TIME SLICE DISPLAYS

Seismic reflection surveys are usually displayed as vertical two dimensional profiles that exhibit subsurface strike and dip information. In order to acquire an accurate description of this subsurface information, numerous 2-D reflection profiles must be interpreted. Because 2-D profiles usually offer a coarse sampling of the subsurface, there is a great potential

for error. In contrast, a 3-D reflection survey consists of a dense concentration of common depth points distributed over a 3-dimensional grid which provides time planes (Horizontal time slices) common to all depth points (Brown et al, 1982). Subsurface reflection information can be accurately interpreted by observing dip and strike changes with respect to time. Thus, the 3-D grid offers a very fine sampling of the subsurface while a two dimensional grid offers a very coarse sampling of the subsurface. By decomposing the subsurface into small time increments, the interpreter can accurately judge the size and shape of a subsurface geologic structure. However, the poor reflection data in the Yucca Mountain area, produced no interpretable results from the horizontal time slices. Figure 35 represents time slices produced by SIRC. These time slices range from .370 to .480 seconds and are color coded for amplitude strength. In hypothetical terms, a time slice cut through a very strong reflection would be color coded black, and as the reflection strength (amplitude) changes the shade would change. If a reflection event dips from northeast to southwest, corresponding time slices would be color coded black as they intersect the dipping event; therefore, if a black color exists for time slice at .370 seconds at the northeast end of a line, the same color would appear at a time at .480 seconds at the southwest end of a line. This would infer the dip of the strong reflecting event. As figure 35 shows this survey produced no interpretable time slice data.

RECOMMENDATIONS

Subsurface Inc. has reviewed in depth all seismic reflection surveys recorded in the Yucca Mountain region. It is conclusive that useful seismic reflection data cannot be acquired in this area even using the elaborate techniques outlined in this report. The seismic reflection method was developed and has been employed primarily in sedimentary rock environments. Rugged volcanic areas such as Yucca Mountain are not well suited to the seismic reflection technique. Many powerful noise suppression techniques were tested in this survey with none of these techniques producing useful reflection information. Additional seismic reflection studies will undoubtedly produce negative results and Subsurface Inc. discourages any additional seismic reflection surveys in the Yucca Mountain complex.

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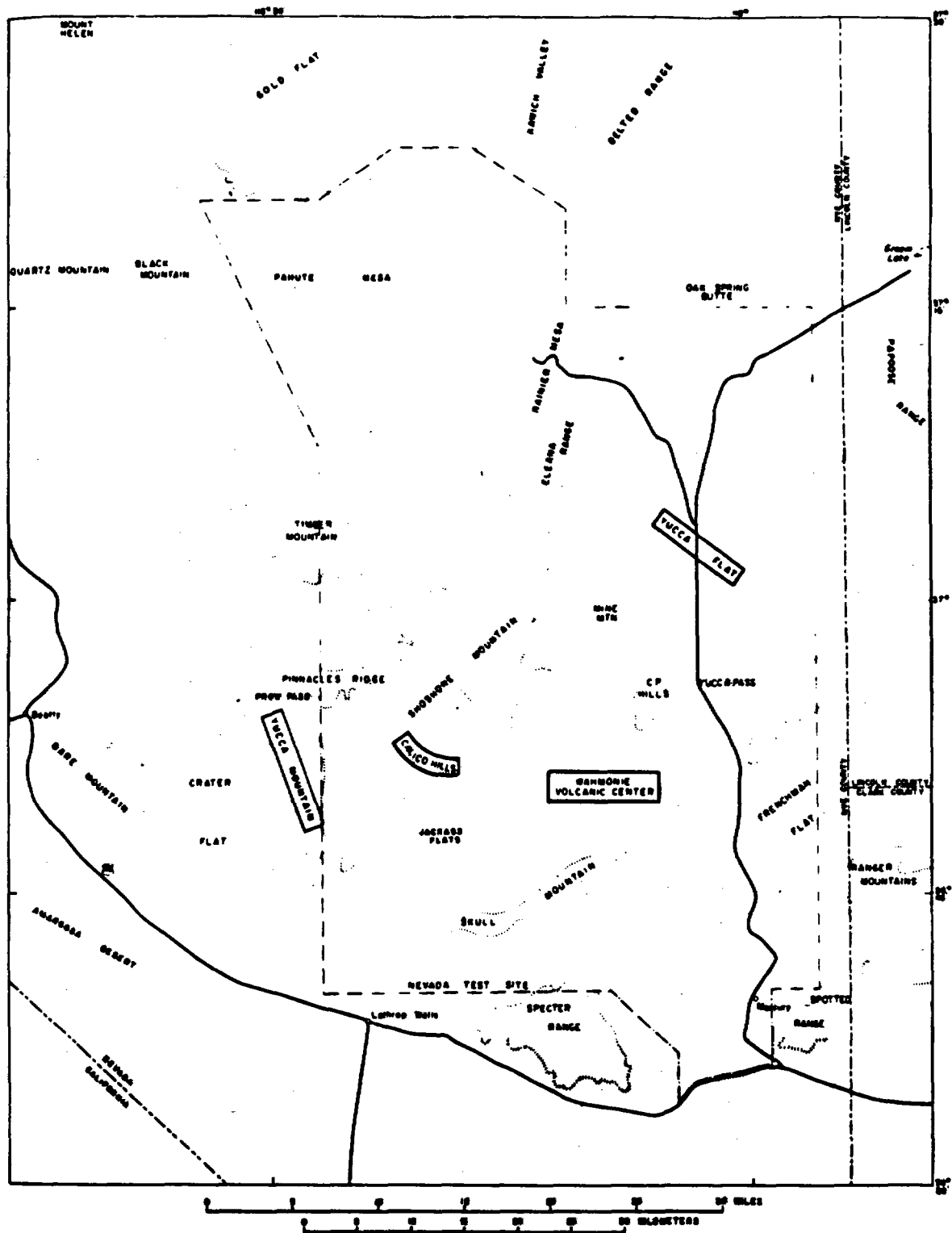
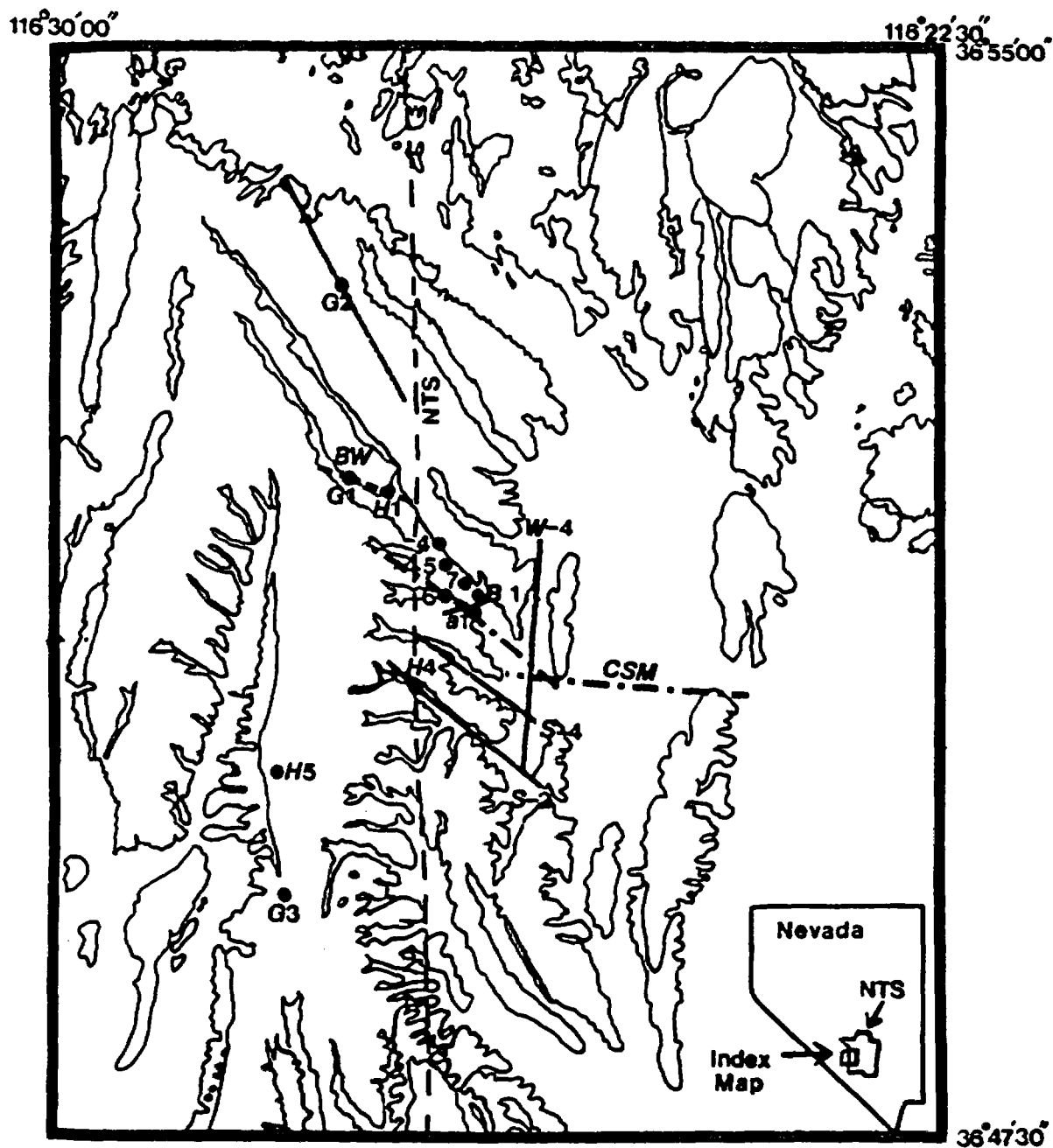


Figure 1.-- Index map of the Nevada Test Site and vicinity showing the areas of investigation

Figure 1A



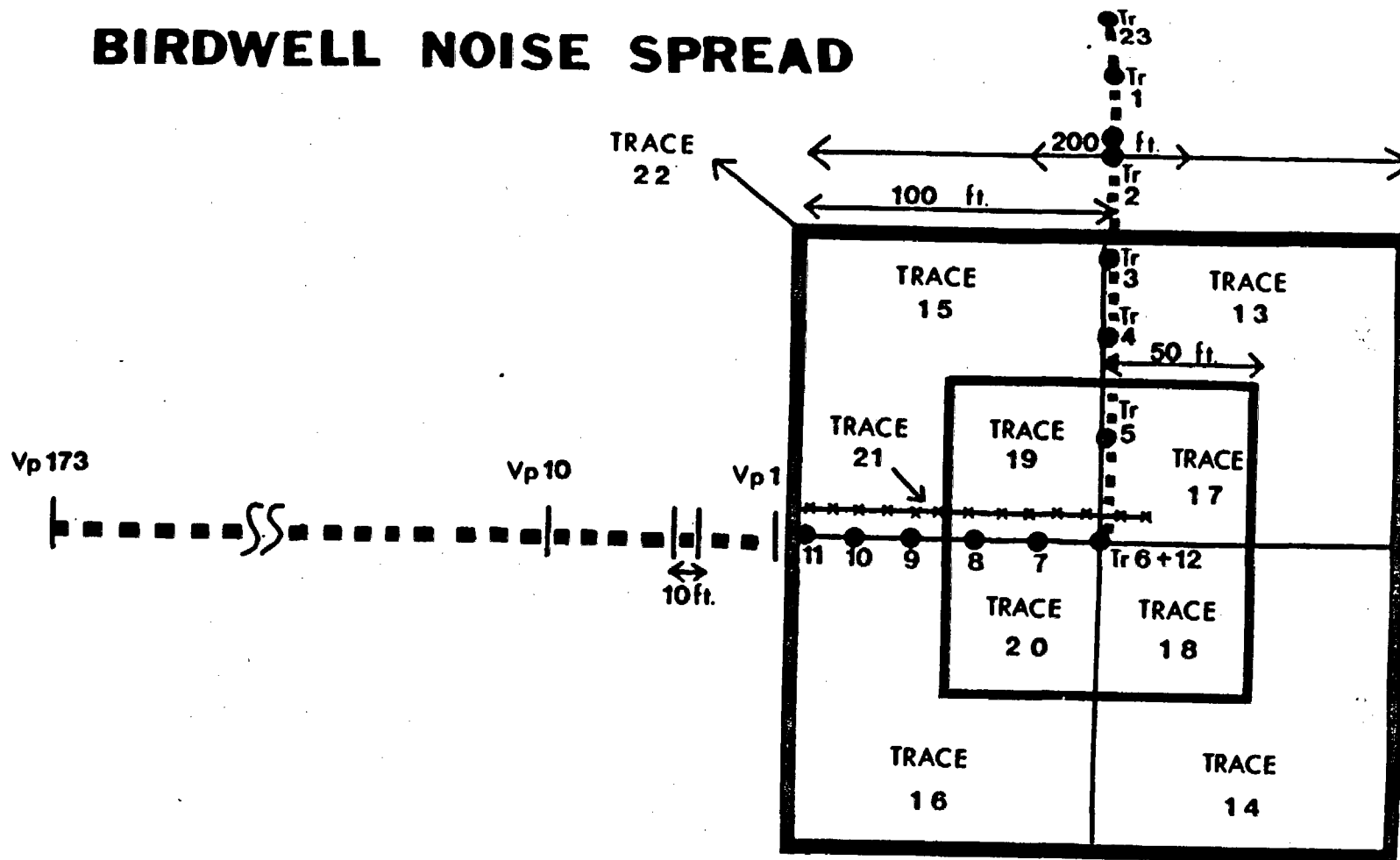
1 0 1 mile
1 0 1 kilometer

Yucca Mountain Index Map

LEGEND

- - SSI/SIRC
- . - CSM
- - - BIRDWELL

BIRDWELL NOISE SPREAD

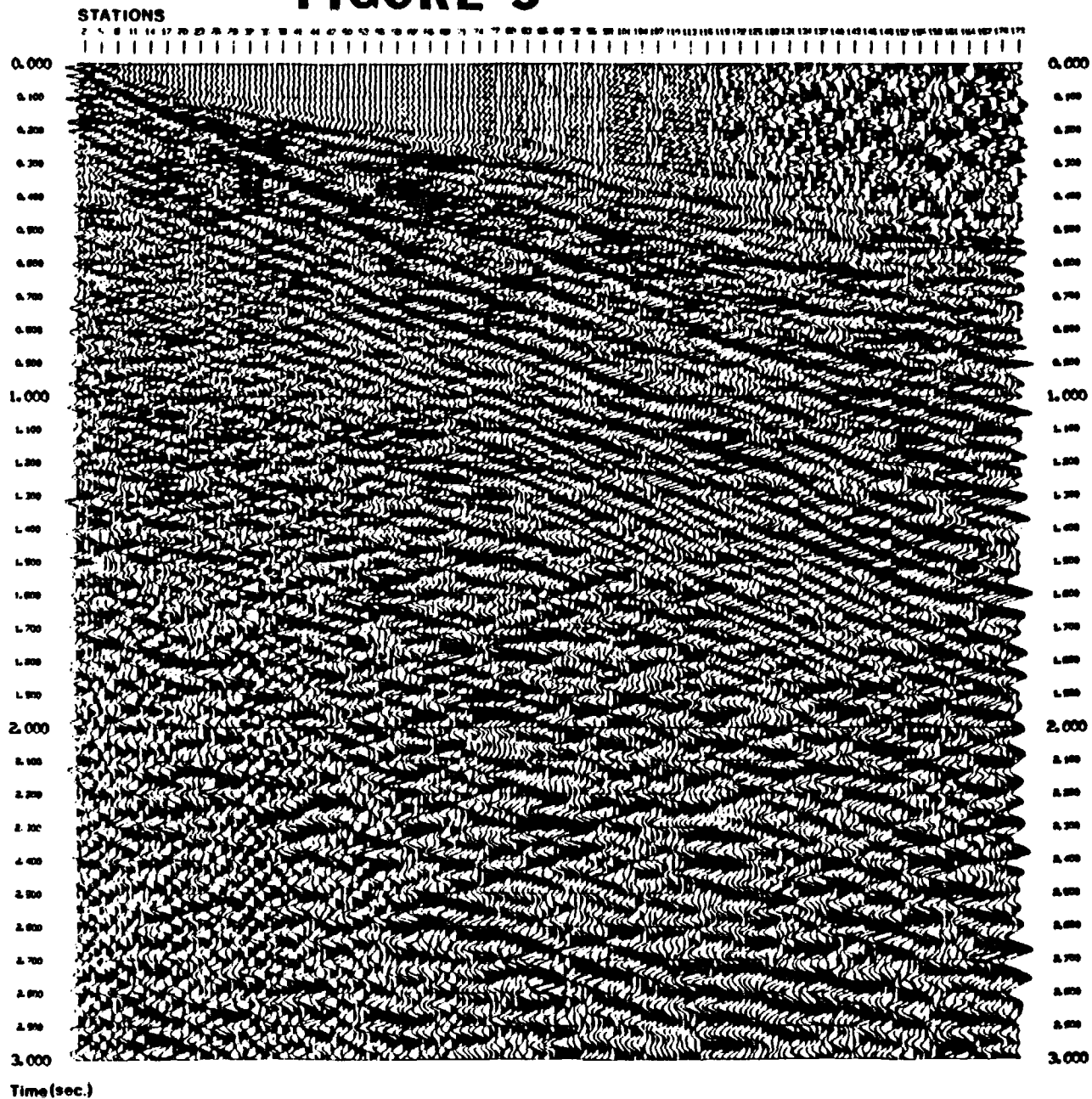


25

- Trace 22 (200 x 200 ft. grid 144 geophones)
- Traces 23, 1-6 (Form perpendicular part of L spread bunched group of 6 geophones 30 ft. apart)
- Traces 6-11 (In line part of L spread bunched group of 6 geophones 20 ft. apart)
- Trace 12 (Bunched group of 6 geophones)
- Traces 13-16 (Consist of a 100 x 100 ft. grid 144 geophones each)
- Traces 17-20 (Consist of a 50 x 50 ft. grid 144 geophones each)
- Trace 21 (Array of 12 clustered geophones covering 105 ft)

figure 2

FIGURE 3



BIRDWELL FIELD RECORD

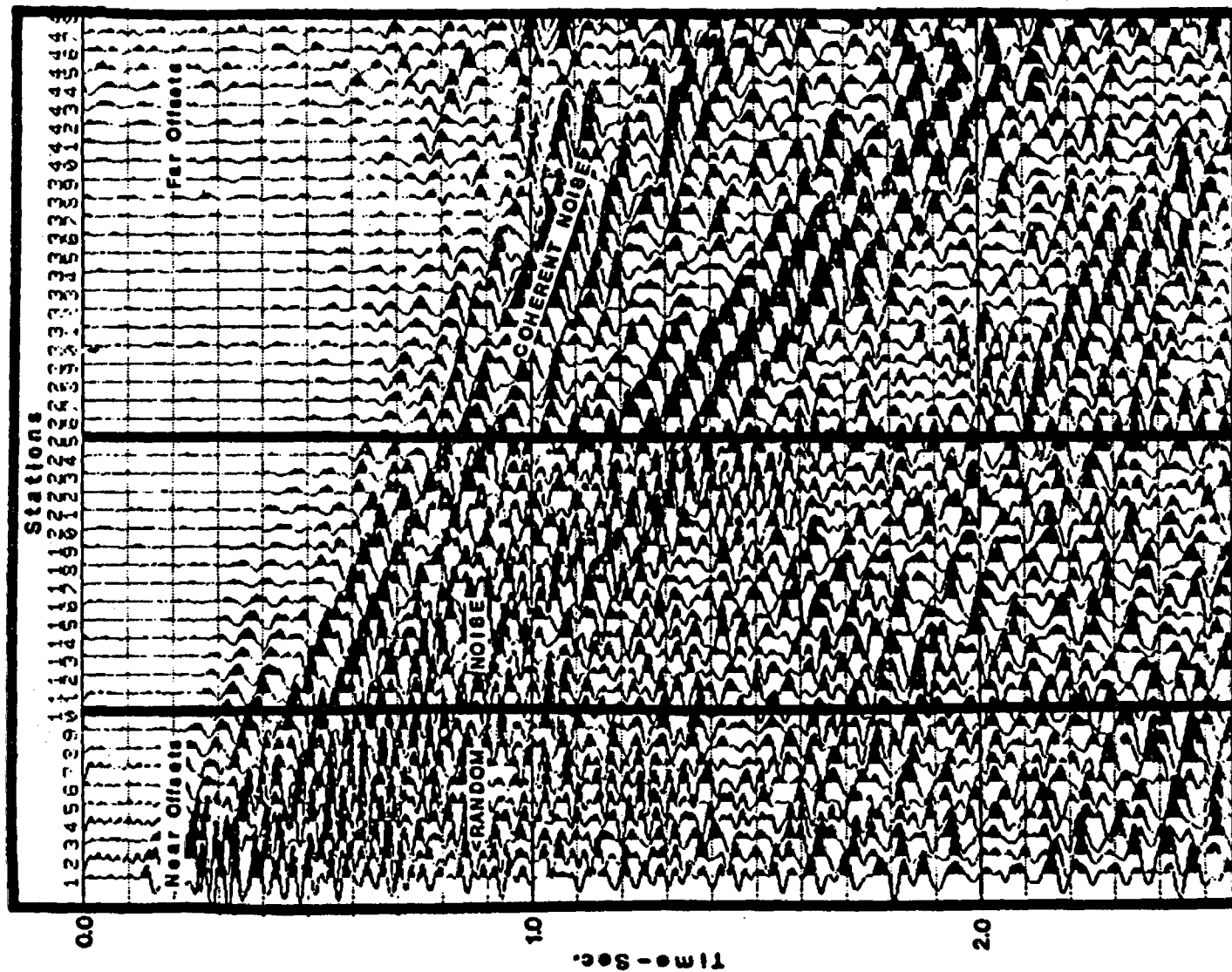


figure 4

Normal Moveout Stack

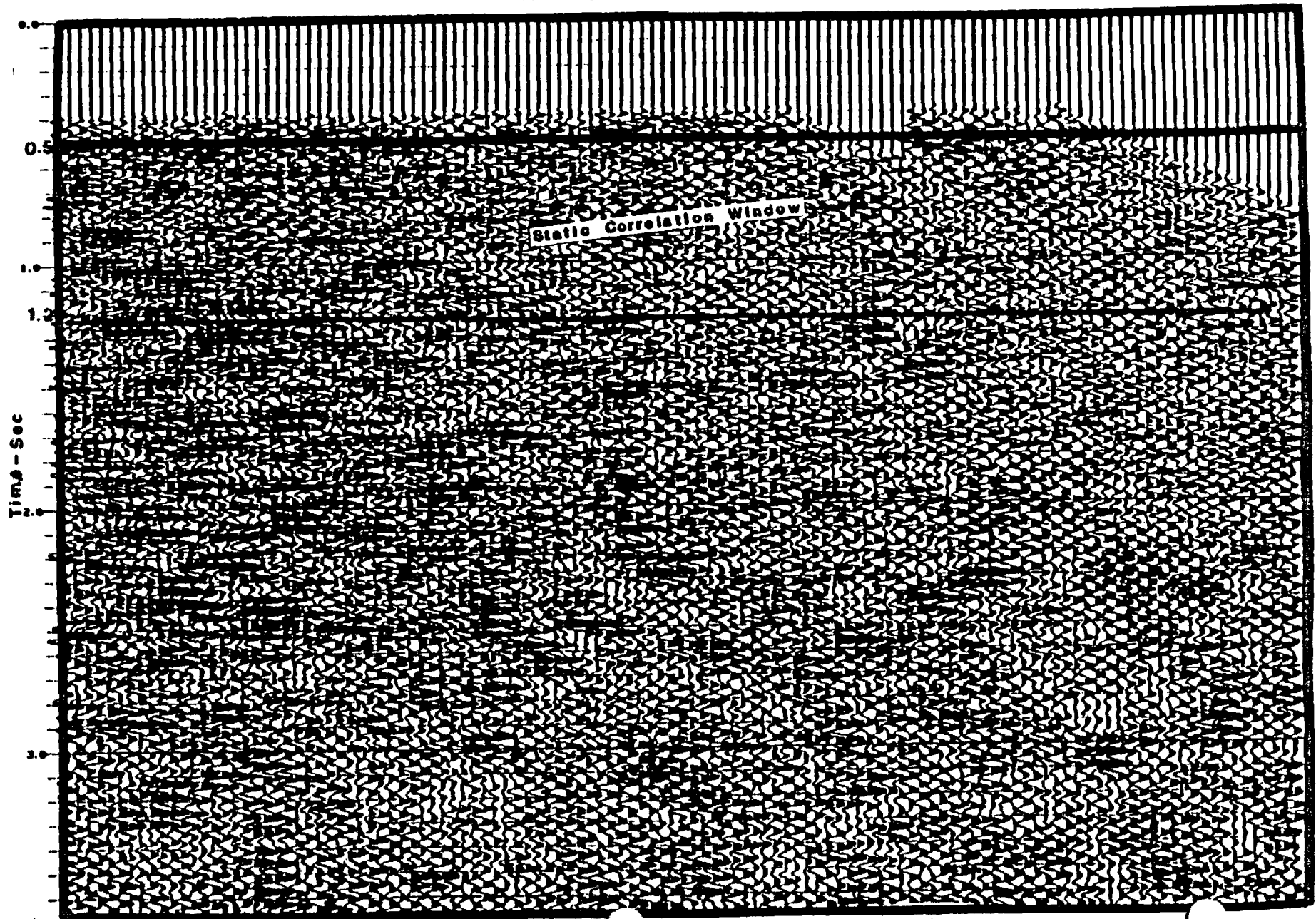


figure 5

BIRDWELL SSC

Automatic Statics Stack

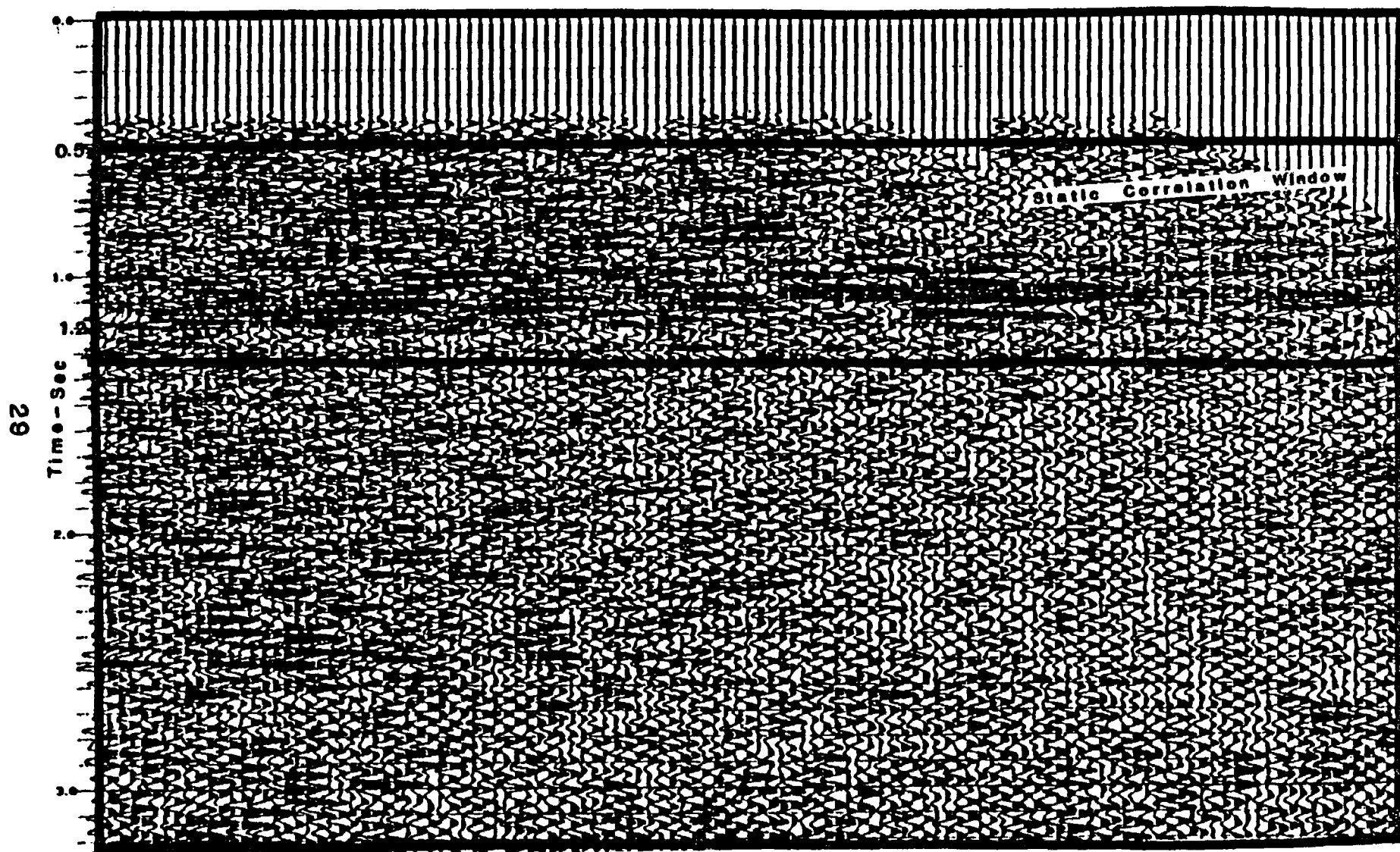


figure 6

BIRDWELL SSC

Velocity Filter Mute Stack

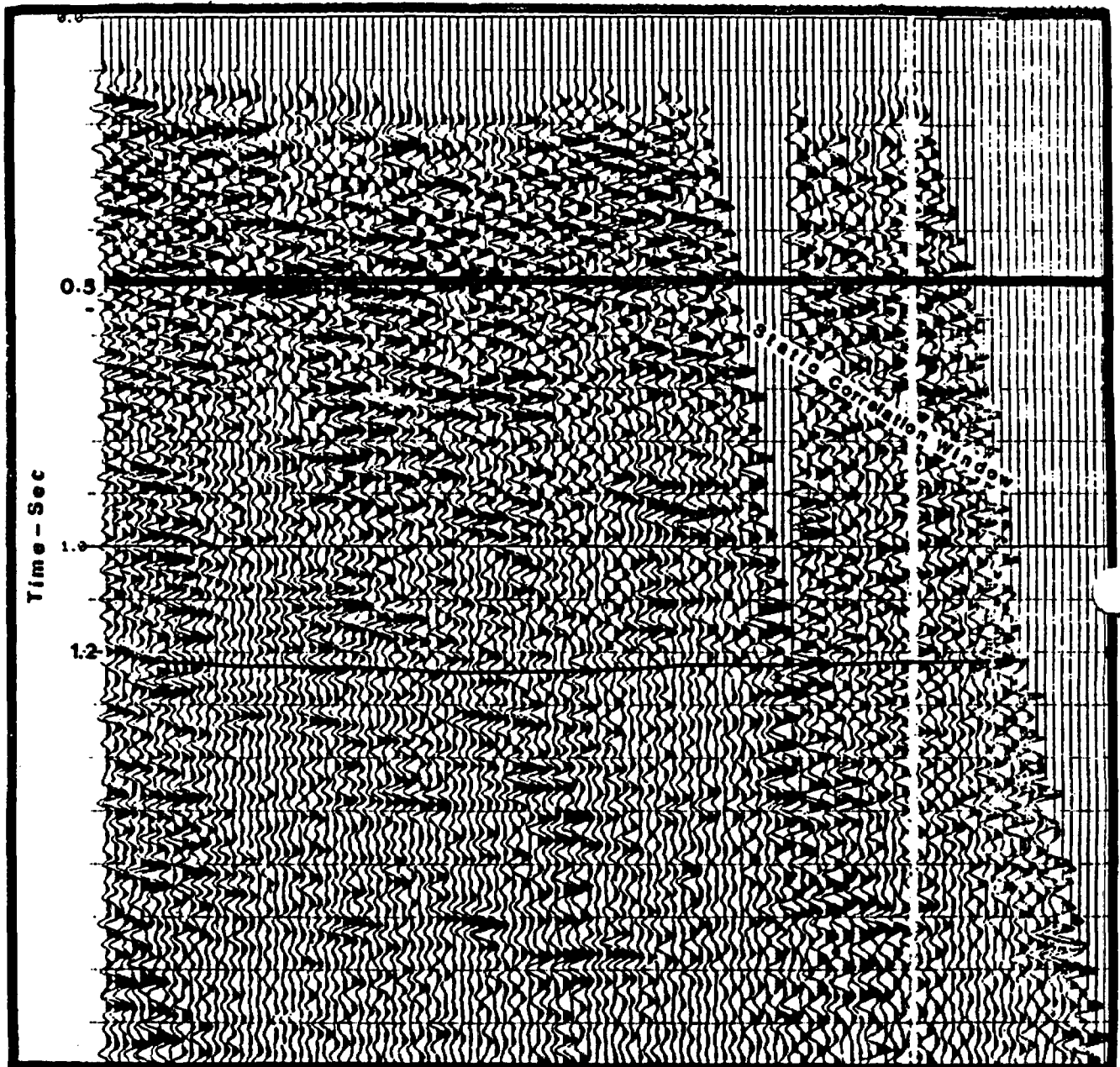


figure 7

ATTENUATION (DB)

WAVE LENGTH

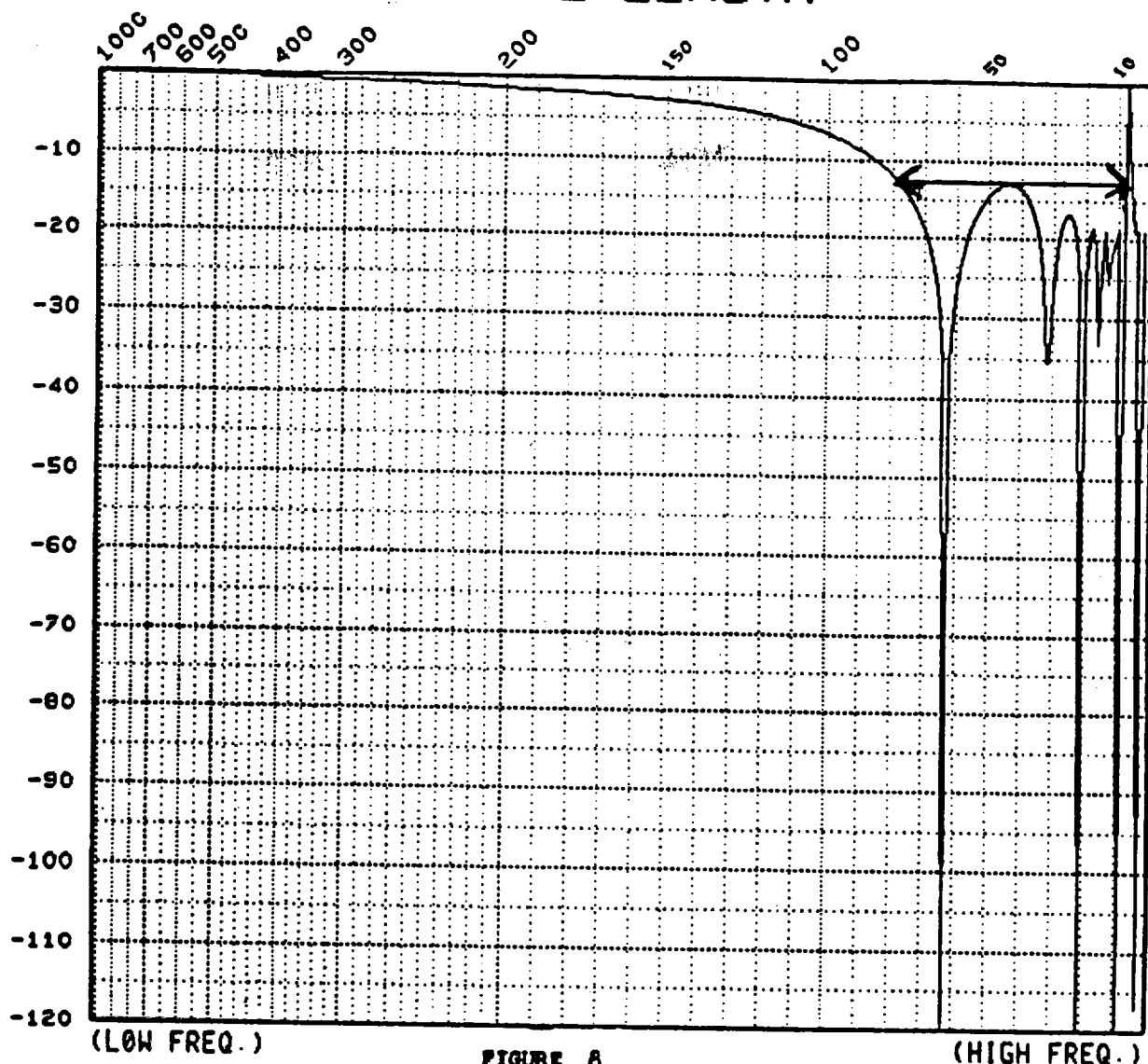


FIGURE 8

SPACING	7
LENGTH	56
WEIGHTS	1 1 1 1 1 1 1 1

POINTS	9
ELEMENTS	9

SPACING	55
LENGTH	0
WEIGHTS	1

POINTS	1
ELEMENTS	1

S/N IMPROVEMENT
(AMBIENT NOISE ATTENUATION POWER) 23 03 DB

The COLORADO SCHOOL of MINES COMBINED FIELD TECHNIQUE

TOTAL FIELD EFFORT 12DB FOR BAND 10 TO 70

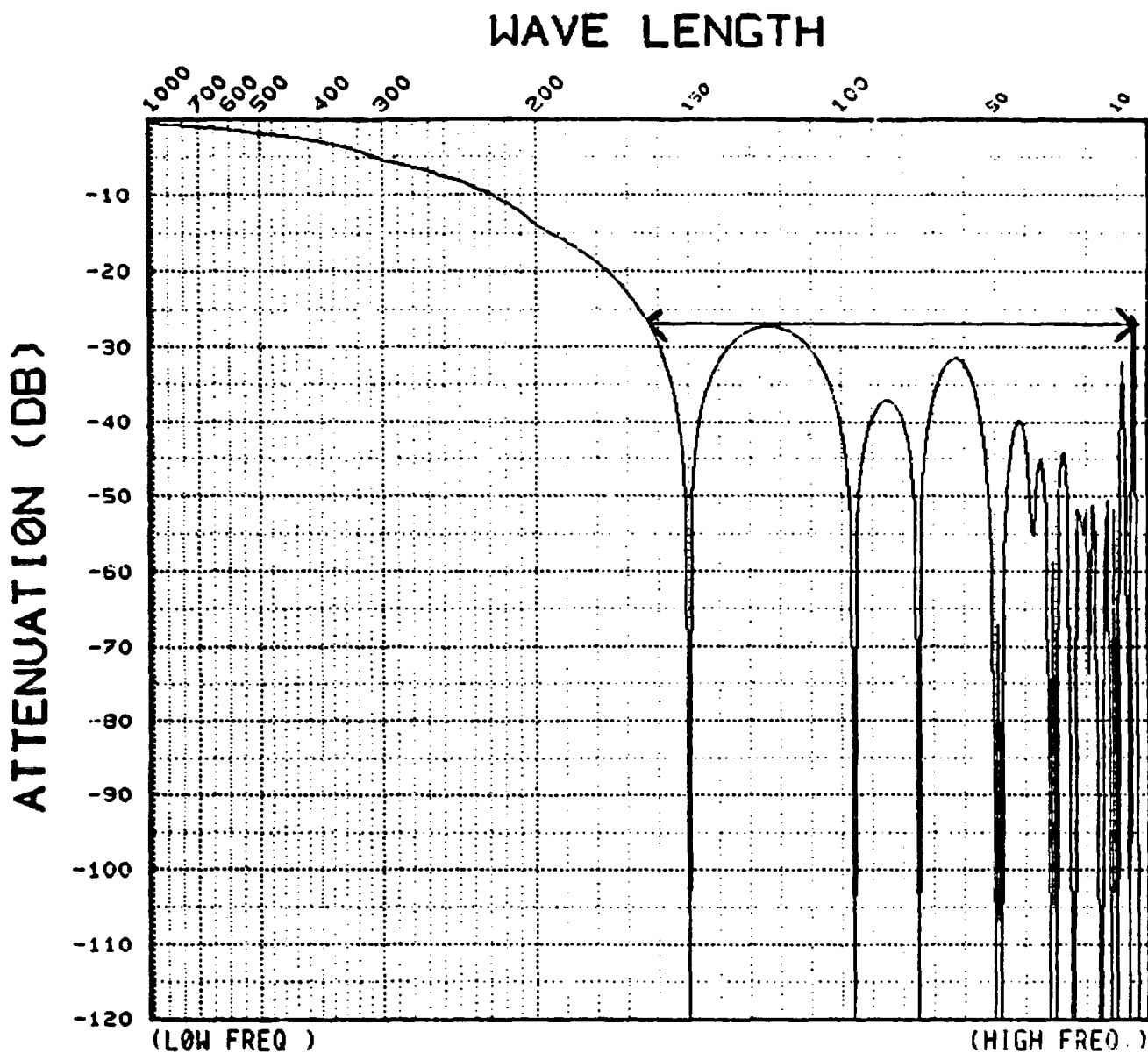


FIGURE 9

SPACING	5	POINTS	30
LENGTH	145	ELEMENTS	30
WEIGHTS	1 1		

SPACING	8	POINTS	12
LENGTH	88	ELEMENTS	12
WEIGHTS	1 1		

S/N IMPROVEMENT
(AMBIENT NOISE ATTENUATION POWER) 37 38 DB

BIRDWELL COMBINED FIELD TECHNIQUE

TOTAL FIELD EFFORT 29 DB FOR BAND 12 TO 160.

ATTENUATION (DB)

WAVE LENGTH

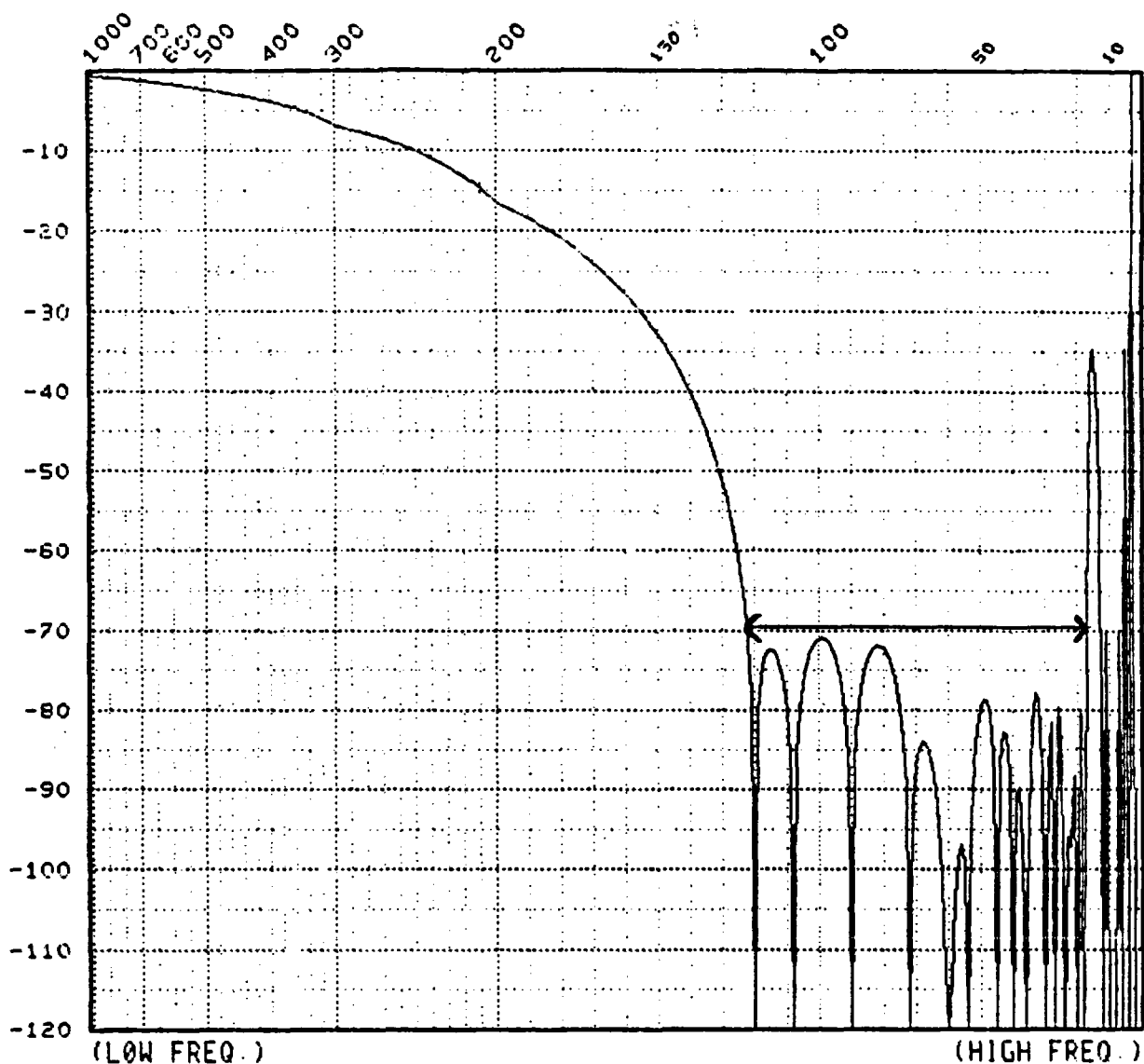


FIGURE 10

SPACING	12	POINTS	14
LENGTH	156	ELEMENTS	54
WEIGHTS	1 2 3 4 5 6 6 6 6 5 4 3 2 1		

SPACING	15	POINTS	15
LENGTH	210	ELEMENTS	96
WEIGHTS	1 2 4 6 8 10 11 12 11 10 8 6 4 2 1		

S/N IMPROVEMENT (AMBIENT NOISE ATTENUATION POWER) 30 35 DB

SEISMIC INTERNATIONAL RESEARCH/SEISDATA SERVICES COMBINED FIELD TECHNIQUE

(VIBRATOR SOURCE)
TOTAL FIELD EFFORT 68 DB FOR BAND 18 T0122

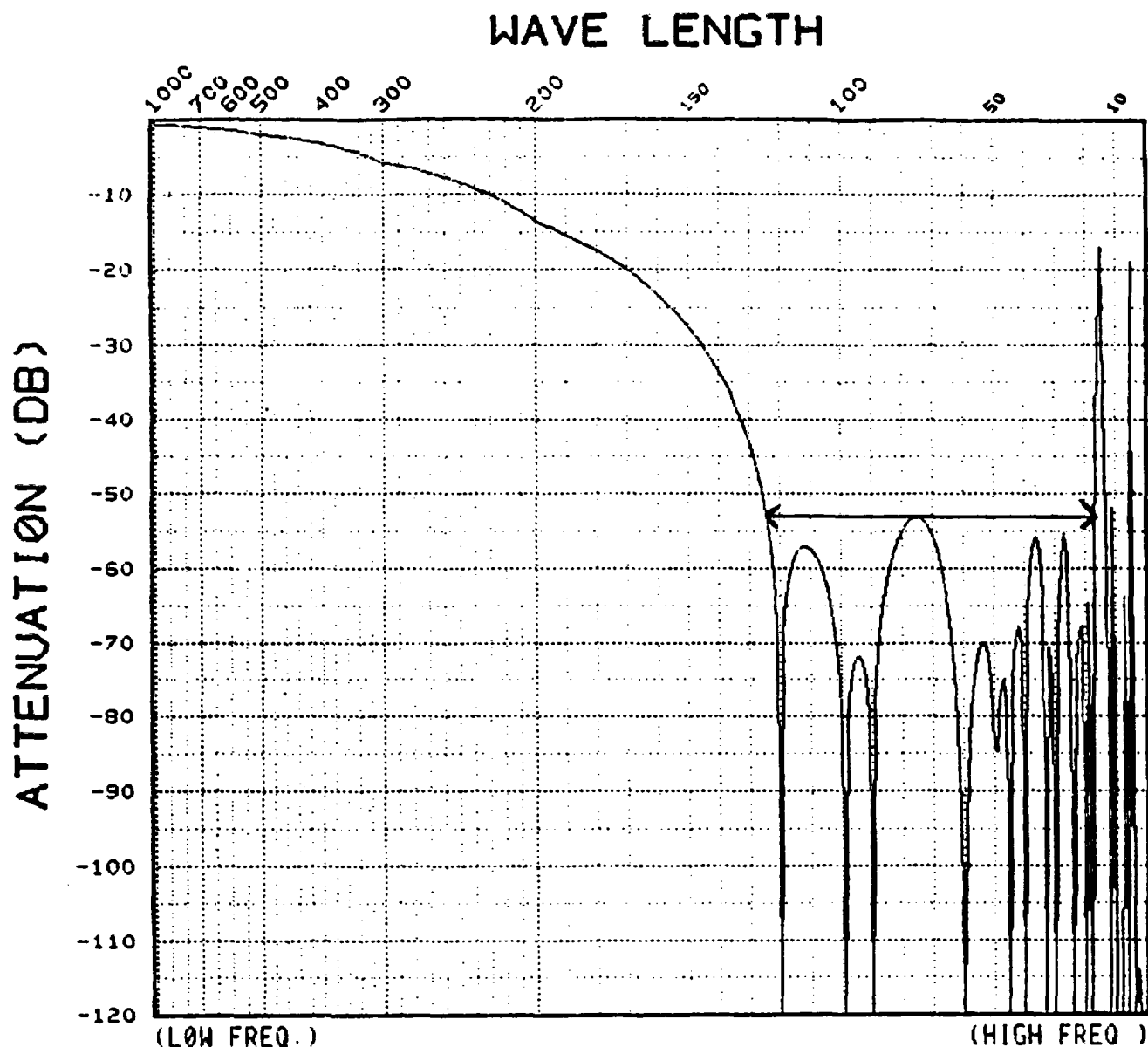


FIGURE 11

SPACING	9	POINTS	11
LENGTH	88	ELEMENTS	11
WEIGHTS	1 1 1 1 1 1 1 1 1 1 1		

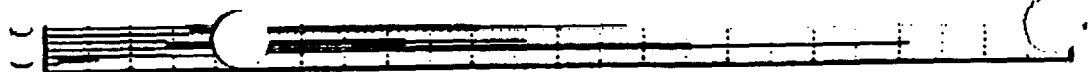
SPACING	15	POINTS	15
LENGTH	210	ELEMENTS	96
WEIGHTS	1 2 4 6 8 10 11 12 11 10 8 6 4 2 1		

S/N IMPROVEMENT (AMBIENT NOISE ATTENUATION POWER) 25 78 DB

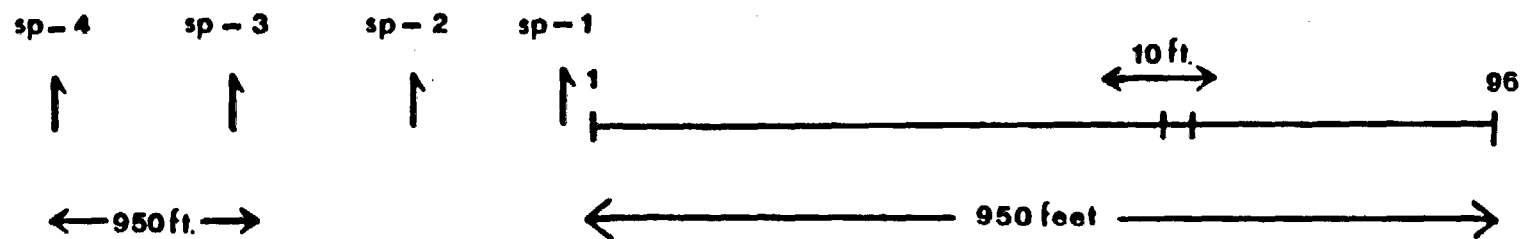
SEISMIC INTERNATIONAL RESEARCH/SEISDATA SERVICES COMBINED FIELD TECHNIQUE

(PRIMACORD SOURCE)

TOTAL FIELD EFFORT 53 DB FOR BAND 18 TO 122



In Line Noise Spread Configuration



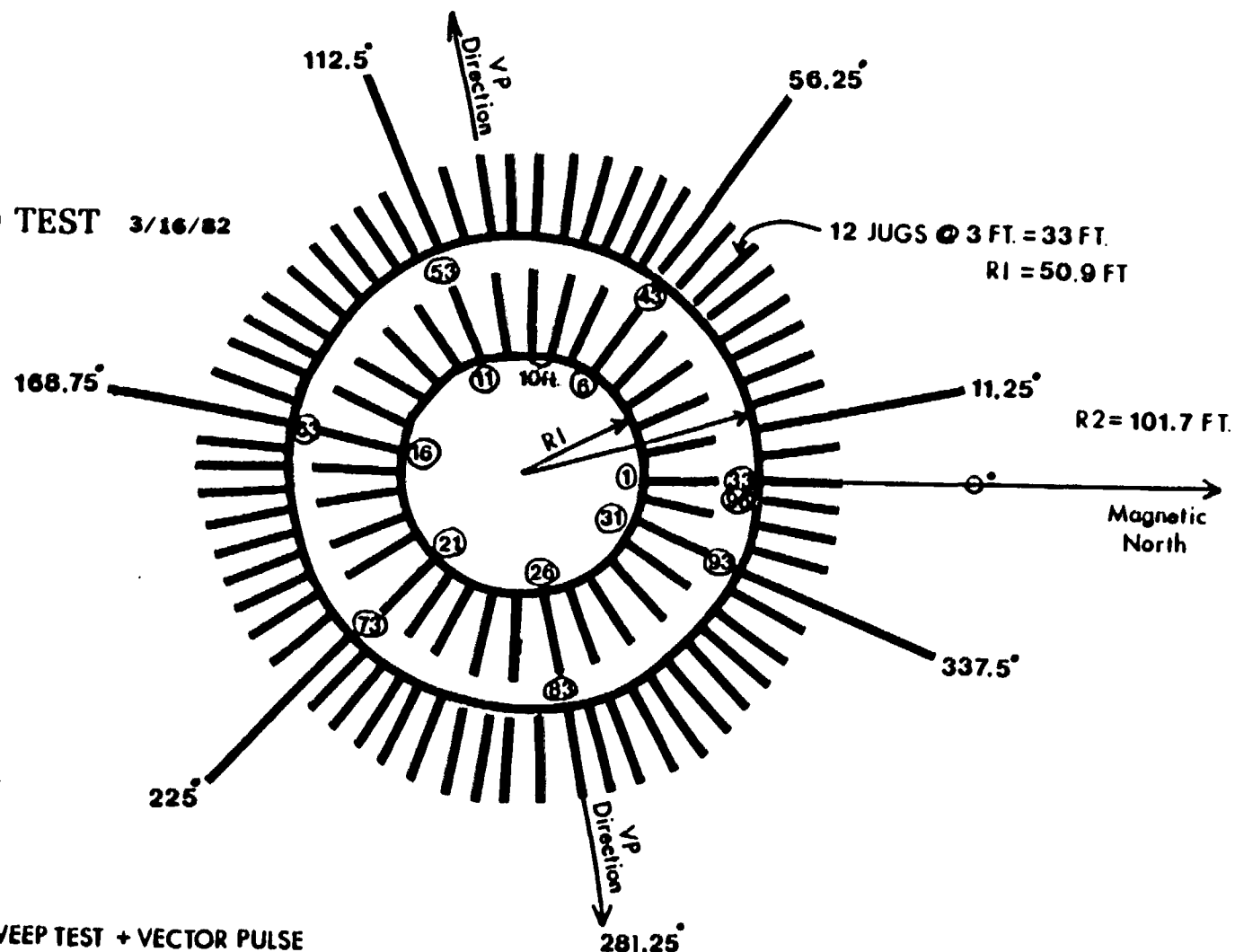
96 Recording stations @ 10 feet

12 Bunched geophones per station

Shot points separated by 950 feet

figure 12

TORNADO TEST 3/16/82



* = FULL SWEEP TEST + VECTOR PULSE

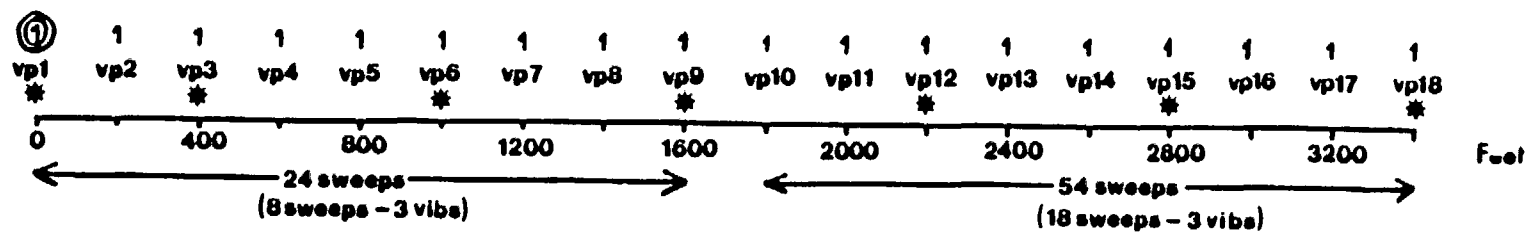


Figure 13

← 24 sweeps
(8 sweeps - 3 vib)

← 18 sweeps
(18 sweeps - 3 vib)

Figure 13

DEPT OF ENERGY FENIX & SCISSON

U S G S

YUCCA MOUNTAIN AREA
NEVADA TEST SITE - THE COUNTY, NEVADA

IN LINE 100000 100000

FIELD ACQUISITION
BY SFI-DATA SERVICES INC. FORM 003 APRIL 1982
96 CHANNEL 005-10 INSTRUMENTS 4 SECONDS 2 MS
LOW LUT FILE 0.1 HIGH LUT FILE 0.2
96 STATIONS AT 1000 INTERVALS THE DRIVE SPREAD
12 100000 100000 100000 100000

SP-101 SP-102 200 PRIMALED AT 400 DEPTH 6 HOLE
SP-103 SP-104 200 PRIMALED AT 400 DEPTH 12 HOLE

RECORD 1 0 SP 101 10 FEET TO 960 FEET OFFSET
RECORD 2 0 SP 102 970 FEET TO 1970 FEET OFFSET
RECORD 3 0 SP 103 1980 FEET TO 2980 FEET OFFSET
RECORD 4 0 SP 104 2990 FEET TO 3990 FEET OFFSET

TIME · SEC

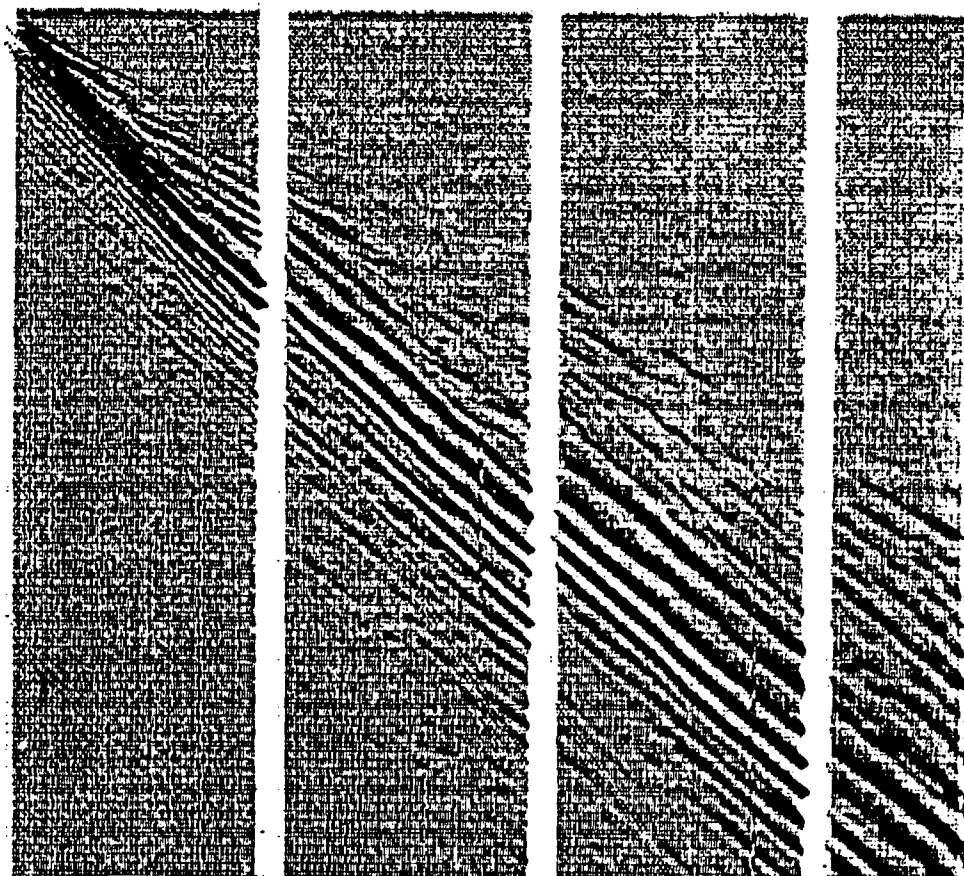


FIGURE 14

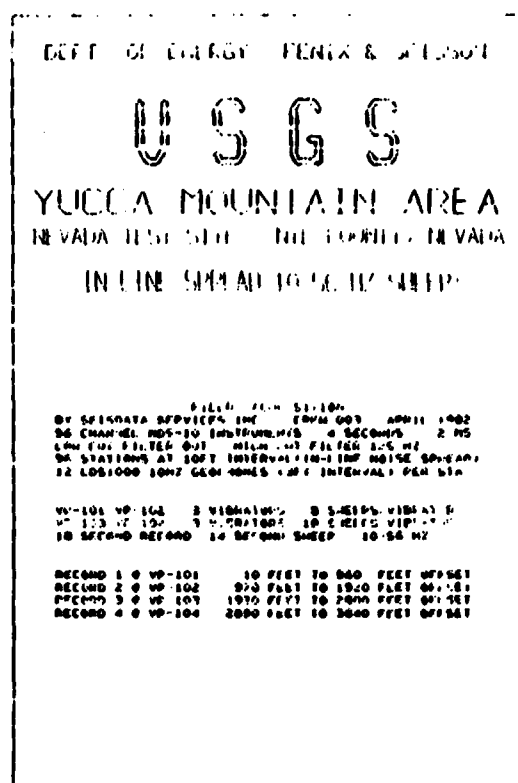
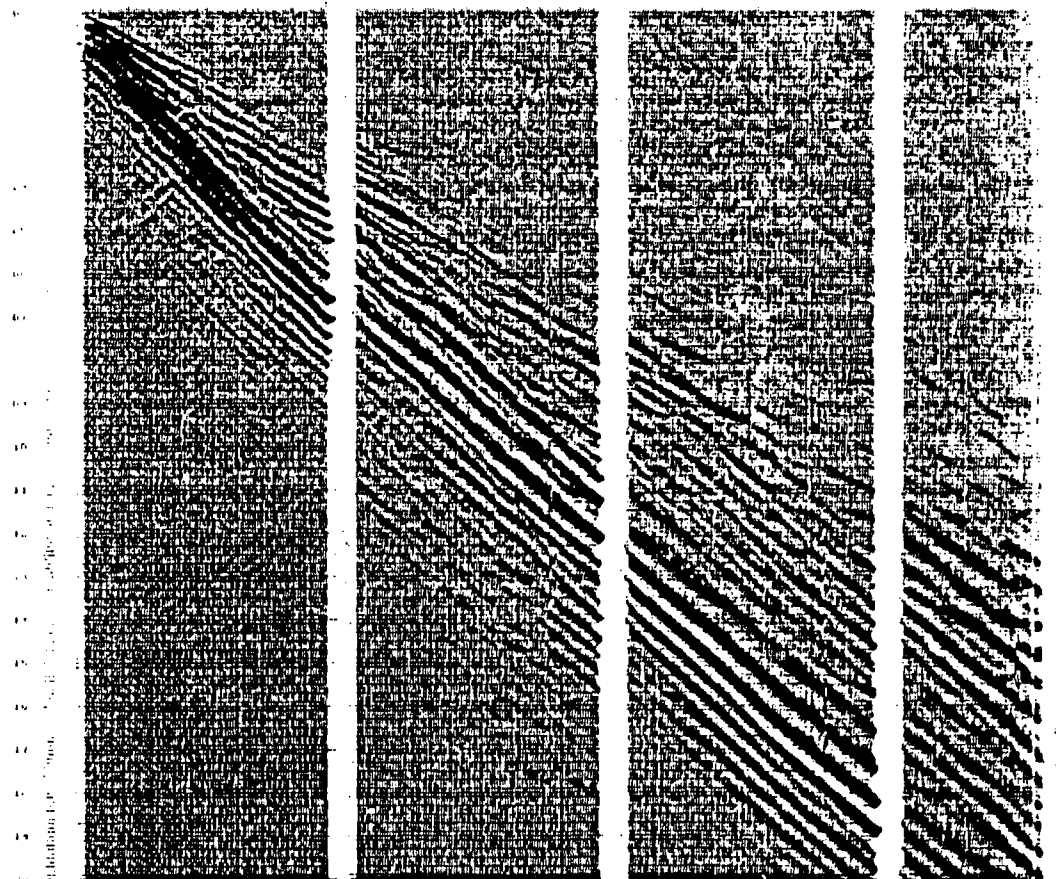


FIGURE 15

TIME-SEC



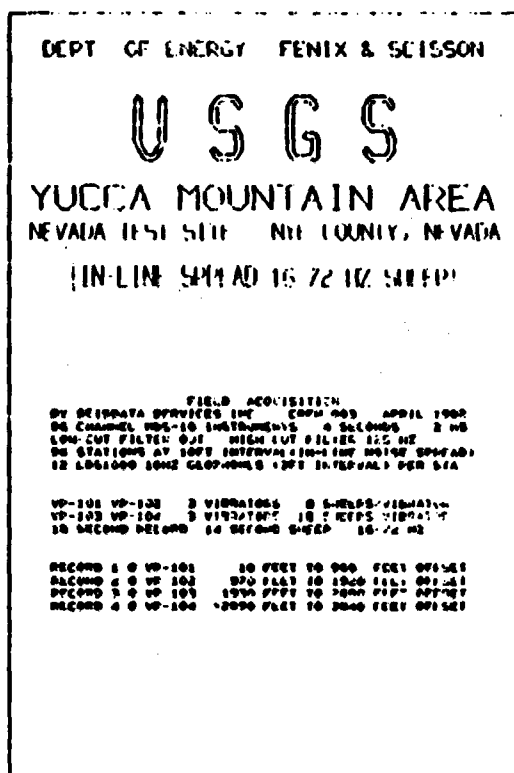
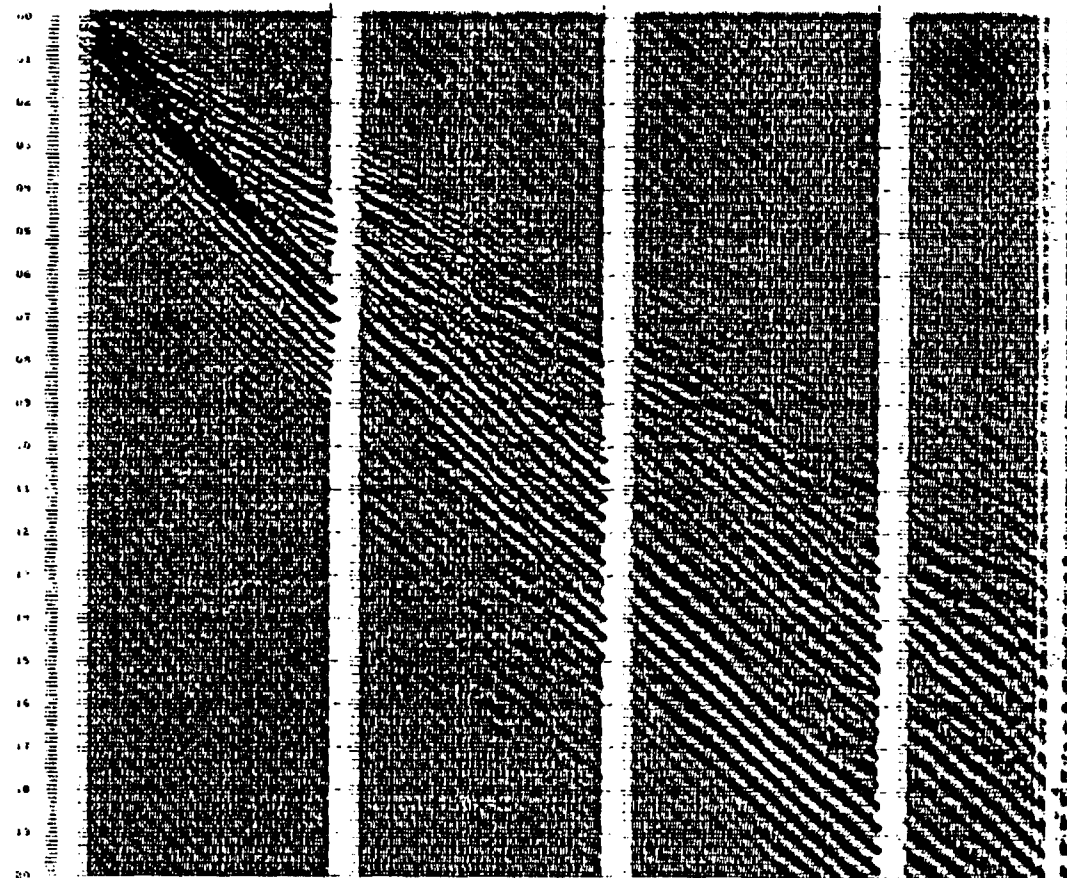


FIGURE 16

TIME · SEC



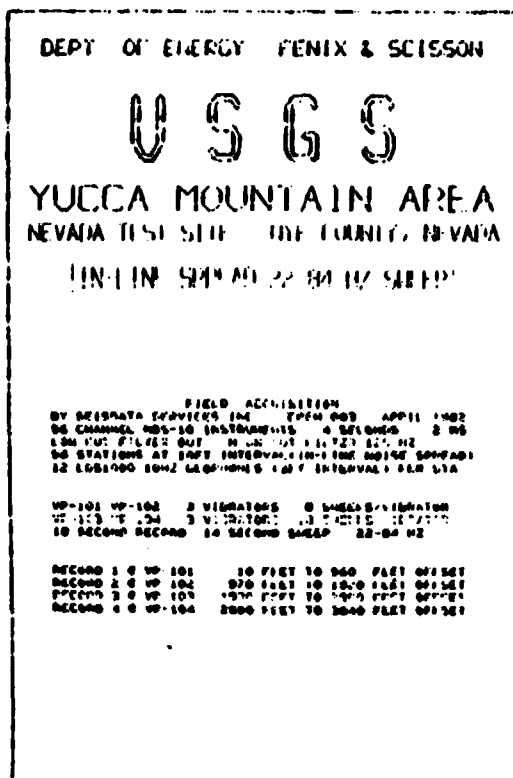
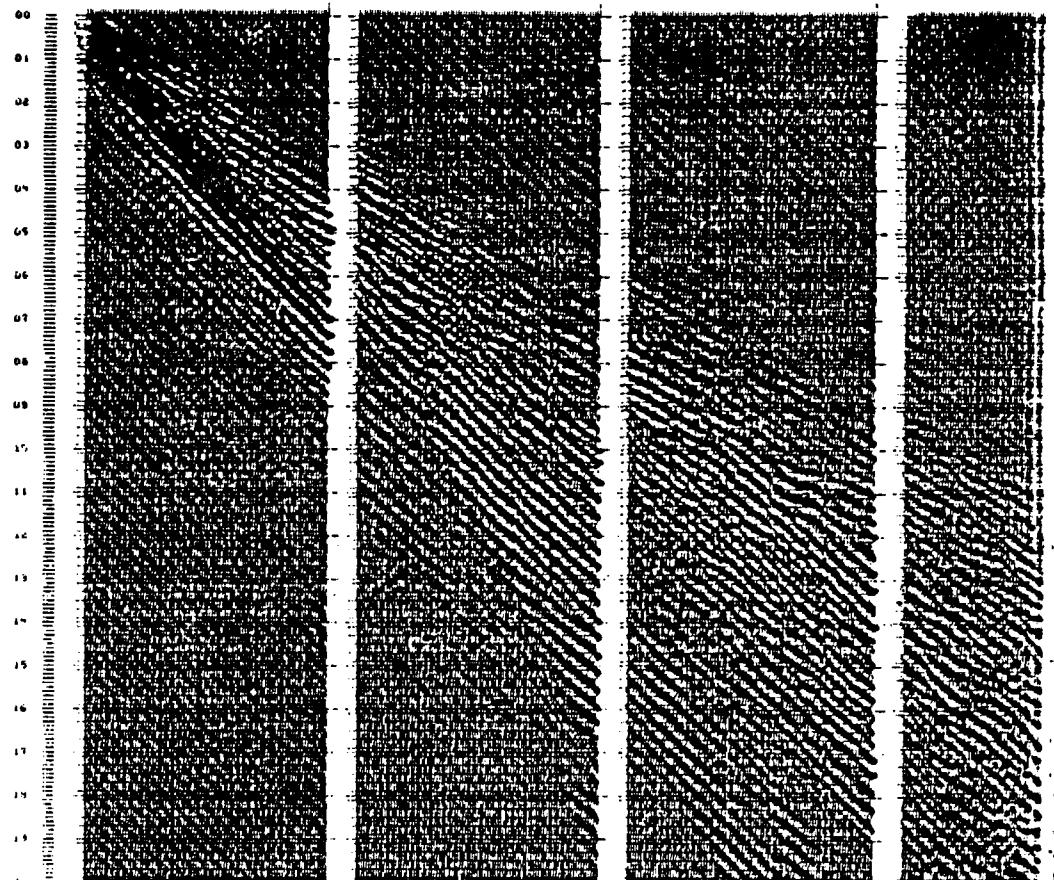


FIGURE 17

TIME-SEC



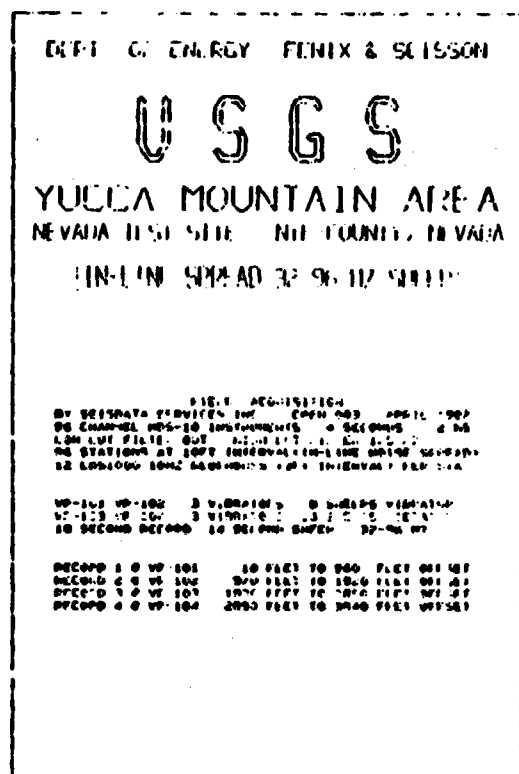
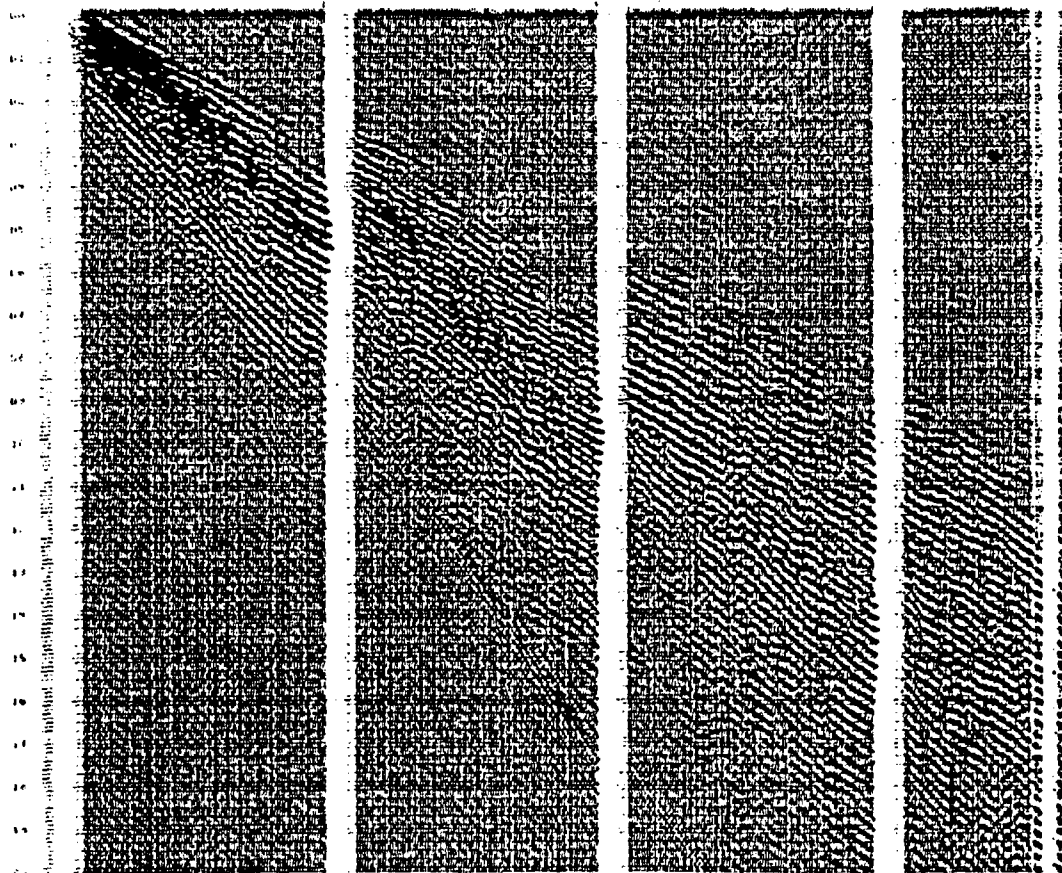


FIGURE 18

TIME-SEC



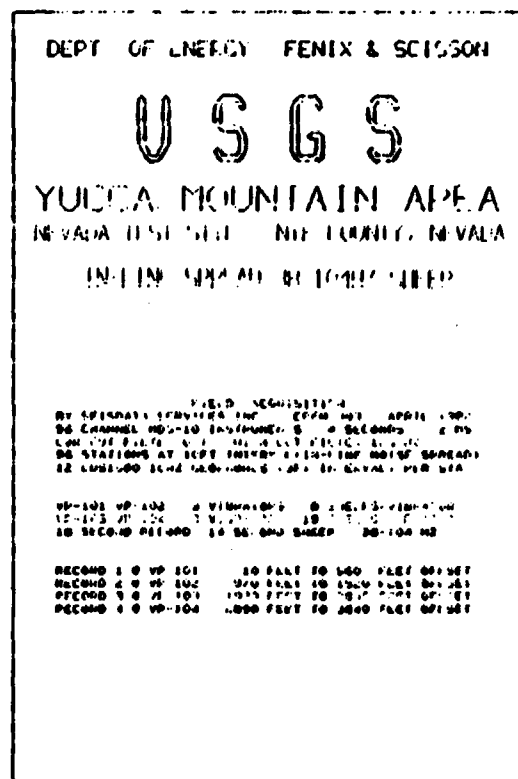
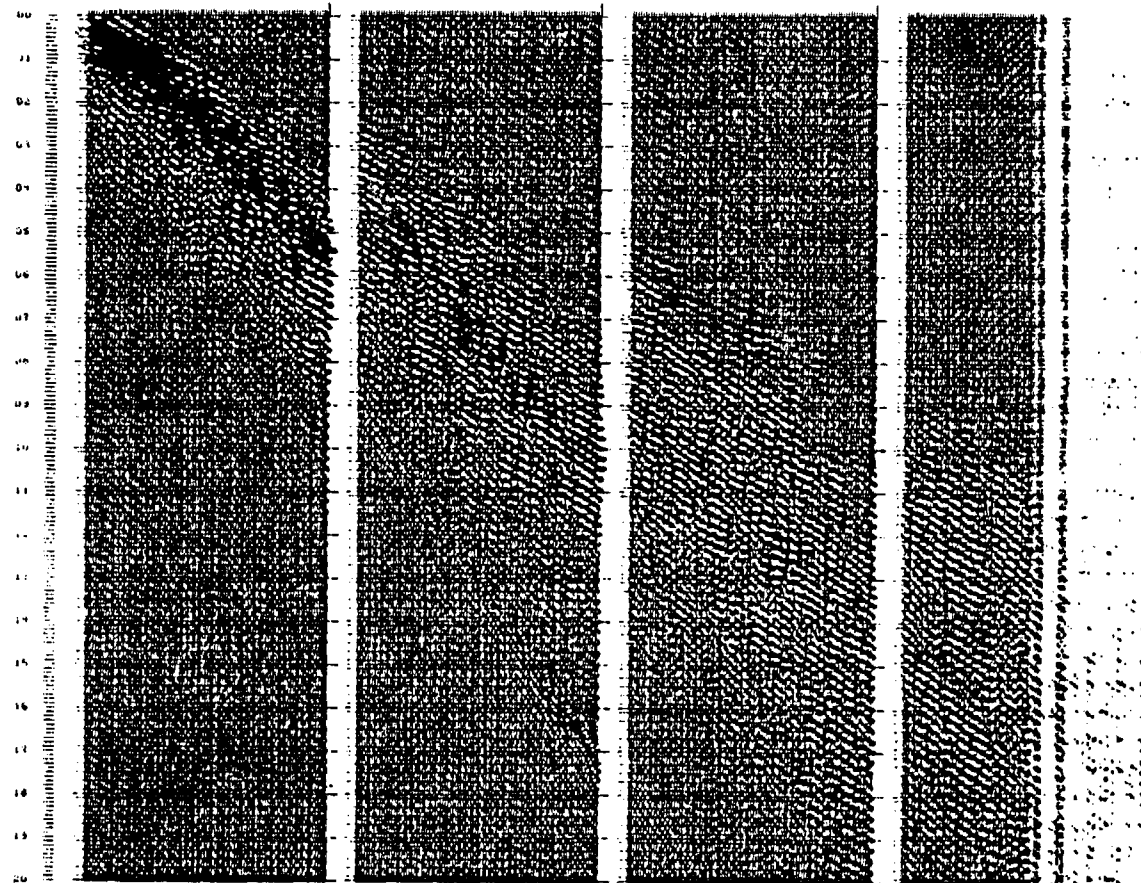


FIGURE 19

CS-3M11



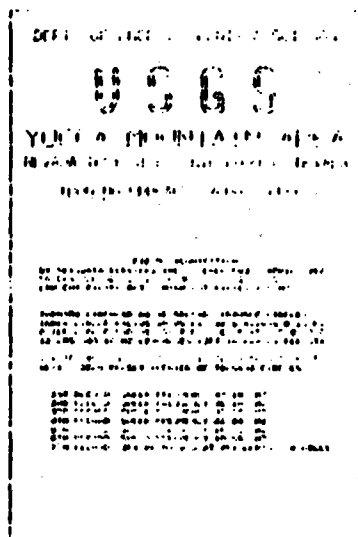
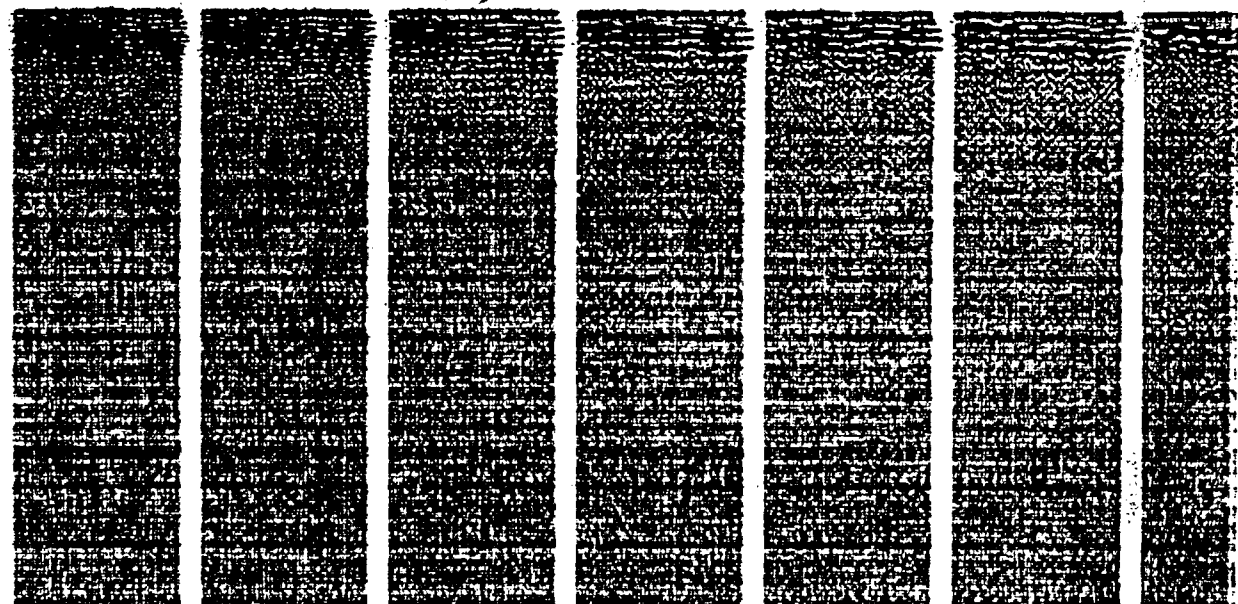


FIGURE 20

Time-sec



[illegible]

TIME·sec

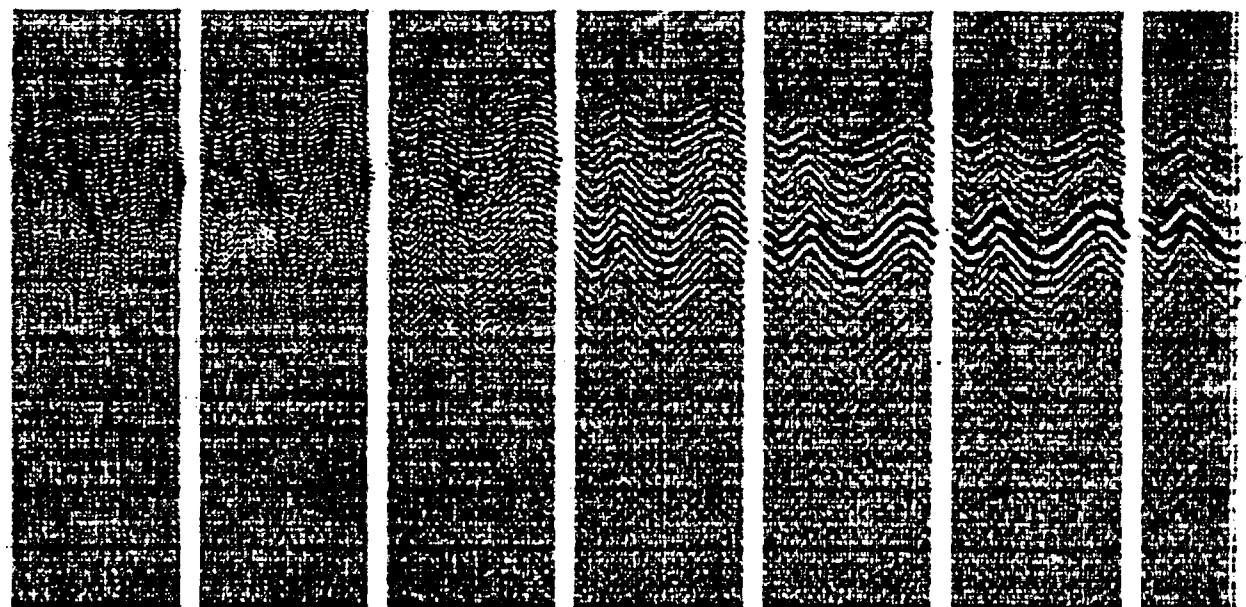
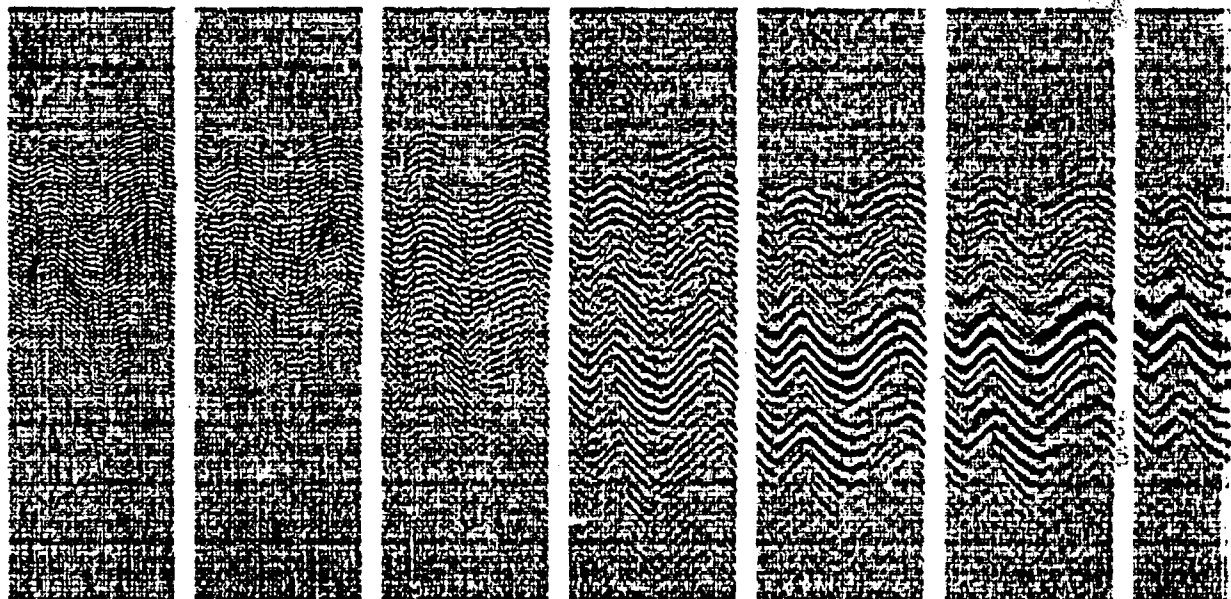


FIG 23

Time-sec



0369

100-443887-100

FILE# 00704470200

[illegible]

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1st	2nd	3rd	4th	5th	6th	7th	8th	9th	10th	11th	12th	13th	14th	15th	16th	17th	18th	19th	20th	21st	22nd	23rd	24th	25th	26th	27th	28th	29th	30th	31st	32nd	33rd	34th	35th	36th	37th	38th	39th	40th	41st	42nd	43rd	44th	45th	46th	47th	48th	49th	50th	51st	52nd	53rd	54th	55th	56th	57th	58th	59th	60th	61st	62nd	63rd	64th	65th	66th	67th	68th	69th	70th	71st	72nd	73rd	74th	75th	76th	77th	78th	79th	80th	81st	82nd	83rd	84th	85th	86th	87th	88th	89th	90th	91st	92nd	93rd	94th	95th	96th	97th	98th	99th	100th

Time-sec

FIG 24

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NEVADA Ins. Co., NEW YORK, NEW YORK

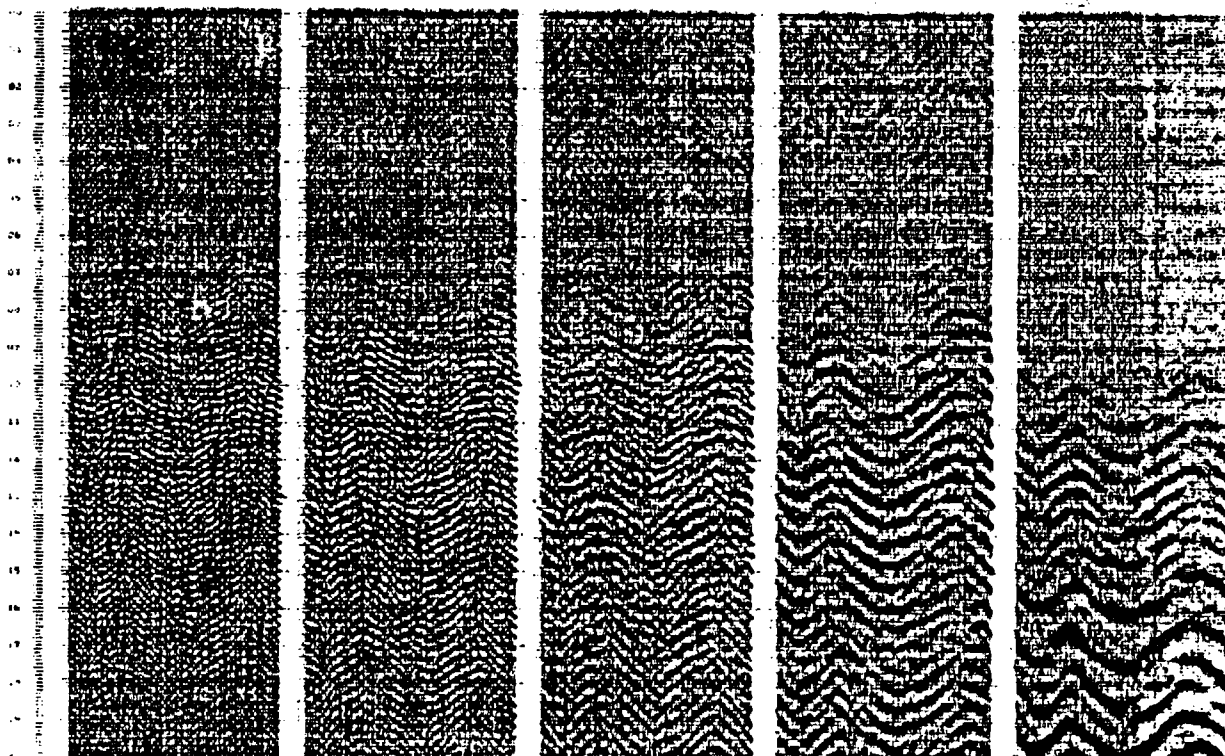
10424-114-400 04/91

FILED IN 100-44117-100
 BY 100-44117-100
 100-44117-100

[illegible]

1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369</
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FIG 25



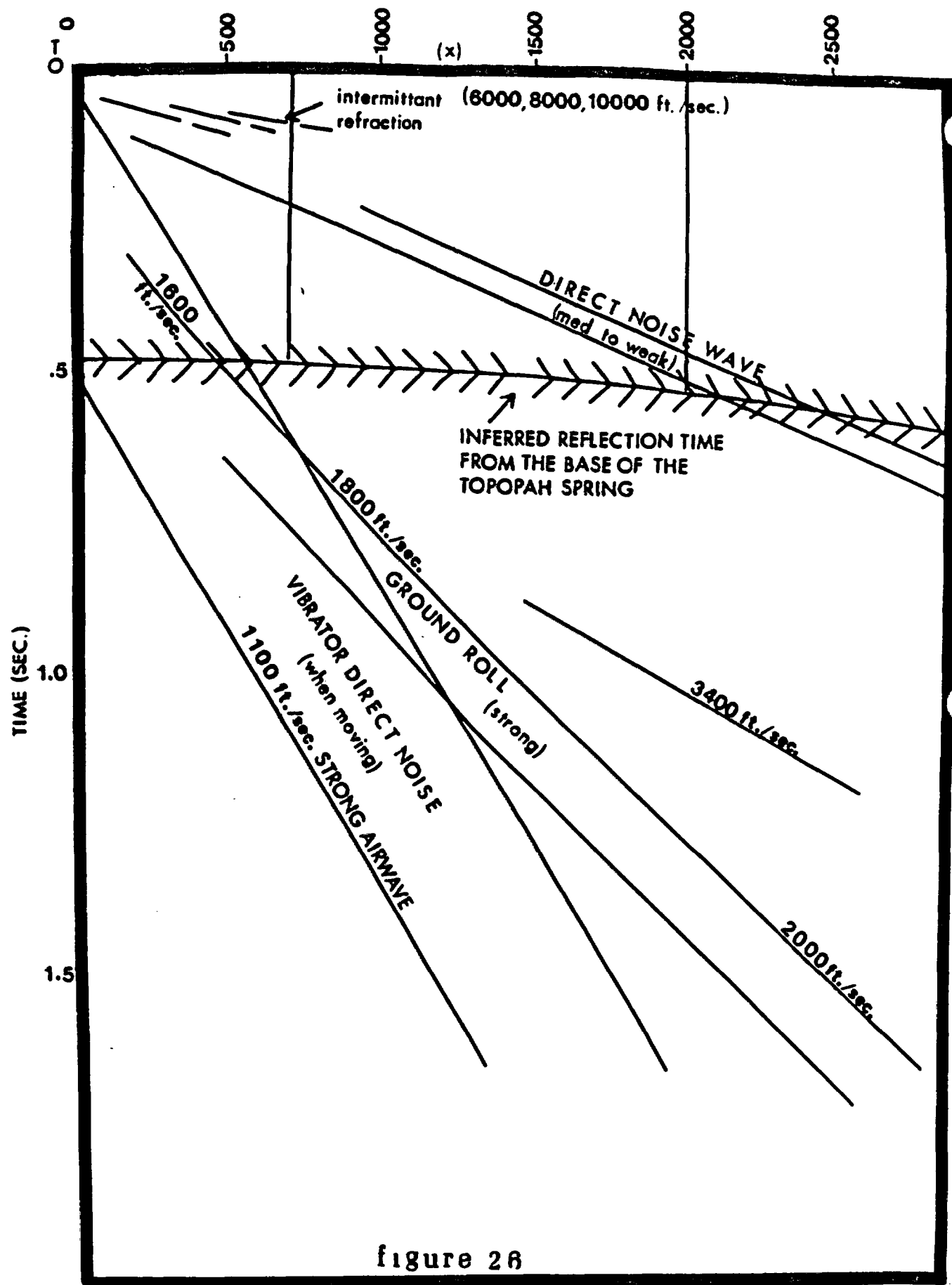


figure 26

SCHEMATIC — SIGNAL AND NOISE

THREE DIMENSIONAL TRAVERSES

RECEIVER

x

x

x

x

4 X 1 4 X 24

TOTAL CDP FOLD 192

[illegible]

TOTAL CDP FOLD 288

[illegible]

TOTAL CDP FOLD 384

- 1). 4 x 24 at 100 ft. = 800-2800 ft.
- 2). 6 x 16 at 100 ft. = 800-2300 ft.
- 3). 8 x 12 at 100 ft. = 800-1900 ft.
- 4). 4 x 24 at 50 ft. = 400-1550 ft.
- 5). 6 x 16 at 50 ft. = 400-1200 ft.
- 6). 8 x 12 at 50 ft. = 400-1000 ft.

FIGURE 27

V S G S

LINE W-4 STACK EASTERN HALF

FIELD ACQUISITION

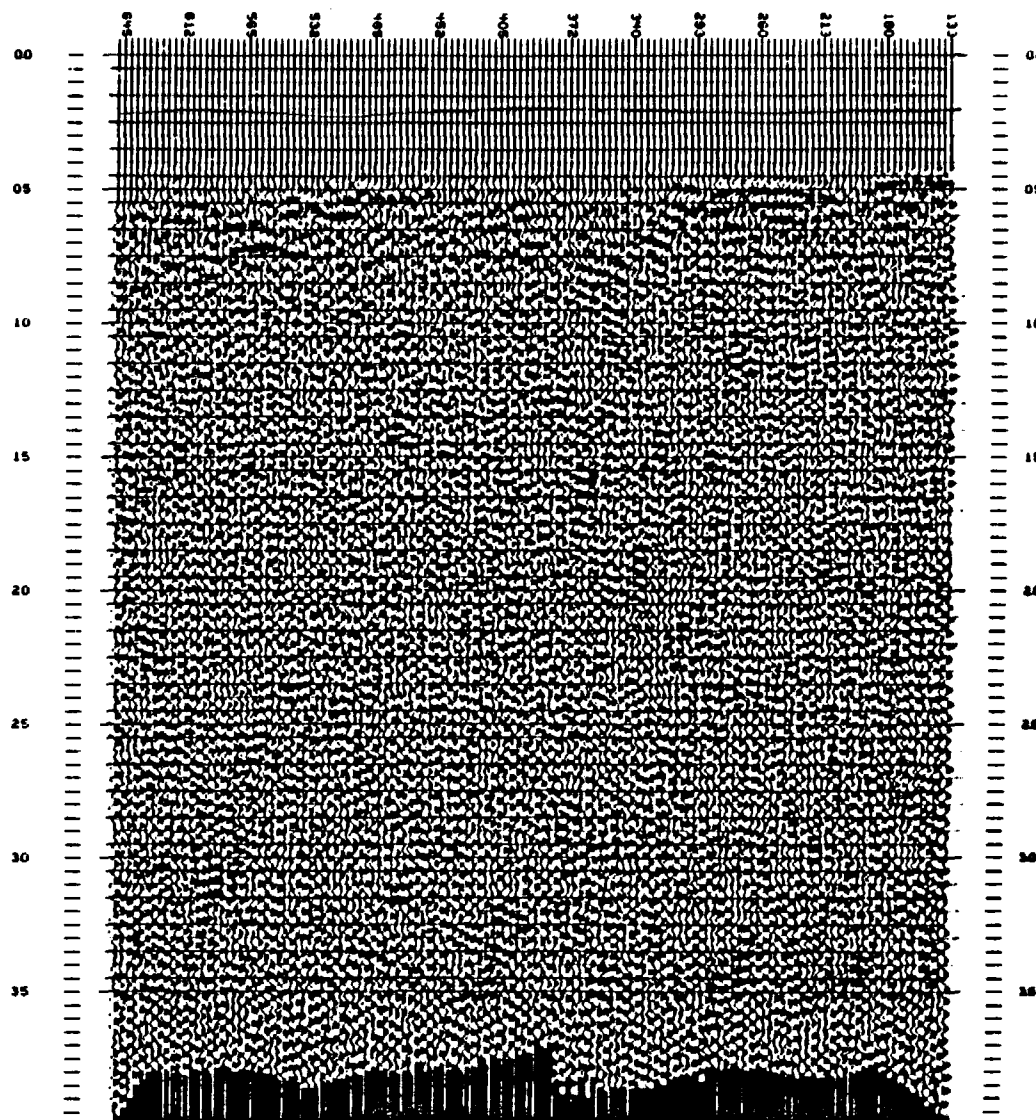
BY SEIDATA SERVICES INC. CERN 003 APR-JUN 1982
30 CHANNEL NIS-10 4 SEC 2 MD 517.0 OUT-10-12822
20 AREA 0 STATIONS BY 74 ROAD 1874 INT 100 FT 5/MI
RAW INTERVAL (M/S) 100FT TO STA 364. THEN 210 FEET
RECEIVED STATION MATRIX 0-0Y-12 SOURCE 0-0Y-1
SOURCE MATRIX OFFEND 040FT TO NEAR RECEIVER ROW
00 L81000 10 MI GEOPHYSIC STATION (SET UP N-TO-S)
ARRAY 1 2 4 6 8 10 11 12 11 10 8 6 4 2 1 INT 10FT
10 SEISMIC SOURCES PRINCIPAL CHANNELS AND VIB
2FT DC AT 4FT 11 & 22 MILE ARRAY 5FT & 10FT INT
2 VIBS 02P 0FT (0 POS 012-0FT) 10 CHIPS/VIB - 64
ARRAY 1 2 3 4 5 6 6 6 6 4 3 2 1 NORTH/SOUTH
LENGTH 162.5FT (DOUBLED FOR 210FT ROWS) 10-32 MI
16SEC RECORD 12SEC SLEEP TOTAL TECHNIQUE - GOOD
STATION 101 TO 682 PROGRESSIVE NORTH TO SOUTH

PROCESSING INFORMATION
SEPTEMBER 10, 1982

REFERENCE DATUM +5000 FT VCONR 8000 FT/SEC
DEMAGNIFIED RES-0 TO RES-9 RECORD & TRACK EDITING
CPDS GATHERED NORTH-SOUTH IN 3-SFT INTERVALS THRU
MIDPOINT OF RANGS 205-270/200-273. THEN 105 FT INT
EITHER EASTERN EIGHT COLUMNS OF CPDS (1 TO 8)
RESAMPLE TO 4 MS BANDPASS FILTER 10 TO 30 KHZ
DIGITAL AUTOMATIC GAIN CONTROL(AGC) SCENE OPERATOR
NORMAL MOVEOUT (2-MAY TIME IN MS - RMS VELOCITY)
100-8000 400-8000 600-8000 1200-10000 2000-12000
CDP STACKING (FOLD 110)
BANDPASS FILTER 10-30 KHZ DIGITAL ABC 1000 MS LEN

FIGURE 28

Time-sec



DEPT OF ENERGY FENIX & SCISSON

U S G S

YUCCA MOUNTAIN AREA
NEVADA TEST SITE NYE COUNTY, NEVADA

LINE W-4 STACK CENTER COPS

FIELD ACQUISITION

BY SEISDATA SERVICES INC. CREW 009 APR-JUN 1982
96 CHANNEL MD5-10 4 SEC 2 MS FILT OUT-TO-125HZ
30 AREA 8 STATIONS BY 74 RONG (STA INT 100 FT E/W)
RONG INTERVAL (M/S) 100FT TO STA 384, THEN 210 FEET
RECEIVER STATION MATRIX 8-0Y-12 SOURCE 8-0Y-1
SOURCE MATRIX OFFEND 840FT TO NEAR RECEIVER RONG
96 LRS1000 10 HZ GEOPHONES-STATION (SET UP N-TO-S)
ARRAY 1 2 4 8 16 32 64 128 256 512 1024 INT 15FT
TWO SEISMIC SOURCES PRIMACORD CHARGES AND VIBS
SPT PC AT SPT 11 & 22 HOLE ARRAY SPT & 10FT INT
3 VIBS 930 SPT (8 PDS 012 SPT) 10 SHEEPS/VIB - 64
ARRAY 1 2 3 4 5 6 8 16 32 64 128 NORTH/SOUTH
LENGTH 182 SPT (DOUBLED FOR 210FT RONG) 10-62 HZ
10SEC RECORD 12SEC SLEEP TOTAL TECHNIQUE - 6000
STATION 101 TO 682 PROGRESSING NORTH TO SOUTH

PROCESSING INFORMATION

SEPTEMBER 10, 1982
REFERENCE DATUM +5000 FT VCONR 8000 FT/SEC
DEMULTIPLY SEG-S TO SEG-Y RECORD & TRACE EDITING
COPS GATHERED NORTH-SOUTH IN 52 SPT INTERVALS THRU
MIDPOINT OF RONG 305-372/380-372, THEN 105 FT INT
GATHER CENTER FIVE COLUMNS OF COPS (8 TO 10)
RESCALE TO 4 MS BANDPASS FILTER 10 TO 30 HZ
DIGITAL AUTOMATIC GAIN CONTROL (AGC) SOURCE OPERATOR
NORMAL MOVEOUT (2-MAY TIME IN MS - RMS VELOCITY)
100-8000 400-8000 800-8000 1200-10000 2000-12000
COP STACKING (FOLD 100)
BANDPASS FILTER 10-30 HZ DIGITAL AGC 1000 MS LEN

Time-sec

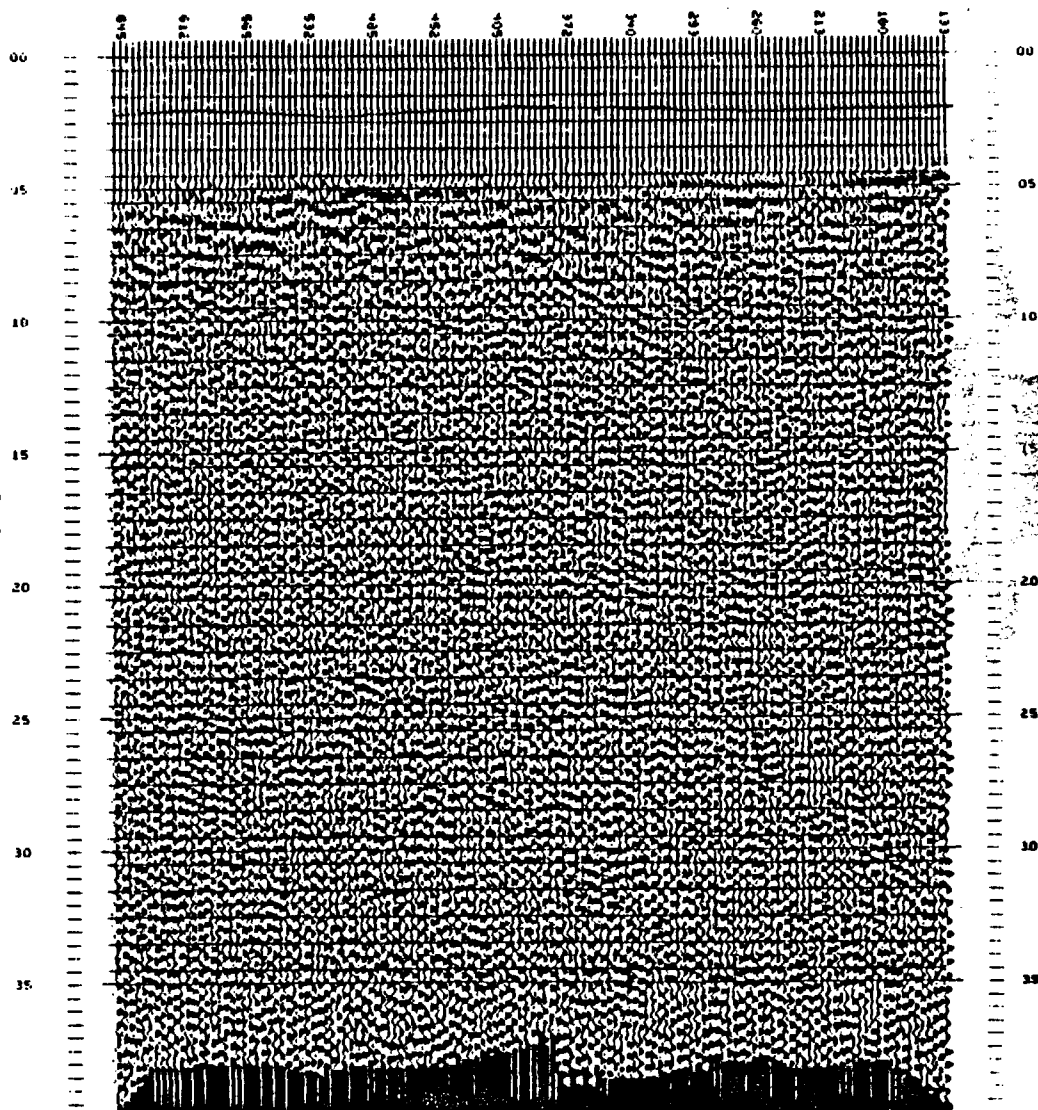


FIGURE 29

DEPT OF ENERGY FENIX & SCISSON

U S G S

YUCCA MOUNTAIN AREA
NEVADA TEST SITE NYE COUNTY, NEVADA

LINE W-4 STACK WESTERN CDP 14

FIELD ACQUISITION

BY SEISDATA SERVICES INC. CASH 003 APR-JUN 1982
96 CHANNEL NOS-10 4 SEC 2 MS FILY OUT-TO-125MHZ
30 AREA 8 STATIONS BY 74 ROWS (STA INT 100 FT E/W)
ROW INTERVAL (N/S) 105FT TO STA 264. THEN 210 FEET
RECEIVER STATION MATRIX 8-BY-12 SOURCE 8-BY-1
SOURCE MATRIX OFFEND 840FT TO NEAR RECEIVER ROW
96 LRS1000 10 MZ GEOPHONES/STATION (SET UP N-TO-S)
ARRAY 1 2 4 6 8 10 11 12 11 10 8 6 4 2 1 INT 15FT
TWO SEISMIC SOURCES PRIMACORD CHARGES AND VIBS
3FT PC AT 4FT 11 6 22 HOLE ARRAY 5FT 6 10FT INT
3 VIBS 637 5FT (8 PGS 612 5FT) 10 SWEEPS/VIB = 54
ARRAY 1 2 3 4 5 6 6 6 4 3 2 1 NORTH/SOUTH
LENGTH 162 5FT (DOUBLED FOR 210FT ROWS) 16-62 MZ
16SEC RECORD 12SEC SWEPT TOTAL TECHNIQUE = 6808
STATION 101 TO 692 PROGRESSSES NORTH TO SOUTH

PROCESSING INFORMATION

SEPTEMBER 10, 1982
REFERENCE DATUM +5000 FT VCONR 8000 FT/SEC
DEMULPLEX SEG-B TO SEG-Y RECORD & TRACE EDITING
CDPS GATHERED NORTH-SOUTH IN 105 FT INTERVALS
GATHER ONE WESTERN CDP COLUMN (14)
RESAMPLE TO 4 MS BANDPASS FILTER 10 TO 30 MZ
DIGITAL AUTOMATIC GAIN CONTROL (AGC) 500MS OPERATOR
NORMAL MOVEOUT (2-MAY TIME IN MS - RMS VELOCITY)
100-6000 400-8000 600-8000 1200-10800 2000-13000
CDP STACKING (FOLD 28)
BANDPASS FILTER 10-36 MZ DIGITAL AGC 1000 MS LEN

Time-sec

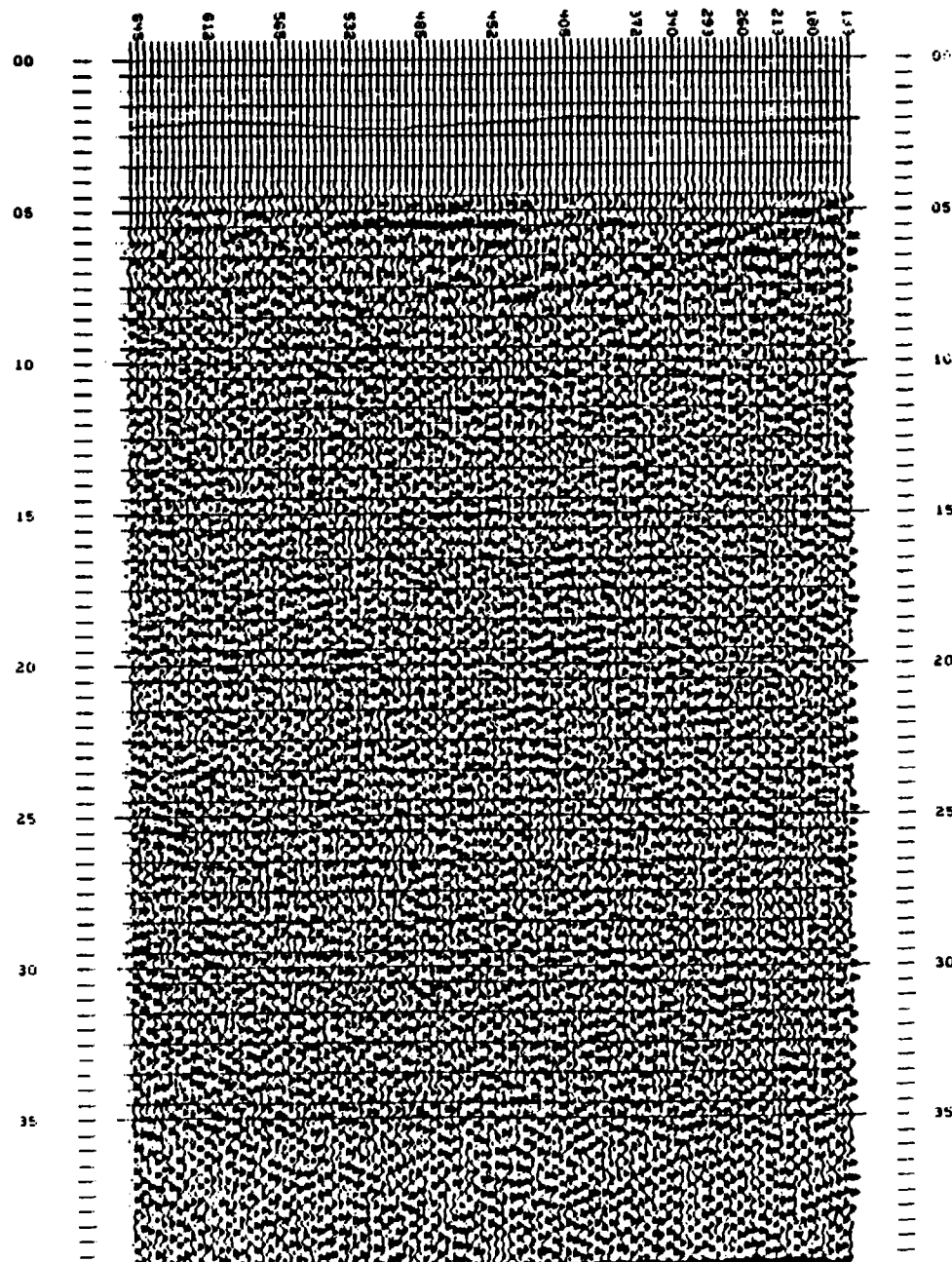


FIGURE 30

DEPT OF ENERGY FENIX & SCISSON

U S G S

YUCCA MOUNTAIN AREA
NEVADA TEST SITE NYE COUNTY, NEVADA

W-4 OPTIMUM PROFILE (105' CDP)

FIELD ACQUISITION

BY SEISDATA SERVICES INC CREN 003 APR-JUN 1982
36 CHANNEL MD5-10 4 SEC 2 MS FILT OUT-TO-125HZ
30 AREA 8 STATIONS BY 74 ROWS (STA INT 100 FT E/W)
ROW INTERVAL (N/S) 105FT TO STA 384, THEN 210 FEET
RECEIVER STATION MATRIX 8-BY-12 SOURCE 8-BY-1
SOURCE MATRIX OFFEND 840FT TO NEAR RECEIVER ROW
36 LRS1000 10 HZ GEOPHONES/STATION (SET UP N-TO-S)
ARRAY 1 2 4 6 8 10 11 12 11 10 8 6 4 2 1 INT 15FT
TWO SEISMIC SOURCES PRIMACORD CHARGES AND VIBS
SPT PC AT 4FT 11 & 22 HOLE ARRAY SPT 2 10FT INT
3 VIBS 037 SPT (8 POS 012 SPT) 10 SHEEPS/VIB = 34
ARRAY 1 2 3 4 5 6 6 6 6 4 3 2 1 NORTH/SOUTH
LENGTH 162 SPT (DOUBLED FOR 210FT ROWS) 16-62 HZ
16SEC RECORD 12SEC SWEET TOTAL TECHNIQUE = 6800
STATION 101 TO 632 PROGRESSS NORTH TO SOUTH

PROCESSING INFORMATION

SEPTEMBER 10, 1982

REFERENCE DATUM +5000 FT VCORR 8000 FT/SEC
DEMULPLEX SEG-B TO SEG-Y RECORD & TRACE EDITING
CDPS GATHERED NORTH-SOUTH IN 105 FT INTERVALS
RESAMPLE TO 4 MS BANDPASS FILTER 10 TO 30 HZ
DIGITAL AUTOMATIC GAIN CONTROL (AGC) 500MS OPERATOR
NORMAL MOVEOUT (2-MV TIME IN MS - RMS VELOCITY)
100-8000 400-8000 600-8000 1200-10800 2000-12000
CDP STACKING (OPTIMUM PROFILE FOLD 384)
BANDPASS FILTER 10-36 HZ DIGITAL AGC 1000 MS LEN

Time-sec

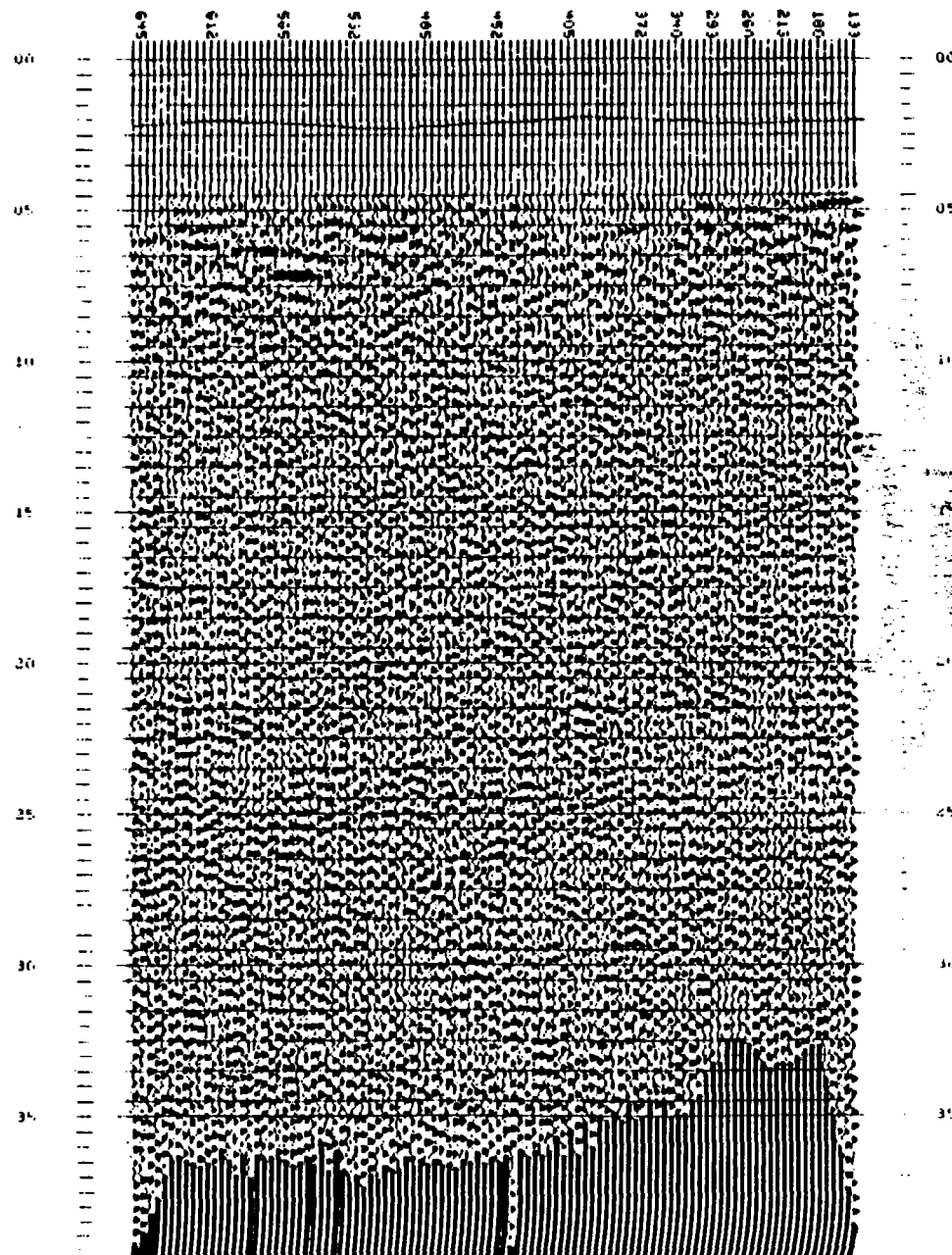


FIGURE 31

DEPT OF ENERGY FENIX & SCISSON

U S G S

YUCCA MOUNTAIN AREA
NEVADA TEST SITE NYE COUNTY, NEVADA

THREE-D LINE G-2 STACK

FIELD ACQUISITION

BY SEISDATA SERVICES INC. CREW 003 JUNE 1982
96 CHANNEL MDS-10 INSTRUMENTS 4 SECONDS 2 MS
FIELD FILTER 12 TO 125 HZ REC MADE HAS GP 1FP
96 LRS1000 10HZ GEOPHONES PER GROUND STATION
RECEIVER MATRIX 4-BY-24 100 FT STATION INTERVAL
SINGLE HOLE DYNAMITE SHOT 10-25LB 195/200FT DEPTH
SOURCE OFFSET 400FT TO NEAR RECEIVER, 2700FT FAR
STATION 101-240 SE/NE SHOTPOINTS 1-19 SE/NE

PROCESSING INFORMATION
SEPTEMBER 10, 1982

REFERENCE DATUM +5000 FT VCORR 0000 FT/SEC
DEMULPLEX SEG-B TO SEG-Y RECORD & TRACE EDITING
ARRANGE TRACES TO THREE-D COMMON DEPTH POINTS(CDP)
RESAMPLE TO 4 MS BANDPASS FILTER 10 TO 30 HZ
DIGITAL AUTOMATIC GAIN CONTROL(AGC) 500MS OPERATOR
NORMAL MOVEOUT (2-MAY TIME IN MS - RMS VELOCITY)
100-6000 480-8000 600-8000 1200-10800 2000-12000

CDP STACKING (MAXIMUM FOLD 92)

1ST DISPLAY FILTER 10-30HZ DIGITAL AGC 1000MS
2ND DISPLAY TIME SERIES INTEGRATION

Time-sec

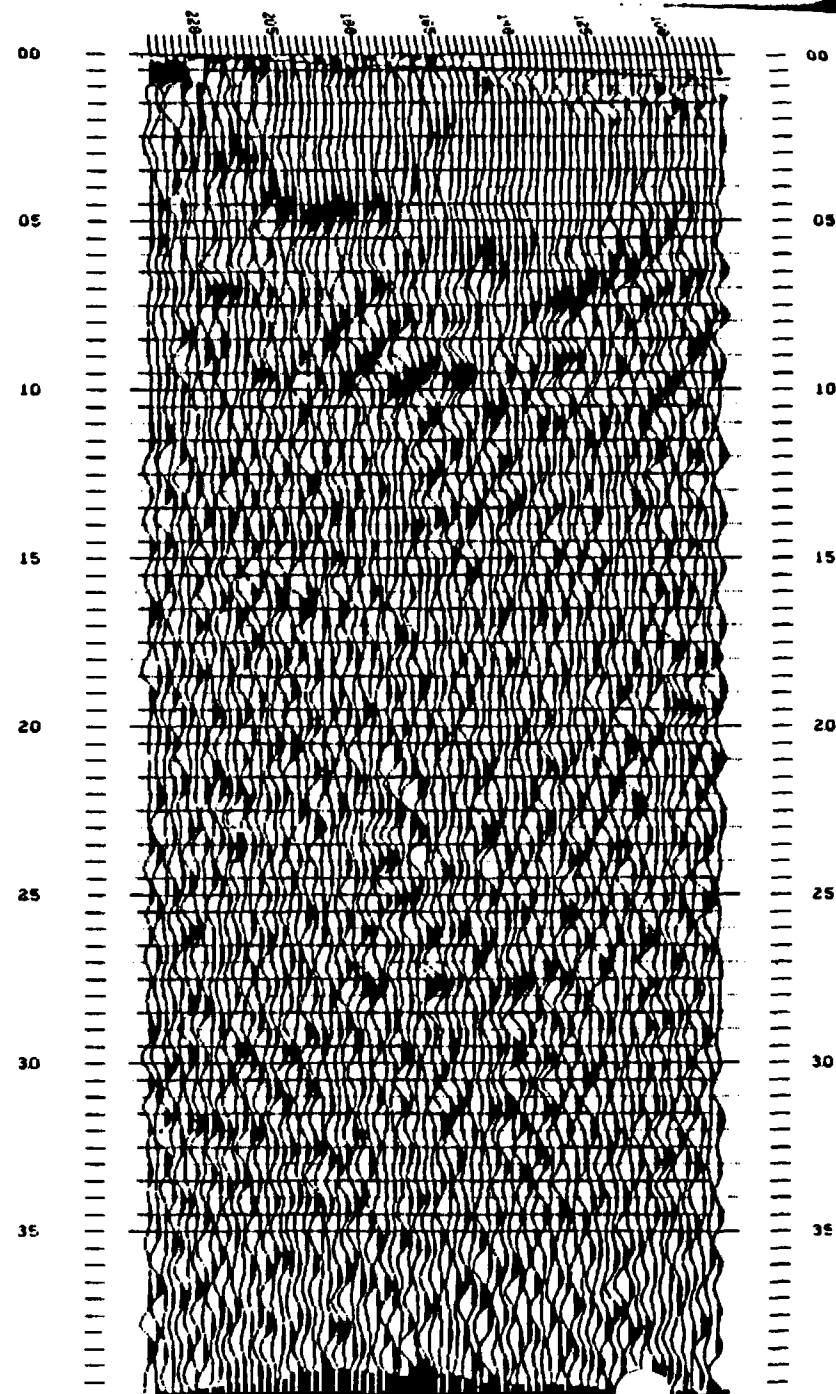


FIGURE 32

U S G S

THREE-D LINE 5-2 STACK

FIGURE 5 ■ *Continued*

[illegible]

DECLASSIFICATION INFORMATION
DATE 10/20/2010 BY 60322

[illegible]

REF ID: A66042

TIME: sec

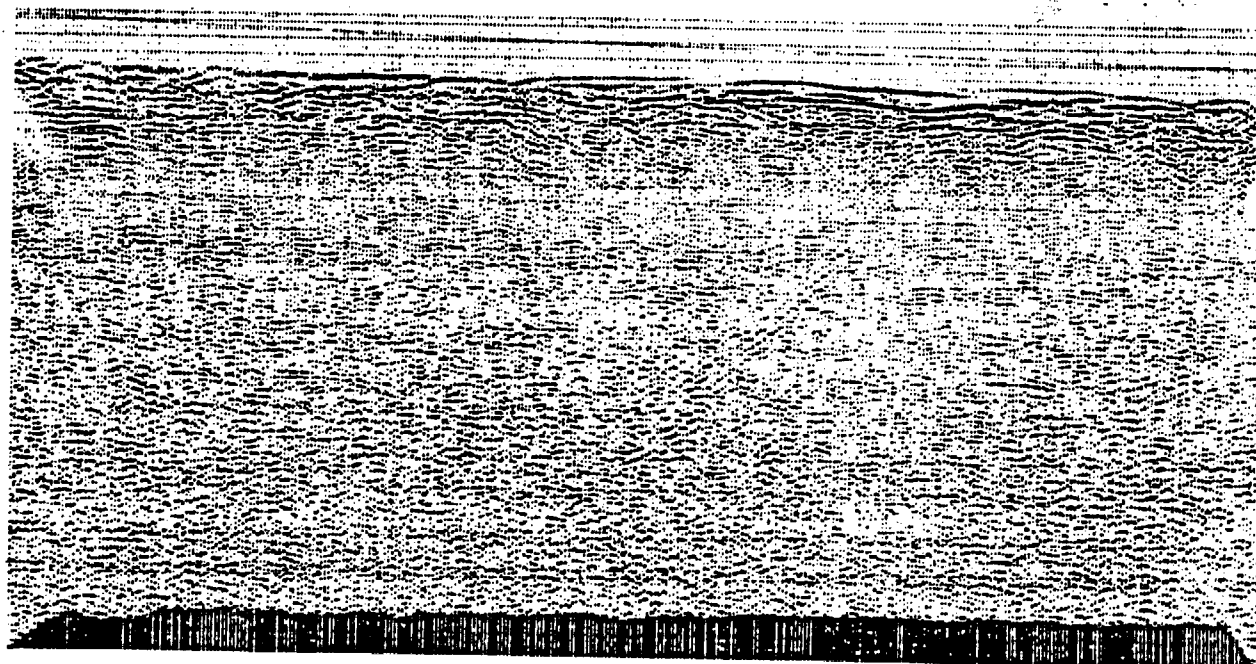


FIGURE 33

DEPT OF ENERGY FENIX & SCISSON

USGS

YUCCA MOUNTAIN AREA
NEVADA TEST SITE NYE COUNTY, NEVADA

THREE-D LINE S-4 STACK

FIELD ACQUISITION

BY SEISDATA SERVICES INC. CASE# 000 JULY 1982
56 CHANNELS 10-10 0 SEC 2 ND FILTER 12 - 62 HZ
30 AREA 6 STATIONS BY 116 BORE 50 FT STATION INT
12 LOGS 1000 10 HZ GEOPHONES-STATION 0 FT INTERVAL
RECEIVED STATION DATA 6-07-10 100 TOTAL STA
VECTOR PULSE SOURCE (NORTH 6-07-10) (OFFEND 450 FT)
GAIN PC BURIED PIGIN 7 HOLE ARRAY 100' SPACING
STATION 101 TO 066 (NORTHWEST-TO-SOUTHEAST)

PROCESSING INFORMATION
SEPTEMBER 10, 1982

REFERENCE DATUM +5000 FT VCONV 0000 FT/SEC
DEMUTIPLEX 128-0 TO 065-V RECORD & TRACE EDITING
ARRANGE TRACES TO THREE-D COMMON DEPTH POINTS(CDP)
RESAMPLE TO 4 MS BANDPASS FILTER 10 TO 50 HZ
DIGITAL AUTOMATIC GAIN CONTROL (AGC) GAIN OPERATOR
EARLY ROUTING AND AVERAGE SUPPRESSION ROUTING
NORMAL MOVEOUT 12-MAV TIME IN MS - RMS VELOCITY
100-0000 000-0000 1000-0000 0000-10000
POST-MOVEOUT MUTE (10000-10000) DATUM STATICS
CDP STACKING (MAXIMUM FOLD 200)
BANDPASS FILTER 10-30 HZ DIGITAL AGC 1000 MS LEN

Time·sec

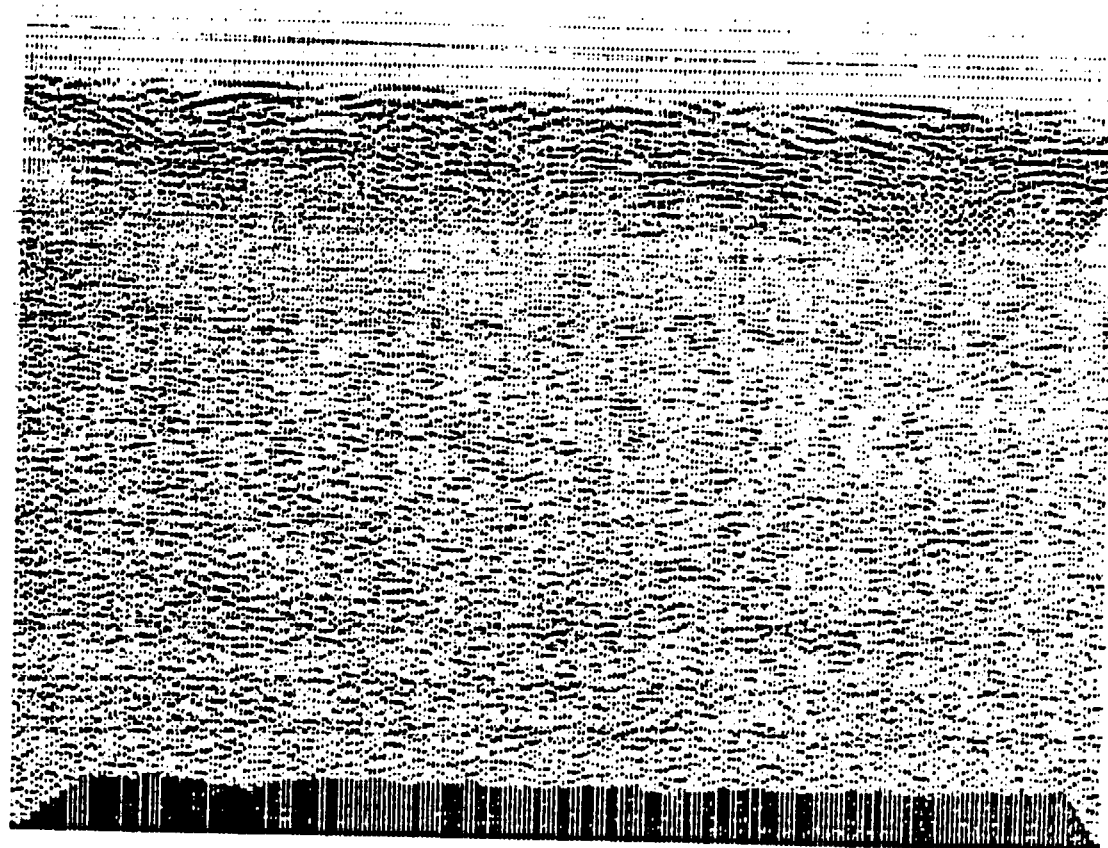
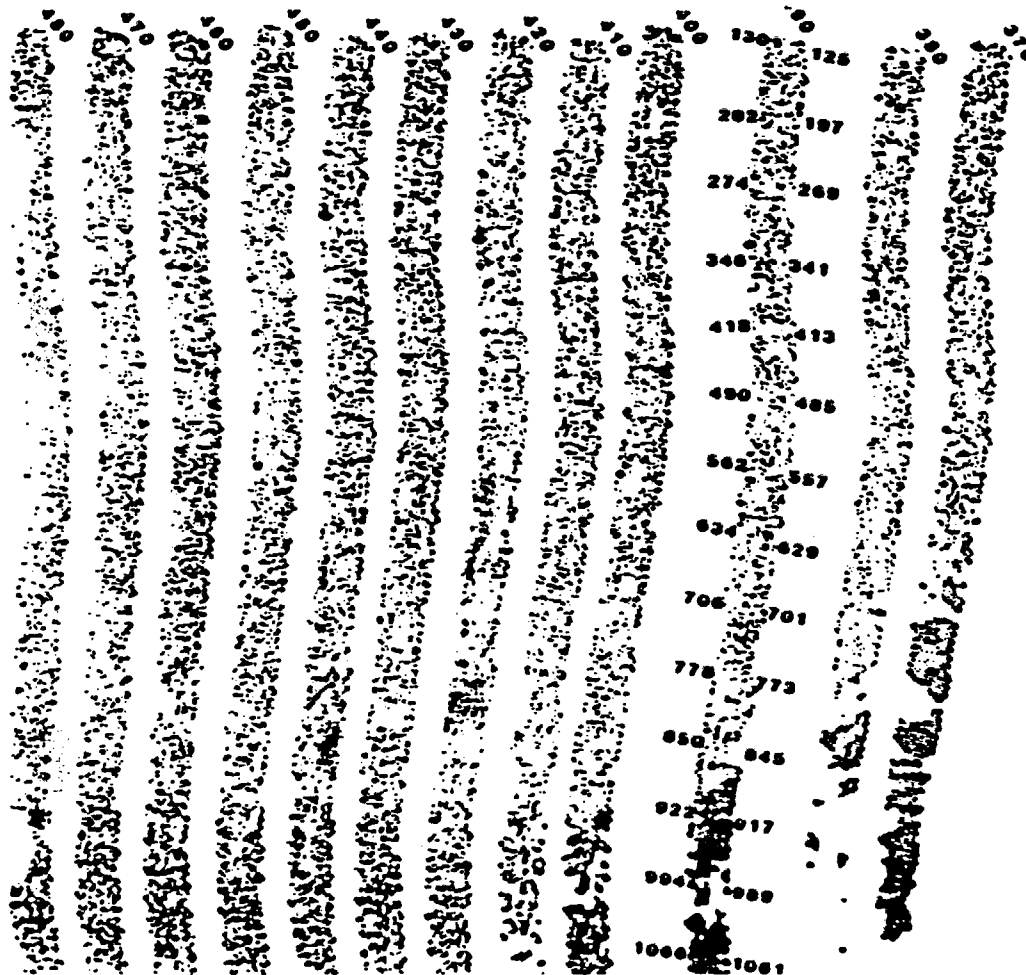


FIGURE 34



TIME

YUCCA MOUNTAIN

3-D

TIME SLICES

LINE S-2

NORTH

FIG 35

SCALE 1" = 1000